



**Institute of
Applied Physics**

Friedrich-Schiller-Universität Jena

Lens Design I

Lecture 2: Properties of optical systems I

2024-04-18

Ziyao Tang



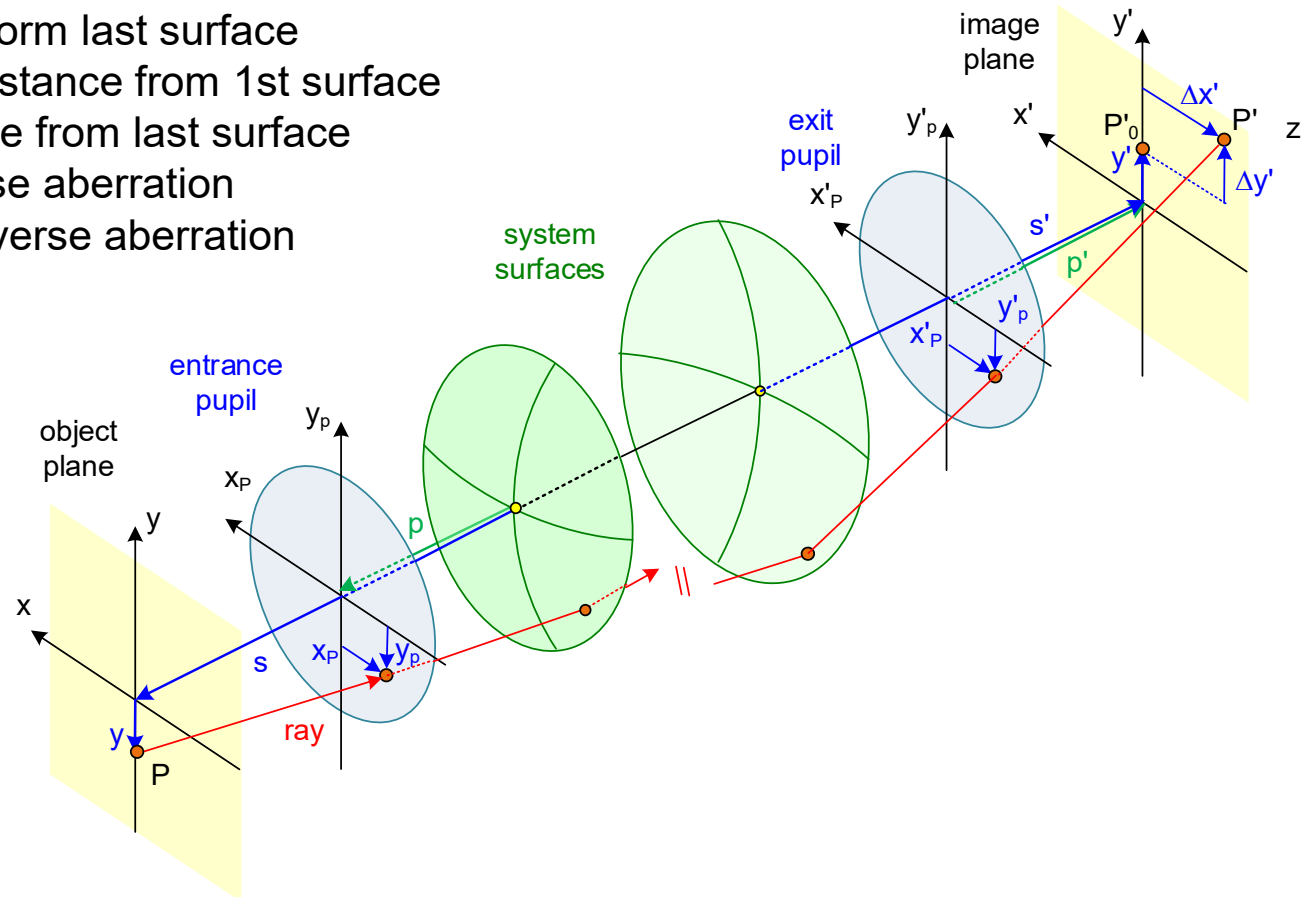
Preliminary Schedule - Lens Design I 2023

1	04.04.	Basics	Zhang	Introduction, Zemax interface, menus, file handling, preferences, Editors, updates, windows, coordinates, System description, 3D geometry, aperture, field, wavelength
2	18.04.	Properties of optical systems I	Tang	Diameters, stop and pupil, vignetting, layouts, materials, glass catalogs, raytrace, ray fans and sampling, footprints
3	25.04.	Properties of optical systems II	Tang	Types of surfaces, cardinal elements, lens properties, Imaging, magnification, paraxial approximation and modelling, telecentricity, infinity object distance and afocal image, local/global coordinates
4	02.05.	Properties of optical systems III	Tang	Component reversal, system insertion, scaling of systems, aspheres, gratings and diffractive surfaces, gradient media, solves
5	16.05.	Advanced handling I	Tang	Miscellaneous, fold mirror, universal plot, slider, multiconfiguration, lens catalogs
6	23.05.	Aberrations I	Zhang	Representation of geometrical aberrations, spot diagram, transverse aberration diagrams, aberration expansions, primary aberrations
7	30.05.	Aberrations II	Zhang	Wave aberrations, Zernike polynomials, measurement of quality
8	06.06.	Aberrations III	Tang	Point spread function, optical transfer function
9	13.06.	Optimization I	Tang	Principles of nonlinear optimization, optimization in optical design, general process, optimization in Zemax
10	20.06.	Optimization II	Zhang	Initial systems, special issues, sensitivity of variables in optical systems, global optimization methods
11	27.06.	Correction I	Zhang	Symmetry principle, lens bending, correcting spherical aberration, coma, astigmatism, field curvature, chromatical correction
12	04.07.	Correction II	Zhang	Field lenses, stop position influence, retrofocus and telephoto setup, aspheres and higher orders, freeform systems, miscellaneous

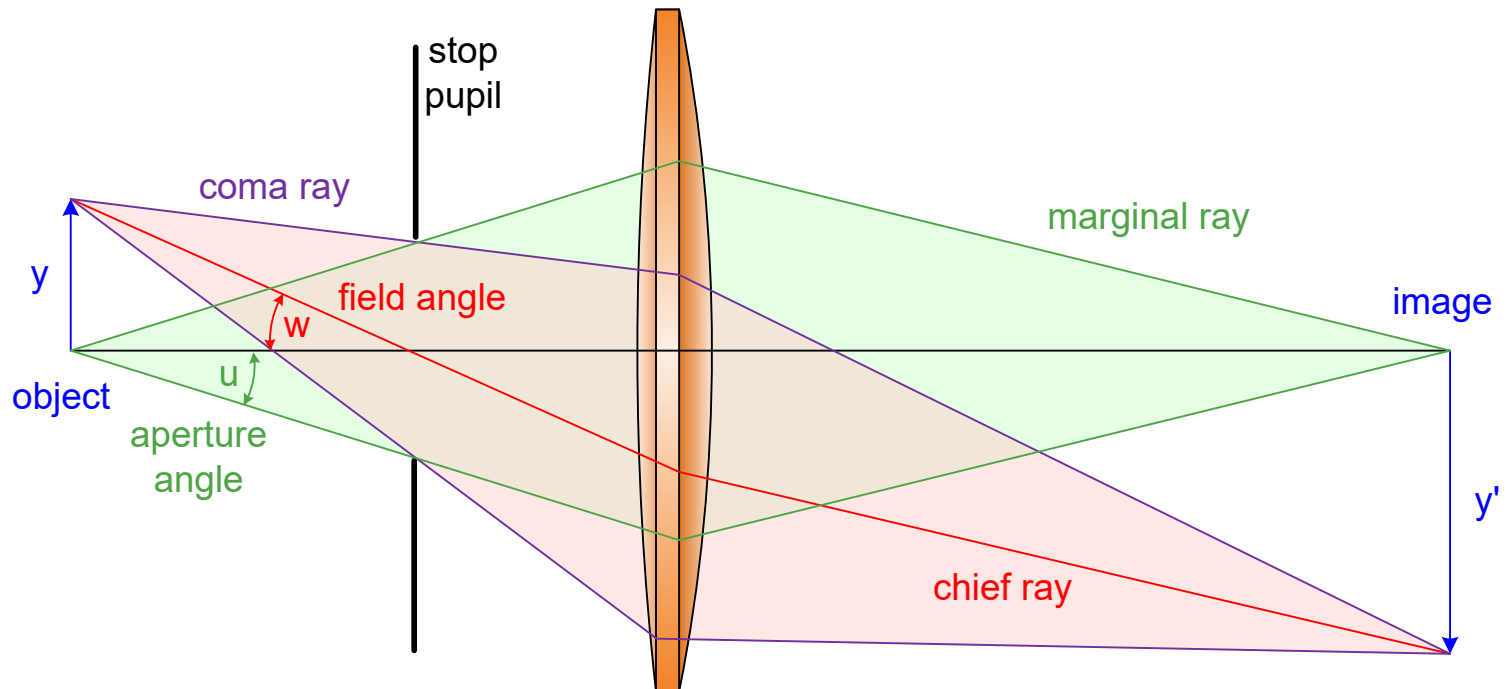


1. Stop and Pupil
2. Vignetting
3. Materials and glass catalogs
4. Raytrace
5. Ray fans and sampling
6. Footprints

x, y	object coordinates, especially object height
x', y'	image coordinates, especially image height
x_p, y_p	coordinates of entrance pupil
x'_p, y'_p	coordinates of exit pupil
s	object distance from 1st surface
s'	image distance from last surface
p	entrance pupil distance from 1st surface
p'	exit pupil distance from last surface
$\Delta x'$	sagittal transverse aberration
$\Delta y'$	meridional transverse aberration

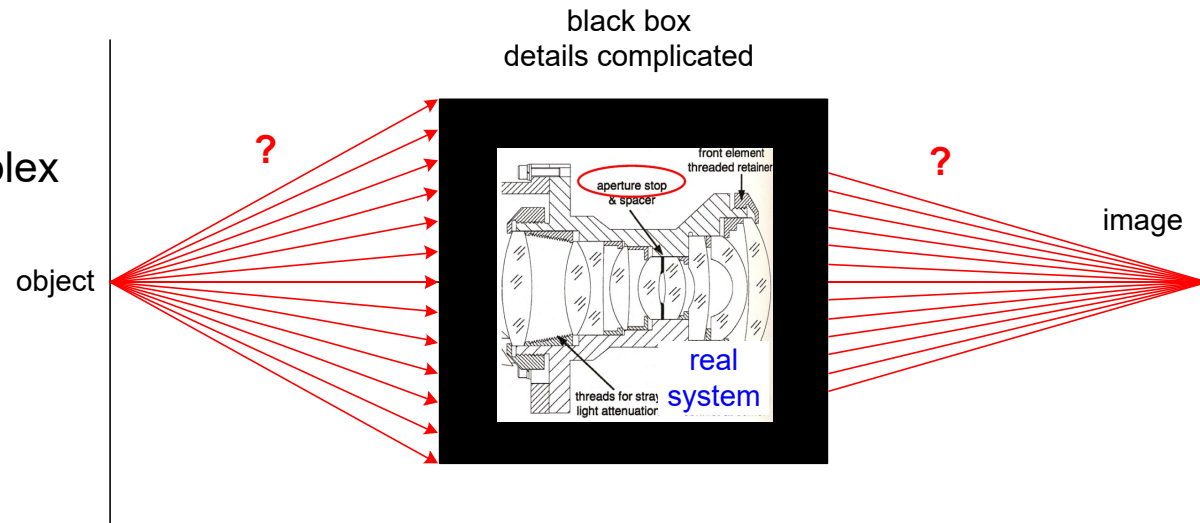


- Stop: determine chief ray and marginal ray
 1. chief ray angle w
 2. aperture cone angle u
- The chief ray gives the center line of the oblique ray cone of an off-axis object point
- The coma rays limit the off-axis ray cone
- The marginal rays limit the axial ray cone

