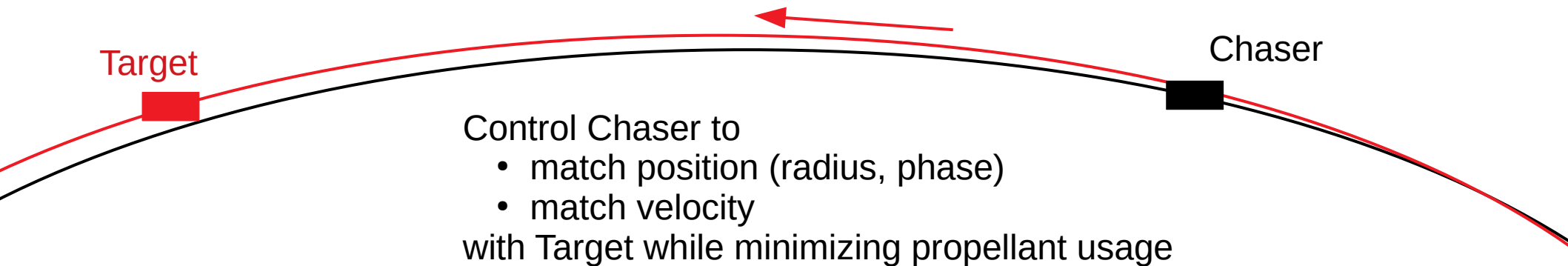


Comparing Optimization and Estimation Techniques for Low-Thrust Spacecraft Rendezvous

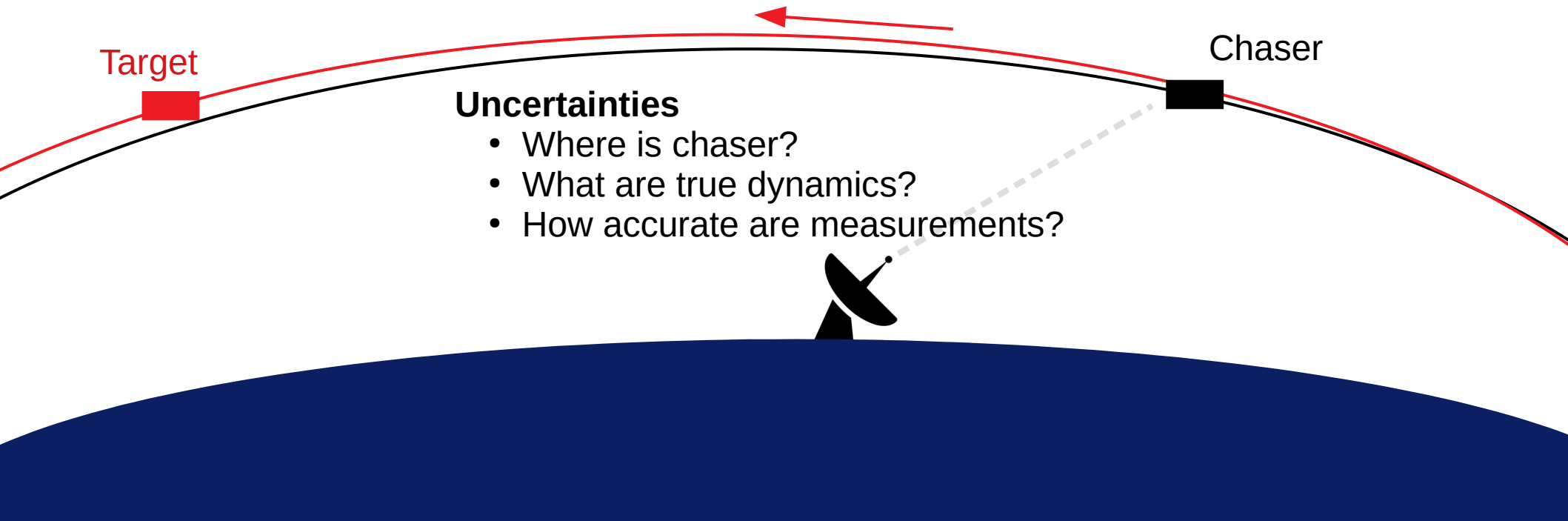
Andrew Cox, Mike Sparapany, Collin York, Waqar Zaidi
April 25, 2018

