

Lecture 11
of
EEE307

Electronics for Communications

**Department of Electrical & Electronic Engineering
Xi'an Jiaotong-Liverpool University (XJTLU)**

Friday, 29th November 2019

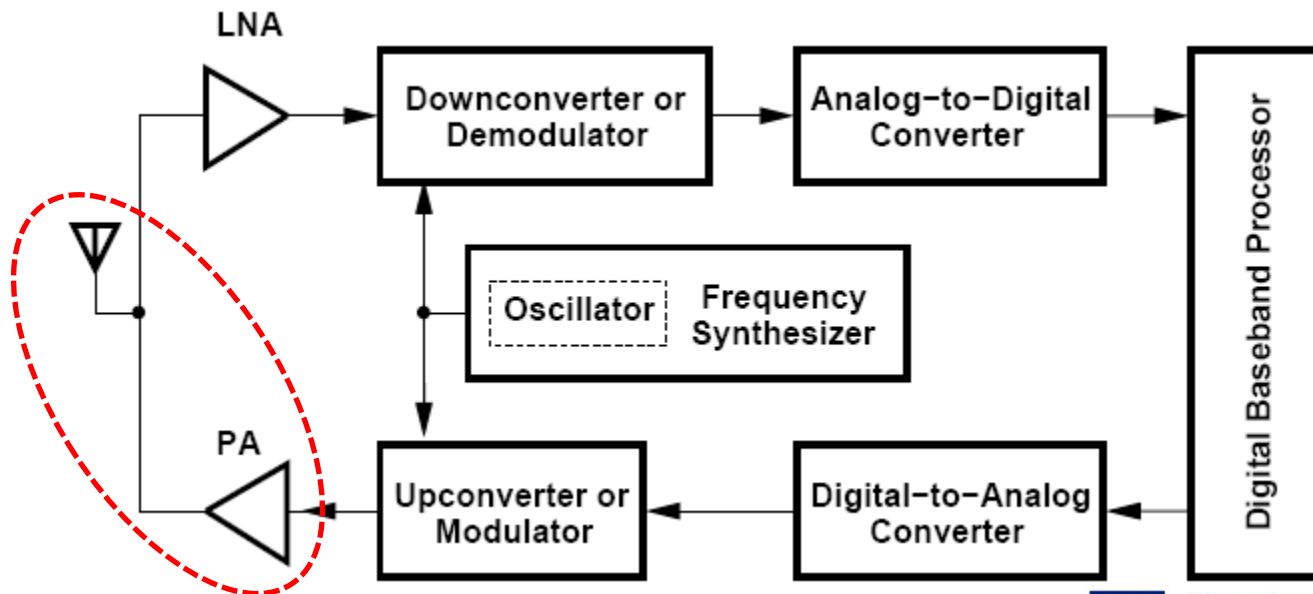
- ❑ Large-signal Amplification
 - efficiency & linearity consideration
 - common-source configuration
- ❑ Classification of Power Amplifiers
 - classes A, B, AB, C – linear type
 - classes E & F – switching type



Wireless Transceiver

(antenna driven by transmitter)

- ❑ In using **radio waves** to transmit and receive information, the **transmitter** has to drive the **antenna** with a high power level so that the **electromagnetic** (EM) signal is strong enough to reach certain desirable distances.



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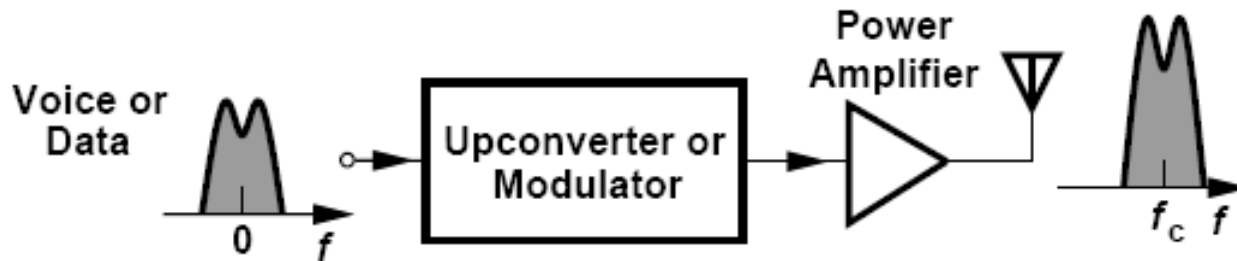
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Radio Transmitter

(deliver RF power to antenna)

- In radio transmitters, the **power amplifier (PA)** is the key building block to deliver electrical power *efficiently* to the **antenna** for generating EM waves which carry the information.

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- While the RF PA is also a signal amplification circuit, its design and construction is not simply scaling up the small-signal amplifiers (e.g. LNA) to deliver higher output power.

RF Power Amplifier

(power consumption & efficiency)

- ❑ To deliver high enough power (e.g. 1 W or 30 dBm) to the **antenna**, the RF PA consumes most power in a radio transceiver.
- ❑ High **power consumption** in RF PAs is unavoidable and the key issue is **efficiency**.
- ❑ **Power efficiency** is particularly important for *portable* applications because we want to extend the battery life or reduce the battery weight.
- ❑ It would be a serious **thermal management** problem if the efficiency is low.
 - **power loss \Rightarrow heat dissipation.**



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RF Power Amplifier

(50% efficiency in maximum power transfer)

- ❑ With the importance of **efficiency** in RF PAs, the consideration of maximum power transfer (by **conjugate matching**) in small-signal amplifiers (e.g. LNA) is not quite applicable.
 - It is also unclear to define impedances in a large-signal, nonlinear system like RF PAs.
- ❑ Even with conjugate matching for maximum power transfer, the **efficiency** is only 50% at best.
 - 50% of the DC power supplied to the RF PA would dissipate as **heat** \Rightarrow thermal management problems at the chip level or package level
 - possible heat sink requirement

RF Power Amplifier

(other performance parameters & trade-off)

- ❑ Apart from **efficiency**, **linearity** and output power (as well as the power gain) are other important performance parameters in RF PAs.
 - In modern wireless communication systems, complex **modulation schemes** (with amplitude & phase modulations combined together) are employed to increase the data throughput. This places higher **linearity** requirement on RF PAs.
- ❑ The RF PA design typically involves the **trade-off** between **efficiency** and **linearity**.
 - It is performance and cost **trade-off**.
 - It is difficult to satisfy all requirements.