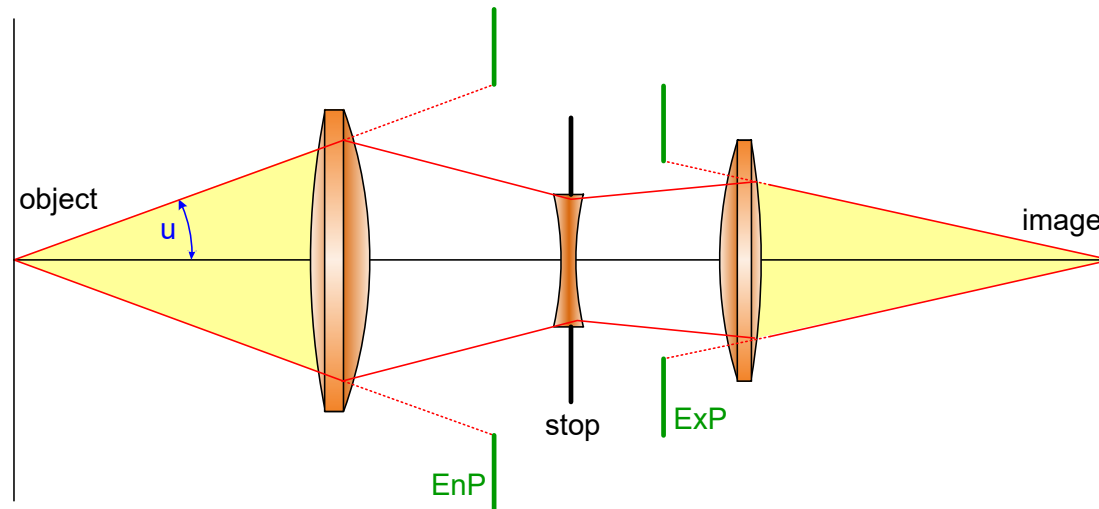


Optical system stop

- The physical stop defines the aperture cone angle u
- The real system may be complex



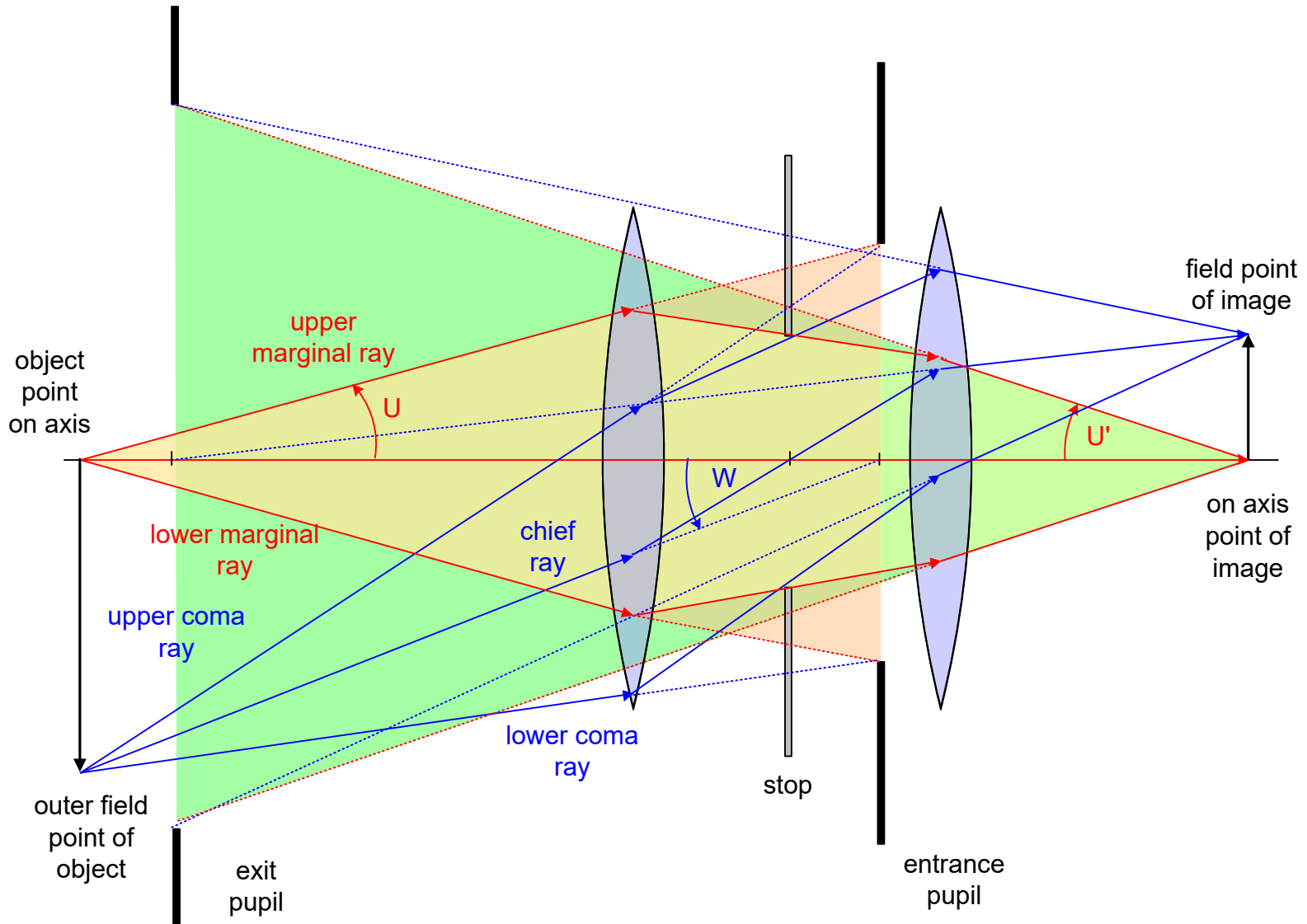
- The entrance pupil fixes the acceptance cone in the object space
- The exit pupil fixes the acceptance cone in the image space



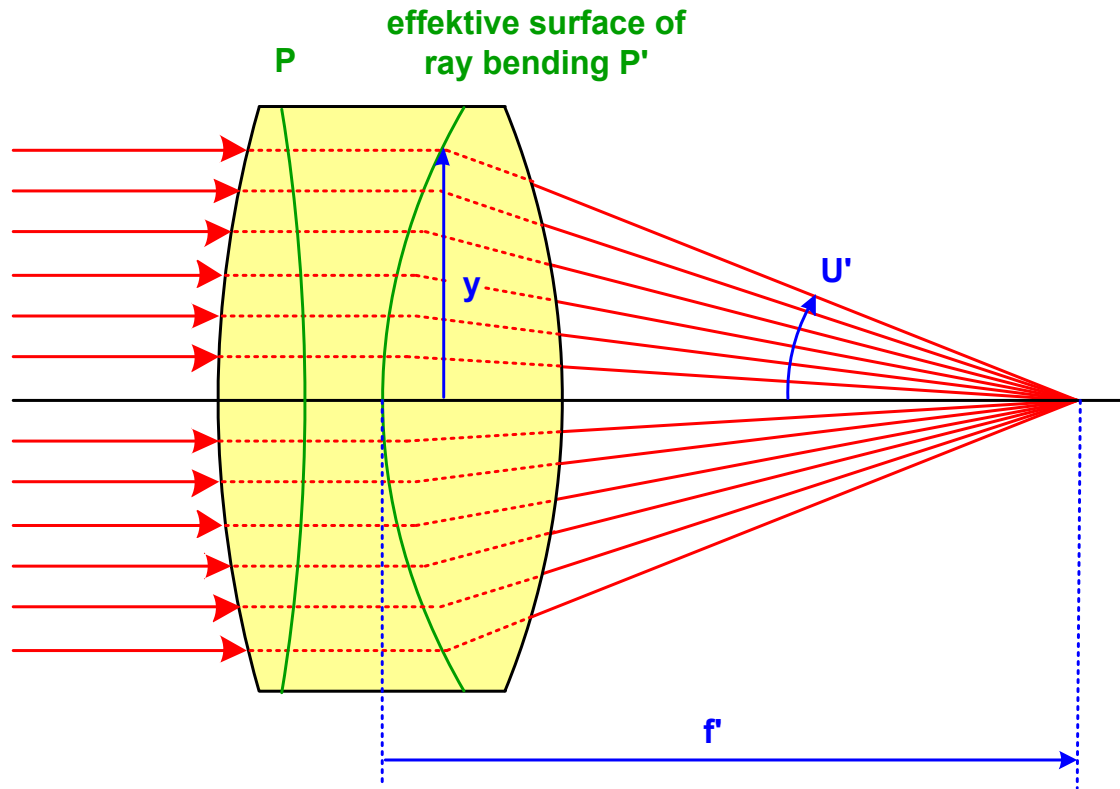
Relevance of the system pupil :

- Brightness of the image
Transfer of energy
- Resolution of details
Information transfer
- Image quality
Aberrations due to aperture
- Image perspective
Perception of depth
- Compound systems:
matching of pupils is necessary, location and size