AAE 568 Course Project, Purdue University

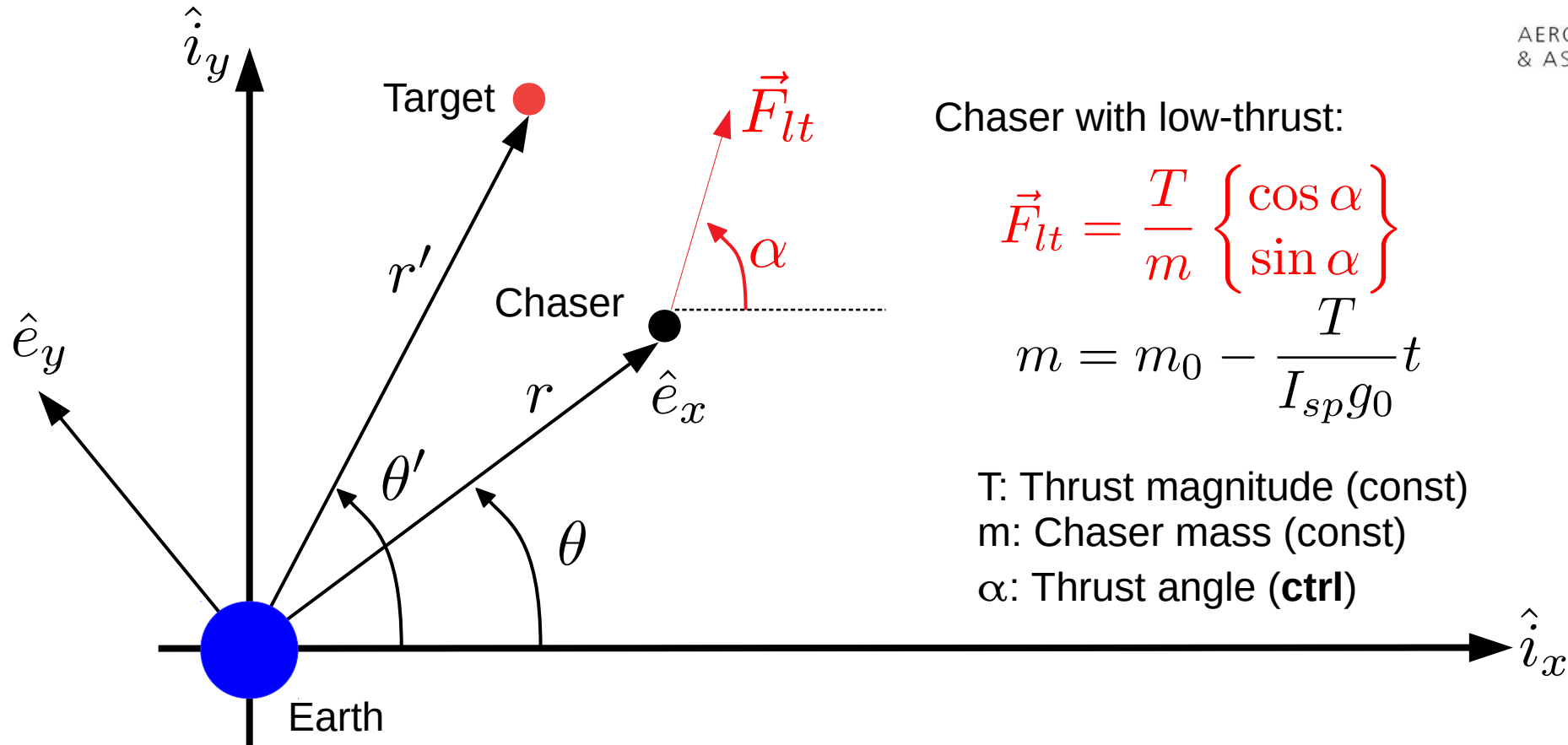
Problem Motivation



Problem Motivation, Cont'd



Low-Thrust Control



Chaser with low-thrust:

$$\vec{F}_{lt} = \frac{T}{m} \begin{Bmatrix} \cos \alpha \\ \sin \alpha \end{Bmatrix}$$

$$m = m_0 - \frac{T}{I_{sp}g_0}t$$

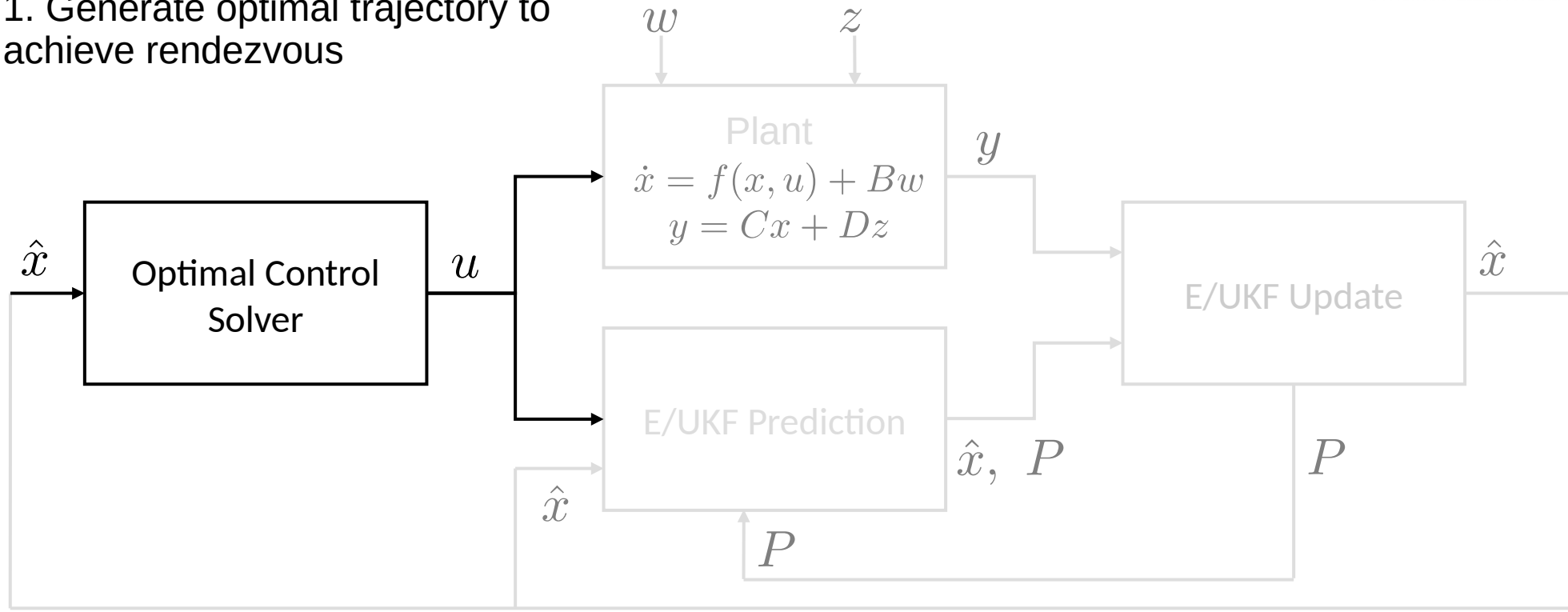
T: Thrust magnitude (const)