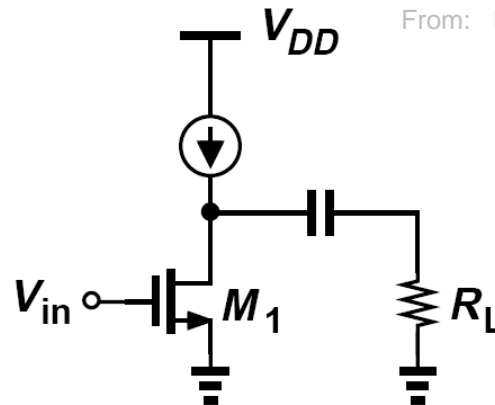
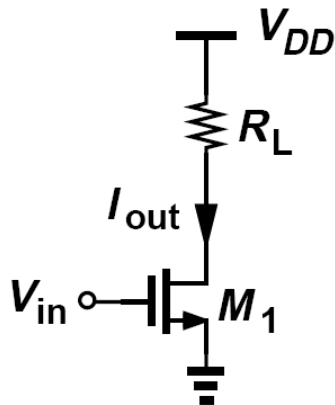
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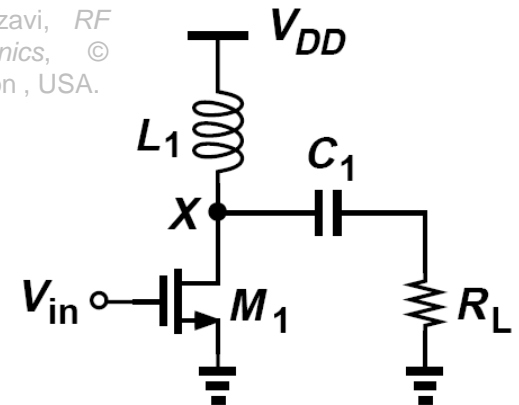
RF Power Amplifier

(common-source configuration)

- ❑ An RF PA can be realised in CMOS technology using the standard **common-source** (CS) configuration as in small-signal amplifiers (e.g. LNA).
 - One difference in RF PAs is the large current (e.g. 200 mA) flowing through the single transistor in the CS amplifier.



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- The CS amplifier can have a resistive, current source or inductive load.



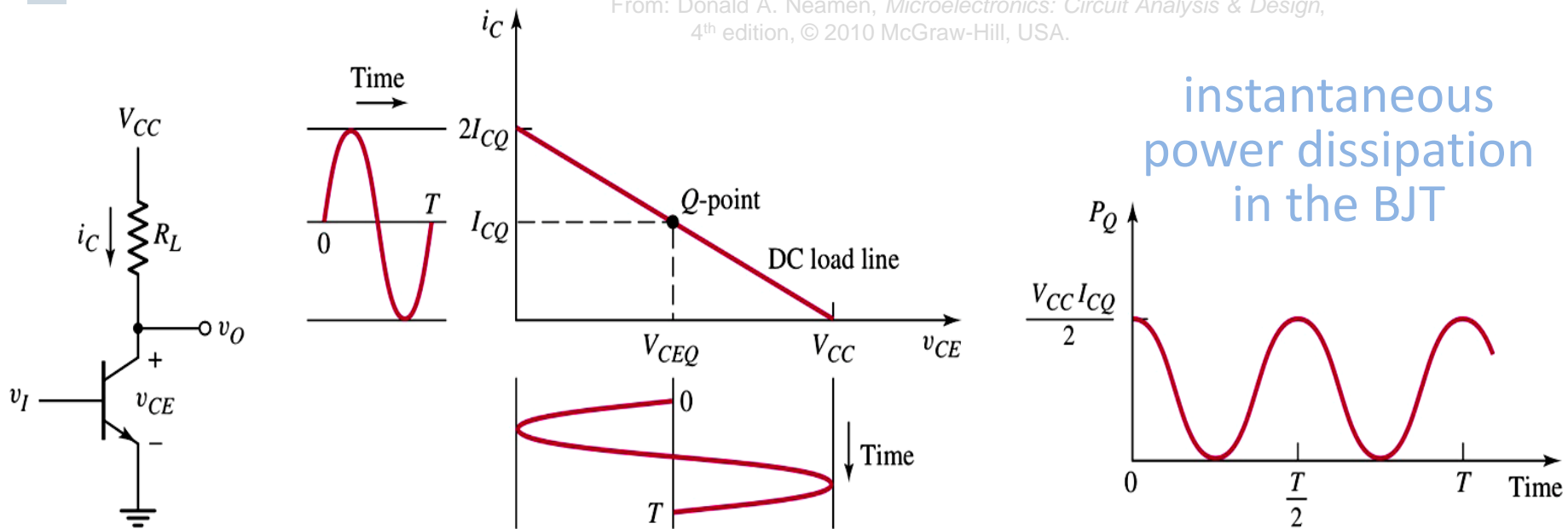
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RF Power Amplifier

(common-emitter configuration)

- ❑ The use of the CS configuration in the RF PA is the same as that in the low-frequency PA design (e.g. audio amplifiers). The BJT counterpart is the common-emitter (CE) amplifier.

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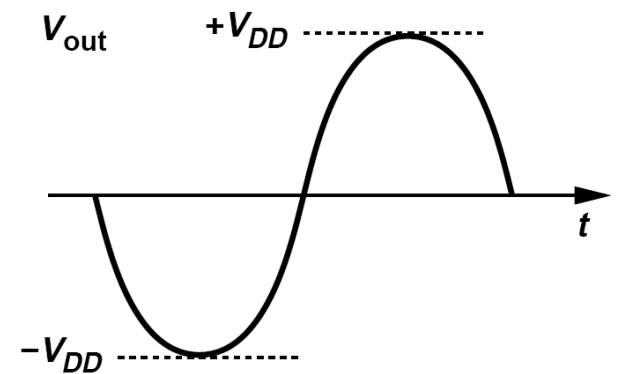
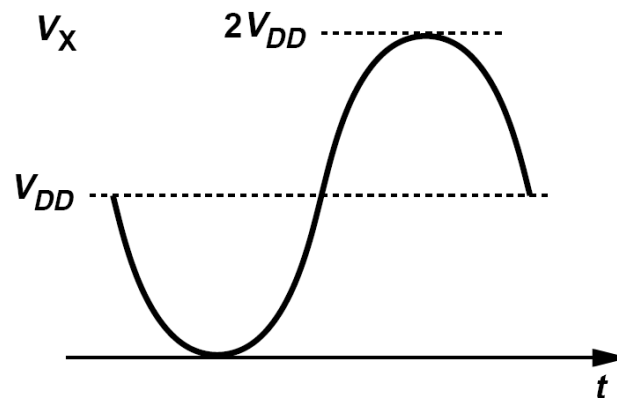
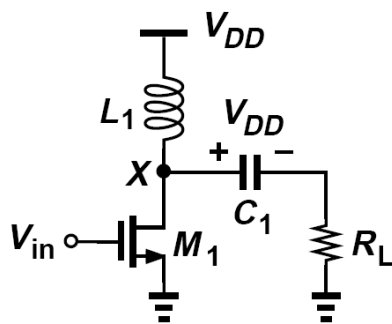
- The CE amplifier shown here is in class-A operation.

RF Power Amplifier

(inductive load & peak voltage)

- ❑ In the RF PA design with the common-source configuration, an **inductive load** is typically used.
 - With the inductive load, the instantaneous voltage at the drain terminal of the MOSFET can be as high as $|2V_{DD}|$ while the output swing is between $-V_{DD}$ and $+V_{DD}$.

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- This implies the high breakdown voltage requirement of the MOSFET.

