

3-4

电桥平衡时 $\frac{R_2}{R_1} = \frac{R_4}{R_3} = n$

9

∴ 应变片接 R_1, R_2 处时, 若 $n=1$:

$$e = \left(\frac{R_1 + \Delta R}{R_1 + R_2} - \frac{R_3}{R_3 + R_4} \right) E = \frac{\Delta R}{R_1 + R_2} E = \frac{\Delta R}{2R_1} E$$

应变片接 R_1, R_3 处时:

$$e = \left(\frac{R_1 + \Delta R}{R_1 + R_2 + 4R} - \frac{R_3 - \Delta R}{R_3 + R_4 - 4R} \right) E = \frac{\Delta R (R_1 + R_3)}{12R_1 + 4R (2R_1 - \Delta R)} E$$

可见, 接 R_1 和 R_2 时线性度好于接 R_1 和 R_3 时

3-7

对变极距式差动电容位移测量:

$$\frac{C_2}{C_1} = \frac{d_0 + \Delta d}{d_0 - \Delta d}$$

$$\frac{\Delta e}{C_0} = \frac{C_2 - C_1}{C_0} = \frac{2\Delta d}{d_0} + O\left(\left(\frac{\Delta d}{d_0}\right)^3\right)$$

对单电容局部线性位移测量: Δd 三次及以上高阶项

$$\frac{\Delta e}{C_0} = -\frac{\Delta d}{d_0} + O\left(\left(\frac{\Delta d}{d_0}\right)^3\right) \quad \Delta d \text{ 二次及以上高阶项}$$

由高阶项次数可知, 差动电容结构线性度和灵敏度更好. ✓

4-9

i 闭环: $S_{U_0} = \frac{U_0}{\dot{X}} = \frac{-mR}{S_f} \frac{1}{1 + K/(S_d S_s S_f)}$

此时 $S_d S_s S_f \gg K$, $K/(S_d S_s S_f)$ 可忽略.

故 $S_{uo} = -\frac{mR}{S_f}$ 与弹性系数 k 无关. ✓

开环: $S_{uo} = \frac{u_o}{\ddot{x}} = -\frac{S_s S_d}{\omega_o^2} = -\frac{mR S_s S_d}{k}$ ✓

此时 S_{uo} 与弹性系数 k 有关.

4-10

已知 $\omega_o = 2000 \text{ Hz}$, $\zeta = 0.5$

$\omega = 1200 \text{ Hz}$ 时:

$$\Delta = \left| \frac{y}{A} - \frac{y_o}{A} \right|$$

这不是相对误差

$$= \left| \frac{\omega^2 / \omega_o^2}{\sqrt{(1 - \frac{\omega^2}{\omega_o^2})^2 + (2\zeta \frac{\omega}{\omega_o})^2}} - \frac{\omega}{\omega_o} \right| \approx 5\%$$

y_o/A

14%

$\omega = 400 \text{ Hz}$ 时:

$$\Delta = \left| \frac{y}{A} - \frac{y_o}{A} \right| = \dots \approx 0.079\%$$

2%

∴ $\omega = 400 \text{ Hz}$ 时系统误差小于 $\omega = 1200 \text{ Hz}$ 时的系统误差

5-2

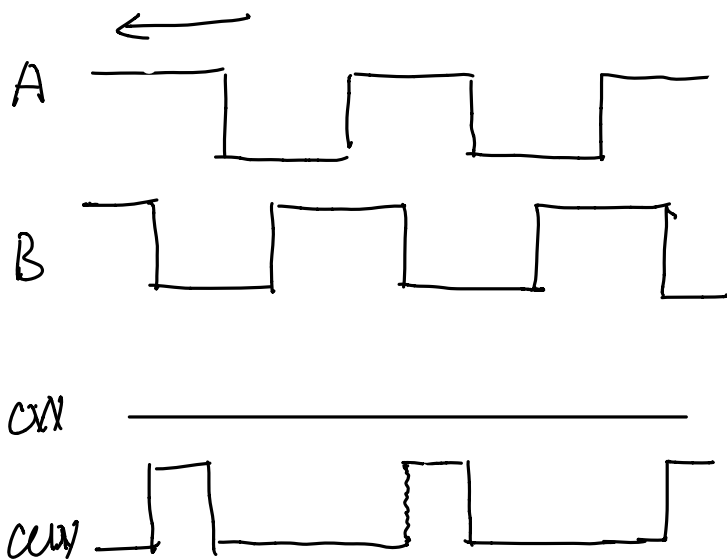
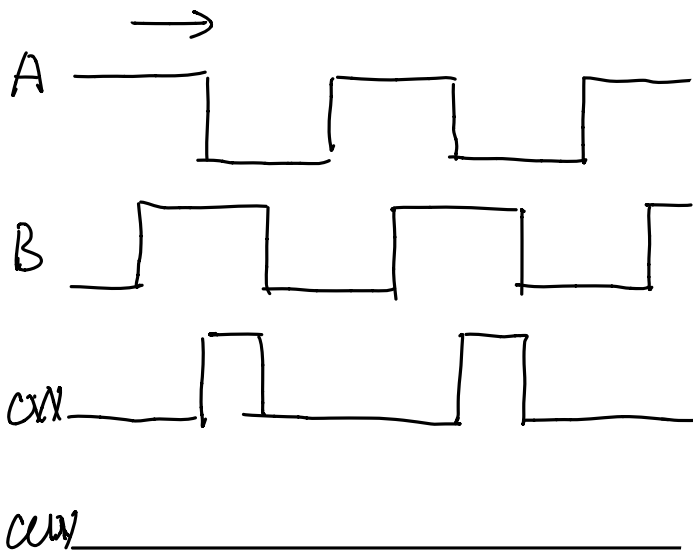
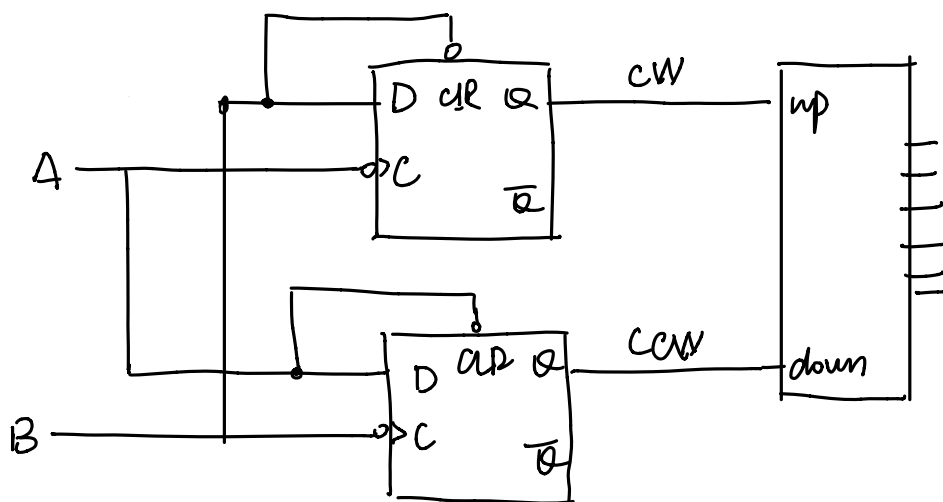
主尺; 副尺

