

## **Metrology and Sensing**

Lecture 12-3: Optical Coherence Tomography

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### Contents



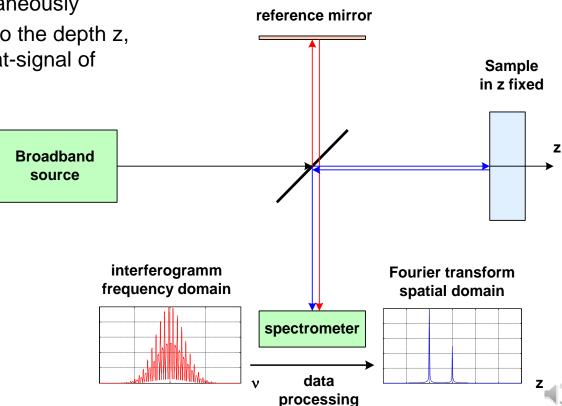
- Fourier domain OCT
- Swept source OCT
- Examples



#### Fourier Domain OCT



- Spectral Domain-OCT:
  - broad band source
  - reference mirror fixed in position, no A-scan necessary
  - signal splitted by spectrometer
- The high-frequency content of the signal is analyzed: full spectral resolution, no coarse envelope
- All depth are measured simultaneously
- The frequency is proportional to the depth z, measured is the overlayed beat-signal of all scatterers