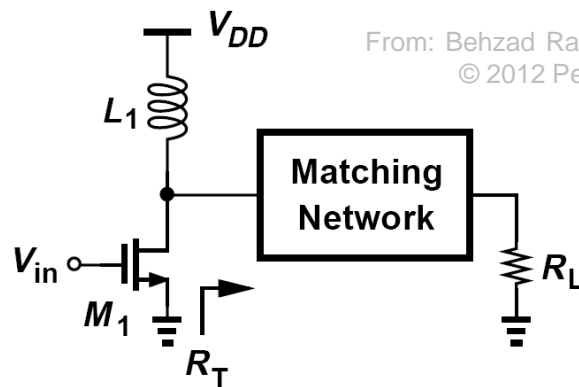


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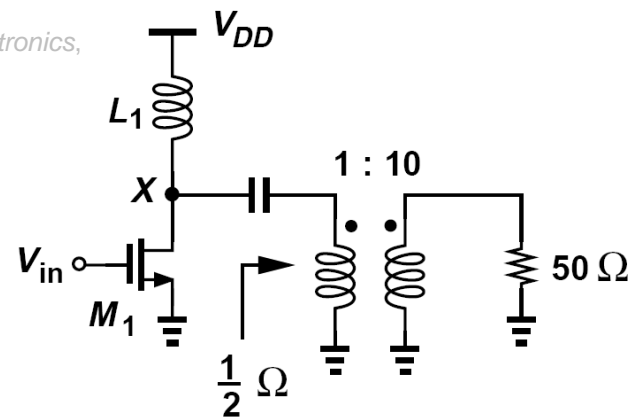
RF Power Amplifier

(inductive load & peak voltage)

- ❑ In order to reduce the peak voltage experienced by the transistor in the CS configuration, **matching network** is typically used between the RF PA and the antenna load.



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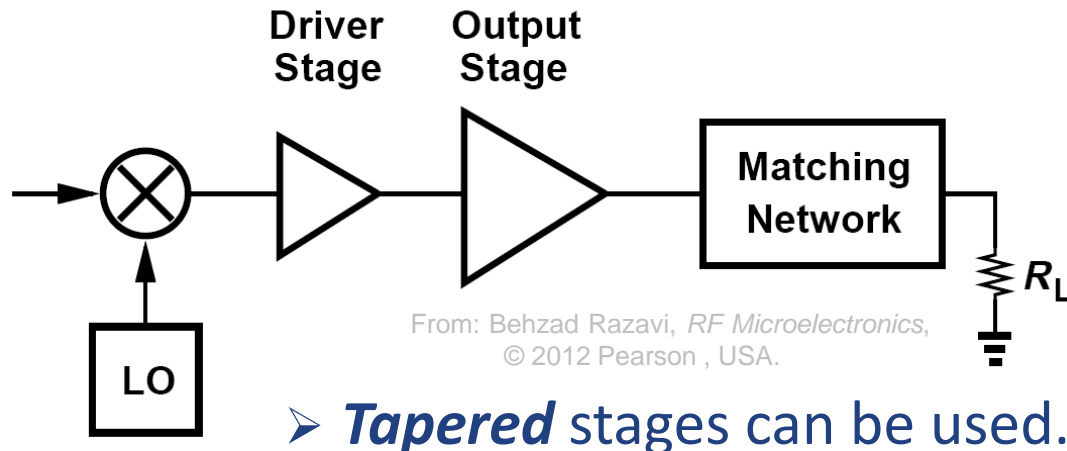


- The **matching network transforms** the load resistance to a much lower value (e.g. 50Ω to 0.5Ω).
- LC circuits and transformers can be used for the **impedance transformation**.

RF Power Amplifier

(high currents & tapered stages)

- ❑ With the **matching network** for **impedance transformation**, the peak-to-peak voltage swing experienced by the transistor in the RF PA can be lowered.
- ❑ To deliver the same power to antenna load with a reduced voltage swing, it means that the current flowing into the RF PA must be increased.



- It needs a large size (W/L) for the MOSFET in the RF PA. Large size however causes large input capacitance.



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RF Power Amplifier

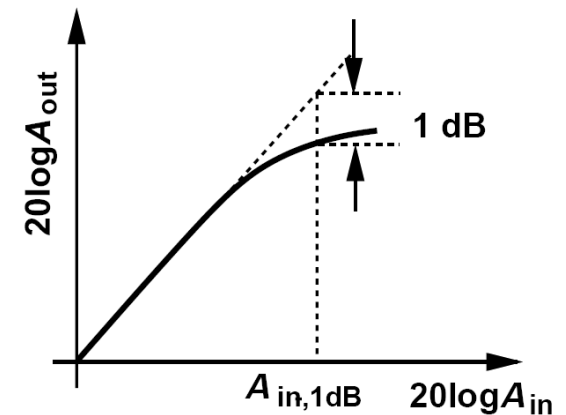
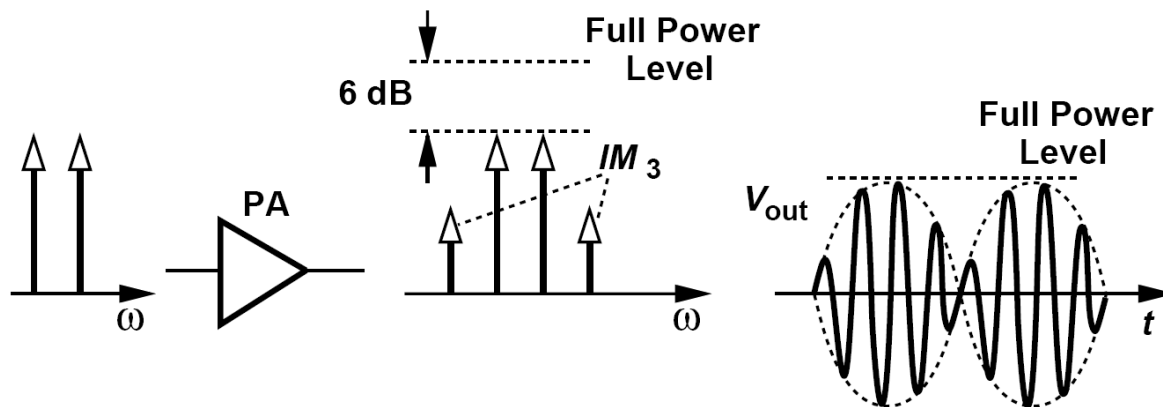
(efficiency definitions)

- ❑ Two common definitions of **efficiency** are used in quantifying the performance of RF PAs:
 - the **drain efficiency** (when the MOS transistors are used): $\eta = \frac{P_{out}}{P_{supp}}$
 - the **power added efficiency (PAE)**: $\eta_{PAE} = \frac{P_{out} - P_{in}}{P_{supp}}$
- where P_{out} is the output power delivered to the load and P_{supp} is the DC power supplied to the RF PA.
- ❑ The **drain efficiency** η and **PAE** η_{PAE} will be very close if the RF PA has large enough power gain.

RF Power Amplifier

(linearity)

- ❑ To gauge the **linearity** performance, the RF PA characterisation begins with two generic tests of nonlinearity based on unmodulated tones: **intermodulation** and **compression**.



- The **3rd order intercept point (IP3)** and **1-dB compression point (P_{1dB})** are specified.

