

8803 - Mobile Manipulation: Force Control

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- February 19, 2008

Force Control Strategies

- Logic Branching
- Continuous Force Control
 - Direct Feedback
 - Position/Velocity Feedback
- Position Control & Force Control
 - Impedance Control (Classic & Revised)
 - Hybrid Control

Logic Branching

Brief Description:

- Execute specified position/force commands
- Switch behavior on perceived input

Motivation:

- Handle Uncertainty
- Achieve Very Low Tolerances

Ernst '61, Baber '73, Inoue '74

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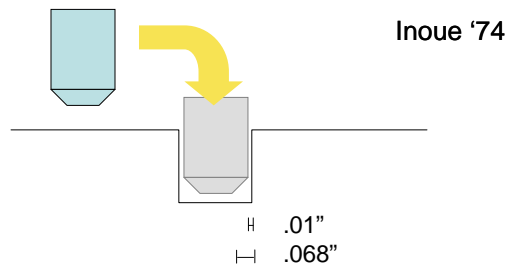
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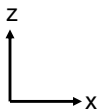
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Peg In Hole

Case 1: Loose Fit



Suppose our positioning error is $< .068''$



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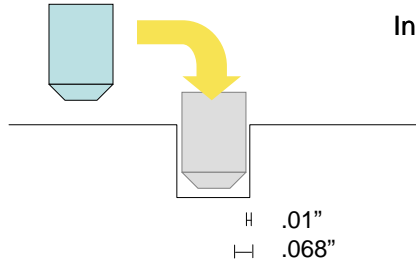
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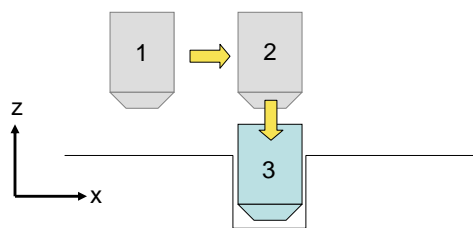
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Case 1: Loose Fit

Inoue '74



Suppose our positioning error is $< .068$ "



- 1) Position Control X
- 2) PUSH-INTO
 - $F_z = \text{Insert Force}$
 - $F_x = 0$

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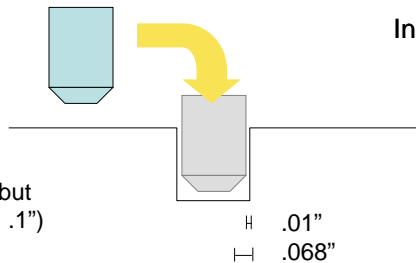
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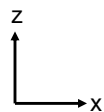
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Case 2: Loose Fit with Uncertainty

Inoue '74



Our positioning error is $< .068$ " but
Starting position is uncertain ($\pm .1$ ")



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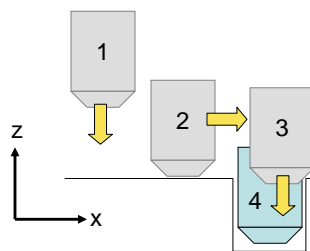
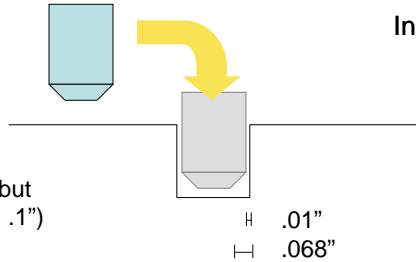
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Peg In Hole

Case 2: Loose Fit with Uncertainty

Inoue '74

Our positioning error is $< .068''$ but
Starting position is uncertain ($\pm .1''$)



- 1) $Z = Z - \Delta$ Until $F_z > 0$
- 2) DROP-INTO
 - $X = X + \Delta$
 - F_z = Small Contact Force
 - F_x = Small Sliding Force Until $F_x > \text{Threshold}$
- 3) PUSH-INTO

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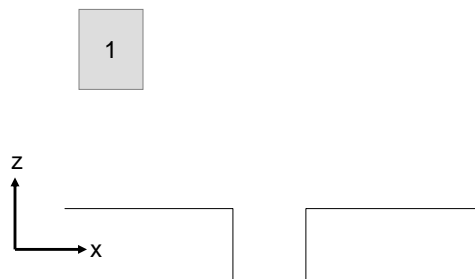
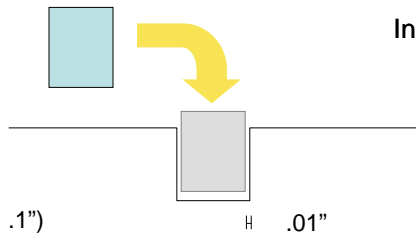
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Case 3: Close Fit