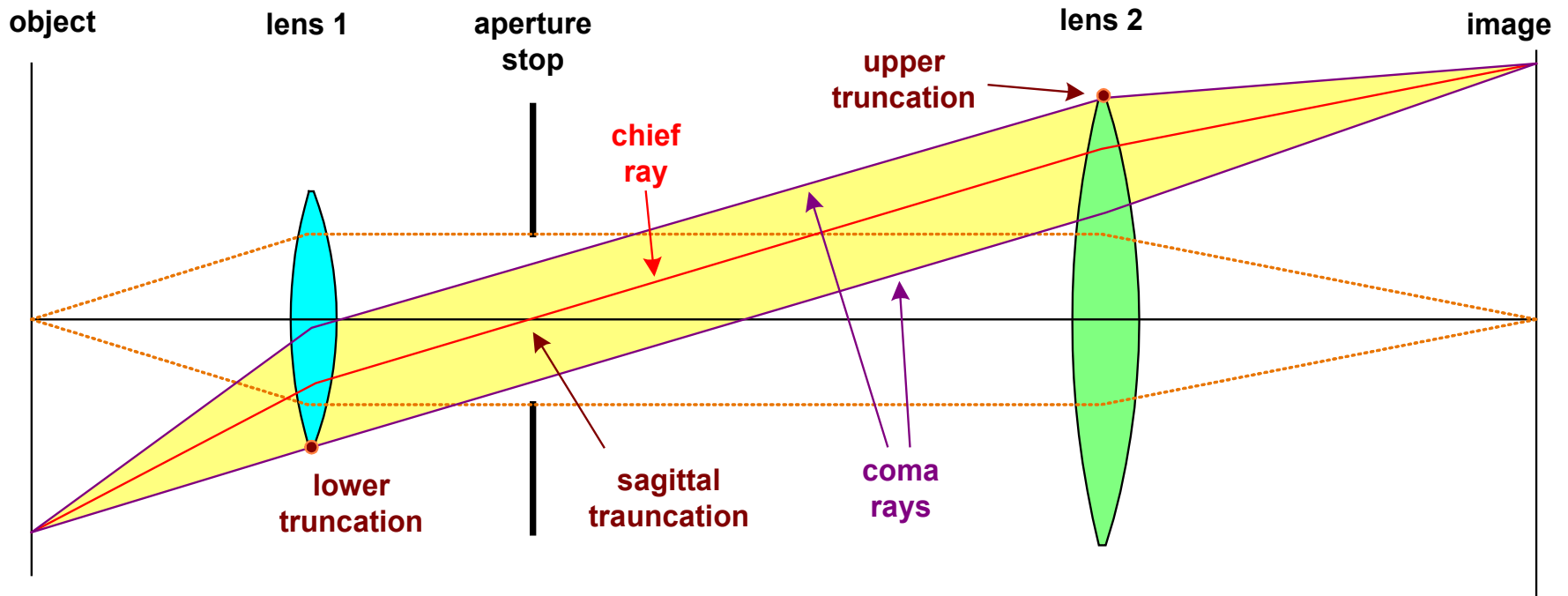
Entrance and exit pupil



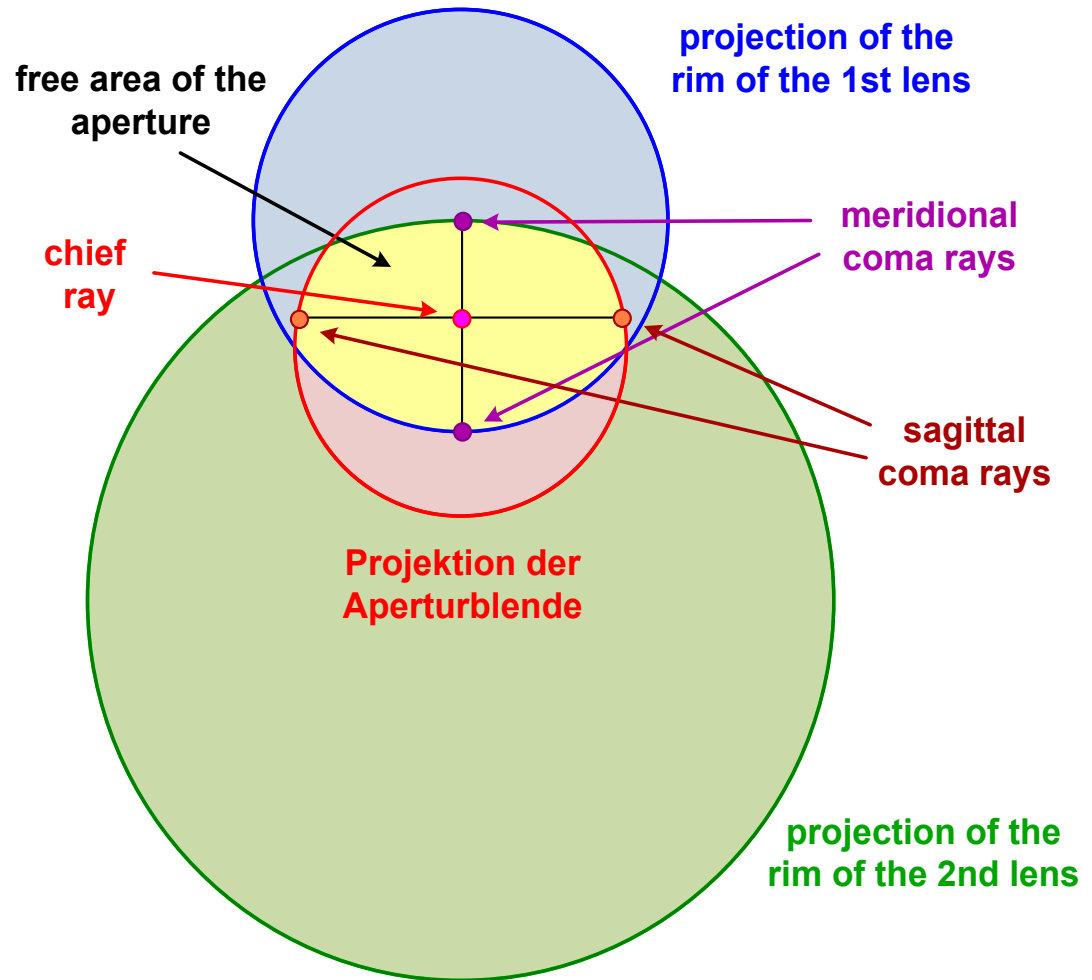
- Generalization of paraxial picture:
Principal surface works as effective location of ray bending
- Paraxial approximation: plane
- Real systems with corrected
sine-condition (aplanatic):
principal sphere



- 3D-effects due to physical sizes
- Truncation of the ray bundles at different surfaces for the upper and the lower part of the cone



- Truncation of the light cone with asymmetric ray path for off-axis field points
- Intensity decrease towards the edge of the image
- Definition of the chief ray: ray through energetic centroid
- Vignetting can be used to avoid uncorrectable coma aberrations in the outer field
- Effective free area with extrem aspect ratio: anamorphic resolution



- Important types of optical materials:
 1. Glasses
 2. Crystals
 3. Liquids
 4. Plastics, cement
 5. Gases
 6. Metals

- Optical parameters for characterization of materials
 1. Refractive index, spectral resolved $n(\lambda)$
 2. Spectral transmission $T(\lambda)$
 3. Reflectivity R
 4. Absorption
 5. Anisotropy, index gradient, eigenfluorescence,...

- Important non-optical parameters
 1. Thermal expansion coefficient
 2. Hardness
 3. Chemical properties (resistance,...)

Test wavelengths



λ in [nm]	Name	Color	Element
248.3		UV	Hg
280.4		UV	Hg
296.7278		UV	Hg
312.5663		UV	Hg
334.1478		UV	Hg
365.0146	i	UV	Hg
404.6561	h	violett	Hg
435.8343	g	blau	Hg
479.9914	F'	blau	Cd
486.1327	F	blau	H
546.0740	e	grün	Hg
587.5618	d	gelb	He
589.2938	D	gelb	Na
632.8			HeNe-Laser
643.8469	C'	rot	Cd
656.2725	C	rot	H
706.5188	r	rot	He
852.11	s	IR	Cä
1013.98	t	IR	Hg
1060.0			Nd:YAG-Laser

- Description of dispersion:

Abbe number
$$\nu(\lambda) = \frac{n(\lambda) - 1}{n_{F'} - n_{C'}}$$

- Visual range of wavelengths:

$$V_e = \frac{n_e - 1}{n_{F'} - n_{C'}}$$

- Typical range of glasses

$$\nu_e = 20 \dots 120$$

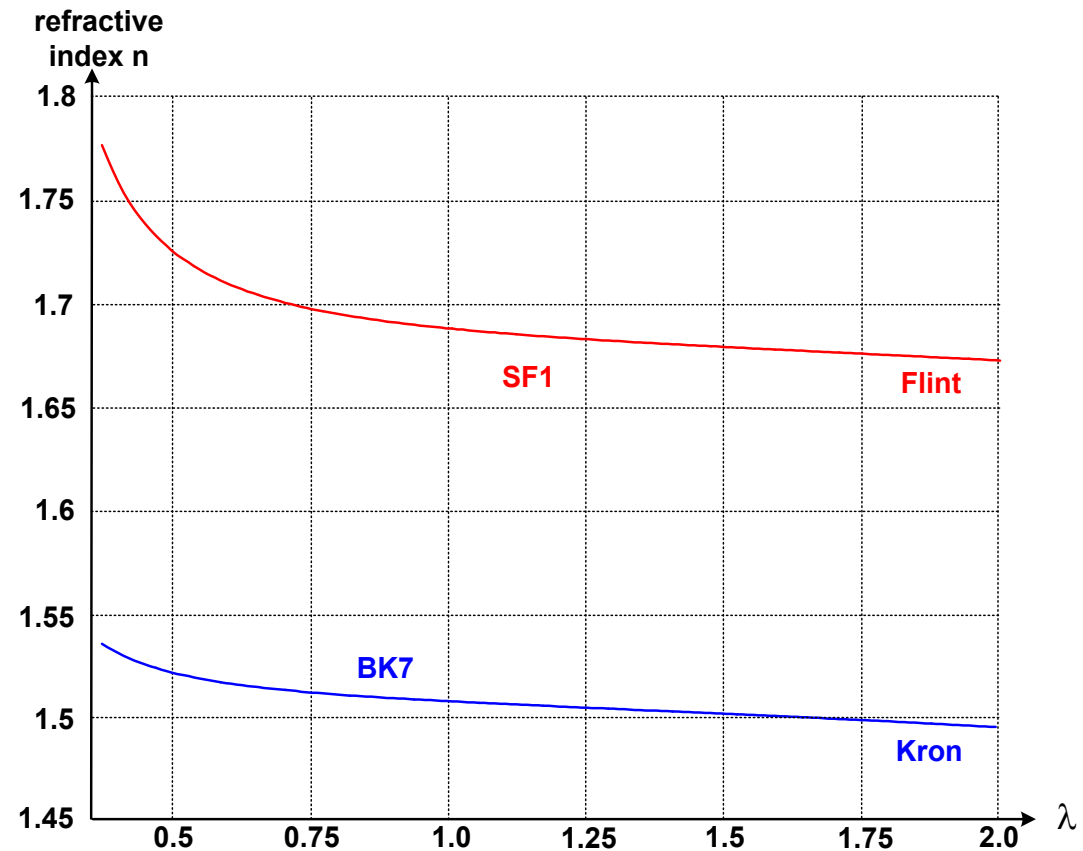
- Two fundamental types of glass:

Crown glasses:

n small, ν large

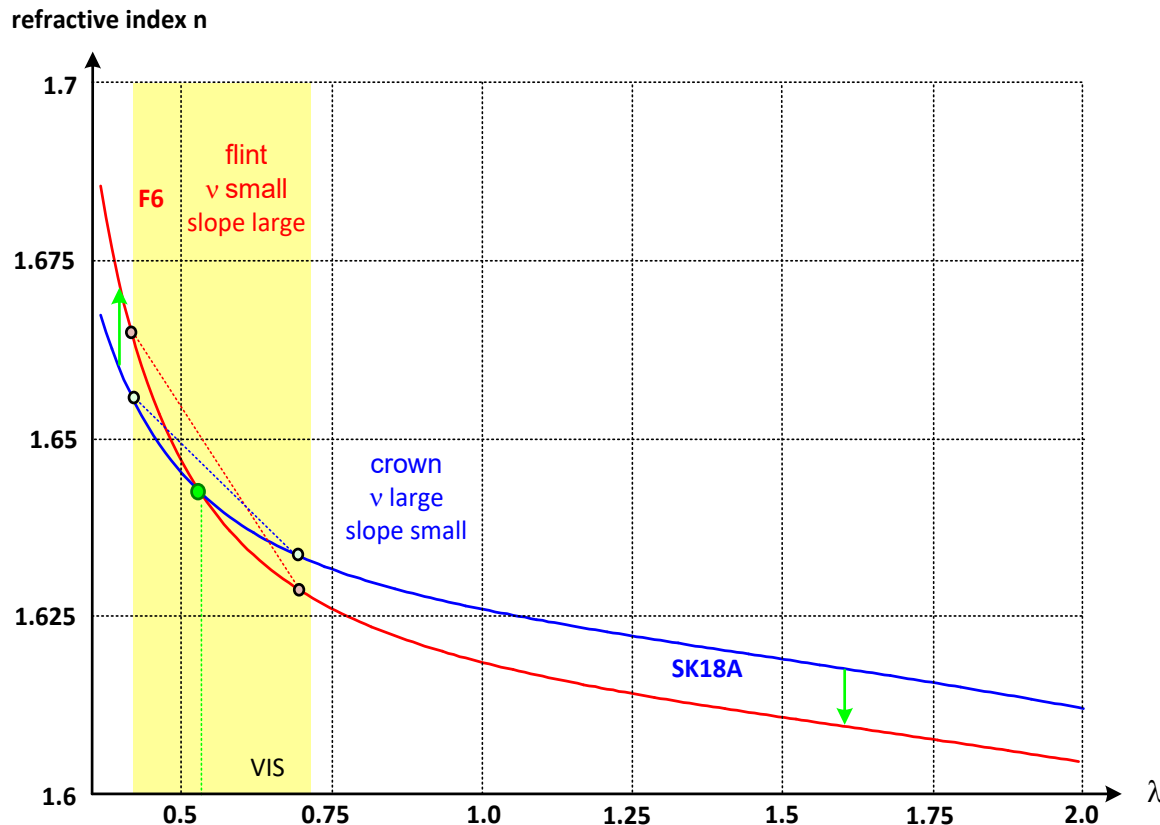
Flint glasses

n large, ν small



Material with different dispersion values:

- Different slope and curvature of the dispersion curve
- Stronger change of index over wavelength for large dispersion
- Inversion of index sequence at the boundaries of the spectrum possible



- Schott formula
empirical

$$n = \sqrt{a_o + a_1 \lambda^2 + a_2 \lambda^{-2} + a_3 \lambda^{-4} + a_4 \lambda^{-6} + a_5 \lambda^{-8}}$$

- Sellmeier
Based on oscillator model

$$n(\lambda) = \sqrt{A + B \frac{\lambda^2}{\lambda^2 - \lambda_1^2} + C \frac{\lambda^2}{\lambda^2 - \lambda_2^2}}$$

- Bausch-Lomb
empirical

$$n(\lambda) = \sqrt{A + B \lambda^2 + C \lambda^4 + \frac{D}{\lambda^2} + \frac{E \lambda^2}{(\lambda^2 - \lambda_o^2) + \frac{F \lambda^2}{\lambda^2 - \lambda_o^2}}}$$

- Herzberger
Based on oscillator model

$$n(\lambda) = a_o + a_1 \lambda^2 + \frac{a_2}{\lambda^2 - \lambda_o^2} + \frac{a_3}{(\lambda^2 - \lambda_o^2)^2}$$

mit $\lambda_o = 0.168 \mu m$

- Hartmann
Based on oscillator model

$$n(\lambda) = a_o + \frac{a_1}{a_3 - \lambda} + \frac{a_4}{a_5 - \lambda}$$

- Relative partial dispersion :
Change of dispersion slope with λ
- Definition of local slope for selected wavelengths relative to secondary colors

$$P_{\lambda_1\lambda_2} = \frac{n(\lambda_1) - n(\lambda_2)}{n_{F'} - n_{C'}}$$

- Special selections for characteristic ranges of the visible spectrum

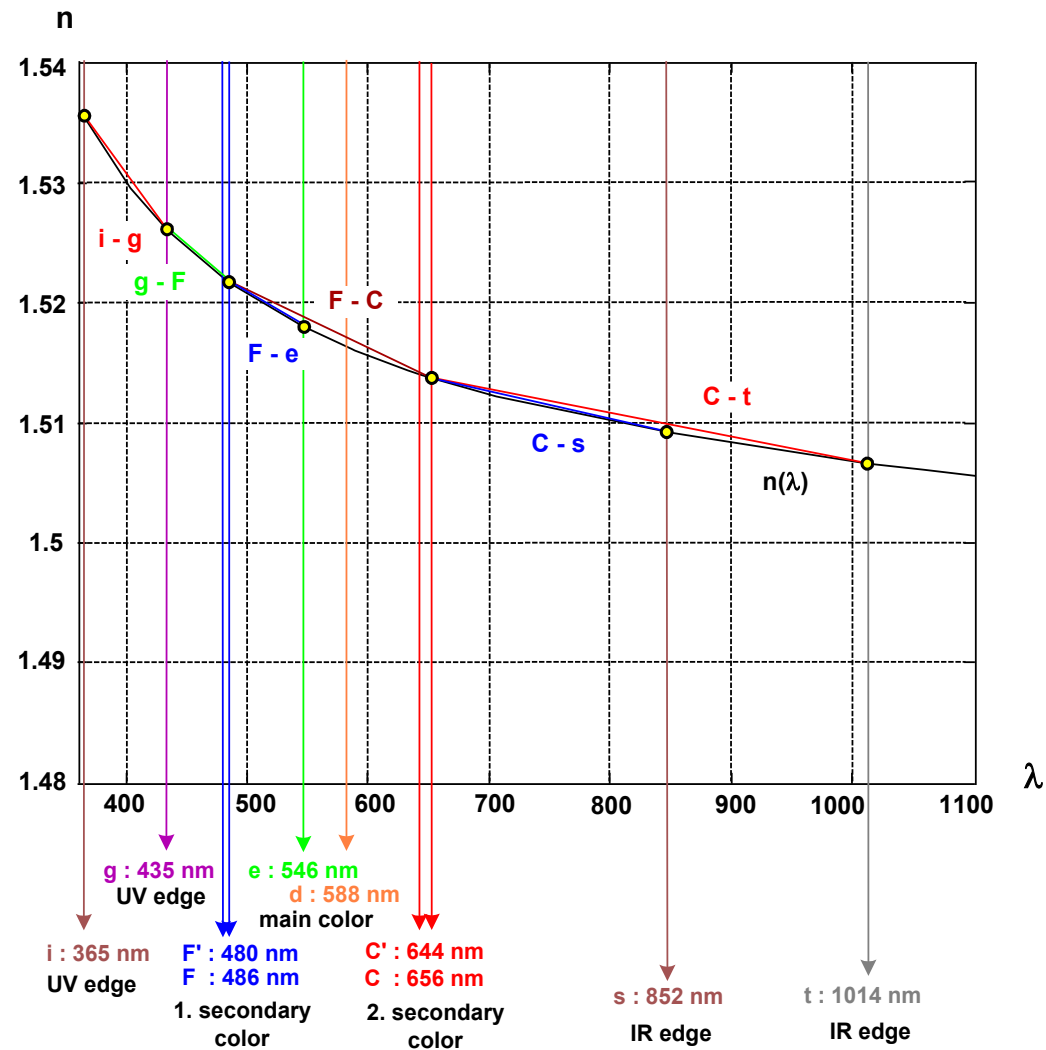
$\lambda = 656 / 1014 \text{ nm}$ far IR

$\lambda = 656 / 852 \text{ nm}$ near IR

$\lambda = 486 / 546 \text{ nm}$ blue edge of VIS

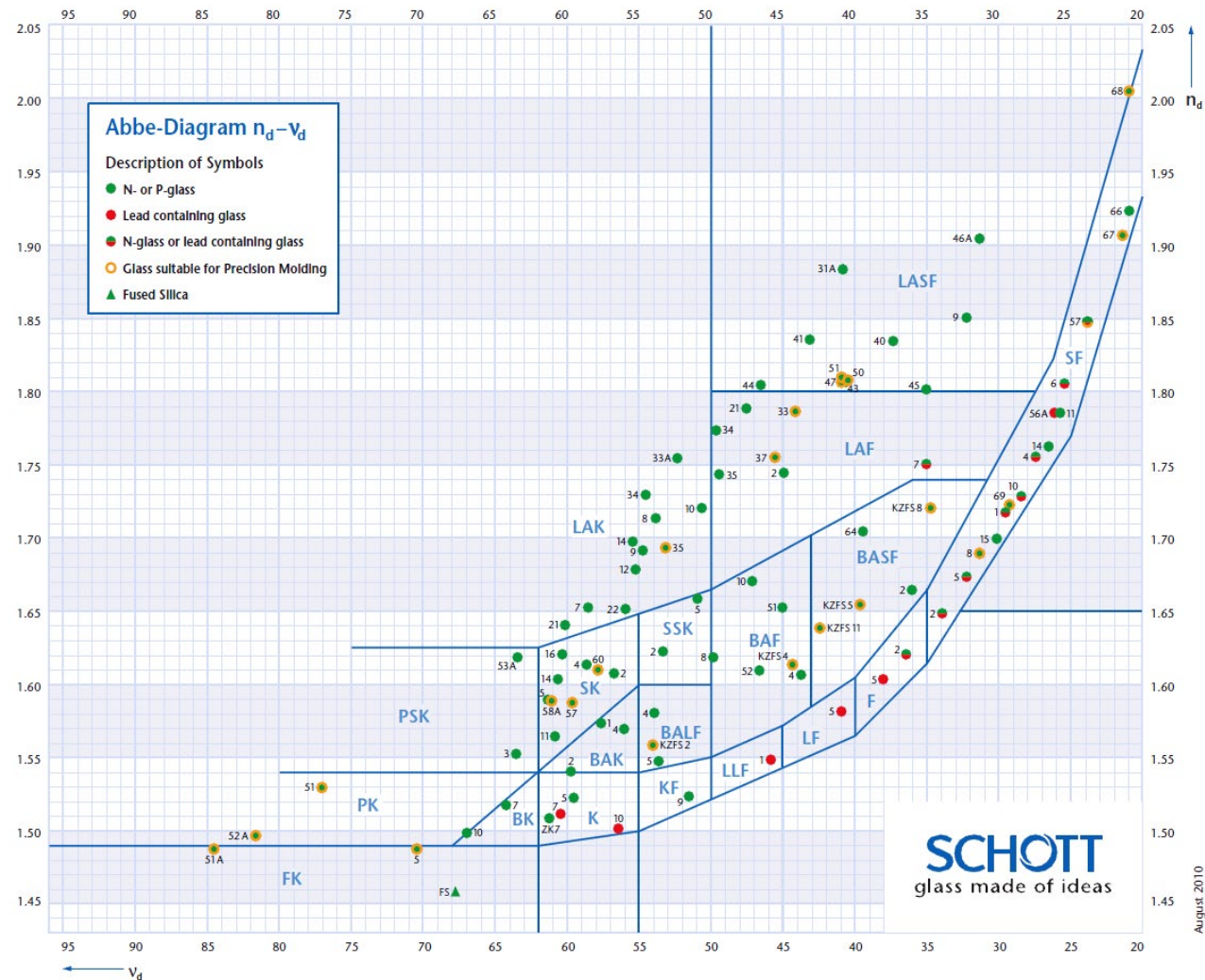
$\lambda = 435 / 486 \text{ nm}$ near UV

