

1 Paraxial system layout

- a) Suppose a divergent ray bundle with numerical aperture of $NA = 0.2$ at the wavelength $\lambda = 500$ nm. Establish a first paraxial lens with a focal length to get a collimated beam with diameter 24 mm.
- b) After a distance of 10 mm a second paraxial lens with focal length $f_2 = 30$ mm focusses the ray. Behind the focal point a third paraxial lens should collimated the beam again for a diameter of 36 mm.
- c) Now in a distance of 20 mm a focussing paraxial lens with focal length $f = 100$ is added. Finally a negative lens with $f = -70$ mm is added in an appropriate distance to change the numerical aperture in the image space to 0.05. Find the final image distance. What is the magnification of the system ?

Solution:

a) Wavelength and numerical aperture are inserted. Then we set the focal length by a pickup to have the same value as the first object distance. This guarantees a collimated output beam. In the merit function a PARY value of $D/2 = 12$ mm is required, the first distance is variable. Alternatively without using the optimization, the value can be calculated by hand with $\tan(u) = \sin(u)/\cos(u) = D/2/f = 58.788$ mm or approximated with the slider.

Lens Data Editor												
Edit Solve View Help												
Surf	Type	Comment	Radius	Thickness	Glass	Semi-Diameter	Conic	Par 0 (unused)	Par 1 (unused)	Par 2 (unused)	Par 3 (unused)	Par 4 (unused)
OBJ	Standard		Infinity	58.78775	V	0.00000	0.00000					
STO	Paraxial			0.00000		12.00000			58.78775	P	1	
IMA	Standard		Infinity	-		12.00000	0.00000					

Merit Function Editor: 5.186251E-011												
Edit Design Tools View Help												
Oper #	Type	Surf	Wave	Hx	Hy	Px	Py	Target		Weight		
1: PARY	PARY	2	1	0.00000	0.00000	0.00000	1.00000	12.00000		1.00000		

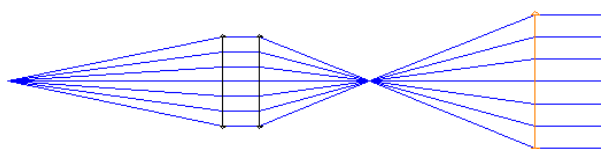
b) The 3rd lens must have a focal length of $36/24 \times 30 = 45$ mm. The air distances are correspondingly.

Lens Data Editor										
Edit Solve View Help										
Surf	Type	Comment	Radius	Thickness	Glass	Semi-Diameter	Conic	Par 0 (unused)	Focal Length	
OBJ	Standard		Infinity	58.78775	V	0.00000	0.00000			
STO	Paraxial			10.00000		12.00000			58.78775	P
2	Paraxial			30.00000		12.00000			30.00000	
3	Standard		Infinity	45.00000		0.00000	0.00000			
4	Paraxial			20.00000		18.00000			45.00000	
IMA	Standard		Infinity	-		18.00000	0.00000			

Normalized X Field Coord (Hx) : 0.0000000000
 Normalized Y Field Coord (Hy) : 0.0000000000
 Normalized X Pupil Coord (Px) : 0.0000000000
 Normalized Y Pupil Coord (Py) : 1.0000000000

Real Ray Trace Data:

Surf	X-coordinate	Y-coordinate	Z-coordinate
OBJ	-0.0000000000E+000	-0.0000000000E+000	0.0000000000E+000
1	0.0000000000E+000	1.2000000000E+001	0.0000000000E+000
2	0.0000000000E+000	1.2000000000E+001	0.0000000000E+000
3	0.0000000000E+000	0.0000000000E+000	0.0000000000E+000
4	0.0000000000E+000	-1.8000000000E+001	0.0000000000E+000
5	0.0000000000E+000	-1.8000000000E+001	0.0000000000E+000



c) A second optimization selects the distance of lens 4 to obtain the numerical aperture by PARB to be 0.05. The image distance is obtained by QUICK FOCUS. The lens data are