Inoue '74

Positioning error $> .01$ and
Starting position is uncertain ($\pm .1''$)



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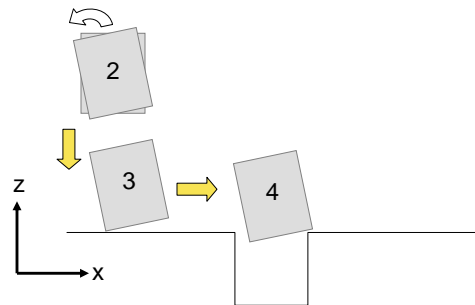
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Case 3: Close Fit

Inoue '74

Positioning error $> .01$ and
Starting position is uncertain ($\pm .1$ ")



- 1) Position Control θ to .1
- 2) DROP-INTO

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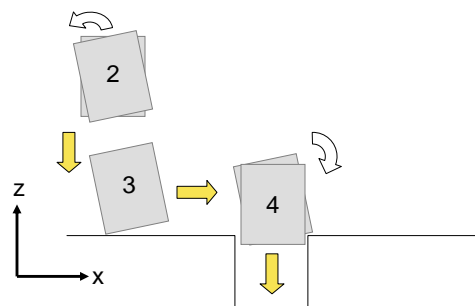
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Peg In Hole

Case 3: Close Fit

Inoue '74

Positioning error $> .01$ and
Starting position is uncertain ($\pm .1$ ")



- 1) Position Control θ to .1
- 2) DROP-INTO
- 3) Torque θ until $\tau > \text{threshold}$
- 4) PUSH-INTO

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Continuous Strategies

- Discrete branching:
 - Advantageous for handling Uncertainty/Tolerances
 - Very useful as part of a system
 - Could be more time efficient
- Continuous Strategies:
 - Coordination of multi-axis motions
 - Responds to continuously changing force-torque information
 - Achieves forces with greater precision

Nevins '73, Whitney '77 Raibert & Craig '81, Mason '81, Khatib '87...

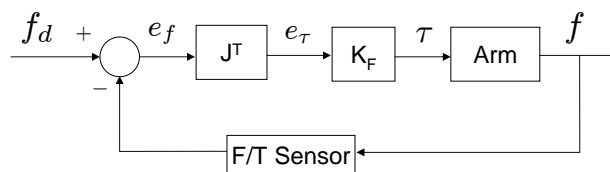
Continuous Force Control

- Feed-forward:

Continuous Force Control

- Feed-forward: $\tau = \mathbf{J}^T \mathbf{F}$
- How do we do Feedback?

Force-based Feedback Control



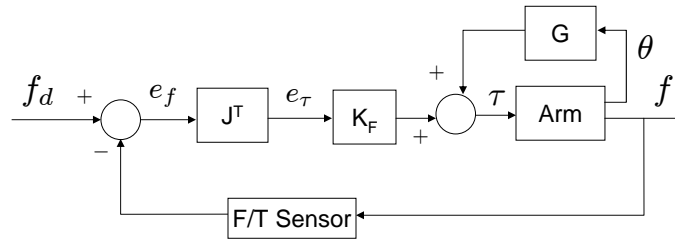
$$\tau = -K_F J^T (f - f_d)$$

Is K_F in Joint Space or Workspace?

Will it work well?

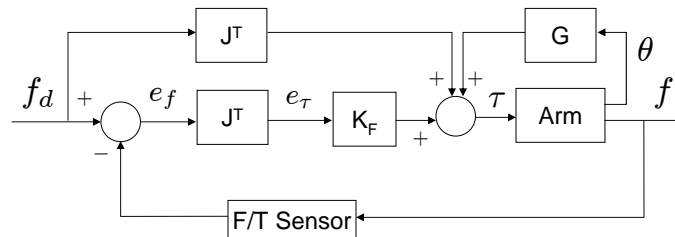
Whitney '85

Force-based Control (Linearization)



$$\tau = G - K_F J^T (f - f_d)$$

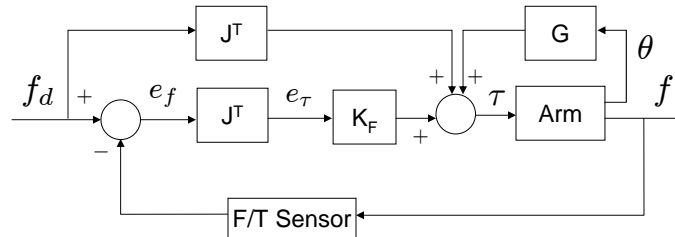
Force-based Control (Feed-forward)