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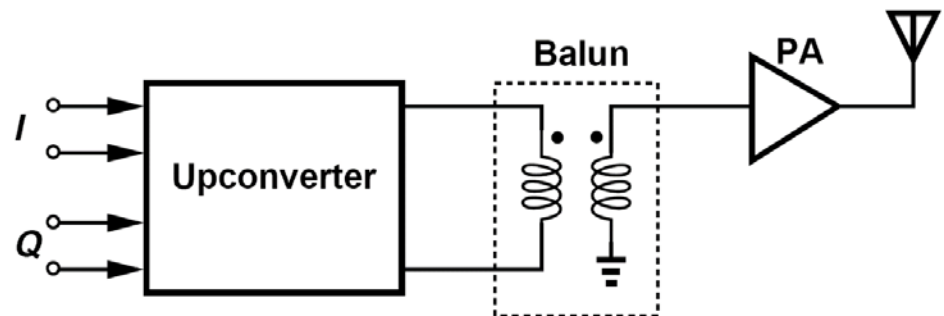
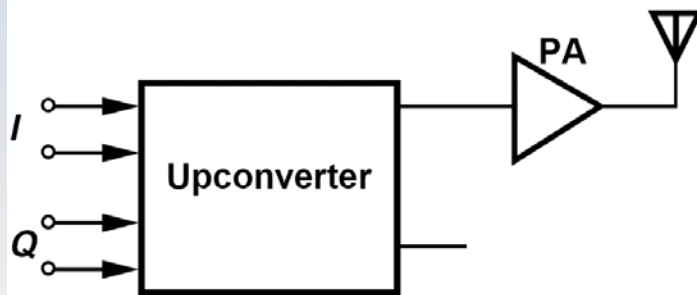
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RF Power Amplifier

(differential upconverter output)

- ❑ As the **antenna** is typically *single-ended*, most stand-alone RF PAs are single-ended.
- ❑ To avoid wasting half of the transmitter signal gain with the ***differential*** output signal from the upconverter, a **balun** can be used between the upconverter and the ***single-ended*** RF PA.

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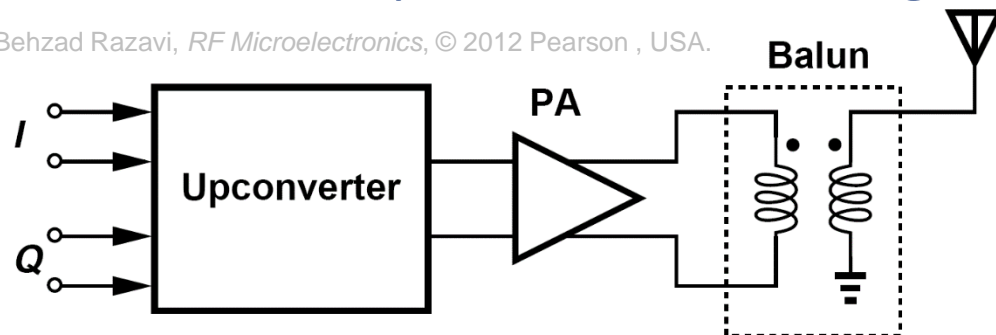
- A **balun** is a transformer used to convert an unbalanced signal to a balanced one or vice versa.

RF Power Amplifier

(differential RF PA)

- ❑ As the RF PA circuit typically use some inductors, large **transient currents** can be induced easily in high frequency operation.
- ❑ A **differential** realisation of RF PAs can ease significantly the adverse effects of the large **transient currents** compared with the **single-ended** RF PAs.

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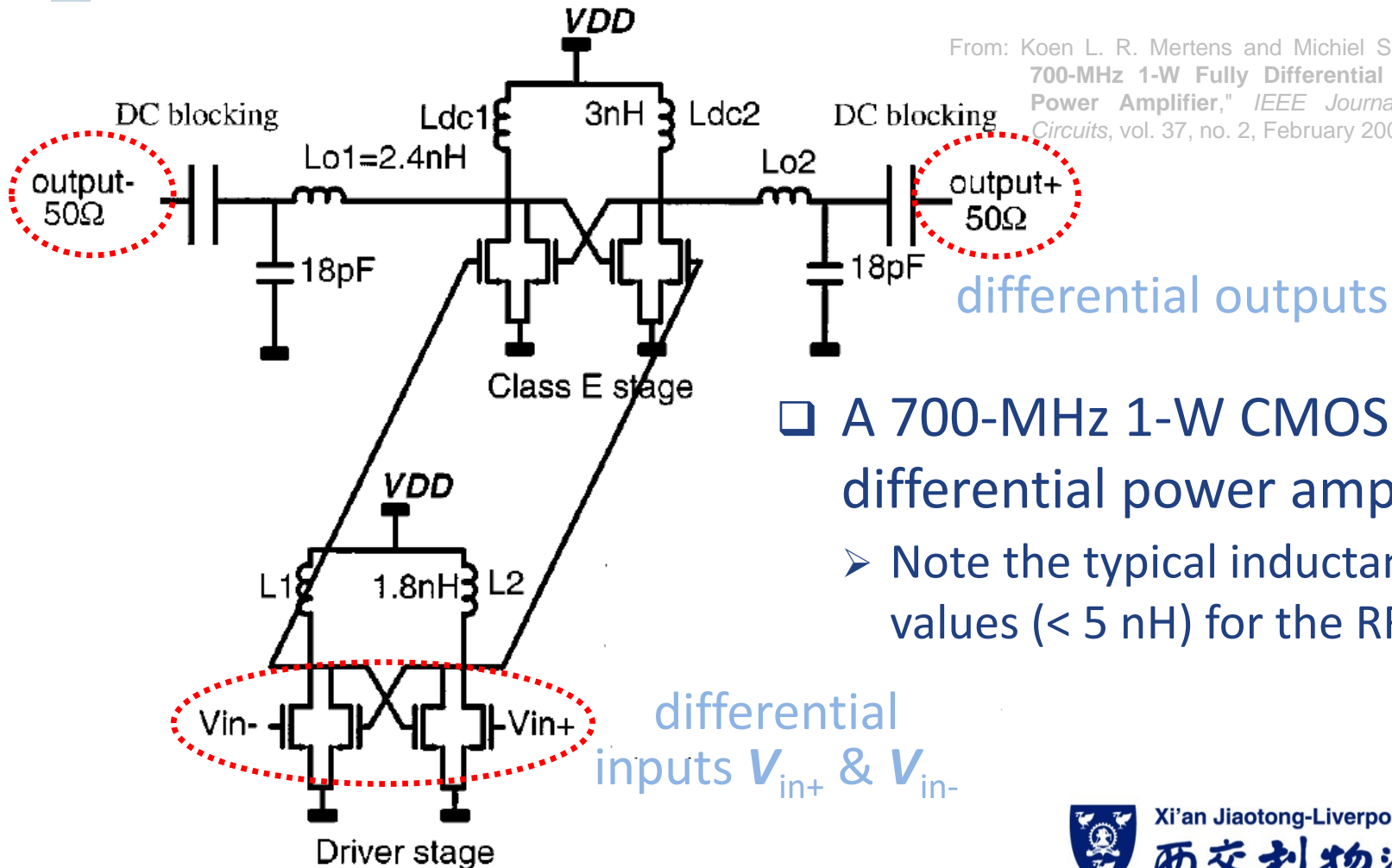
- With a **differential** RF PA, a **balun** is used to convert balanced signal to feed the single-ended antenna.



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RF Power Amplifier

(differential implementation)



- A 700-MHz 1-W CMOS differential power amplifier
 - Note the typical inductance values (< 5 nH) for the RF PA.



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Classification of Power Amplifiers

(different classes & design trade-off)

- ❑ Despite the apparent simple circuit construction, power amplifiers are traditionally categorised in quite a number of classes: A, B, AB, C, D, E, F etc.
 - The varying classes of RF PAs indicate the difficulty in the design **trade-off** to *optimise* the performance, especially **efficiency** and **linearity**.
- ❑ RF PAs of class A, B, AB and C have almost the same schematic circuit (e.g. CS or CE configuration) in terms of the power amplification transistor.
 - They are distinguished primarily by the bias condition of the transistor.

Classification of Power Amplifiers

(linear & switching RF PAs)

- ❑ RF PAs of class A, B, AB and C share an attribute that both the input and output **waveforms** are presumably **sinusoidal**.
 - They generally display better **linearity** in the signal amplification.
 - The power amplification transistors work as a voltage-controlled current source.
- ❑ RF PAs of class D, E and F are of the switching type that improves the **efficiency**.
 - The transistor works as a switch.
 - The waveforms are not sinusoidal.

