

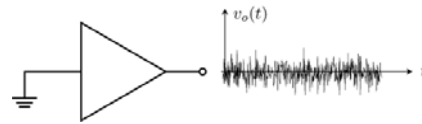
EECS240 – Spring 2010

Lecture 5: Electronic Noise



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Noise in Amplifiers



- All amplifiers generate noise
 - Comes from carrier random thermal motion and discreteness of charge
- Noise is random
 - Has to be treated statistically – can't predict actual value
 - Deal with mean (average), variance, spectrum

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Electronic Noise

- Why is noise important?
 - Sets minimum signals we can deal with – often sets lower limit on power
- Signal-to-noise ratio
 - Signal Power $P_{\text{sig}} \sim (V_{\text{DD}})^2$
 - Noise Power $P_{\text{noise}} \sim k_B T/C$
 - $\text{SNR} = P_{\text{sig}} / P_{\text{noise}}$
- Technology Scaling
 - V_{DD} goes down \rightarrow lower signal
 - Increase C to compensate \rightarrow increases power

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Thermal Noise of a Resistor

- Origin: Brownian Motion
 - Thermally agitated particles
 - E.g. ink in water, electrons in a conductor
- Available noise power: $P_N = k_B T \Delta f$
 - Noise power in bandwidth Δf delivered to a matched load
 - Example: $\Delta f = 1\text{Hz} \rightarrow P_N = 4 \times 10^{-21}\text{W} = -174\text{ dBm}$
 - Reference: J.B. Johnson, "Thermal Agitation of Electricity in conductors," Phys. Rev., pp. 97-109, July 1928.

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Types of "Noise"

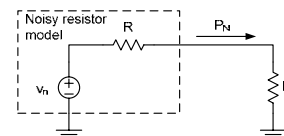
- Interference
 - Not "fundamental" – deterministic
 - Signal coupling
 - Capacitive, inductive, substrate, etc.
 - Supply noise
- Device noise
 - Caused by discreteness of charge
 - "fundamental" – thermal noise
 - "manufacturing process related" – flicker noise

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Resistor Noise Model



$$P_N = k_B T \Delta f = \frac{\overline{v_n^2}}{4R}$$

Mean square noise voltage:

$$\overline{v_n^2} = 4k_B T R \Delta f$$

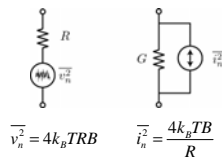
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Thermal Noise

- Present in all dissipative elements
 - i.e., resistors
- Independent of DC current flow
- Random fluctuations of $v(t)$ or $i(t)$
 - Mean is 0
 - Distribution (pdf) is Gaussian
 - Power spectral density is "white"
 - Up to ~THz frequencies
 - $k_B T = 4 \times 10^{-21} \text{ J}$ ($T = 290\text{K} = 16.9^\circ\text{C}$)
- Example:
 - $R = 1\text{k}\Omega \rightarrow 4\text{nV}/\sqrt{\text{Hz}}$
 - 1MHz bandwidth $\rightarrow \sigma = 4\mu\text{V}$



Calculating Noise in Passive Networks

- Capacitors and inductors only shape spectrum:

$$\overline{v_{on,T}^2(f)} = \sum_x |H_x(s)|_{s=j2\pi f}^2 \overline{v_x^2(f)}$$

Thermal Noise in Capacitors?

Noise in Diodes

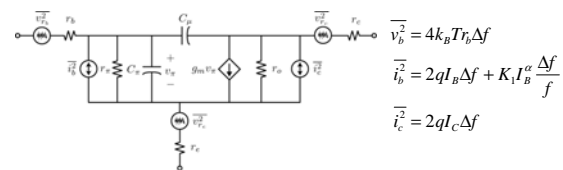
- Shot noise
 - Zero mean, Gaussian pdf, white
 - Proportional to current
 - Independent of temperature
- Example:
 - $I_D = 1\text{mA} \rightarrow 17.9\text{pA}/\sqrt{\text{Hz}}$
 - 1MHz bandwidth $\rightarrow \sigma = 17.9\text{nA}$
- Shot noise versus thermal noise
 - $g_{\text{diode}} = I_D / (k_B T / q)$
 - Thermal noise density: $4k_B T g_{\text{diode}} = 4qI_D$
 - Shot noise half of this (current flow in 1 direction)

$$\overline{i_n^2} = 2qI_D \Delta f$$

Noise Calculations

- Noise calculations
 - Instantaneous voltages add
 - Power spectral densities add
 - RMS voltages do NOT add
- Example: $R_1 + R_2$ in series

