

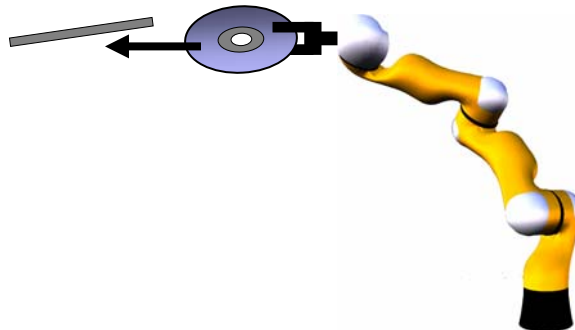
## 8803 - Mobile Manipulation: Control

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- Robotics & Intelligent Machines @ GT
- Georgia Institute of Technology
- Atlanta, GA 30332-0760
- February 19, 2008

## How do we make the robot move?

Today: Control of Dynamical Systems & Robots

Thursday: Strategies for Combining Position & Force



## The Robot is a Dynamic System

### What is a Dynamic System?

- A system whose variables are time-dependent
- Inputs and Outputs vary with time

### How can we describe a dynamic system?

- Input-output differential equations
- Free-body diagrams
- State-variable matrix
- Transfer functions
- Block diagrams

## Control

### What is Control?

Given the system state, choose input to get a desired output.

## Car Cruise Control



$$m\ddot{x} + b\dot{x} = f$$

$$\ddot{x} + \frac{b}{m}\dot{x} = \frac{f}{m}$$

State Variable Form:

$$\ddot{x} = \left[-\frac{b}{m}\right] \dot{x} + \left[\frac{1}{m}\right] f$$

## Car Cruise Control (Open Loop)



$$m\ddot{x} + b\dot{x} = f$$

Steady State  $\rightarrow$  Let  $\ddot{x} = 0$

$$0 + b\dot{x}_{ss} = f$$

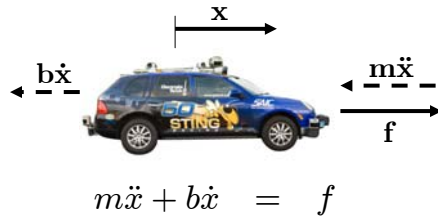
$$\dot{x}_r = \dot{x}_{ss} = \frac{f}{b}$$

$$u = f = b\dot{x}_r$$

State Variable Form:

$$\ddot{x} = \left[-\frac{b}{m}\right] \dot{x} + \left[\frac{1}{m}\right] f$$

## Car Cruise Control (Open Loop)

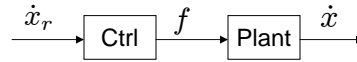


Steady State  $\rightarrow$  Let  $\ddot{x} = 0$

$$0 + b\dot{x}_{ss} = f$$

$$\dot{x}_r = \dot{x}_{ss} = \frac{f}{b}$$

$$f = b\dot{x}_r$$



State Variable Form:

$$\ddot{x} = \left[-\frac{b}{m}\right] \dot{x} + \left[\frac{1}{m}\right] f$$



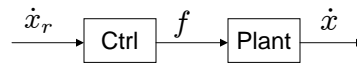
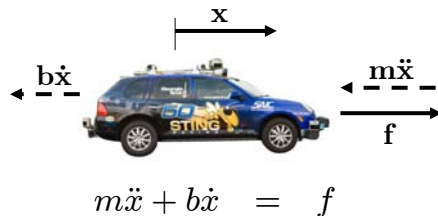
$$\ddot{x} = \left[-\frac{b}{m}\right] \dot{x} + \left[\frac{b}{m}\right] \dot{x}_r$$

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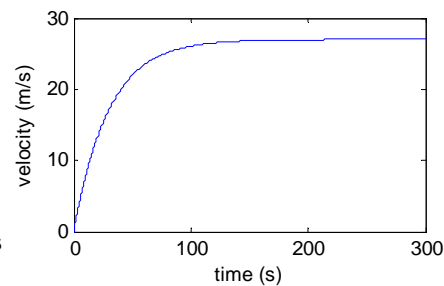
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## Car Cruise Control (Open Loop)



State Variable Form:

$$\ddot{x} = \left[-\frac{b}{m}\right] \dot{x} + \left[\frac{b}{m}\right] \dot{x}_r$$



$m = 1500\text{kg}$   $b = 50\text{Ns/m}$   $v_r = 27\text{m/s}$

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## Car Steering



State Variable Form:

$$\begin{bmatrix} \dot{\theta} \\ \ddot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & -\frac{b}{J} \end{bmatrix} \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{J} \end{bmatrix} \tau$$