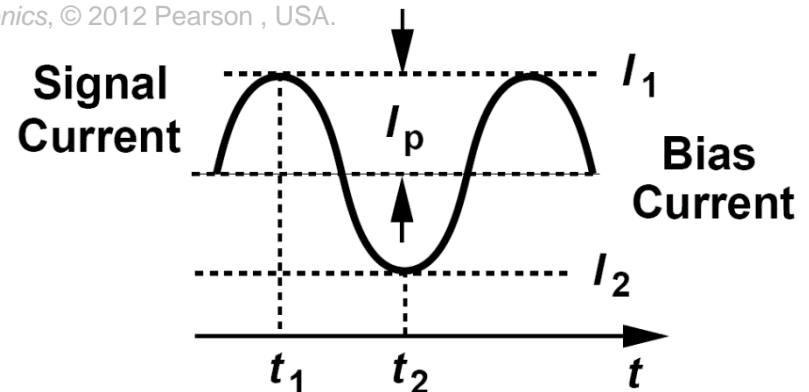
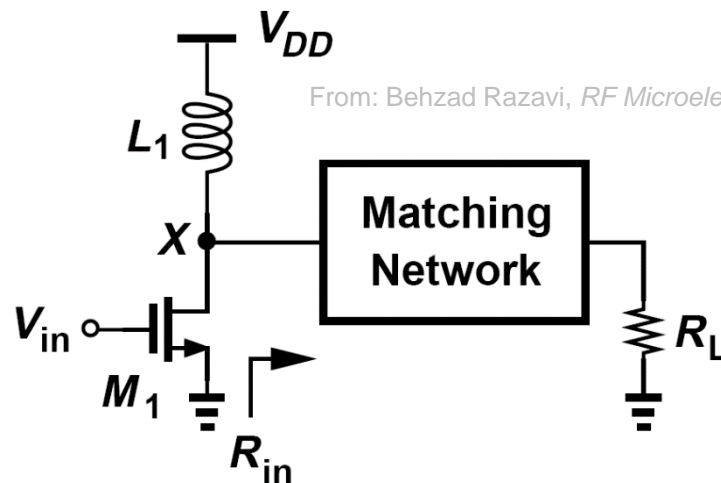


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Class A Power Amplifiers

(linear power amplifier)

- In the common-source (or common-emitter in the BJT case) configuration, a class A power amplifier has the transistor always on and operating *linearly* across the full input and output range.



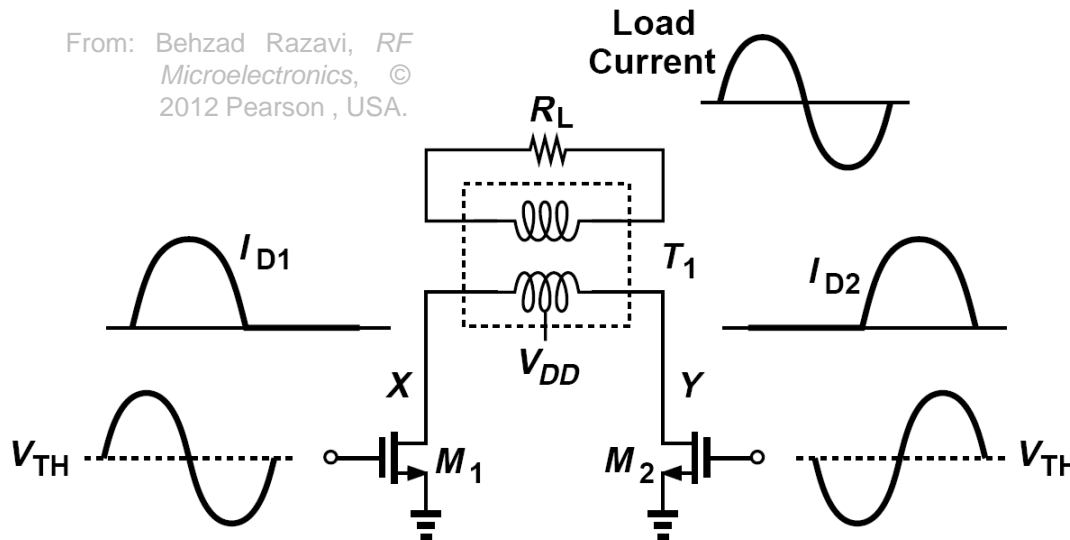
$$\eta = \frac{V_{DD}^2 / (2R_{in})}{V_{DD}^2 / R_{in}} = 50\%$$

Class B Power Amplifiers

(on half of the cycle)

- ❑ In a class B power amplifier, the power amplification transistors are on only during half of the cycle of the sinusoidal signal.
 - Two transistors can be employed as parallel stages and each transistor conducts only half of the cycle.

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- Class B power amplifiers have better efficiency than class A.

- $\eta_B = \pi/4 \approx 79\%$.



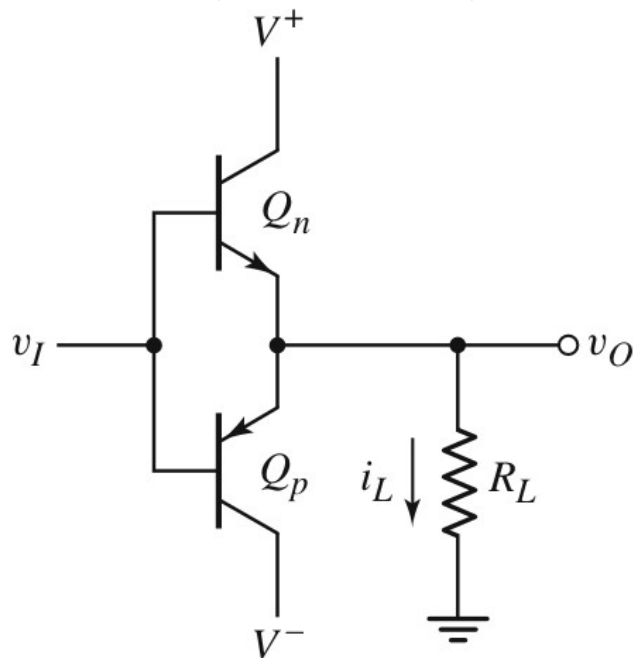
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Class B Power Amplifiers

(use of complementary transistors)

- A class B power amplifier can also be implemented using a pair of **complementary** transistors (e.g. npn & pnp BJTs, nMOSFET & pMOSFET).