$$\tau = J^T f_d + G - K_F J^T (f - f_d)$$

Similar to Volpe '93

Force-based Control (Feed-forward Term)



$$\tau = J^T f_d + G - K_F J^T (f - f_d)$$

- Non-zero steady-state error
- Can be oscillatory

Similar to Volpe '93

Options

- Integral Control

$$\tau = J^T f_d + G - K_{FI} \int_0^t J^T (f - f_d) dt$$

- Increase Feed-Forward Term

Volpe '93

Options

- Integral Control

$$\tau = \cancel{J^T f_d} + G - K_{FI} \int_0^t J^T (f - f_d) dt$$

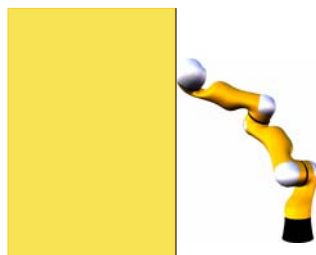
- Increase Feed-Forward Term

Volpe '93

Position-based Force Control

Workspace dynamics: $\bar{G}(q) = f$

Workspace dynamics with contact: $\bar{G}(q) = f + f_E$



Position-based Force Control

Workspace dynamics: $\bar{G}(q) = f$

Workspace dynamics with contact: $\bar{G}(q) = f + f_E$

Generic Position Controller: $f = \bar{G}(q) - K_p(x - x_d)$

Controlled System Dynamics: $\bar{\bar{G}}(q) = \bar{G}(q) - K_p(x - x_d) + f_E$



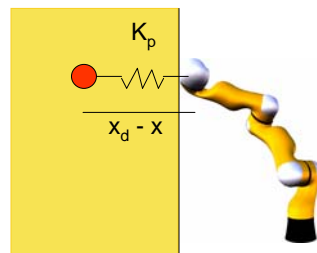
Position-based Force Control

Workspace dynamics: $\bar{G}(q) = f$

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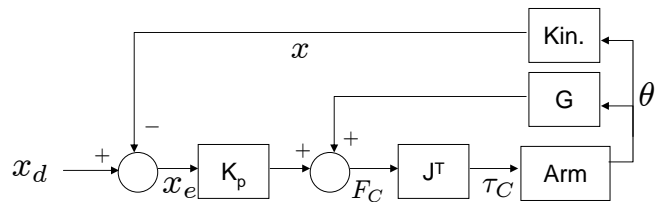


$$K_p(x - x_d) = f_E$$

$$x_d = -K_p^{-1} f_E + x$$

Position-based Force Control: Feedback

Position Control:



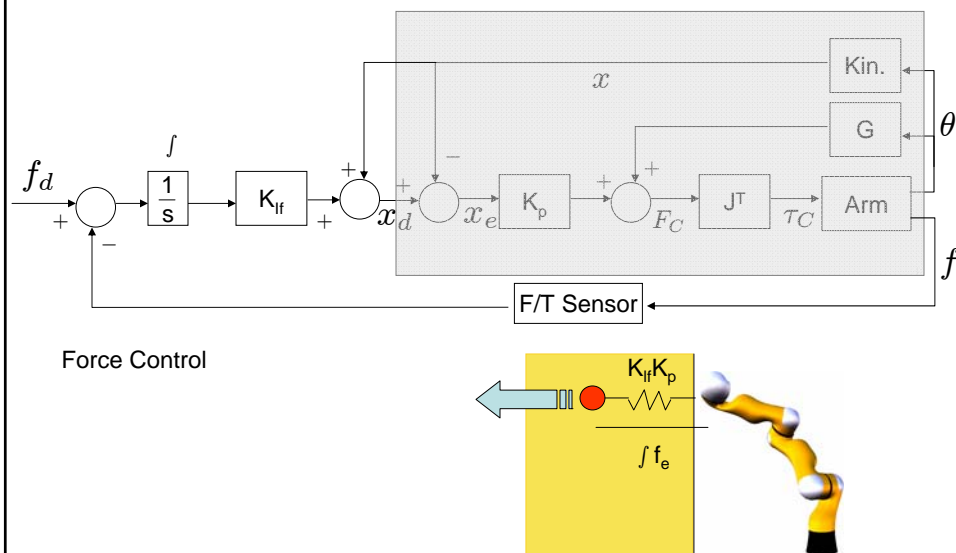
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Position-based Force Control: Feedback



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Position Control + Force Control

Impedance Control

- Continuous relationship between position/force
- Simulates behavior of a simple mechanical system