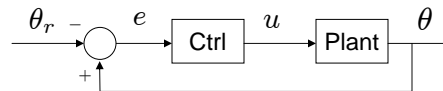
$$\begin{aligned} J\ddot{\theta} + b\dot{\theta} &= \tau \\ \ddot{\theta} &= -\frac{b}{J}\dot{\theta} + \frac{1}{J}\tau \end{aligned}$$

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## Car Steering (Proportional Control)



State Variable Form:

$$\begin{bmatrix} \dot{\theta} \\ \ddot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{K_p}{J} & -\frac{b}{J} \end{bmatrix} \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{K_p}{J} \end{bmatrix} \theta_r$$

$$\begin{aligned} J\ddot{\theta} + b\dot{\theta} &= \tau \\ \ddot{\theta} &= -\frac{b}{J}\dot{\theta} + \frac{1}{J}\tau \end{aligned}$$

$$\tau = -K_p(\theta - \theta_r)$$

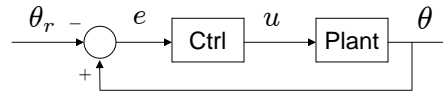
$$\ddot{\theta} = -\frac{b}{J}\dot{\theta} - \frac{K_p}{J}\theta + \frac{K_p}{J}\theta_r$$

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## Car Steering (Proportional Control)

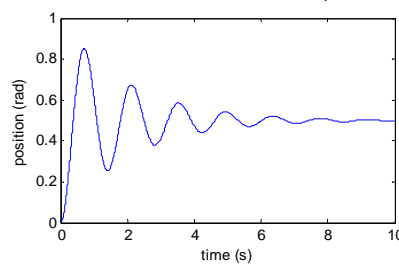


State Variable Form:

$$\begin{bmatrix} \dot{\theta} \\ \ddot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{K_p}{J} & -\frac{b}{J} \end{bmatrix} \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{K_p}{J} \end{bmatrix} \theta_r$$

$$\begin{aligned} J\ddot{\theta} + b\dot{\theta} &= \tau \\ \ddot{\theta} &= -\frac{b}{J}\dot{\theta} + \frac{1}{J}\tau \\ \tau &= -K_p(\theta - \theta_r) \\ \ddot{\theta} &= -\frac{b}{J}\dot{\theta} - \frac{K_p}{J}\theta + \frac{K_p}{J}\theta_r \end{aligned}$$

$$J = .1 \text{ kgm}^2 \quad b = .1 \text{ Nms} \quad \theta_r = .5 \text{ rad}$$

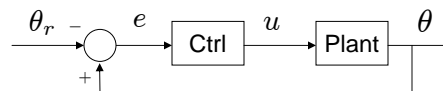


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## Car Steering (Proportional Control)



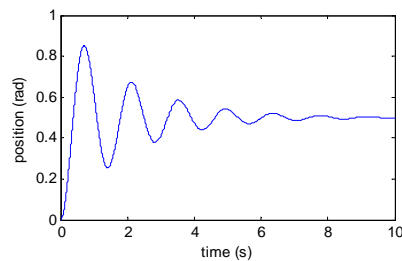
$$\tau = -K_p(\theta - \theta_r)$$

$$\ddot{\theta} = -\frac{b}{J}\dot{\theta} - \frac{K_p}{J}\theta + \frac{K_p}{J}\theta_r$$

Stability?

Exponential Convergence?

Limitations?

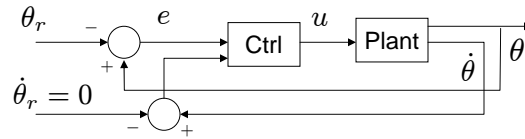


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## Car Steering (PD Control)



State Variable Form:

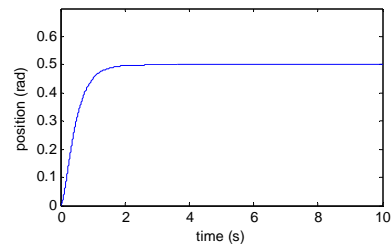
$$\begin{bmatrix} \dot{\theta} \\ \ddot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{K_p}{J} & -\frac{b+K_d}{J} \end{bmatrix} \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{K_p}{J} \end{bmatrix} \theta_r$$

$$J\ddot{\theta} + b\dot{\theta} = \tau$$

$$\ddot{\theta} = \frac{b}{J}\dot{\theta} + \frac{1}{J}\tau$$

$$\tau = -K_d(\dot{\theta} - \dot{\theta}_r) - K_p(\theta - \theta_r)$$

$$\ddot{\theta} = -\frac{b}{J}\dot{\theta} - \frac{K_d}{J}\dot{\theta} - \frac{K_p}{J}\theta + \frac{K_p}{J}\theta_r$$