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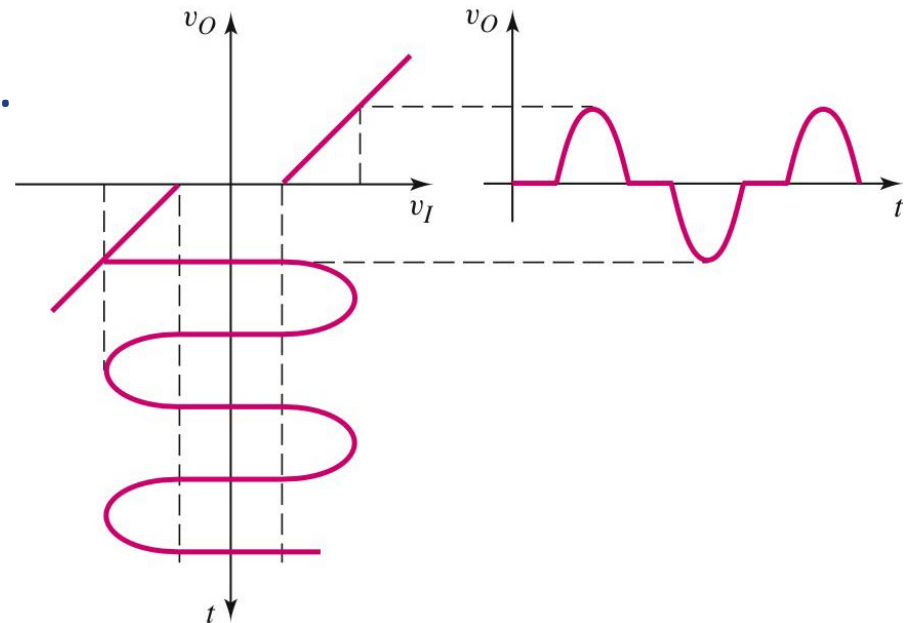
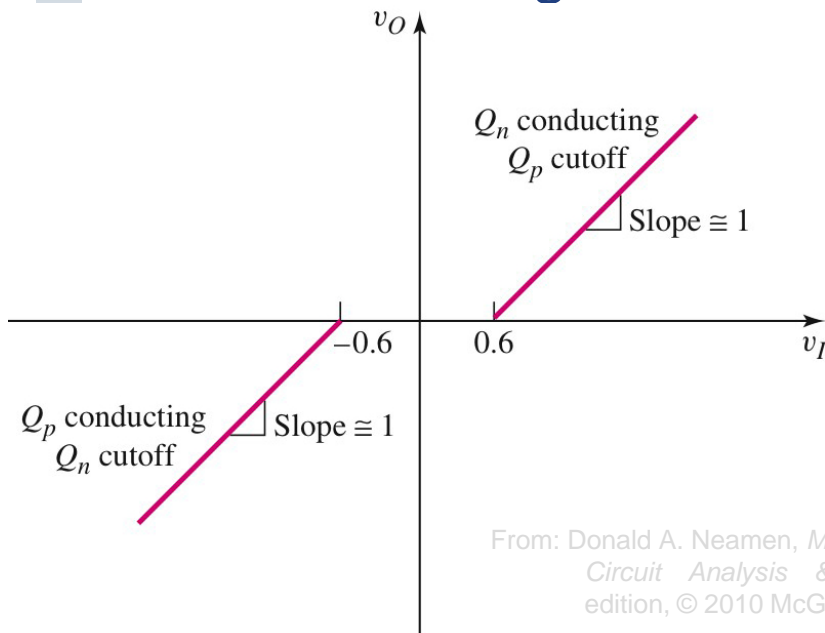
➤ This configuration is called a **complementary push-pull output stage** as used in audio amplifiers.

- BJT Q_n conducts during the positive half of the input cycle while Q_p conducts during the negative half-cycle.

Push-Pull Output Stage

(crossover distortion)

- ❑ In the simple **complementary** push-pull output stage, the voltage transfer characteristics have a range of input voltage around 0 V where both transistors are cut-off and the output voltage is zero.
 - It causes signal distortion.



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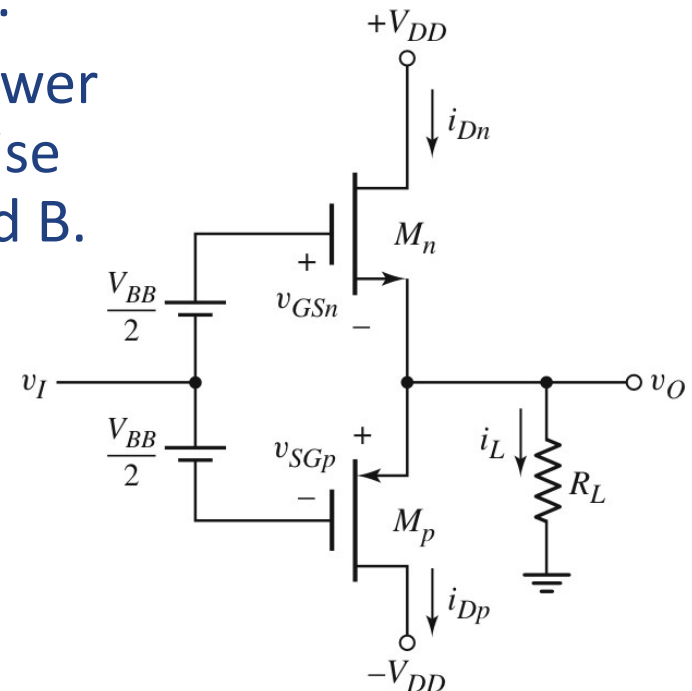
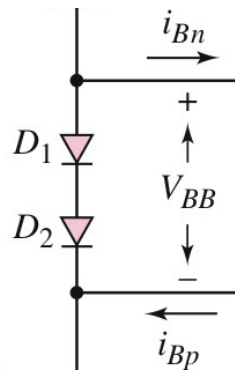
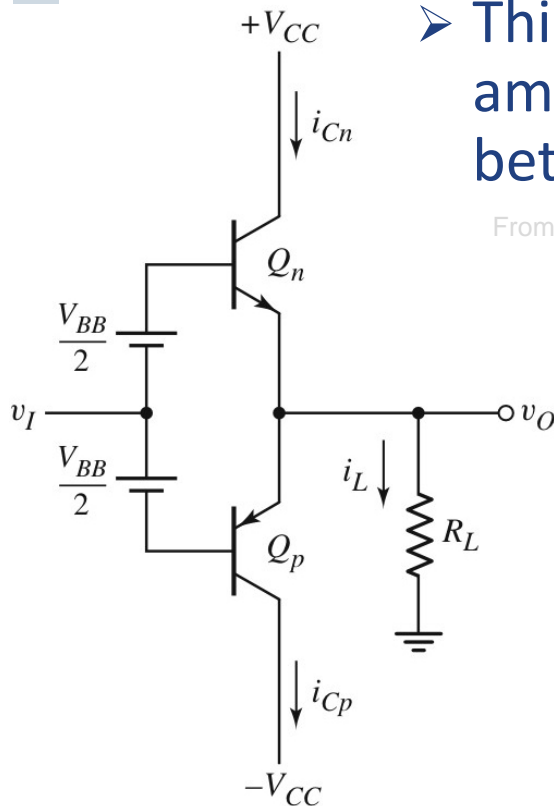
Class AB Power Amplifiers

(crossover distortion elimination)

- ❑ Crossover distortion in the **complementary push-pull output stage** can be avoided by applying a small bias voltage on each output transistor.

➤ This is the class AB power amplifier, a compromise between classes A and B.