$\lambda = 365 / 435 \text{ nm}$ far UV



Glass diagram

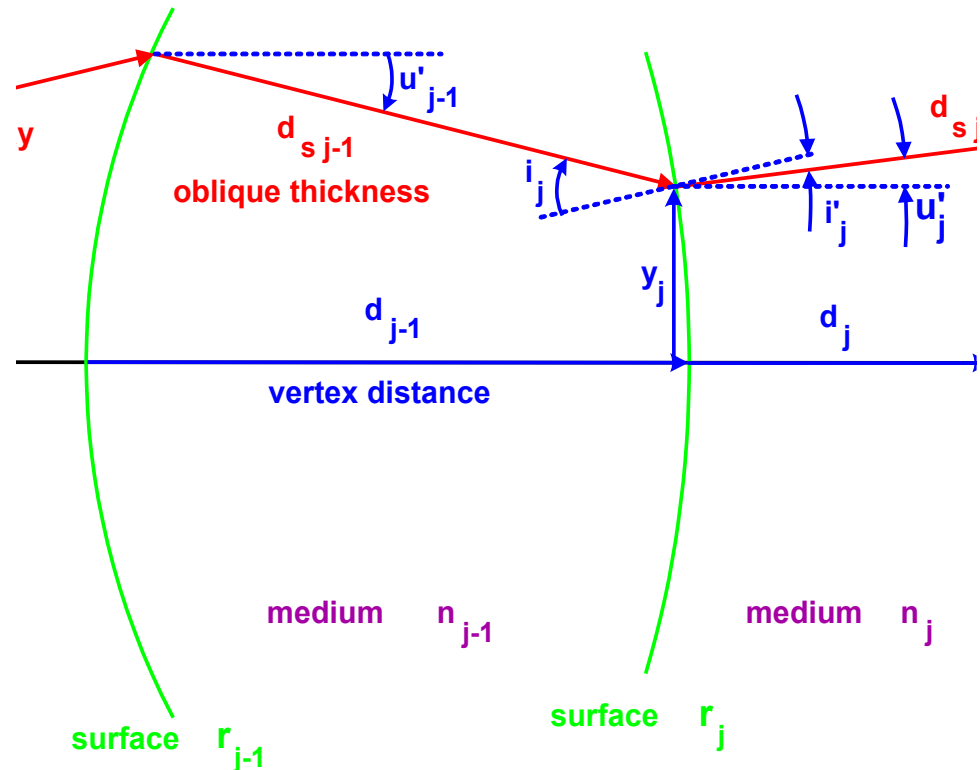
- Usual representation of glasses:
diagram of refractive index vs dispersion $n(v)$
- Left to right:
decreasing Abbe number
Increasing dispersion

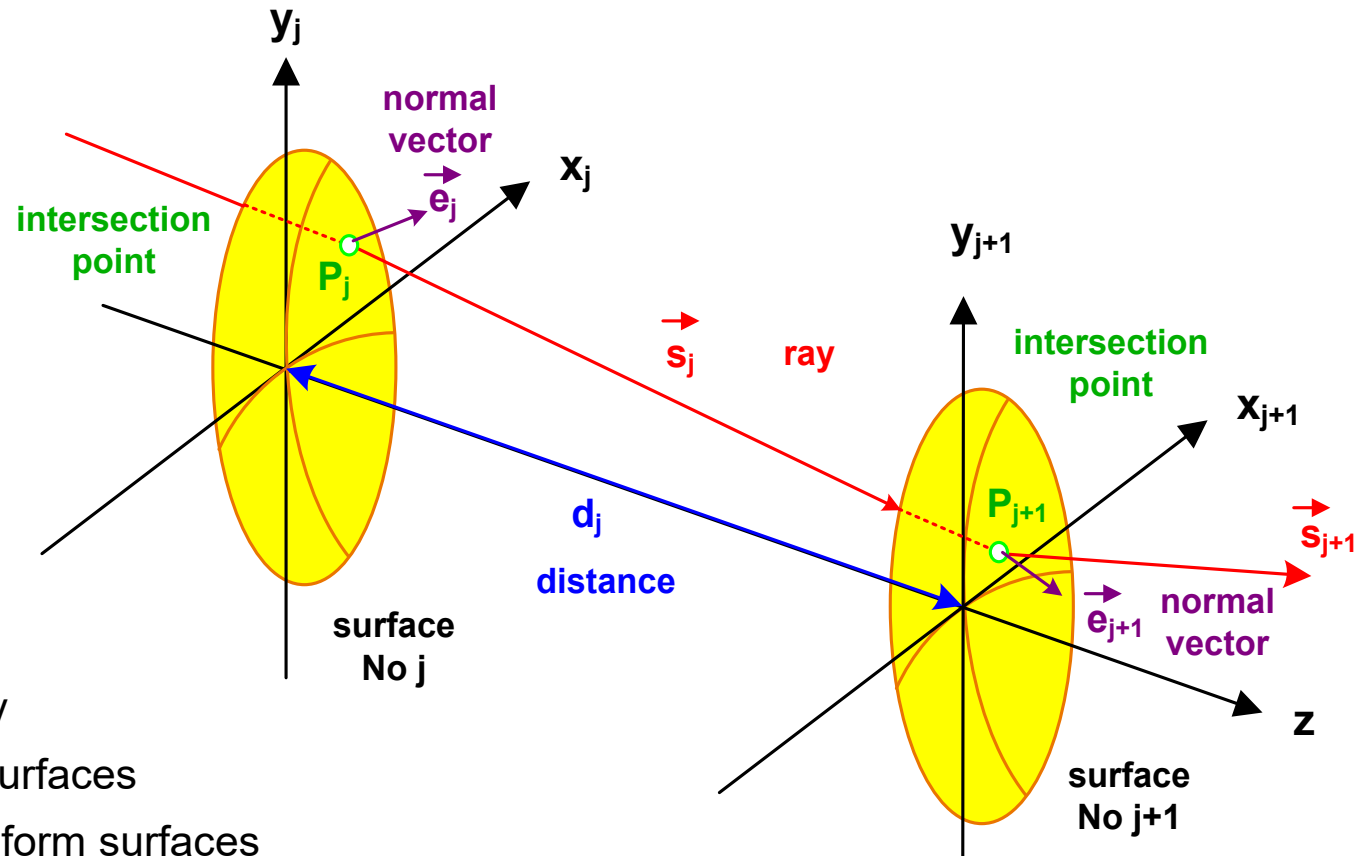




Scheme of raytrace

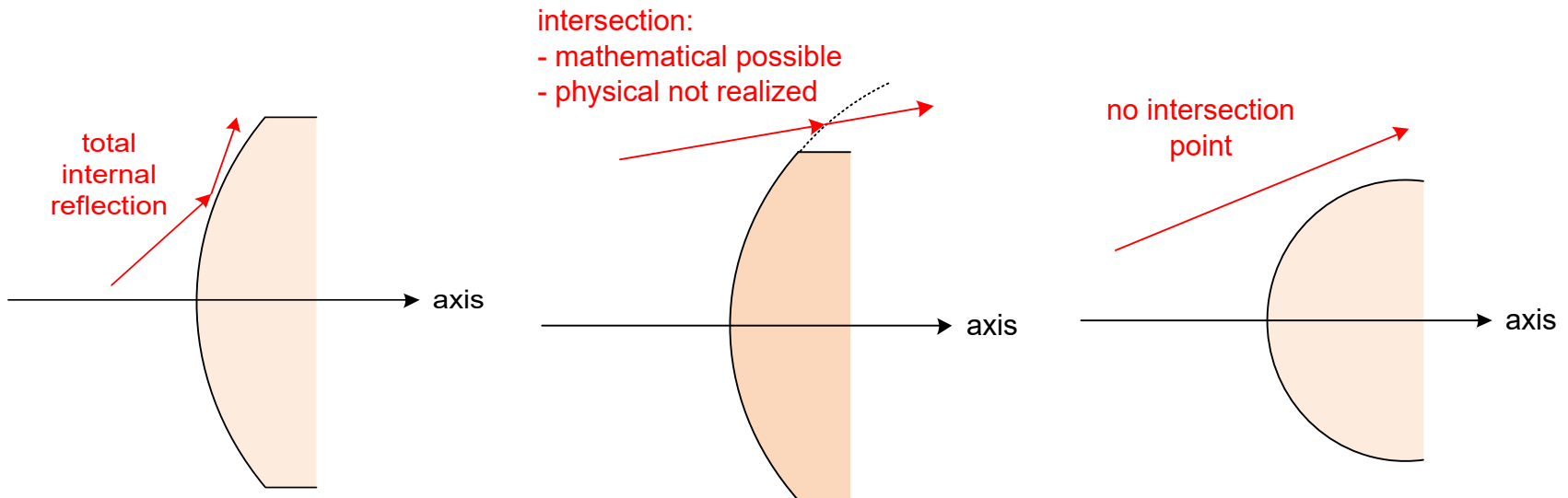
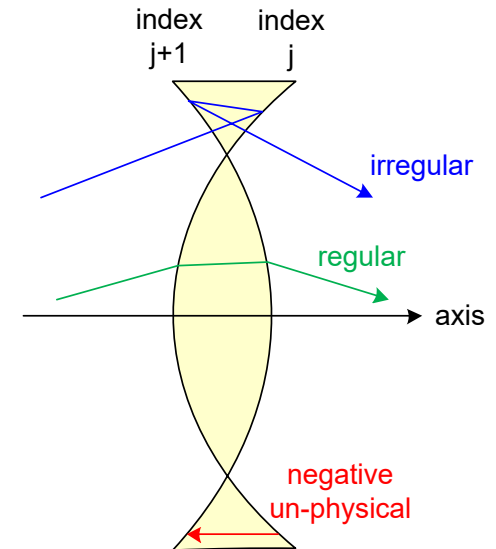
- Ray: straight line between two intersection points
- System: sequence of spherical surfaces
- Data: - radii, curvature $c=1/r$
 - vertex distances
 - refractive indices
 - transverse diameter
- Surfaces of 2nd order:
Calculation of intersection points
analytically possible: fast
computation





- General 3D geometry
- Tilt and decenter of surfaces
- General shaped free form surfaces
- Full description with 3 components
- Global and local coordinate systems