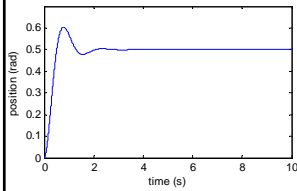


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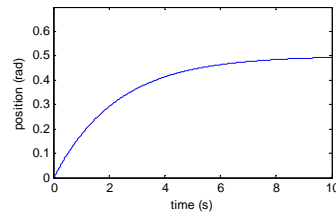
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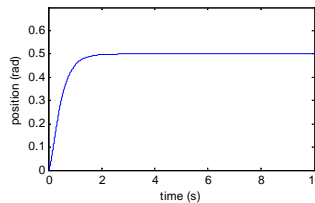
## PD Control



Under-damped



Over-damped



Critically damped (Just Right)

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## PD Control (Selecting Gains)

$$\begin{aligned}\ddot{\theta} &= -\frac{b + K_d}{J}\dot{\theta} - \frac{K_p}{J}(\theta - \theta_r) \\ \ddot{\theta} &= -K'_d\dot{\theta} - K'_p(\theta - \theta_r)\end{aligned} \quad \Rightarrow \quad \ddot{\theta} + K'_d\dot{\theta} + K'_p\theta = K'_p\theta_r$$

Characteristic Polynomial:  $s^2 + K'_d s + K'_p$

Standard Form:  $s^2 + 2\xi\omega_n s + \omega_n^2$

Damping Ratio:  $\xi$   
Natural Frequency:  $\omega_n$

$$\begin{aligned}K'_p &= \omega_n^2 \\ K'_d &= 2\xi\omega_n\end{aligned} \quad \xrightarrow{\xi=1} \quad \begin{aligned}K'_p &= \omega_n^2 \\ K'_d &= 2\omega_n = 2\sqrt{K'_p}\end{aligned}$$

## PD Control (Selecting Gains)

Starting Point:  $K'_p = \omega_n^2$   
 $K'_d = 2\omega_n = 2\sqrt{K'_p}$

What is  $\omega_n$ ?

Gains are limited by:

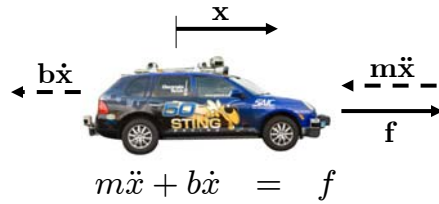
- structural flexibility
- time delay
- sampling rate
- actuator saturation

Optimal Control – Linear Quadratic Regulator

Tuning!

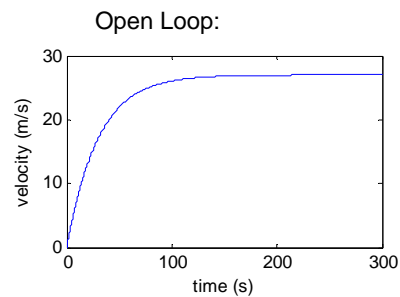
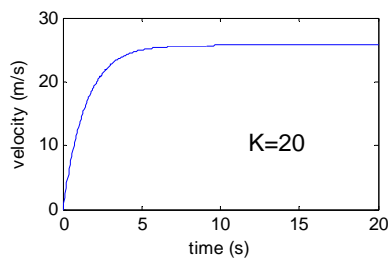


## Car Cruise Control (Closed Loop)



$$m\ddot{x} + b\dot{x} = f$$

$$f = -bK_p(\dot{x} - \dot{x}_r)$$

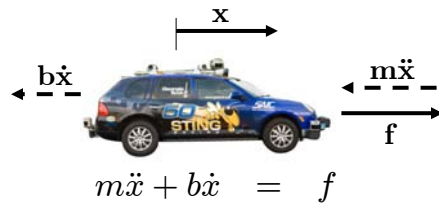


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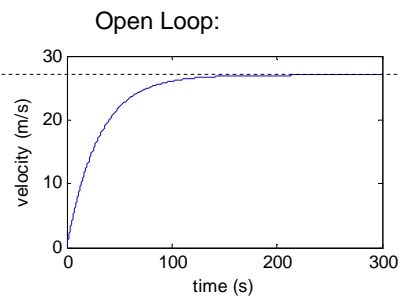
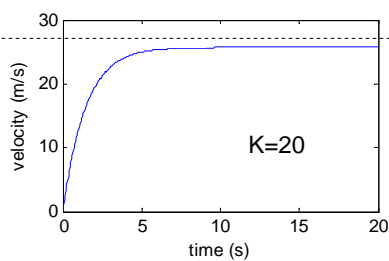
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## Car Cruise Control (Closed Loop)