平滑的三角波

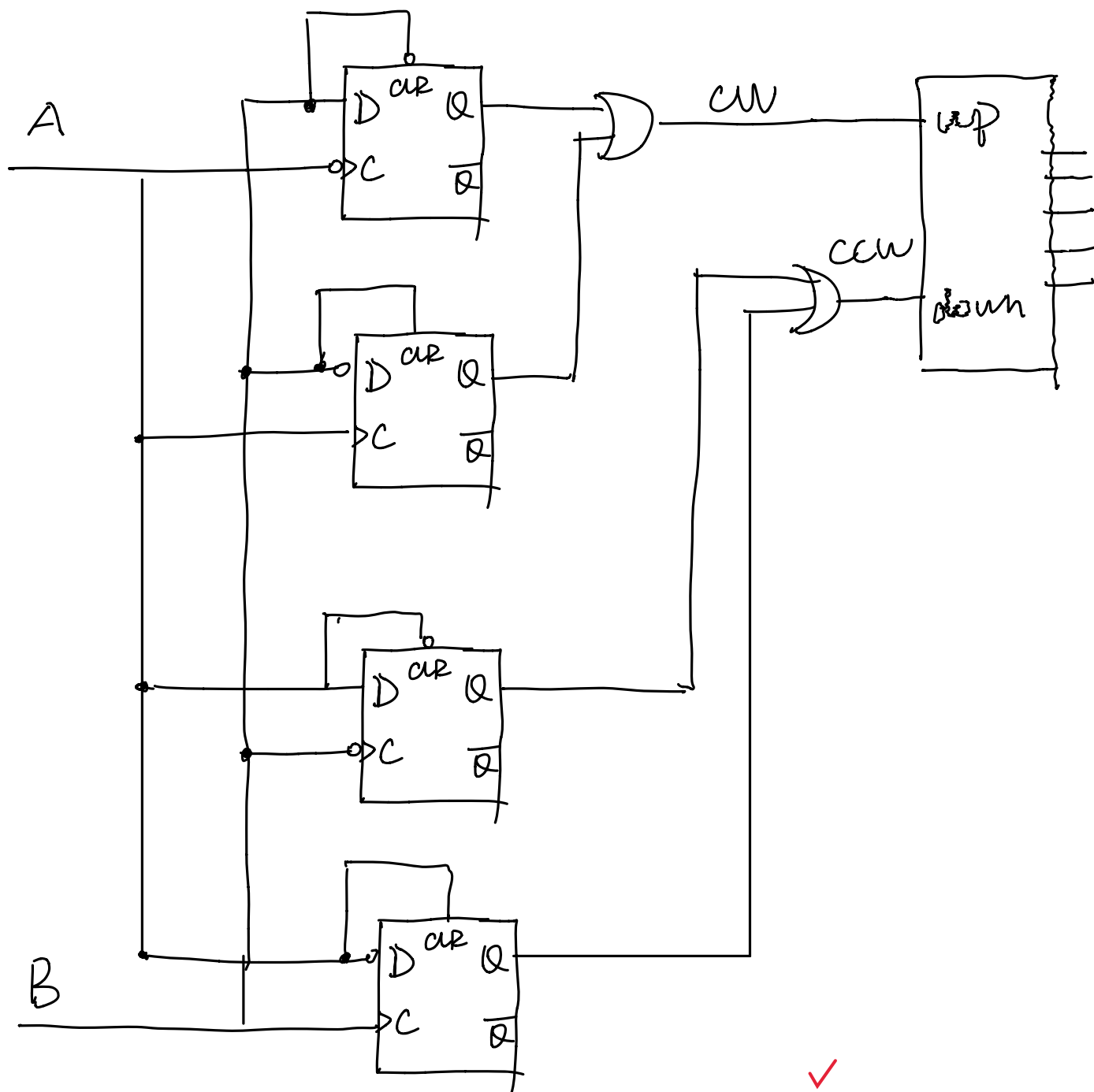
$\frac{1}{4}$; $\frac{\pi}{2}$ ✓

5-4

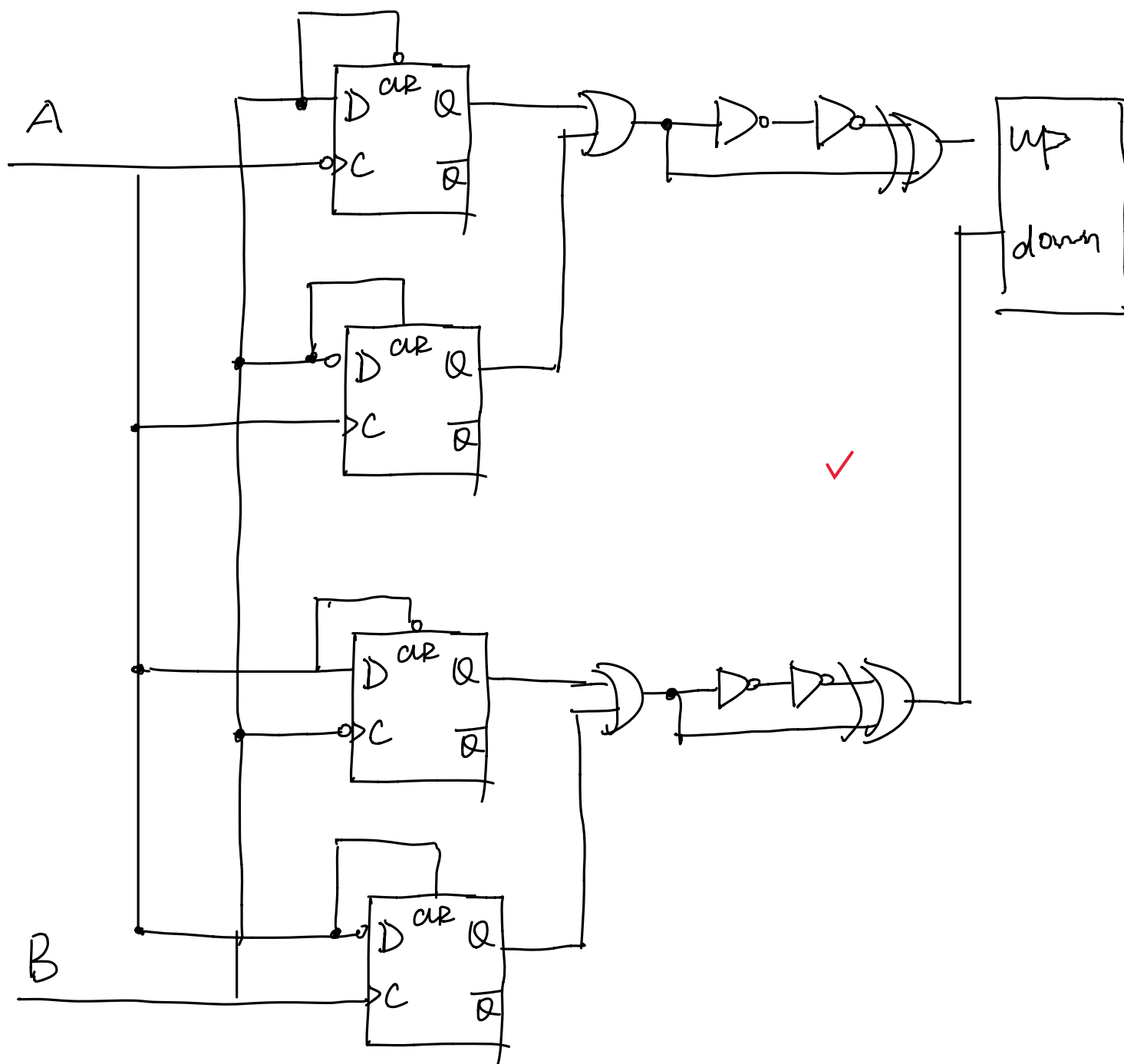
① 鉴向电路:



② 1/2 测量分辨率电路.



③ 1/4测量分辨率电路:



5-5

$$\frac{0.002}{0.2 \sqrt{\frac{1}{2}}} \times 2 = 0.04 V_{pp}$$

/2

0.02Vpp