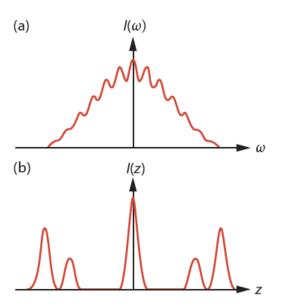


#### Fourier Domain OCT

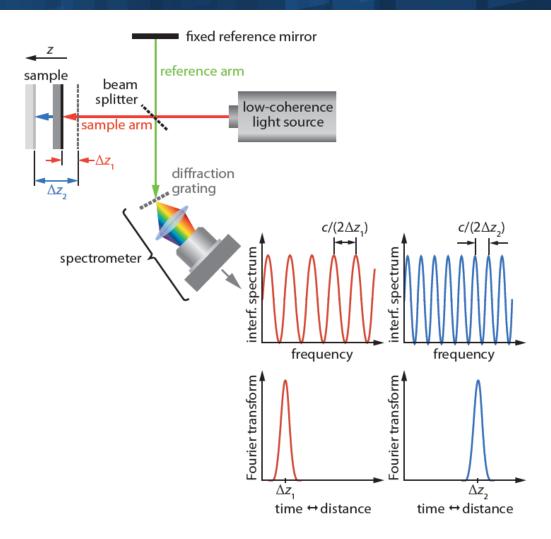


Fourier Domain-OCT: setup

- Signals:
  - a) intensity spectrum
  - b) spatial intensity distribution



Ref: M. Kaschke

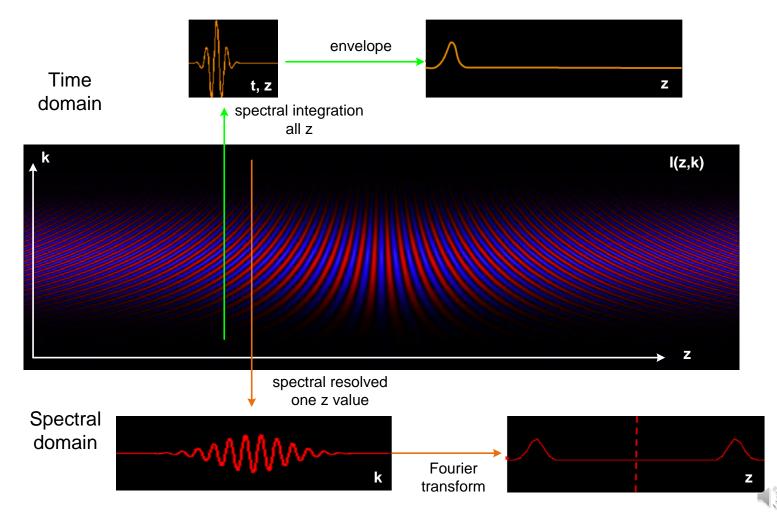




### **OCT Signal Processing**



- Signal evaluation
  - time domain OCT
  - spectral domain OCT



### Properties of Fourier Domain OCT

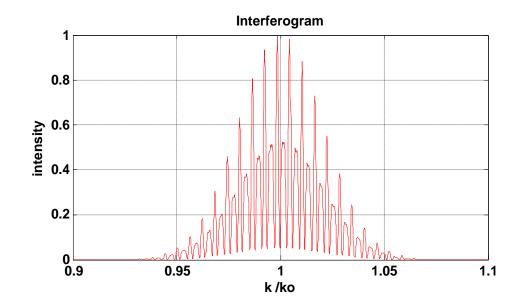


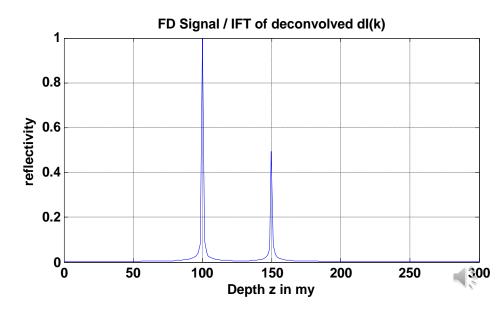
- the modulation frequency depends on the path length difference
- simultaneous measurement of all backscattering contributions: larger sensitivity
  - Fourier transform adds signals coherent
  - noise is added incoherent
- faster image processing due to missing A scan
- signal drop-off with increasing depth spectrometer resolution changes over depth
- positive and negative ∆z cannot be distinguished



### Fourier Domain OCT Example Calculation

- Only z-dependence
- 2 discrete scatterers





### Fourier Domain OCT Signal



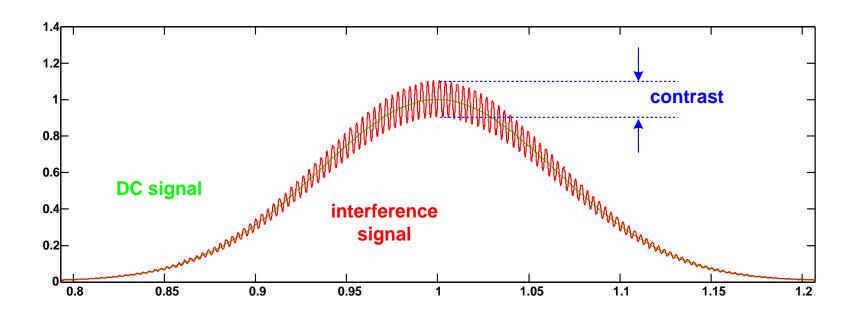
Typical Fourier Domain OCT signal only z-part

$$I_{FD}(k,\omega) = \frac{\rho}{4} \cdot S(k) \cdot \left( r_R^2 + \sum_j \left| r_{Sj} \right|^2 \right) + \frac{\rho}{2} \cdot S(k) \cdot r_R \cdot \sum_j r_{Sj} \cdot \cos(2k(z_R - z_{Sj})) + \frac{\rho}{4} \cdot S(k) \cdot \sum_{j \neq m} r_{Sj} \cdot r_{Sm} \cdot \cos(2k(z_{Sj} - z_{Sm})) \right)$$