BJT Noise



- Just like diodes: shot noise
 - Collector and base noise partially correlated
- Extrinsic resistors contribute noise
 - Small signal resistors (e.g., r_o) don't
 - These aren't physical resistors

Triode MOSFET Noise

- Channel resistance contributes thermal noise
- Channel conductance when $V_{ds} = 0$:

$$g_{ds0} = \mu C_{ox} \frac{W}{L} (V_{GS} - V_{th})$$

- Device is truly a resistor when $V_{ds} = 0$, so:

$$\overline{i_d^2} = 4kTg_{ds0}\Delta f$$

Weak Inversion Noise

Saturation Noise

- Noise distributed along the channel:

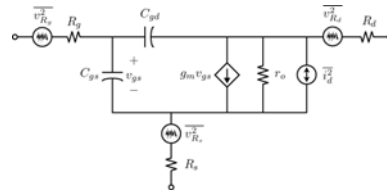
$$\overline{i_d^2} = 4kT \frac{2W}{3L} \mu C_{ox} (V_{GS} - V_T) \Delta f$$

- For long channel model, can substitute γg_m for g_{ds0}

$$\overline{i_d^2} = 4kT \gamma g_m \Delta f$$

- More correct formulation uses inversion charge in the channel [Tsividis]
 - This is what SPICE/BSIM use

FET Noise Model



- Model neglects intrinsic gate noise
- BSIM3 does not directly include α

Thermal Noise for Short Channels

- Strong inversion \rightarrow thermal noise
 - Drain current: g_{ds0} is what you really care about

$$\overline{i_d^2} = 4kT \gamma g_{ds0} \Delta f = 4kT \frac{\gamma}{\alpha} g_m \Delta f$$

- g_m more convenient for input-referred noise
 - For low field (long L), $\gamma = 2/3$ relates g_m to g_{ds}
 - For high field, use α to capture increase in noise
 - High-field noise can be 2-3 times larger than low field

- MOS actually has intrinsic gate induced noise (142/242 topic)
- Gate leakage \rightarrow shot noise

1/f Noise

- Flicker noise
 - $K_{f,NMOS} = 2.0 \times 10^{-29}$ A²/Hz
 - $K_{f,PMOS} = 3.5 \times 10^{-30}$ A²/Hz
 - Strongly process dependent

$$\overline{i_{1/f}^2} = \frac{K_f I_D \Delta f}{L^2 C_{ox} f}$$

- Example: $I_D = 10 \mu A$, $L = 1 \mu m$,
 - $C_{ox} = 5.3 fF/\mu m^2$, $f_{hi} = 1 MHz$

$$\begin{array}{ll} f_{lo} = 1 Hz & \rightarrow \sigma = 722 pA \\ f_{lo} = 1/year & \rightarrow \sigma = 1083 pA \end{array}$$

$$\overline{i_{1/f,total}^2} = \int_{f_{lo}}^{f_{hi}} \frac{K_f I_D}{L^2 C_{ox} f} df = \frac{K_f I_D}{L^2 C_{ox}} \ln \frac{f_{hi}}{f_{lo}}$$

1/f Noise Corner Frequency

• Definition (MOS)

$$\frac{K_f I_D}{L^2 C_{ox} f_{co}} = 4k_B T \gamma g_m \Delta f \quad f_{co} = \frac{K_f I_D}{L^2 C_{ox} 4k_B T \gamma g_m}$$

$$= \frac{K_f}{4k_B T \gamma C_{ox}} \frac{1}{L^2} \frac{1}{g_m / I_D}$$

$$= \frac{K_f}{8k_B T \gamma C_{ox}} \frac{V^*}{L^2}$$

• Example:

- $V^* = 200\text{mV}$, $\gamma = 1$

$$L = 0.35\mu\text{m}$$

$$L = 1.00\mu\text{m}$$

→

NMOS

192kHz

→

24kHz

PMOS

34kHz

4kHz

Noise Calculations with Actives

• Method:

- 1) Create small-signal model
- 2) All inputs = 0 (linear superposition)
- 3) Pick output v_o or i_o
- 4) For each noise source v_x, i_x
Calculate $H_x(s) = v_o(s) / v_x(s)$ (... i_o, i_x)
- 5) Total noise at output is:

$$\overline{v_{on,T}^2(f)} = \sum_x |H_x(s)|_{s=jf}^2 \overline{v_x^2(f)}$$

$$\text{simpler notation: } \overline{v_{on,T}^2(f)} = S_v(f)$$

Tedious but simple ...

SPICE Noise Analysis