m: Chaser mass (const)

α : Thrust angle (**ctrl**)

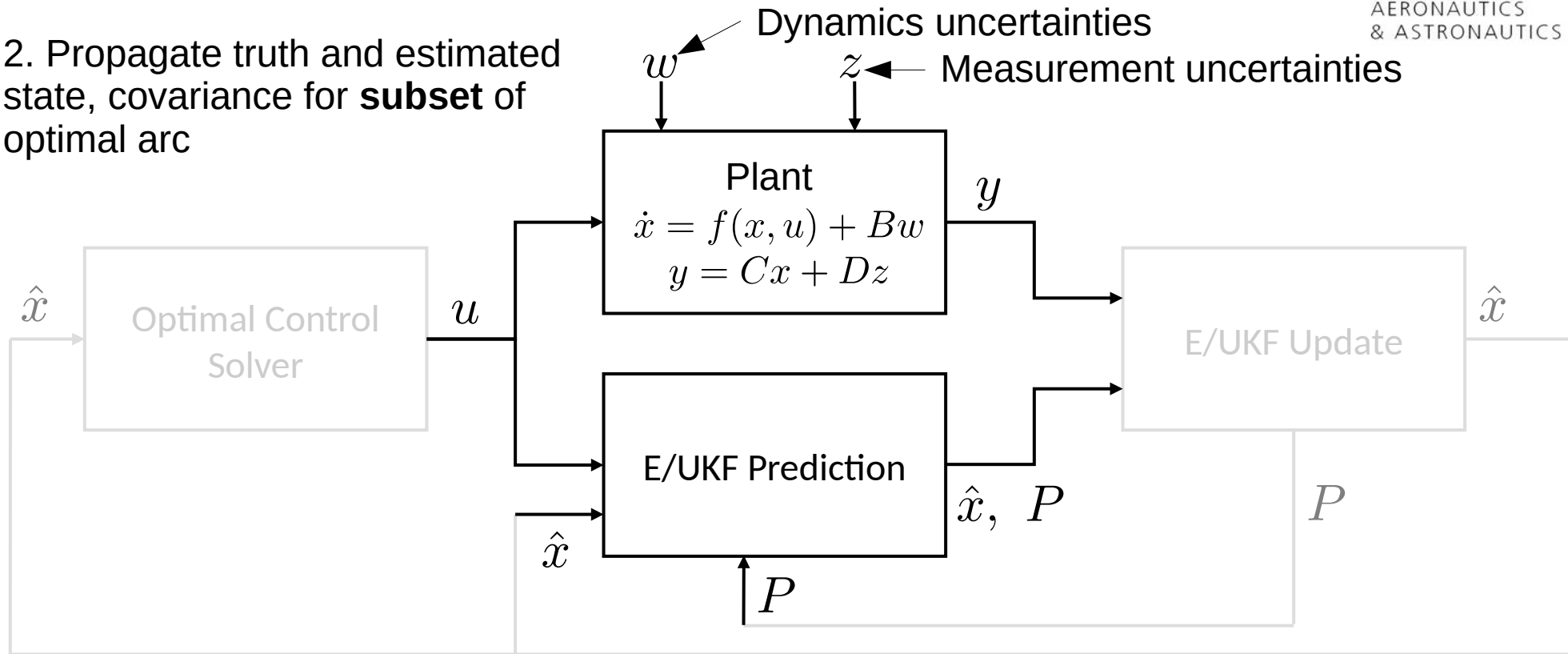
Problem Overview

1. Generate optimal trajectory to achieve rendezvous



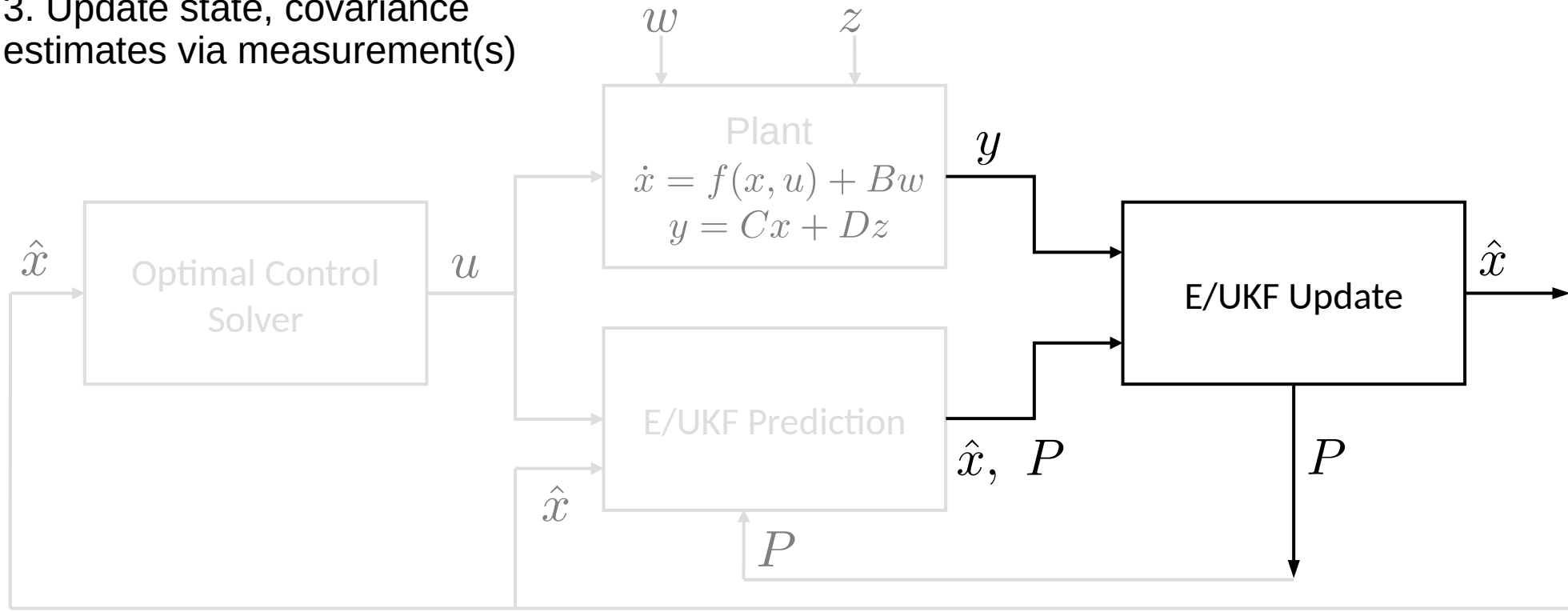
Problem Overview

2. Propagate truth and estimated state, covariance for **subset** of optimal arc



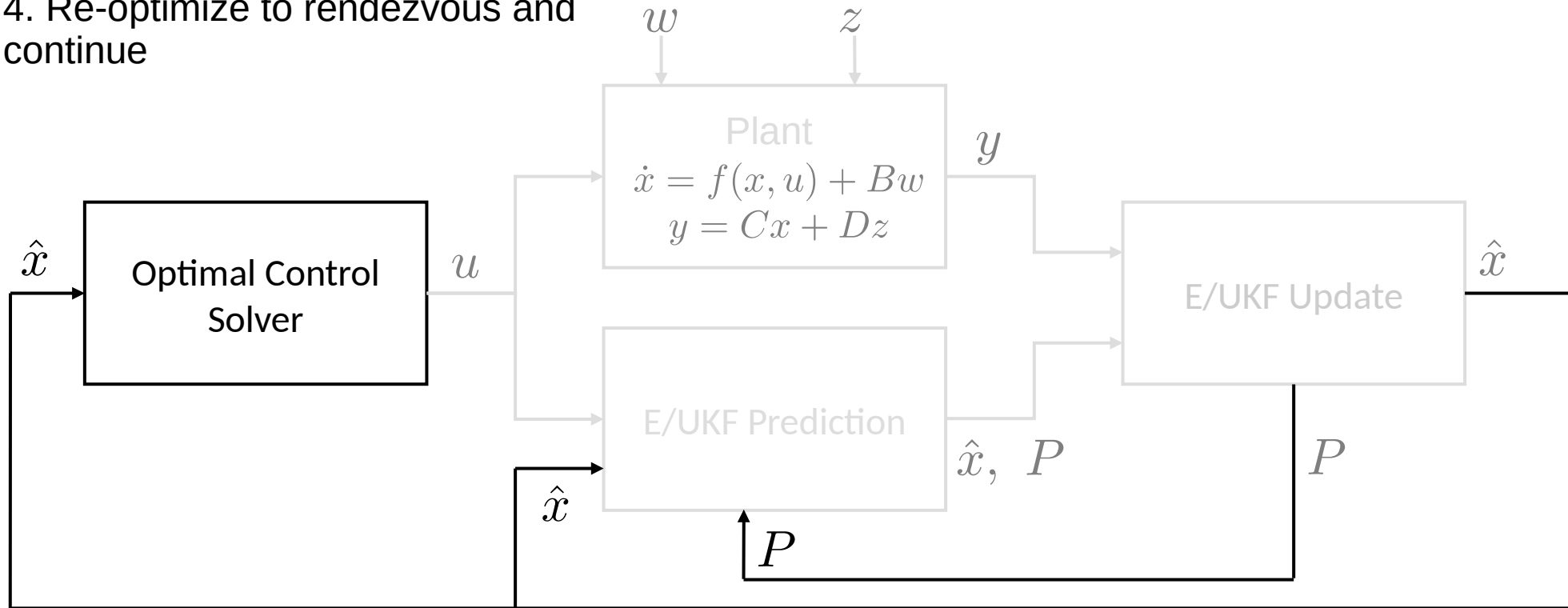
Problem Overview

3. Update state, covariance estimates via measurement(s)



Problem Overview

4. Re-optimize to rendezvous and continue



Optimization Problem Definition

Goal: minimize propellant usage = maximize m_f = minimize t_f

$$\min_{\alpha} J = t_f$$

Subject to:

$$\dot{\vec{x}} = \begin{Bmatrix} \dot{r} \\ \dot{\theta} \\ r\dot{\theta}^2 - \frac{\mu}{r^2} + \frac{T}{m} (C_{\alpha}C_{\theta} + S_{\alpha}S_{\theta}) \\ -2\frac{\dot{r}\dot{\theta}}{r} + \frac{T}{mr} (S_{\alpha}C_{\theta} - C_{\alpha}S_{\theta}) \end{Bmatrix} \quad \vec{x}(t_f) = \begin{Bmatrix} r' \\ \theta'_0 + \dot{\theta}'t \\ \dot{r}'_0 \\ \dot{\theta}'_0 \end{Bmatrix}$$

$$\vec{x}(t_0) = \{r_0 \quad \theta_0 \quad \dot{r}_0 \quad \dot{\theta}_0\}^T, \quad t_0 = 0 \quad t_f = \text{free}$$

Indirect Optimization

- Non-dimensionalize the problem by initial radius, mean motion, and spacecraft mass to help convergence

- Utilize Euler-Lagrange Equations

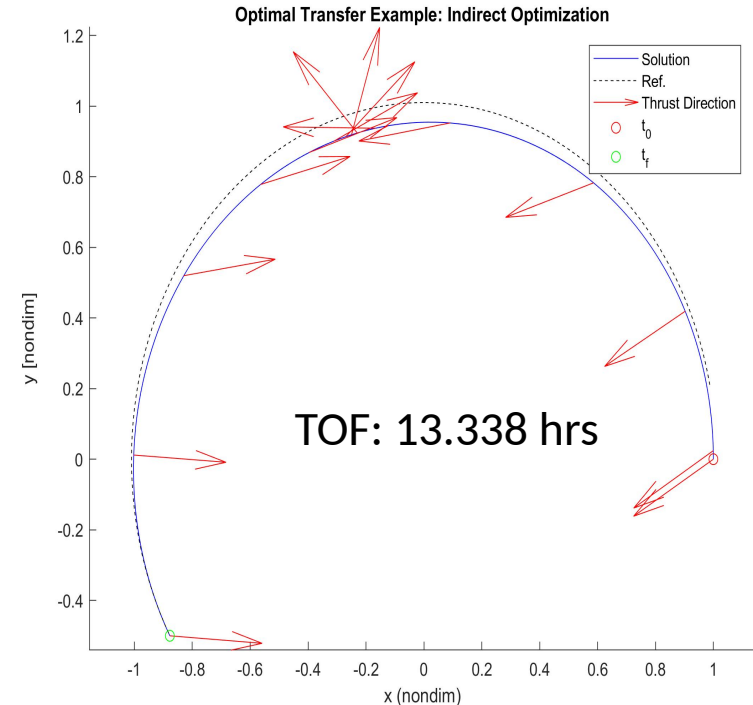
$$\dot{\lambda} = \left(\frac{\partial H}{\partial x} \right)^T \quad \frac{\partial H}{\partial \alpha} = 0$$

- Two-Point Boundary Value Problem requires one more constraint from the Transversality Condition,

$$H_f dt_f - \lambda_f^T dx_f + dg = 0$$

$$H_f dt_f - \lambda_2 \left(\partial \theta_f + \frac{\partial \theta}{\partial t} \Big|_{t_f} dt_f \right) + dt_f = 0$$

$$H_f - \lambda_2 \dot{\theta}' + 1 = 0$$



Direct Optimization

Model dynamics by piecewise 3rd-degree polynomials (control constant along segments)