First term: DC

Second term: interference, cross-correlation, contains information

Third term: autocorrelation between scatterers

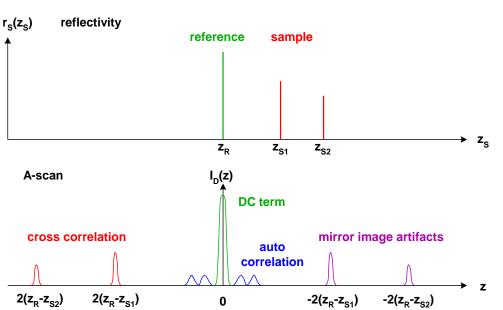


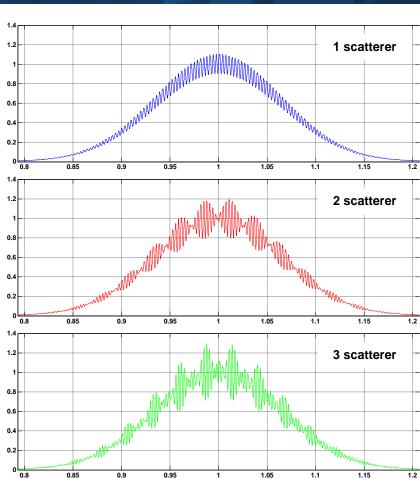


### Fourier Domain OCT Signal



 Signal complexity depends on scatter-distribution

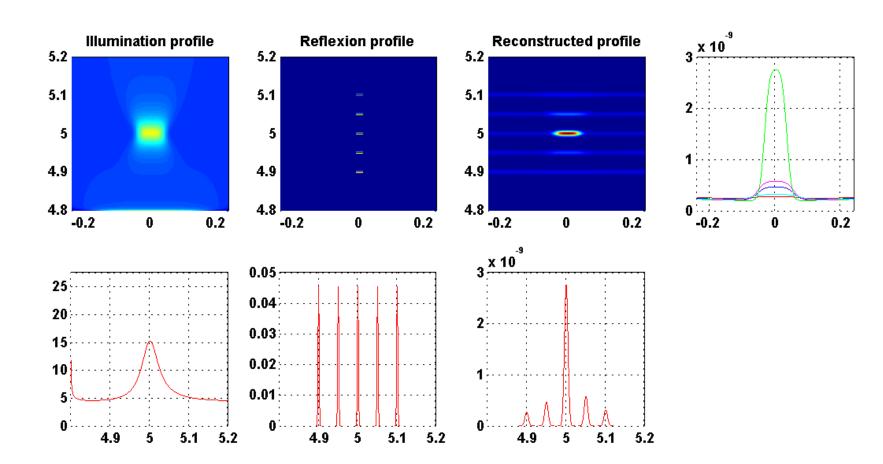






### FD OCT in 3D Gaussian Beams Example

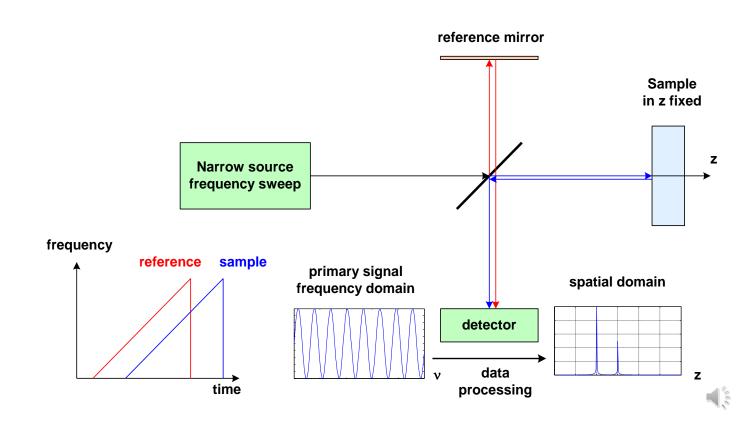
- 5 discrete scatter planes with finite extend
- Without EDF-caustic





### Fourier Domain OCT with Swept Source

- Special setup for Fourier domain OCT:
  - SS-OCT: swept source instead of broad spectral source
  - source has tunable wavelength
  - advantage: no spectrometer necessary
  - usually faster than classical Fourier domain OCT
  - tunable laser expensive