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Classification of Power Amplifiers

(conduction angle less than 180° or π)

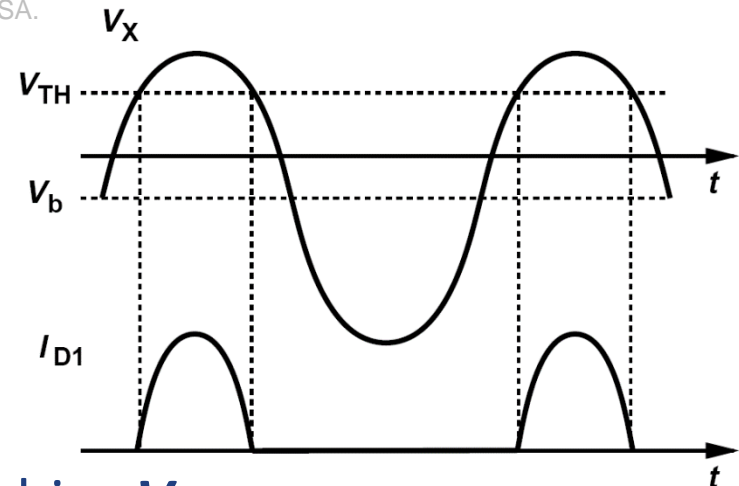
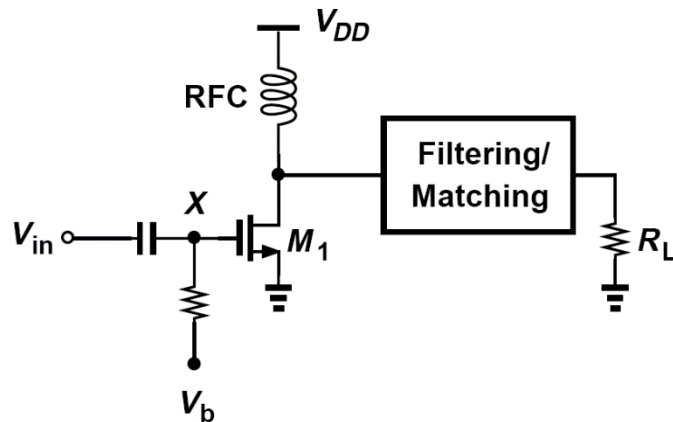
- ❑ In the classification of power amplifiers, it is helpful to distinguish the classes by the **conduction angle**.
 - It is defined as the percentage of the signal period during which the output transistors conduct current multiplied by 360° (or 2π).
- ❑ The conduction angle is 360° (or 2π) for class A power amplifiers, 180° (or π) for class B, and slightly more than 180° (or π) for class AB.

Class C Power Amplifiers

(conduction angle less than π)

- ❑ It can be seen in classes A and B power amplifiers that a smaller **conduction angle** gives higher **efficiency**.
- ❑ In class C power amplifiers, the output transistor is biased to conduct in less than half of the cycle.

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- In the CS configuration, the bias V_b makes V_X above V_{TH} of the MOSFET for only a fraction of the cycle.

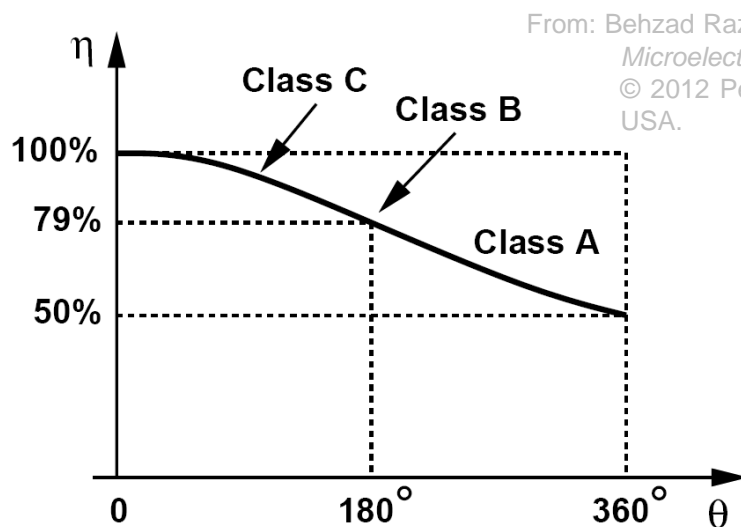


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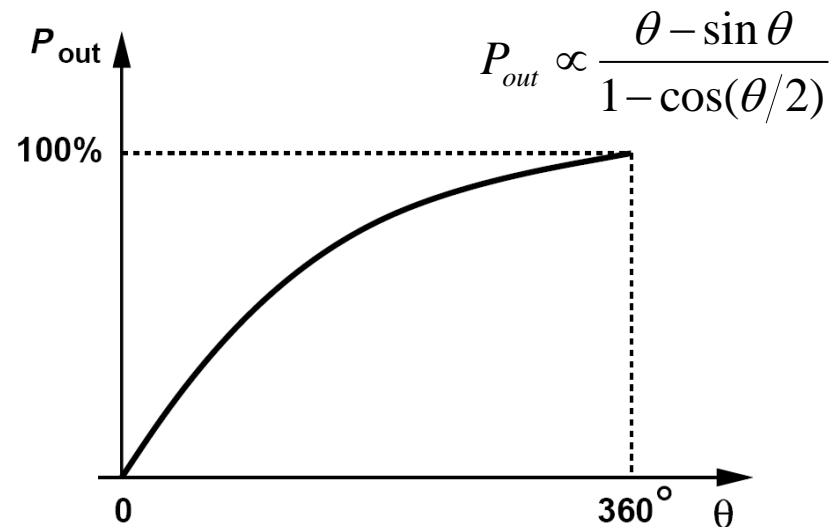
Power Amplifiers

(efficiency & conduction angle)

- As the transistor conducts current for a smaller fraction of the period, class C power amplifiers have higher **efficiency** than that of classes A and B.
- However, the **linearity** and **output power** become worse.



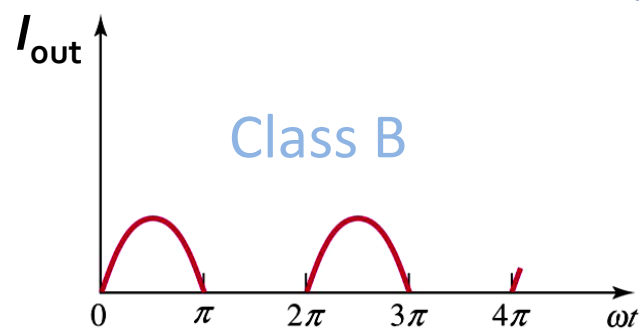
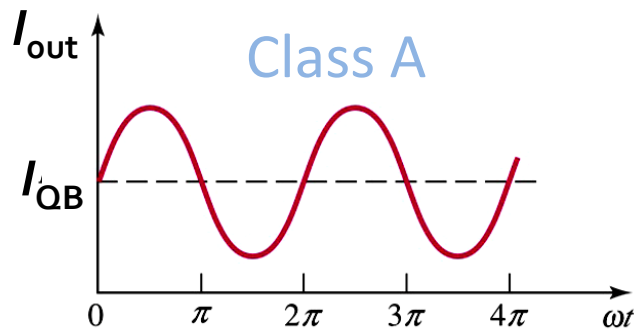
$$\eta = \frac{1}{4} \frac{\theta - \sin \theta}{\sin(\theta/2) - (\theta/2) \cos(\theta/2)}$$



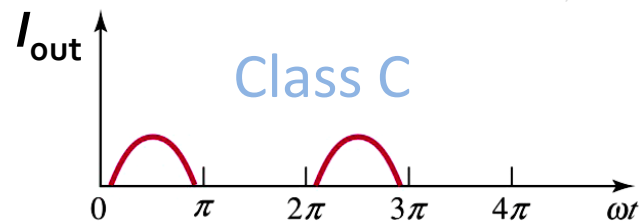
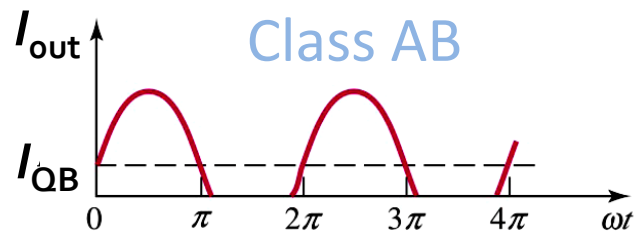
Classes A, B, AB & C

(same type but different conduction angle)

- ❑ Power amplifiers of classes A, B, AB and C are of the same type with the difference in the quiescent biasing for the transistors to conduct in different fraction of the period.