$$m\ddot{x} + b\dot{x} = f$$

$$f = -bK_p(\dot{x} - \dot{x}_r)$$

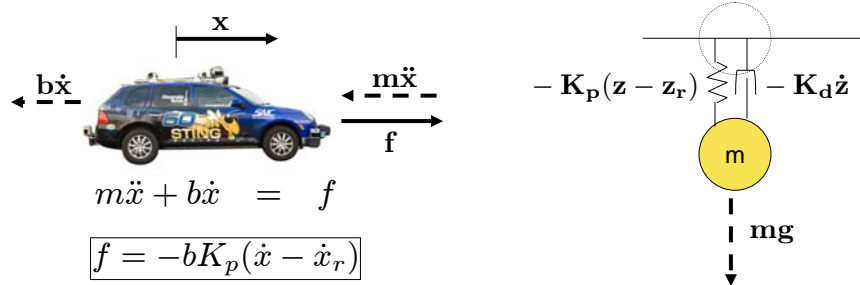


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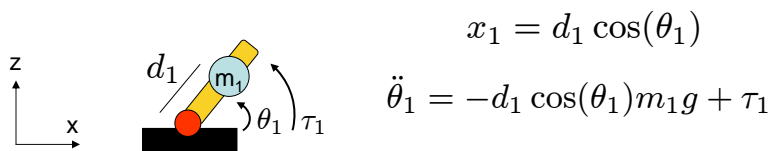
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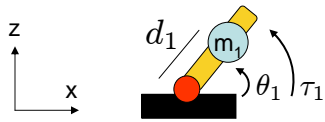
## Another Example



## Manipulator Control (Gravity Compensation)



## Manipulator Control (Gravity Compensation)



$$x_1 = d_1 \cos(\theta_1)$$

$$\ddot{\theta}_1 = -d_1 \cos(\theta_1) m_1 g + \tau_1$$

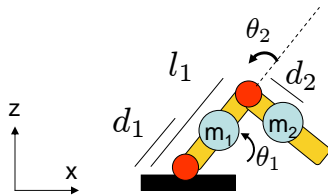
Acceleration due to gravity:

$$\tau_g = -d_1 \cos(\theta_1) m_1 g$$

How do we do position control?

$$\tau_1 = d_1 c_1 m_1 g - K_p(\theta_1 - \theta_{1d}) - K_d \dot{\theta}_1$$

## Manipulator Control (Gravity Compensation)

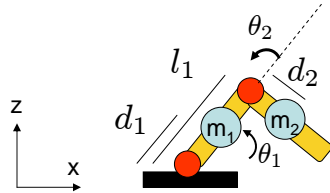


$$x_1 = d_1 c_1$$

$$x_2 = l_1 c_1 + d_2 c_2$$

Torque due to gravity:

## Manipulator Control (Gravity Compensation)



$$x_1 = d_1 c_1$$

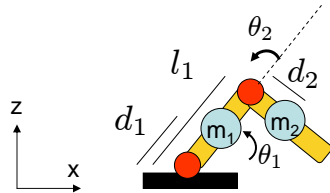
$$x_2 = l_1 c_1 + d_2 c_2$$

Torque due to gravity:

$$\tau_2 = -d_2 c_{12} m_2 g$$

$$\tau_1 = -d_1 c_1 m_1 g - (l_1 c_1 + d_2 c_{12}) m_2 g$$

## Manipulator Control (Gravity Compensation)



$$x_1 = d_1 c_1$$

$$x_2 = l_1 c_1 + d_2 c_{12}$$

Torque due to gravity:

$$\tau_2 = -d_2 c_{12} m_2 g$$

$$\tau_1 = -d_1 c_1 m_1 g - (l_1 c_1 + d_2 c_{12}) m_2 g$$

How do we do position control?