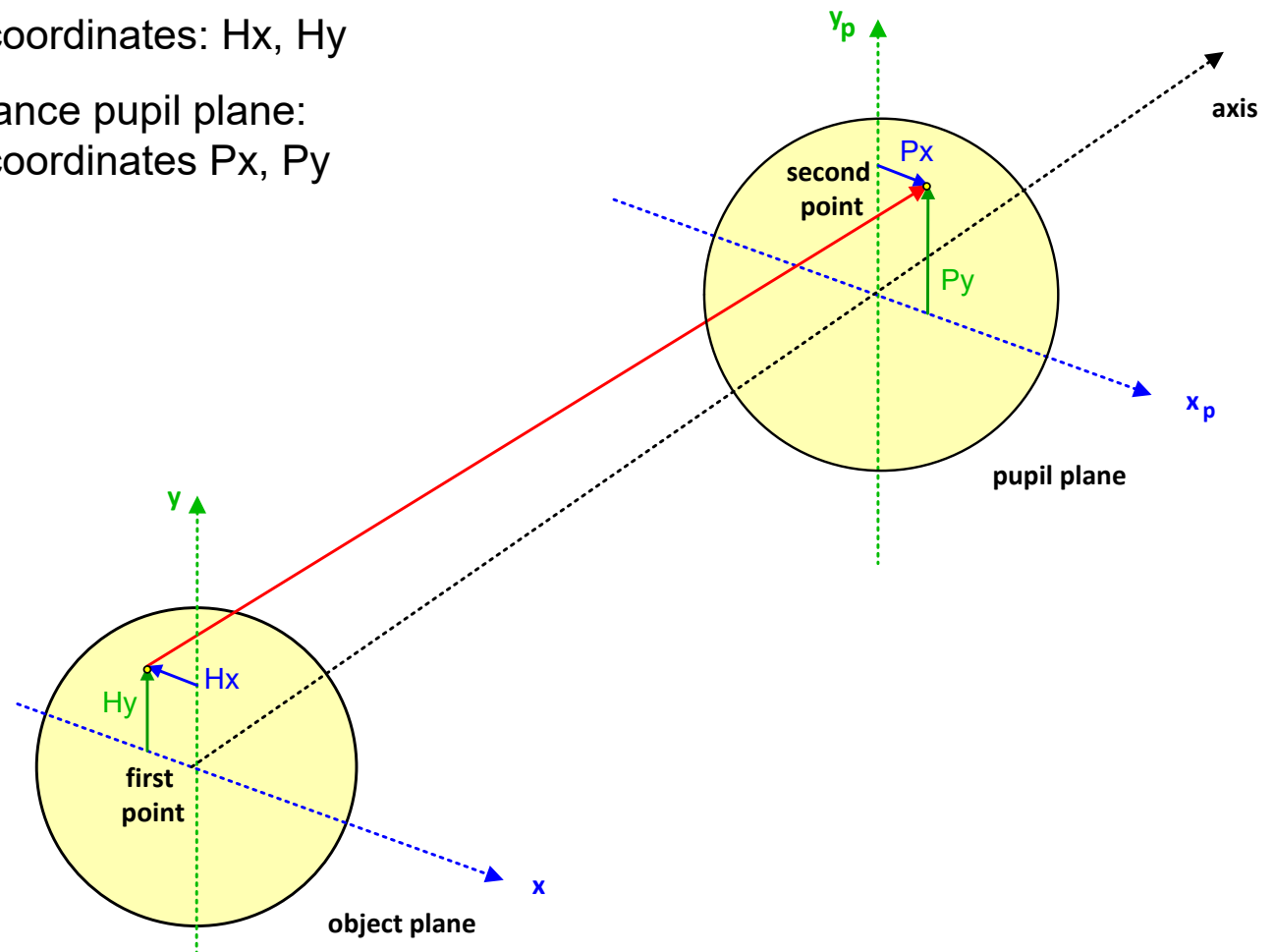
- Vignetting/truncation of ray at finite sized diameter:
can or can not considered (optional)
- No physical intersection point of ray with surface
- Total internal reflection
- Negative edge thickness of lenses
- Negative thickness without mirror-reflection
- Diffraction at boundaries



Single Ray Selection




- Definition of a single ray by two points
- First point in object plane:
relative normalized coordinates: H_x , H_y
- Second point in entrance pupil plane:
relative normalized coordinates P_x , P_y



Raytrace in Zemax

- Selection of 2 points on the ray on object and entrance pupil plane
- Real and paraxial rays are tabulated
- Coordinate reference can be selected to be local or global

3: Single Ray Trace

Settings  3 x 4 Standard Current ?

Hx: 0 Wavelength: 1
Hy: 0 Field: Arbitrary
Px: 0 Type: Direction Cosines
Py: 1 Global Coordinates: ☐

☒ Auto Apply Apply OK Cancel Save Load Reset

Configuration Twyman-Green Interferometer (2).ZMX

Normalized X Field Coord (Hx) : 0,0000000000
Normalized Y Field Coord (Hy) : 0,0000000000
Normalized X Pupil Coord (Px) : 0,0000000000
Normalized Y Pupil Coord (Py) : 1,0000000000

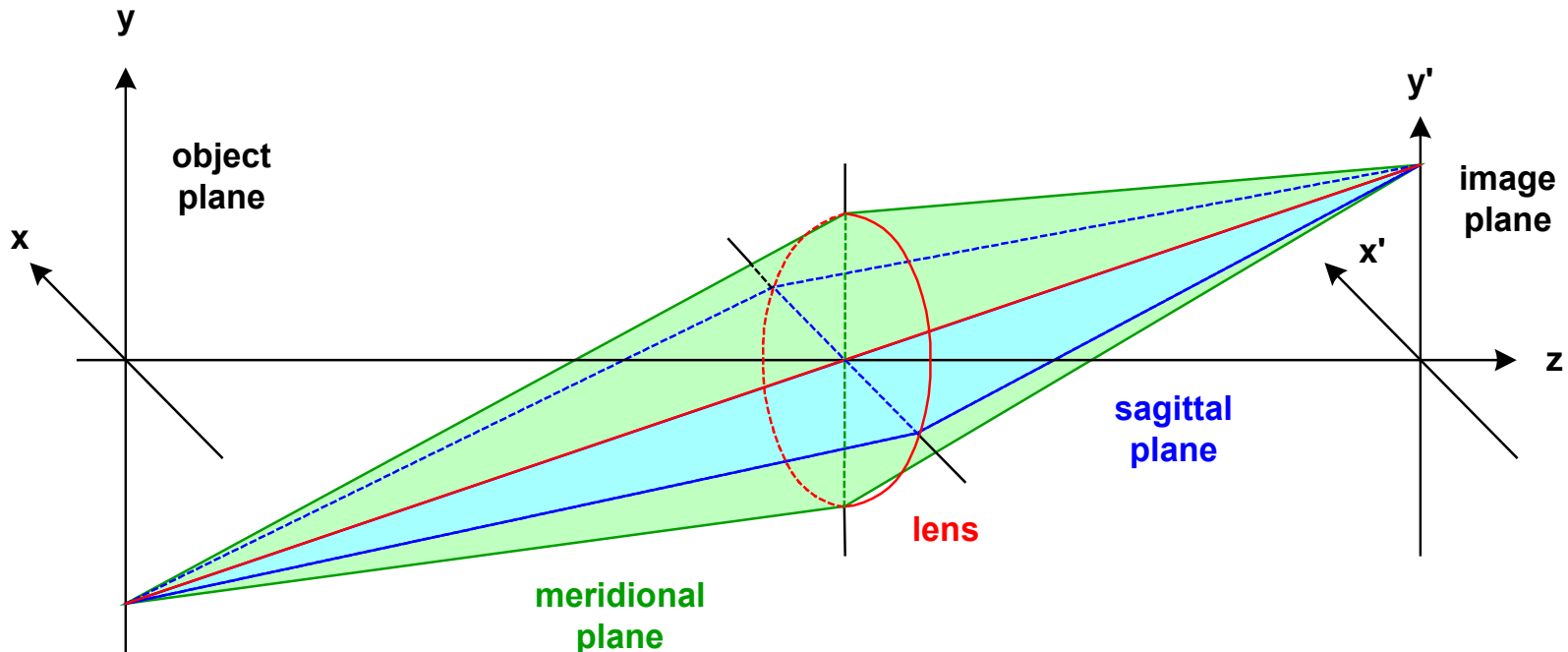
Real Ray Trace Data:

Surf	X-coordinate	Y-coordinate	Z-coordinate	X-cosine	Y-cosine	Z-cosine	X-normal
OBJ	Infinity	Infinity	Infinity	0,0000000000	0,0000000000	1,0000000000	-
1	0,0000000000E+000	5,0000000000E+000	0,0000000000E+000	0,0000000000	0,0000000000	1,0000000000	0,0000000000
15	0,0000000000E+000	5,0000000000E+000	0,0000000000E+000	0,0000000000	0,0000000000	1,0000000000	0,0000000000
16	0,0000000000E+000	7,0710678119E+000	0,0000000000E+000	0,0000000000	0,7071067812	0,7071067812	0,0000000000
17	0,0000000000E+000	7,0710678119E+000	0,0000000000E+000	-0,0000000000	-0,7071067812	0,7071067812	0,0000000000
18	0,0000000000E+000	5,0000000000E+000	0,0000000000E+000	-0,0000000000	0,0000000000	1,0000000000	0,0000000000
19	0,0000000000E+000	5,0000000000E+000	0,0000000000E+000	-0,0000000000	0,0000000000	1,0000000000	0,0000000000
20	0,0000000000E+000	5,0000000000E+000	0,0000000000E+000	-0,0000000000	0,0000000000	1,0000000000	0,0000000000
21	0,0000000000E+000	5,0000000000E+000	0,0000000000E+000	-0,0000000000	0,0000000000	1,0000000000	0,0000000000
22	0,0000000000E+000	5,0000000000E+000	0,0000000000E+000	-0,0000000000	0,0000000000	1,0000000000	0,0000000000
23	0,0000000000E+000	5,0000000000E+000	0,0000000000E+000	0,0000000000	-0,0000000000	1,0000000000	0,0000000000
24	0,0000000000E+000	5,0000000000E+000	0,0000000000E+000	0,0000000000	-0,0000000000	1,0000000000	0,0000000000
25	0,0000000000E+000	5,0000000000E+000	0,0000000000E+000	0,0000000000	-0,0000000000	1,0000000000	0,0000000000
26	0,0000000000E+000	5,0000000000E+000	0,0000000000E+000	0,0000000000	-0,0000000000	1,0000000000	0,0000000000
27	0,0000000000E+000	5,0000000000E+000	0,0000000000E+000	0,0000000000	-0,0000000000	1,0000000000	0,0000000000
28	0,0000000000E+000	5,0000000000E+000	1,2507822281E-001	0,0000000000	-0,0242654438	0,9997050651	0,0000000000
29	0,0000000000E+000	4,8815754337E+000	0,0000000000E+000	0,0000000000	-0,0471925164	0,9988858125	0,0000000000
30	0,0000000000E+000	7,4806915003E-002	0,0000000000E+000	0,0000000000	-0,0471925164	0,9988858125	0,0000000000

Paraxial Ray Trace Data:

Surf	X-coordinate	Y-coordinate	Z-coordinate	X-cosine	Y-cosine	Z-cosine	X-normal
OBJ	Infinity	Infinity	Infinity	0,0000000000	0,0000000000	1,0000000000	-
1	0,0000000000E+000	5,0000000000E+000	0,0000000000E+000	0,0000000000	0,0000000000	1,0000000000	0,0000000000
15	0,0000000000E+000	5,0000000000E+000	0,0000000000E+000	0,0000000000	0,0000000000	1,0000000000	0,0000000000
16	0,0000000000E+000	5,0000000000E+000	0,0000000000E+000	0,0000000000	0,0000000000	1,0000000000	0,0000000000