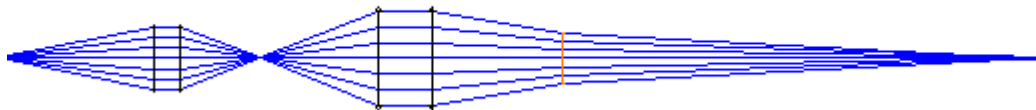
Lens Data Editor									
Edit Solve View Help									
Surf	Type	Comment	Radius	Thickness	Glass	Semi-Diameter	Conic	Par 0 (unused)	Focal Length
OBJ	Standard		Infinity	58.78775		0.00000	0.00000		
STO	Paraxial			10.00000		12.00000			58.78775 P
2	Paraxial			30.00000		12.00000			30.00000
3	Standard		Infinity	45.00000		0.00000	0.00000		
4	Paraxial			20.00000		18.00000			45.00000
5	Paraxial			49.46880 V		18.00000			100.00000
6	Paraxial			181.68480		9.09562			-70.00000
IMA	Standard		Infinity	-		1.4211E-014	0.00000		

Merit Function Editor: 3.078239E-012											
Edit Design Tools View Help											
Oper #	Type	Surf	Wave	Hx	Hy	Px	Py		Target	Weight	Value
1: PARB	PARB	7	1	0.00000	0.00000	0.00000	1.00000		0.05000	1.00000	0.05000

Normalized X Field Coord (Hx) : 0.0000000000
 Normalized Y Field Coord (Hy) : 0.0000000000
 Normalized X Pupil Coord (Px) : 0.0000000000
 Normalized Y Pupil Coord (Py) : 1.0000000000

Real Ray Trace Data:

Surf	X-coordinate	Y-coordinate	Z-coordinate	X-cosine	Y-cosine
OBJ	-0.0000000000E+000	-0.0000000000E+000	0.0000000000E+000	0.0000000000	0.2000000000
1	0.0000000000E+000	1.2000000000E+001	0.0000000000E+000	0.0000000000	0.0000000000
2	0.0000000000E+000	1.2000000000E+001	0.0000000000E+000	0.0000000000	-0.3713906764
3	0.0000000000E+000	0.0000000000E+000	0.0000000000E+000	0.0000000000	-0.3713906764
4	0.0000000000E+000	-1.8000000000E+001	0.0000000000E+000	0.0000000000	0.0000000000
5	0.0000000000E+000	-1.8000000000E+001	0.0000000000E+000	0.0000000000	0.1771529983
6	0.0000000000E+000	-9.0956167796E+000	0.0000000000E+000	0.0000000000	0.0500000000
7	0.0000000000E+000	1.4210854715E-014	0.0000000000E+000	0.0000000000	0.0500000000



The magnification is $0.2 / 0.05 = 4$.

2 Singlet II

Establish a single lens with the following data:

wavelength:	$\lambda = 546.07 \text{ nm}$
object distance	100 mm
thickness of the lens, made of N-BK7	$t = 8 \text{ mm}$
front radius of curvature	$R1 = 45 \text{ mm}$
rear radius of curvature	$R2 = -100 \text{ mm}$
numerical aperture in the object space	$NA = 0.07$
lens diameter	24 mm

- Fix the final distance in the paraxial image plane. Create a layout plot
- Calculate the spot diagram and the transverse ray aberrations.
What is the spot size ?
Is the system diffraction limited ?
What residual aberration is obtained ?
Are also higher order aberrations obtained ?
Determine the image sided numerical aperture by calculating the marginal ray.
- Add an off axis field point with height $y = 10 \text{ mm}$.
Fix the pupil of the system at the rear surface of the lens
Find the best plane for gathering the image. Is the distance increased or decreased ?
Calculate the layout and the spot diagram. What is the dominating aberration for the field point now ?
- Add a second lens and give both lenses roughly the same focal power by keeping the system focal length constant.
Is the system performance improved and diffraction limited ?
Calculate the Seidel aberrations and discuss the opportunities of improving the system for spherical aberration.
Reverse the first lens and reduce the numerical aperture to $NA = 0.04$. Calculate the performance now.
Calculate the point spread function and determine the Strehl ratio on axis.