$$\begin{bmatrix} \tau_1 \\ \tau_2 \end{bmatrix} = \begin{bmatrix} d_2 c_{12} m_2 \\ d_1 c_1 m_1 + (l_1 c_1 + d_2 c_{12}) m_2 \end{bmatrix} g - \mathbf{K}_p \begin{bmatrix} \theta_1 - \theta_{1d} \\ \theta_2 - \theta_{2d} \end{bmatrix} - \mathbf{K}_d \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix}$$

Gains are typically diagonal matrices

## Manipulator Control (Full Model)

$$\mathbf{M}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{G}(\mathbf{q}) = \boldsymbol{\tau}$$

## Manipulator Control (Full Model)

$$\mathbf{M}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{G}(\mathbf{q}) = \boldsymbol{\tau}$$

Augmented PD:

$$\mathbf{M}(\mathbf{q})\ddot{\mathbf{q}}_d + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}}_d + \mathbf{G}(\mathbf{q}) - \boxed{\mathbf{K}_d(\dot{\mathbf{q}} - \dot{\mathbf{q}}_d) - \mathbf{K}_p(\mathbf{q} - \mathbf{q}_d)} = \boldsymbol{\tau}$$

Computed Torque:

$$\mathbf{M}(\mathbf{q})(\ddot{\mathbf{q}}_d - \boxed{\mathbf{K}_d(\dot{\mathbf{q}} - \dot{\mathbf{q}}_d) - \mathbf{K}_p(\mathbf{q} - \mathbf{q}_d)}) + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{G}(\mathbf{q}) = \boldsymbol{\tau}$$

## More Jacobians (Virtual Work)

$$\delta \mathbf{x} = \mathbf{J} \delta \mathbf{q} \quad \mathbf{W} = \mathbf{F}^T \mathbf{x} \quad \delta \mathbf{W} = \mathbf{F}^T \delta \mathbf{x} \quad \delta \mathbf{W} = \boldsymbol{\tau}^T \delta \mathbf{q}$$

$$\mathbf{F}^T \delta \mathbf{x} = \boldsymbol{\tau}^T \delta \mathbf{q}$$

$$\mathbf{F}^T \mathbf{J} \delta \mathbf{q} = \boldsymbol{\tau}^T \delta \mathbf{q}$$

Open Loop Force Control

$$\boldsymbol{\tau} = \mathbf{J}^T \mathbf{F}$$

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## More Jacobians (Virtual Work)

$$\delta \mathbf{x} = \mathbf{J} \delta \mathbf{q} \quad \mathbf{W} = \mathbf{F}^T \mathbf{x} \quad \delta \mathbf{W} = \mathbf{F}^T \delta \mathbf{x} \quad \delta \mathbf{W} = \boldsymbol{\tau}^T \delta \mathbf{q}$$

$$\mathbf{F}^T \delta \mathbf{x} = \boldsymbol{\tau}^T \delta \mathbf{q}$$

$$\mathbf{F}^T \mathbf{J} \delta \mathbf{q} = \boldsymbol{\tau}^T \delta \mathbf{q}$$

Open Loop Force Control

$$\boldsymbol{\tau} = \mathbf{J}^T \mathbf{F}$$

Velocity Jacobian for Link Mass i:  $\mathbf{J}_{vi} \quad \mathbf{J}_{vi}^T \mathbf{g} = ?$

$$\mathbf{G} = -(\mathbf{J}_{v1}^T (m_1 \mathbf{g}) + \mathbf{J}_{v2}^T (m_2 \mathbf{g}) \dots \mathbf{J}_{vn}^T (m_n \mathbf{g}))$$

$$\boldsymbol{\tau} = \mathbf{G}(\mathbf{q}) + \mathbf{J}^T \mathbf{F}$$

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## $\tau = J^T F$ Manipulator Workspace Control

$$M(q)\ddot{q} + C(q, \dot{q})\dot{q} + G(q) = \tau$$

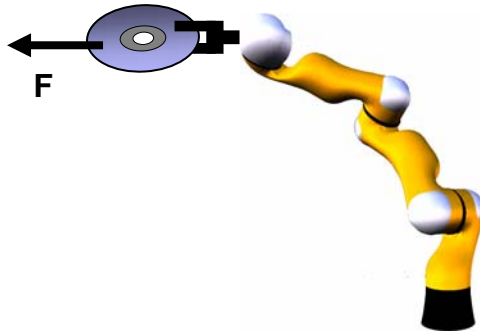
$$\bar{M}(q)\ddot{x} + \bar{C}(q, \dot{q})\dot{x} + \bar{G}(q) = F$$