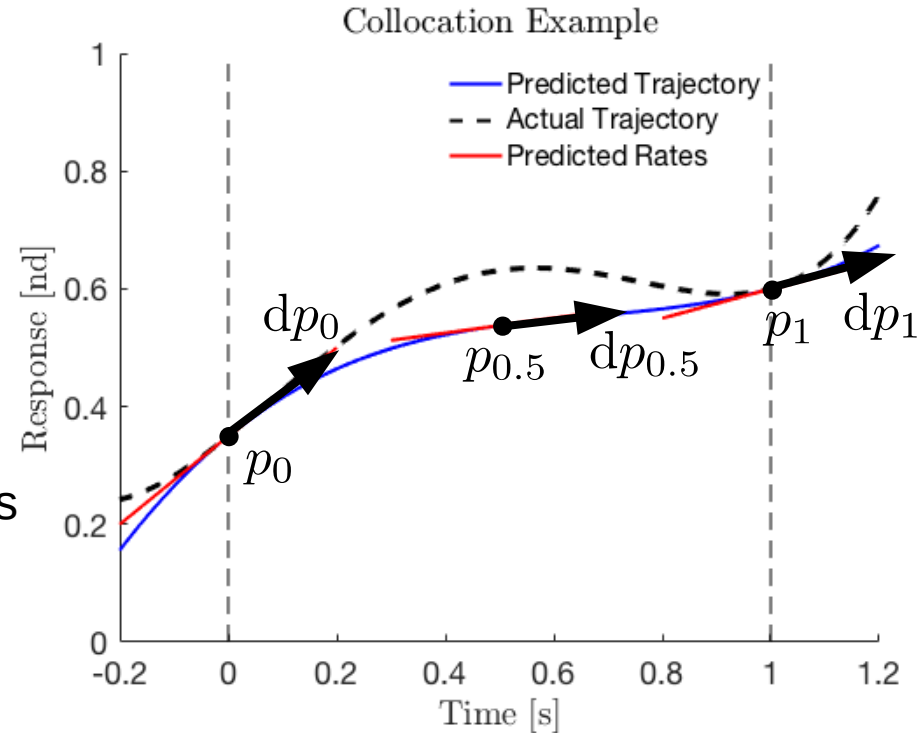
$$\tilde{p}_{0.5} = \frac{1}{2}(p_0 + p_1) + \frac{t_f(dp_0 - dp_1)}{8(N-1)}$$

$$d\tilde{p}_{0.5} = -\frac{3(N-1)(p_0 - p_1)}{2t_f} - \frac{1(dp_0 + dp_1)}{4}$$

$$dp_{0.5} = f(t, \tilde{p}_{0.5})$$

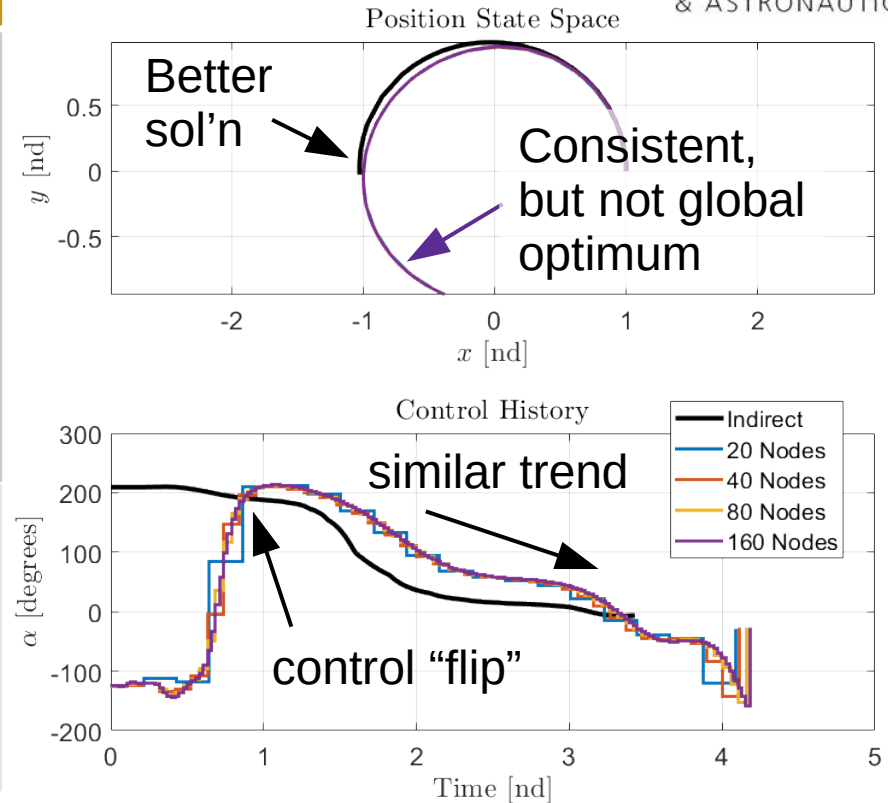
Constraint: $dp_{0.5} - d\tilde{p}_{0.5} = 0 \quad \forall$ polynomial midpoints

Driven by Sequential Quadratic Programming
(SQP from MATLAB's *fmincon*)



Indirect vs. Direct Optimization

	Direct	Indirect
Pros	<ul style="list-style-type: none"> No variational calculus Easy to make initial guess (no costates) Easy to find a potential (suboptimal) solution 	<ul style="list-style-type: none"> Root-solver is simpler Solution guaranteed locally optimal Convincing global optimum with engineering judgement
Cons	<ul style="list-style-type: none"> Unsure if solution is optimal, or even real Numerical optimizer is more complicated 	<ul style="list-style-type: none"> Initial guess hard to make Sensitive to initial guess