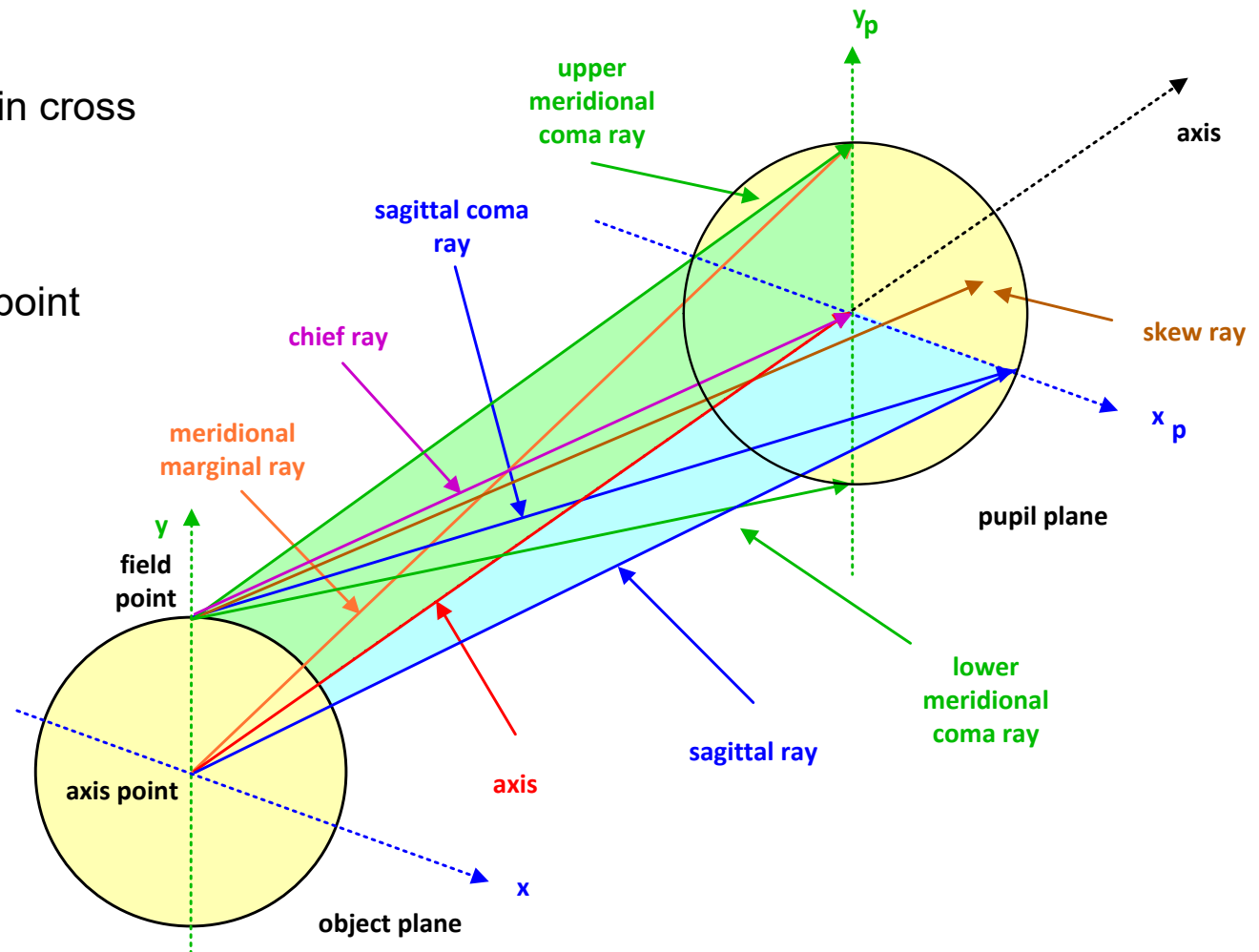
- Off-axis object point:
 - Meridional plane / tangential plane / main cross section plane contains object point and optical axis
 - Sagittal plane: perpendicular to meridional plane through object point



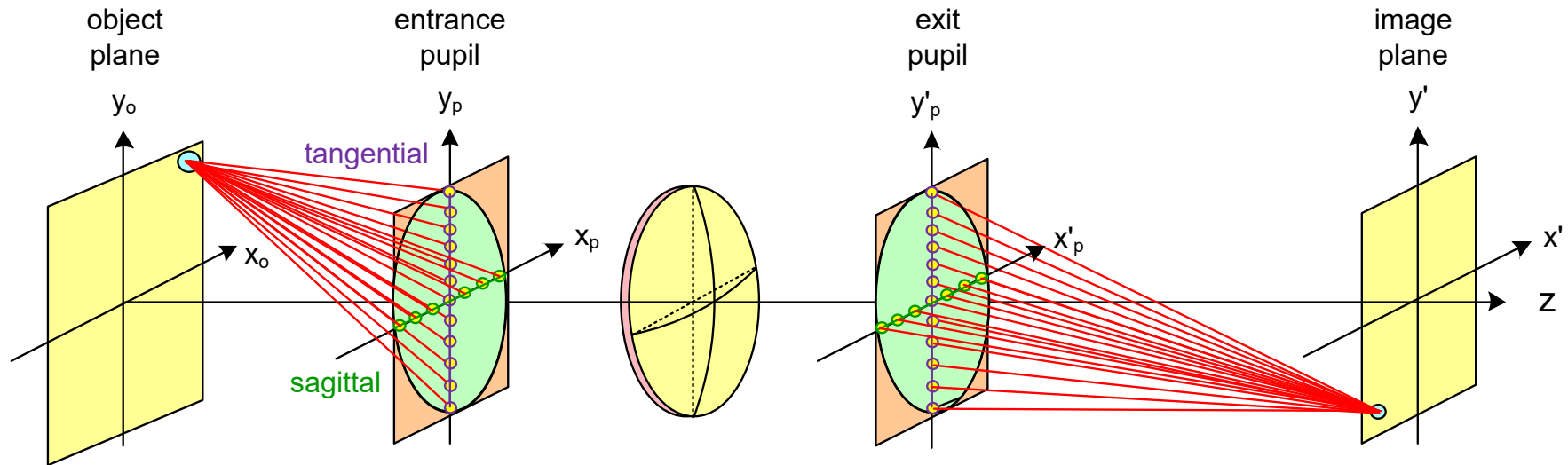
Special rays in 3D



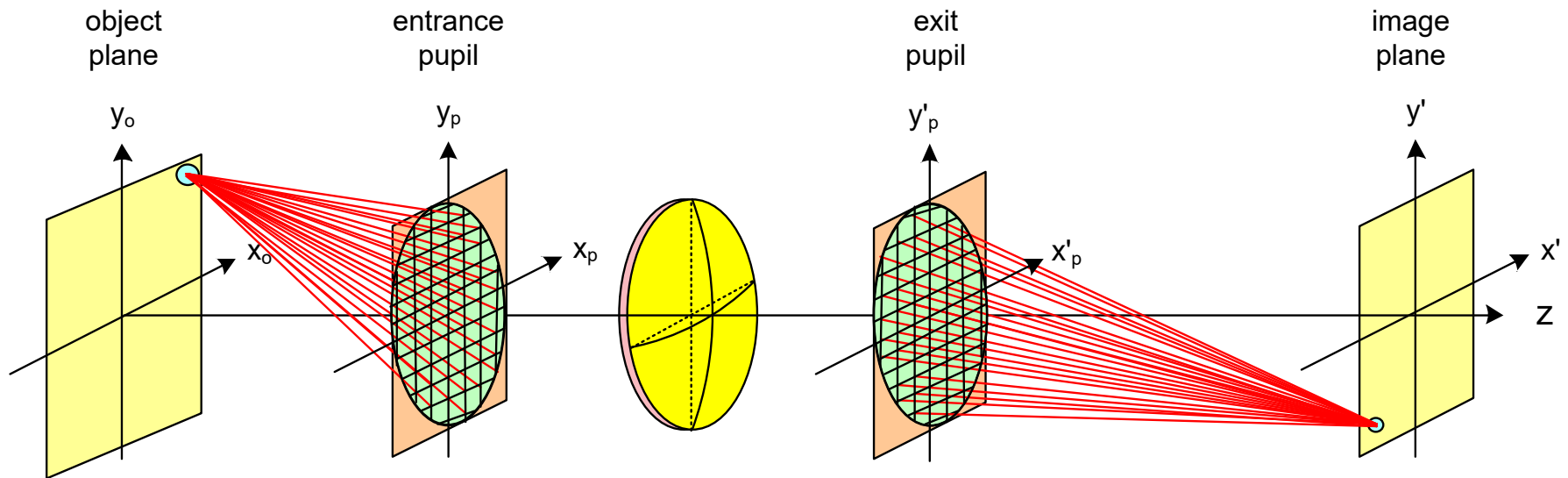
- Meridional rays:
in main cross section plane
- Sagittal rays:
perpendicular to main cross section plane
- Coma rays:
Going through field point
and edge of pupil
- Oblique rays:
without symmetry



- Pupil sampling for calculation of transverse aberrations:
all rays from one object point to all pupil points on x- and y-axis
- Two planes with 1-dimensional ray fans
- No complete information: no skew rays

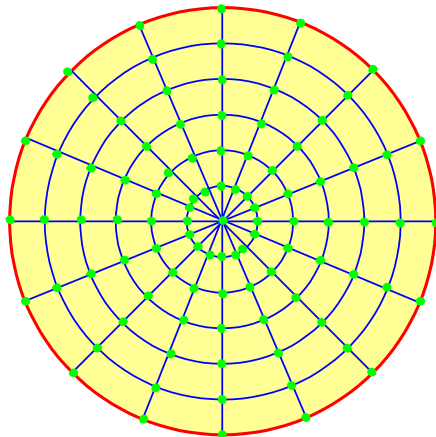


- Pupil sampling in 3D for spot diagram:
all rays from one object point through all pupil points in 2D
- Light cone completely filled with rays

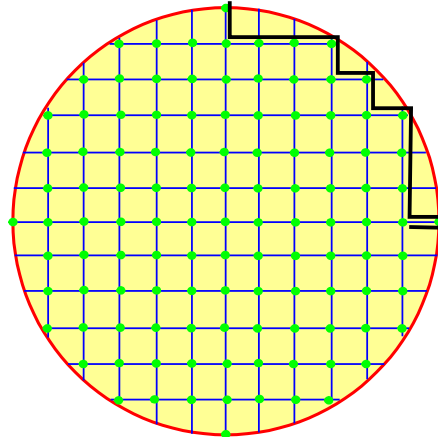


- Criteria:
 1. iso energetic rays
 2. good boundary description
 3. good spatial resolution