Hybrid Control

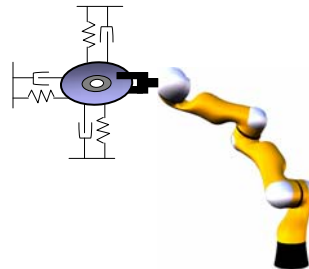
- Selection Matrix identifies directions for position/force
- Allows for precise positioning and force control

Impedance Control

How would the robot respond if its dynamics were actually:

$$\mathbf{M}_d \ddot{\mathbf{x}} - \mathbf{D}_d \dot{\mathbf{x}}_e - \mathbf{K}_d \mathbf{x}_e = \mathbf{f}_E \quad \mathbf{x}_e = (\mathbf{x} - \mathbf{x}_r)$$

- Position tracking when force = 0
- Compliance when force > 0
- Restoration to tracking when force is removed



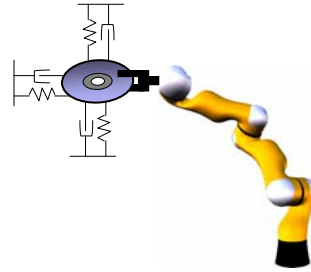
Impedance Control

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- Position tracking when force = 0
- Compliance when force > 0
- Restoration to tracking when force is removed

$$\ddot{\mathbf{x}} = \mathbf{M}_d^{-1}(\mathbf{f}_E + \mathbf{D}_d \dot{\mathbf{x}}_e + \mathbf{K}_d \mathbf{x}_e)$$



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Impedance Control

How would the robot respond if its dynamics were actually:

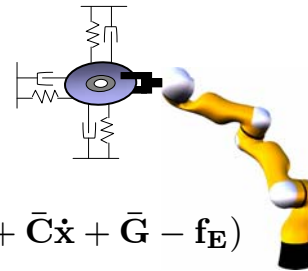
$$\mathbf{M}_d \ddot{\mathbf{x}} - \mathbf{D}_d \dot{\mathbf{x}}_e - \mathbf{K}_d \mathbf{x}_e = \mathbf{f}_E \quad \mathbf{x}_e = (\mathbf{x} - \mathbf{x}_r)$$

- Position tracking when force = 0
- Compliance when force > 0
- Restoration to tracking when force is removed

$$\ddot{\mathbf{x}} = \mathbf{M}_d^{-1}(\mathbf{f}_E + \mathbf{D}_d \dot{\mathbf{x}}_e + \mathbf{K}_d \mathbf{x}_e)$$

Notice the similarity to workspace computed torque:

$$\boldsymbol{\tau} = \mathbf{J}^T(\bar{\mathbf{M}}(\mathbf{M}_d^{-1}(\mathbf{f}_E + \mathbf{D}_d \dot{\mathbf{x}}_e + \mathbf{K}_d \mathbf{x}_e)) + \bar{\mathbf{C}}\dot{\mathbf{x}} + \bar{\mathbf{G}} - \mathbf{f}_E)$$



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Position-based Impedance Control

$$\mathbf{M}_d \ddot{\mathbf{x}} - \mathbf{D}_d \dot{\mathbf{x}}_e - \mathbf{K}_d \mathbf{x}_e = \mathbf{f}_E \quad \mathbf{x}_e = (\mathbf{x} - \mathbf{x}_r)$$

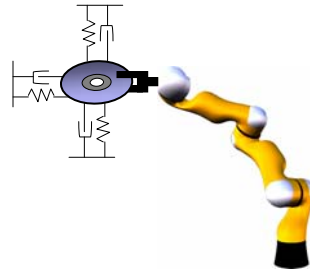
- 1) Simulate the system response to \mathbf{f}_E

$$\ddot{\mathbf{x}}(\mathbf{t} + \Delta \mathbf{t}) = \mathbf{M}_d^{-1}(\mathbf{f}_E + \mathbf{D}_d \dot{\mathbf{x}}(\mathbf{t}) + \mathbf{K}_d \mathbf{x}(\mathbf{t}))$$

$$\dot{\mathbf{x}}(\mathbf{t} + \Delta \mathbf{t}) = \dot{\mathbf{x}}(\mathbf{t}) + \ddot{\mathbf{x}}(\mathbf{t}) \Delta \mathbf{t}$$

$$\mathbf{x}(\mathbf{t} + \Delta \mathbf{t}) = \mathbf{x}(\mathbf{t}) + \dot{\mathbf{x}}(\mathbf{t}) \Delta \mathbf{t}$$