$$\bar{M} = J^{-T} M J^T$$

$$\bar{C} = J^{-T} (C J^{-1} + M \dot{J}^{-1})$$

$$\bar{G} = J^{-T} G$$

$$F = J^{-T} \tau$$



Khatib '80, Murray '94

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## $\tau = J^T F$ Manipulator Workspace Control

$$M(q)\ddot{q} + C(q, \dot{q})\dot{q} + G(q) = \tau$$

$$\bar{M}(q)\ddot{x} + \bar{C}(q, \dot{q})\dot{x} + \bar{G}(q) = F$$

$$\bar{M} = J^{-T} M J^T$$

$$\bar{C} = J^{-T} (C J^{-1} + M \dot{J}^{-1})$$

$$\bar{G} = J^{-T} G$$

$$F = J^{-T} \tau$$

Computed Torque:

$$F = \bar{M}(q)(\ddot{x}_d - K_d(\dot{x} - \dot{x}_d) - K_p(x - x_d)) + \bar{C}(q, \dot{q})\dot{x} + \bar{G}(q)$$

$$\tau = J^T F$$

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## $\tau = \mathbf{J}^T \mathbf{F}$ Manipulator Workspace Control

$$\begin{aligned} \mathbf{M}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{G}(\mathbf{q}) &= \boldsymbol{\tau} & \bar{\mathbf{M}} &= \mathbf{J}^{-T} \mathbf{M} \mathbf{J}^T \\ \bar{\mathbf{C}} &= \mathbf{J}^{-T} (\mathbf{C} \mathbf{J}^{-1} + \mathbf{M} \dot{\mathbf{J}}^{-1}) & \bar{\mathbf{G}} &= \mathbf{J}^{-T} \mathbf{G} \\ \bar{\mathbf{M}}(\mathbf{q})\ddot{\mathbf{x}} + \bar{\mathbf{C}}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{x}} + \bar{\mathbf{G}}(\mathbf{q}) &= \mathbf{F} & \mathbf{F} &= \mathbf{J}^{-T} \boldsymbol{\tau} \end{aligned}$$

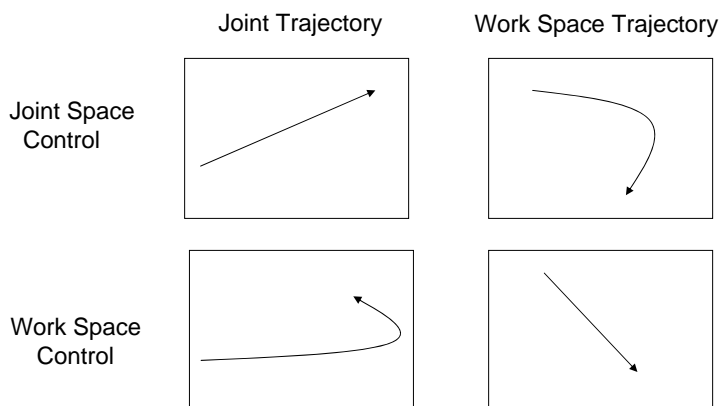
Computed Torque:

$$\begin{aligned} \mathbf{F} &= \bar{\mathbf{M}}(\mathbf{q})(\ddot{\mathbf{x}}_d - \mathbf{K}_d(\dot{\mathbf{x}} - \dot{\mathbf{x}}_d) - \mathbf{K}_p(\mathbf{x} - \mathbf{x}_d)) + \bar{\mathbf{C}}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{x}} + \bar{\mathbf{G}}(\mathbf{q}) \\ \boldsymbol{\tau} &= \mathbf{J}^T \mathbf{F} \end{aligned}$$

Gravity Augmented PD:

$$\begin{aligned} \mathbf{F} &= \bar{\mathbf{G}}(\mathbf{q}) - \mathbf{K}_d(\dot{\mathbf{x}} - \dot{\mathbf{x}}_d) - \mathbf{K}_p(\mathbf{x} - \mathbf{x}_d) \\ \boldsymbol{\tau} &= \mathbf{J}^T \mathbf{F} \end{aligned}$$

## Joint Space vs. Work Space (Step Response)





## Summary

- Dynamic Systems change over time
- Open Loop Control
- Closed Loop PID Control
- Gravity Compensation & Linearization
- Joint Space Position Control
- Work Space Position Control
- Open Loop Force Control

## Thursday

- How do we close the loop on force control?
- What is the relationship between force/position control?
- Can we do both?