Solution

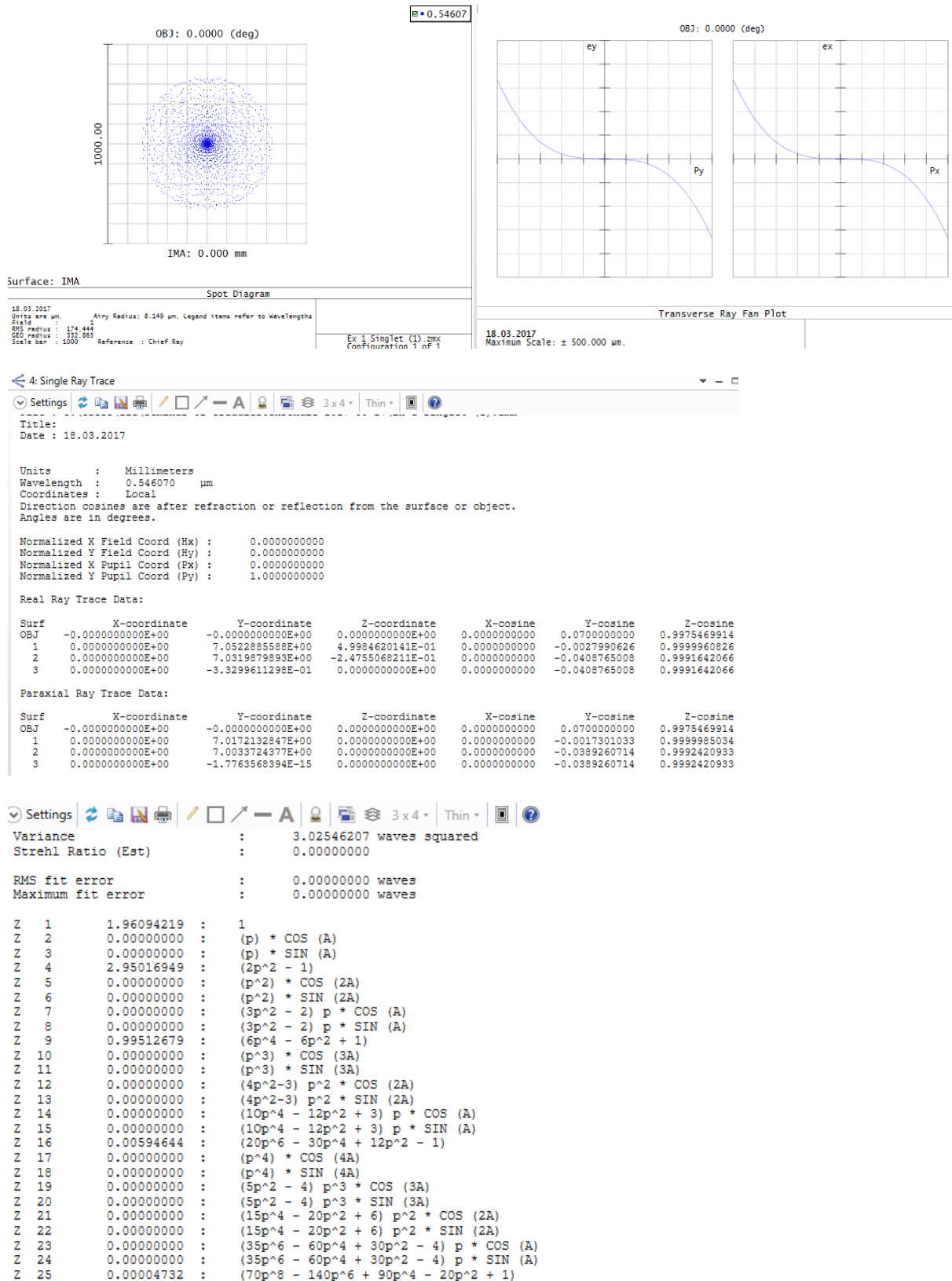
- Starting setup:

	Surf:Type	Comment	Radius	Thickness	Material	Coating	Clear Semi-Di
0	OBJECT Standard ▼		Infinity	100.0000			0.0000
1	(aper) Standard ▼		50.0000	8.0000	N-BK7		12.0000 U
2	STOP (s Standard ▼		-100.00...	179.7783	M		12.0000 U
3	IMAGE Standard ▼		Infinity	-			0.3330



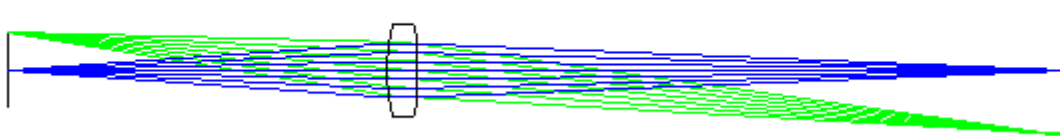
- The spot radius rms value is $175 \mu\text{m}$ and is far above the Airy radius of $8.1 \mu\text{m}$.
The image sided numerical aperture is $NA = 0.0408$, the paraxial value is $NA_i = 0.0389$
The residual aberration is pure spherical aberration.

By inspection the Zernike coefficients it is found $c_9 = 0.995$ and $c_{16} = 0.006$, therefore we have dominating 3rd order spherical aberration.



c)
The distance is decreased by approx. 8 mm.

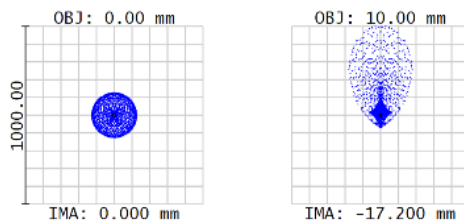
Lens Data									
Update: Editors Only									
Surface 3 Properties									
	Surf>Type	Comment	Radius	Thickness	Material	Coating	Clear	Semi-Di	
0	OBJECT Standard		Infinity	100.0000				10.0000	
1	(aper) Standard		50.0000	8.0000	N-BK7			12.0000	U
2	STOP (ε Standard		-100.00...	171.5061				12.0000	U
3	IMAGE Standard		Infinity	-				17.2702	



From the spot diagram it cannot be distinguished between defocus/curvature, astigmatism and coma. With the Zernikes coefficients, we get:

curvature $c4 = 0.95$
astigmatism $c5 = -2.87$
coma $c8 = -1.81$

This means, the astigmatism is the largest contribution.



Surface: IMA									
Spot Diagram									
18.03.2017									
Units are μm. Airy Radius: 8.149 μm. Legend items refer to Wavelengths									
Field	:	1							
RMS radius	:	93.665	148.738						
GEO radius	:	125.099	501.225						
Field	:	1							
Ex 1 Sina									
Z	1	-0.04184837	:	1					
Z	2	0.00000000	:	(p) * COS (A)					
Z	3	-3.59217247	:	(p) * SIN (A)					
Z	4	0.94674417	:	(2p^2 - 1)					
Z	5	-2.86686119	:	(p^2) * COS (2A)					
Z	6	0.00000000	:	(p^2) * SIN (2A)					
Z	7	0.00000000	:	(3p^2 - 2) p * COS (A)					
Z	8	-1.81457447	:	(3p^2 - 2) p * SIN (A)					
Z	9	0.99464944	:	(6p^4 - 6p^2 + 1)					
Z	10	0.00000000	:	(p^3) * COS (3A)					
Z	11	-0.00913479	:	(p^3) * SIN (3A)					
Z	12	-0.00299627	:	(4p^2-3) p^2 * COS (2A)					
Z	13	0.00000000	:	(4p^2-3) p^2 * SIN (2A)					
Z	14	0.00000000	:	(10p^4 - 12p^2 + 3) p * COS (A)					
Z	15	-0.01263220	:	(10p^4 - 12p^2 + 3) p * SIN (A)					
Z	16	0.00610625	:	(20p^6 - 30p^4 + 12p^2 - 1)					