- 2) Track simulated \mathbf{x} (possibly $\dot{\mathbf{x}}$)



Hybrid Control

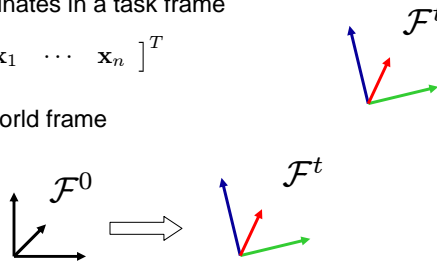
- Task Constraint: **Restriction on the freedom of motion of the manipulator**
- Cannot move in some direction
- Can control forces/moments in that direction

- Degrees of freedom are coordinates in a task frame

$$\mathbf{x} = [\mathbf{x}_1 \quad \cdots \quad \mathbf{x}_n]^T$$

- Task frame is a transformed world frame

$$\mathcal{F}^t = \mathbf{T}_t^0 \mathcal{F}^0$$



Hybrid Control

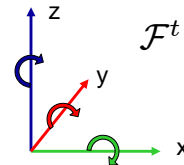
- A motion constraint is described by a selection matrix:

$$\mathbf{S} = \begin{bmatrix} s_1 & & \\ & \dots & \\ & & s_n \end{bmatrix} \quad \mathbf{S}\dot{\mathbf{x}} = \mathbf{0}$$

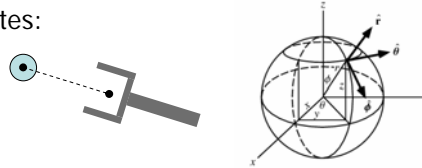
- Coordinates – Cartesian + Fixed Axis (Roll, Pitch Yaw)

$$\mathbf{R}_B^t = R(z_t, \phi)R(y_t, \theta)R(x_t, \psi)$$

$$\mathbf{S}_{RPY} = \mathbf{I} \begin{bmatrix} s_x & s_y & s_z & s_\psi & s_\theta & s_\phi \end{bmatrix}^T$$



- Alternative Coordinates:



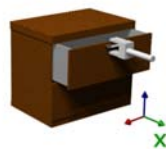
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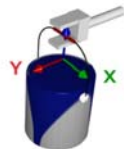
Examples of Constraints



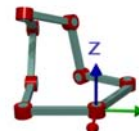
$[0 \ 1 \ 1 \ 1 \ 1 \ 1]$



$[1 \ 1 \ 1 \ 1 \ 1 \ 0]$



Parameterized $[0 \ 0 \ 0 \ 1 \ 1 \ 0]$



Parameterized $[1 \ 1 \ 1 \ 1 \ 1 \ 0]$

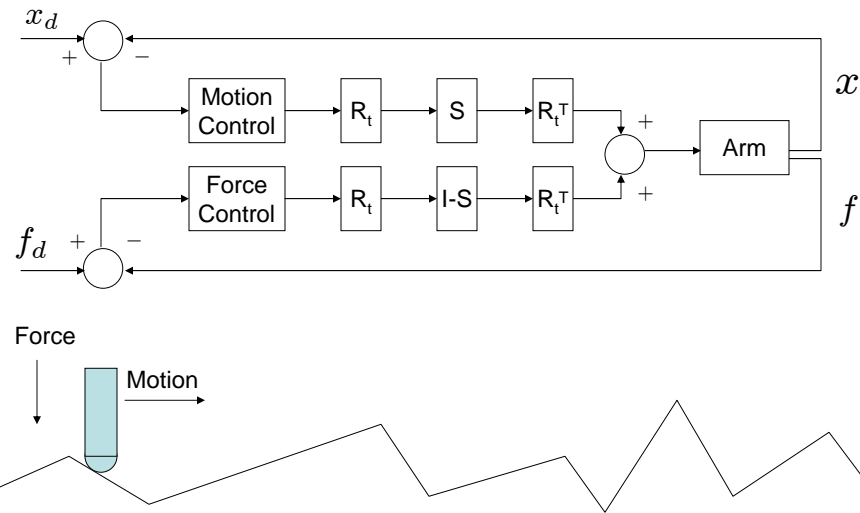
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Hybrid Control



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Best of Both Worlds

- Use task frame to set a center of compliance for impedance control
- Use Impedance Control (not motion control) in hybrid system
- Vary the parameters of Impedance Control according to direction

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Summary

We looked at:

- Logic Branching
- Continuous Force Control (Force and Position Based)
- Hybrid Position/Force Strategies

Your goal:

- Think about how these strategies can help you accomplish the task
- Which subtasks require which type of control?