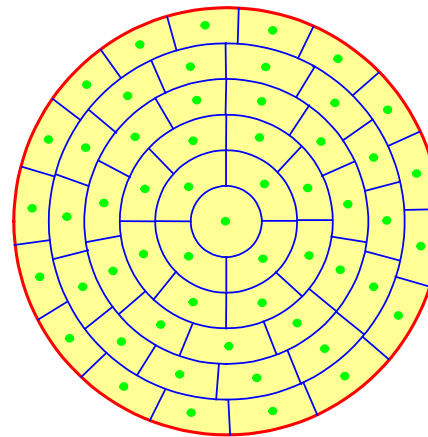
polar grid



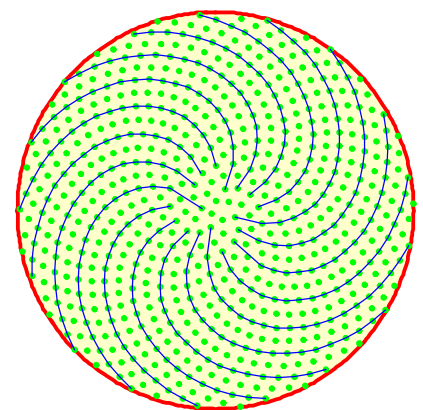
cartesian



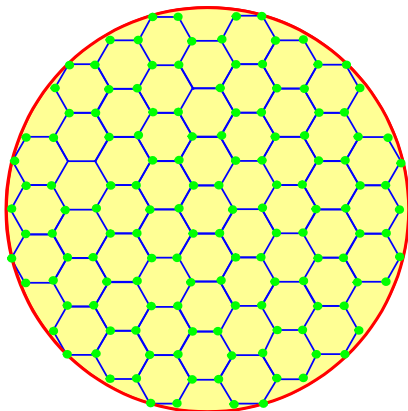
isoenergetic circular



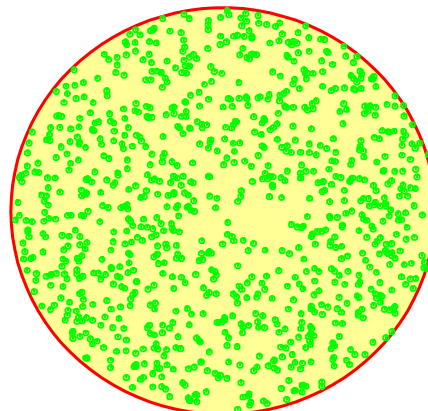
Fibonacci spirals



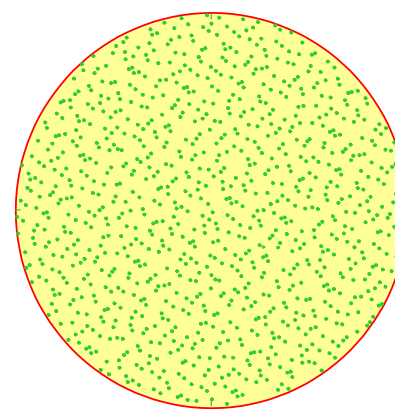
hexagonal



statistical

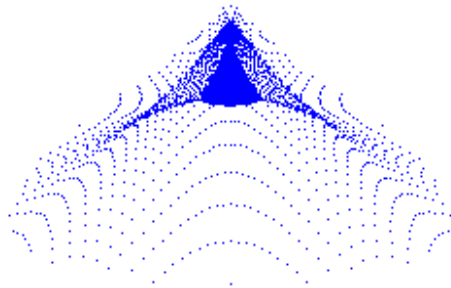


pseudo-statistical (Halton)

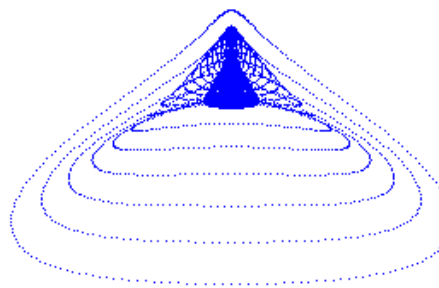


- Artefacts due to regular gridding of the pupil of the spot in the image plane
- In reality a smooth density of the spot is true
- The line structures are discretization effects of the sampling

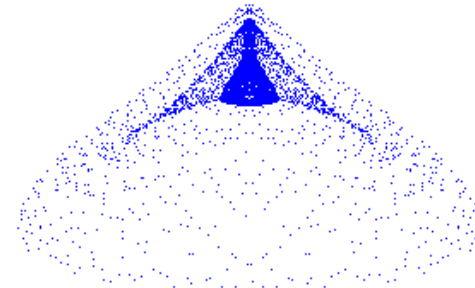
cartesian



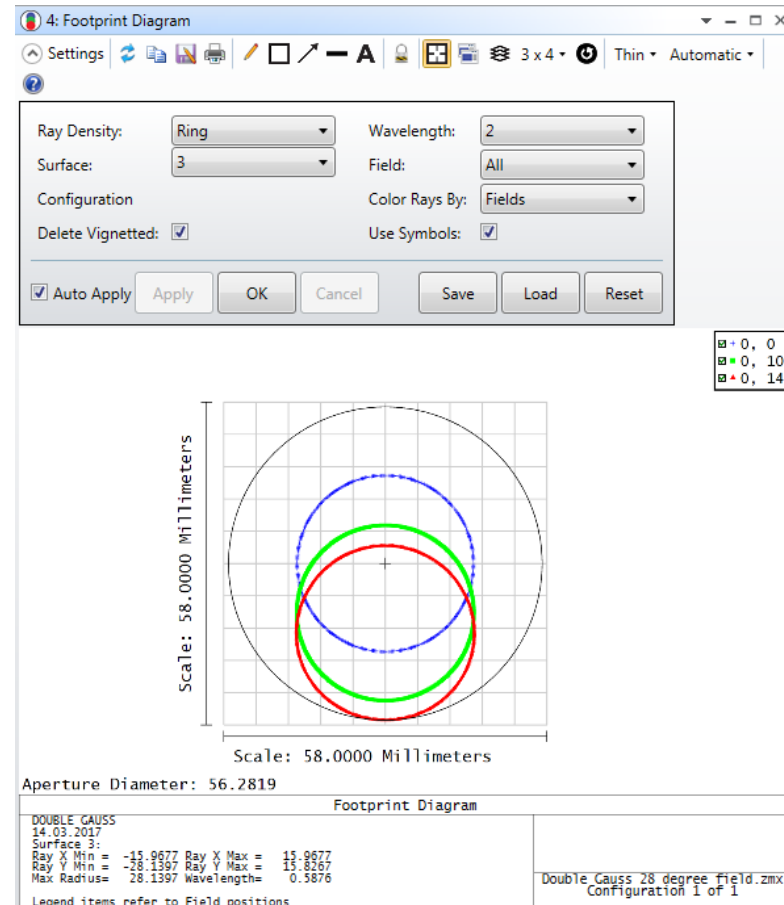
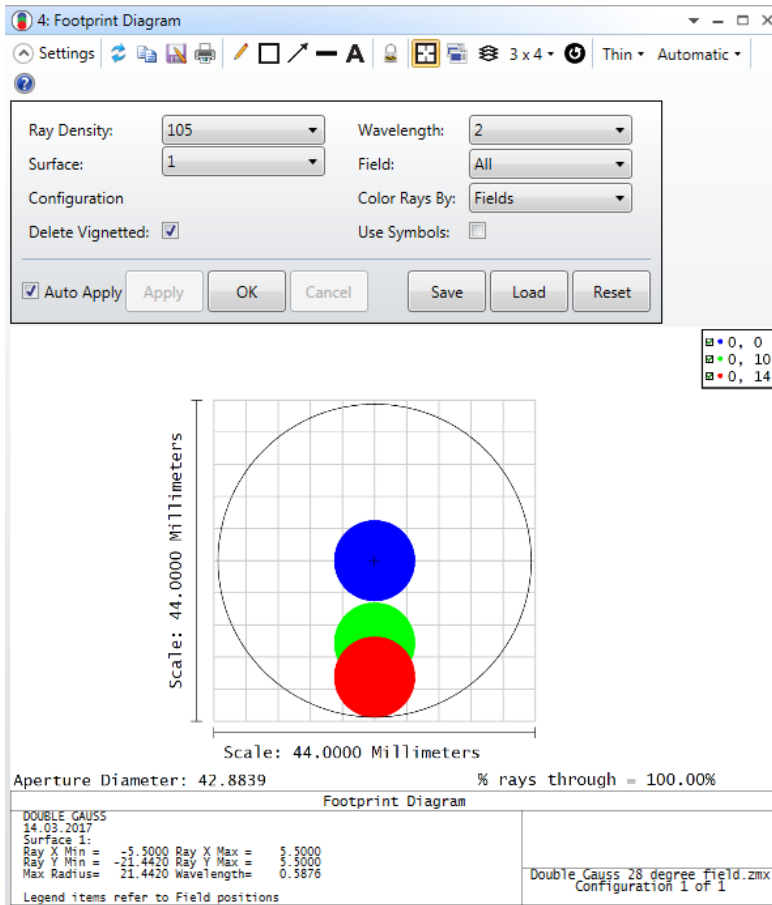
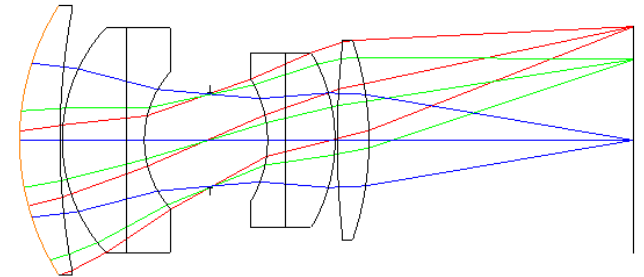
hexagonal



statistical



- Ray bundle cross sections @ specific surfaces
- Equivalent to spot diagram



Exercise 1 Paraxial system layout



- a) Suppose a divergent ray bundle with numerical aperture of $NA = 0.2$ at the wavelength $\lambda = 500 \text{ nm}$. Establish a first paraxial lens with a focal length to get a collimated beam with diameter 24 mm.
- b) After a distance of 10 mm a second paraxial lens with focal length $f_2 = 30 \text{ mm}$ focusses the ray. Behind the focal point a third paraxial lens should collimate the beam again for a diameter of 36 mm.
- c) Now in a distance of 20 mm a focussing paraxial lens with focal length $f = 100$ is added. Finally a negative lens with $f = -70 \text{ mm}$ is added in an appropriate distance to change the numerical aperture in the image space to 0.05. Find the final image distance. What is the magnification of the system ?

Establish a single lens with the following data:

wavelength:	$\lambda = 546.07 \text{ nm}$
object distance	100 mm
thickness of the lens, made of N-BK7	$t = 8 \text{ mm}$
front radius of curvature	$R1 = 45 \text{ mm}$
rear radius of curvature	$R2 = -100 \text{ mm}$
numerical aperture in the object space	$NA = 0.07$
lens diameter	24 mm

- Fix the final distance in the paraxial image plane. Create a layout plot
- Calculate the spot diagram and the transverse ray aberrations.
What is the spot size ?
Is the system diffraction limited ?
What residual aberration is obtained ?
Are also higher order aberrations obtained ?
Determine the image sided numerical aperture by calculating the marginal ray.
- Add an off axis field point with height $y = 10 \text{ mm}$.
Fix the pupil of the system at the rear surface of the lens
Find the best plane for gathering the image. Is the distance increased or decreased ?
Calculate the layout and the spot diagram. What is the dominating aberration for the field point now ?