Estimation Problem Definition

$\dot{x} = f(x, \alpha) + Bw$ Process equations with acceleration noise

$y_k = Cx_k + Dz_k$ Range & range-rate measurements

- w is mean-zero Gaussian white noise with $\sigma = 10^{-8}$ km/s² (J_2 , lunar gravity at GEO)
- z is mean-zero Gaussian white noise with $\sigma_1 = 10$ m, $\sigma_2 = 1$ mm/s
- Continuous-discrete formulations to model continuous gravity perturbation and discrete measurement intervals

Goals:

- Determine appropriate sample time for Extended Kalman Filter (EKF)
- Compare EKF and Unscented Kalman Filter (UKF)

Extended Kalman Filter

Continuous Propagation Equations:

$$\begin{aligned}\dot{\hat{x}} &= f(\hat{x}, \alpha) \\ \dot{P} &= A(\hat{x}(t))P + PA(\hat{x}(t))^T + BWB^T \\ P(0) &= P_0 \\ \text{where } A(\hat{x}(t)) &= \left. \frac{\partial f}{\partial x} \right|_{\hat{x}(t)}\end{aligned}$$

Discrete Update Equations:

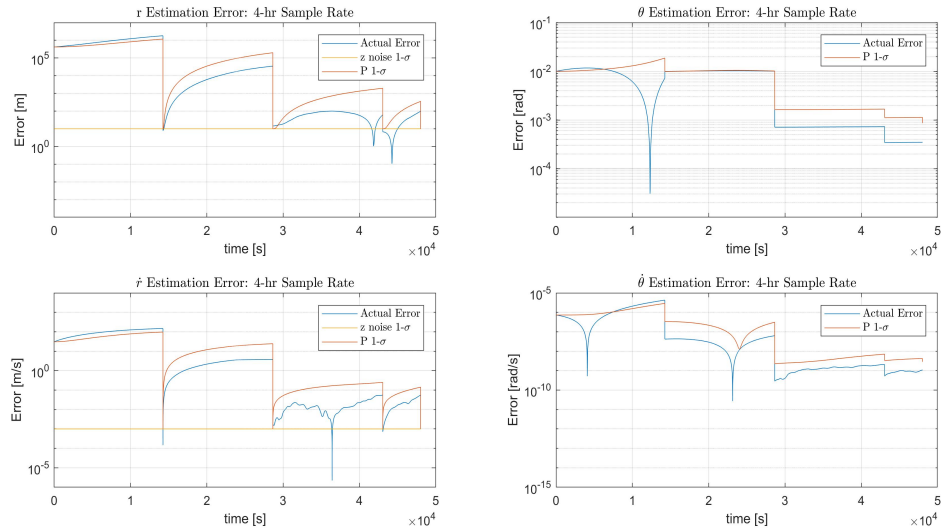
$$\begin{aligned}\hat{x}(t_k^+) &= \hat{x}(t_k^-) + L_k \left(y_k - C\hat{x}(t_k^-) \right) \\ P(t_k^+) &= (I - L_k C)P(t_k^-) \\ \text{where } P(t_k^-)C^T &\left(CP(t_k^-)C^T + DZD^T \right)^{-1}\end{aligned}$$