### Overview on OCT Setups

frequency

domain

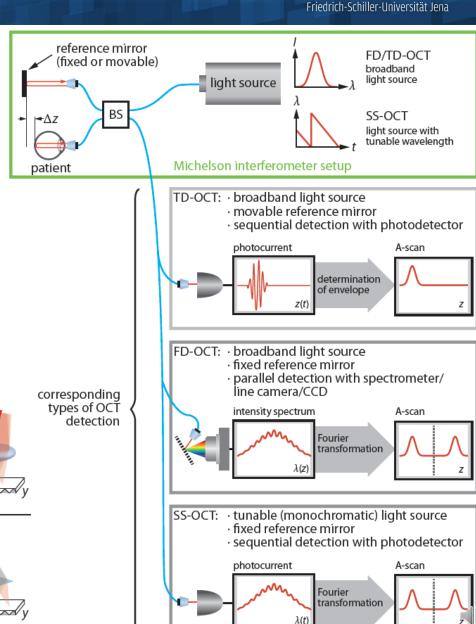
Ref: M. Kaschke

encoding

spatial

time





#### Fourier Domain OCT Signal

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- Field in the reference arm
- Field in the sample arm
- Interference field
- Discrete scattering model: OCT signal

with reflectivities r<sub>i</sub>

 Final signal evaluation
 1st term: DC signal (underground)
 2nd term cross correlation with reference, interesting term
 3rd term autocorrelation between scatterers (small)

$$E_R = \frac{E_0(k,\omega)}{\sqrt{2}} \cdot r_R \cdot e^{i2kz_R}$$

$$E_{S} = \frac{E_{0}(k,\omega)}{\sqrt{2}} \cdot r_{S}(z) \otimes e^{i2kz_{S}}$$

$$I_{FD} = \rho \cdot \left| E_R + E_S \right|^2$$

$$I_{FD}(k,\omega) = \frac{\rho}{2} \left| \frac{E_0(k,\omega)}{\sqrt{2}} \right|^2 \cdot \left| r_R \cdot e^{i \cdot (2kz_R - \omega t)} + \sum_j r_{Sj} \cdot e^{i \cdot (2kz_{Sj} - \omega t)} \right|^2$$

$$r_{S}(z_{S}) = \sum_{j} r_{Sj} \cdot \delta(z_{S} - z_{Sj})$$

$$I_{FD}(k,\omega) = \frac{\rho}{4} \cdot S(k) \cdot \left( r_R^2 + \sum_j \left| r_{Sj} \right|^2 \right)$$

$$+ \frac{\rho}{2} \cdot S(k) \cdot r_R \cdot \sum_j r_{Sj} \cdot \cos\left(2k(z_R - z_{Sj})\right)$$

$$+ \frac{\rho}{4} \cdot S(k) \cdot \sum_{j \neq m} r_{Sj} \cdot r_{Sm} \cdot \cos\left(2k(z_{Sj} - z_{Sm})\right)$$



### Fourier Domain OCT Signal

Signal evaluation: inverse Fourier transform
 DC-term subtracted by difference measurement
 Auto-correlation: mostly negligible

$$I(z) = \hat{F}^{-1}[I(k)] = \hat{F}^{-1}[S(k)] \otimes \left\{ \frac{r_S^2}{2n_S} \cdot \delta(z) + \frac{r_R \cdot r_S}{2n_S} + \frac{1}{16n_S^2} \cdot A_C(r_S(z)) \right\}$$

$$r_S(z) = \frac{n_S}{r_R} \cdot F^{-1} \left[ \frac{\Delta I(k)}{S(k)} \right]$$

Heterodyne efficiency:
 Decrease in signal strength due to scattering underground for gaussian beams

$$\left\langle I^{2}(z) \right\rangle_{cohgate} = \frac{\alpha^{2} P_{R} P_{S} \sigma_{b}}{\pi w_{non}^{2}} \cdot \left[ e^{-2\mu_{s}z} + \frac{4w_{non}^{2}}{w_{non}^{2} + w_{S}^{2}} \cdot e^{-2p_{b}\mu_{s}z} \cdot e^{-\mu_{s}z} \cdot \left(1 - e^{-\mu_{s}z}\right) + \frac{w_{non}^{2}}{w_{S}^{2}} \cdot e^{-4p_{b}\mu_{s}z} \cdot \left(1 - e^{-\mu_{s}z}\right)^{2} \right]$$

$$= \left\langle I^{2} \right\rangle_{0} \cdot \Psi(z)$$