EKF Sampling Time Determination

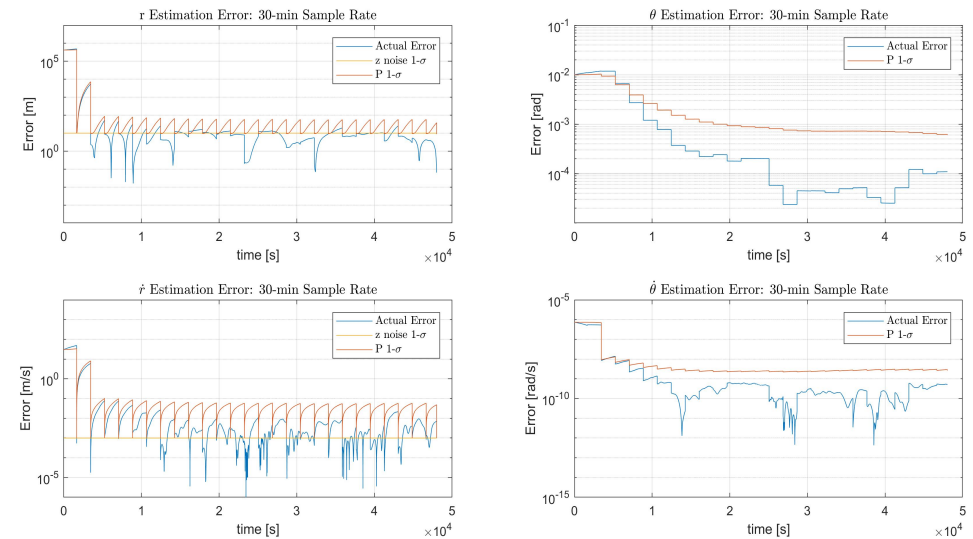


AERONAUTICS
& ASTRONAUTICS

4-Hr Sampling Rate



30-min Sampling Rate



Unscented Kalman Filter

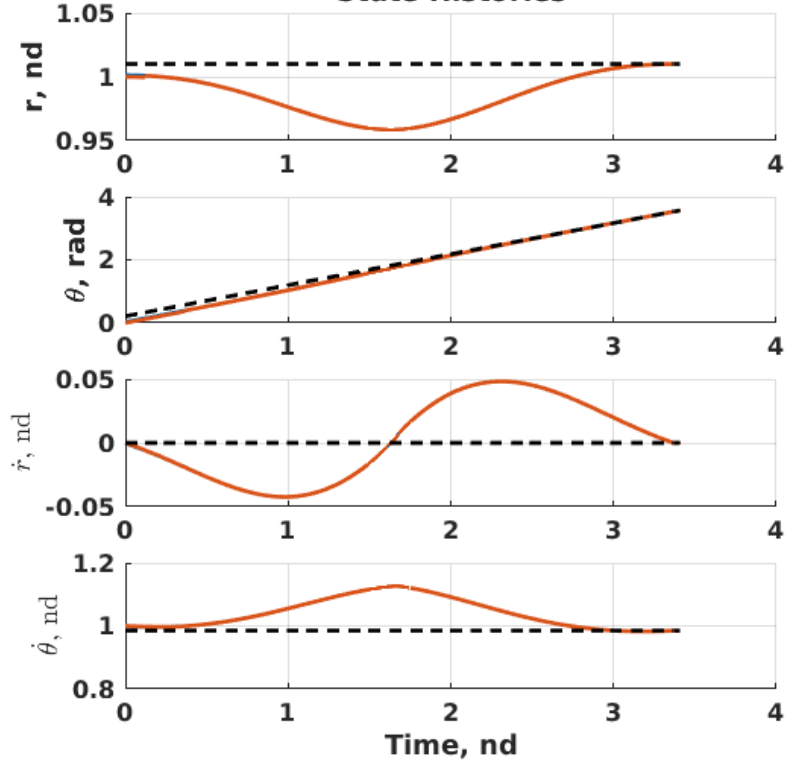
Waqar

Estimation Method Comparison

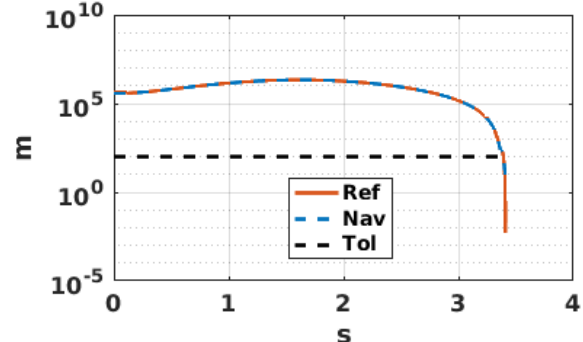
Waqar

Example: Indirect + EKF Results

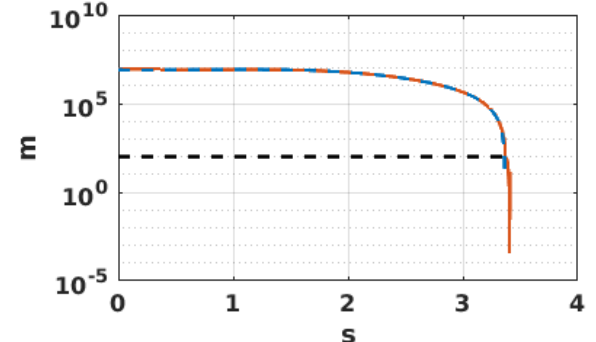
State Histories



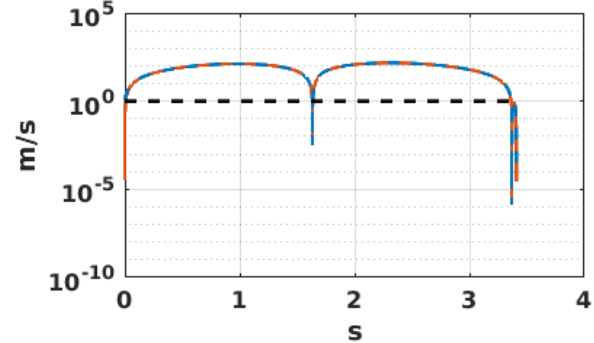
Radial Position Delta From Target



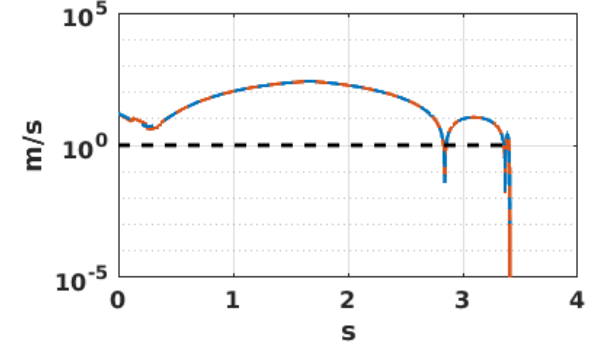
Downtrack Position Delta From Target



Radial Velocity Delta From Target



Downtrack Velocity Delta From Target



Contributions

Andrew: Dynamics derivation, integration of components into mission loop

Michael: Direct optimization implementation, optimizer comparison

Collin: EKF implementation, indirect optimization implementation

Waqar: UKF implementation, estimator comparison

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