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Classes A, B, AB & C RF PAs

(sinusoidal waveform & power dissipation)

- ❑ **Sinusoidal signals** are assumed at the input and output in classes A, B, AB and C **radio-frequency power amplifiers**.
- ❑ If the current and/or voltage waveforms at the drain (or collector) are non-sinusoidal, the output transistors' power dissipation can be minimised.
 - The non-sinusoidal waveforms can minimise the time during which the output transistors conduct current while sustaining a large voltage.
 - The power amplifier efficiency can then be raised by reducing power consumption of the output transistors.
 - **Power** = $V(t) \times I(t)$, where $V(t)$ & $I(t)$ are the output voltage and current of the transistor and may have different phases.

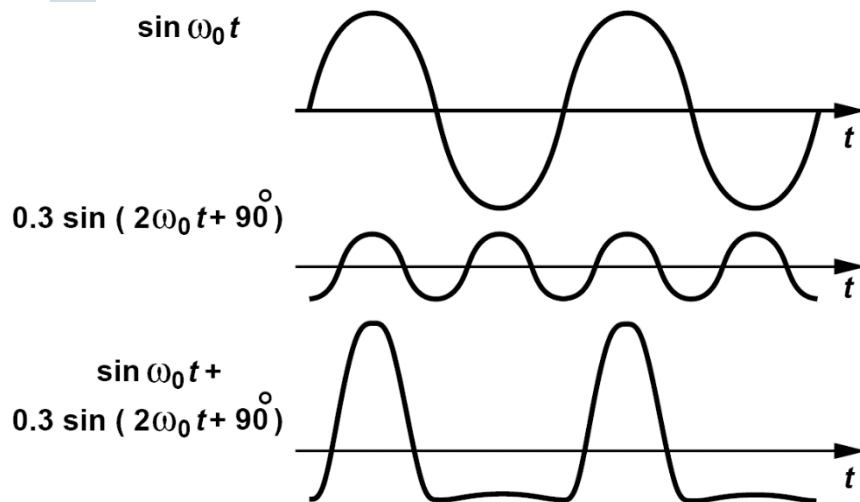


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Non-Sinusoidal Waveforms

(harmonics arising from nonlinearity)

- ❑ With the **large-signal amplification**, the output transistor's current can swing by a large amount. As a result, there can always be some degree of **nonlinearity**.
- ❑ There can be second and/or third **harmonics** (at the drain) arising from large current signals.



➤ The **higher harmonics** can be enhanced to make the waveform non-sinusoidal, reducing the **overlap time** between the voltage across and current flowing in the transistor.



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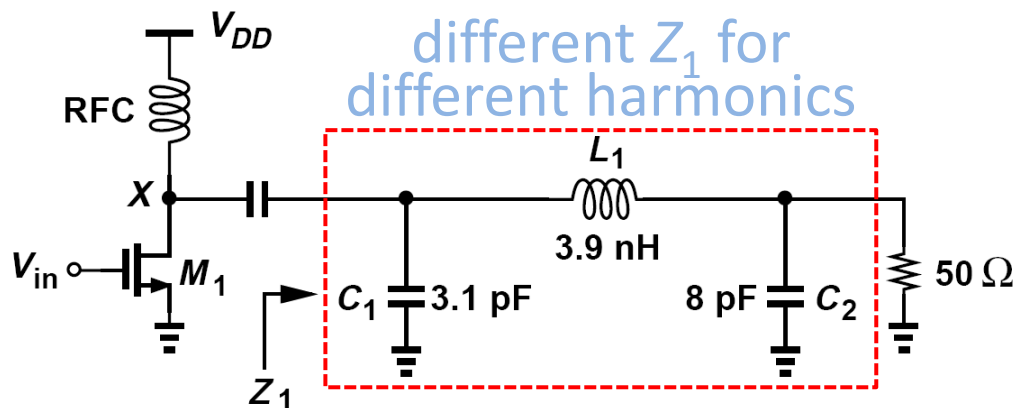
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High-Efficiency Class A RF PA

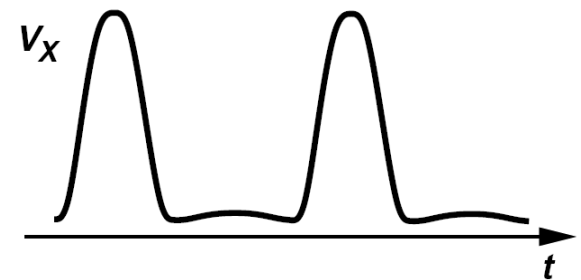
(with harmonic enhancement)

- ❑ The waveform at the drain (or collector in the BJT case) of the output transistor can be shaped by the output **matching network**.
- ❑ The **matching network** can be designed such that its input impedance Z_1 is low at the fundamental and high at the second harmonic.

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V_x at the drain like a square wave

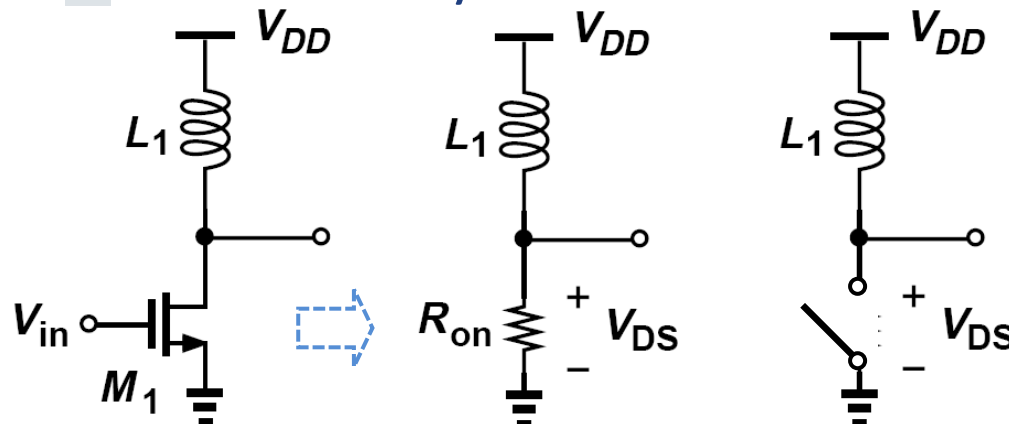


- In the signal delivered to the load, the harmonic content is not raised.

Class E RF Power Amplifier

(transistor as a switch)

- ❑ To further improve the efficiency of RF power amplifiers, the output transistor can be used as a **switch**, instead of a voltage-controlled current source (in classes A, B, AB and C PAs).
 - Ideally, the output transistor turns on and off **abruptly**.
 - To serve as a good **switch**, the on-resistance R_{on} should be very small when the transistor is turned on.



- When it is off, it should be like open-circuit and hence no current flows through it.

Class E RF Power Amplifier

(switching RF PA)

- ❑ Such a circuit configuration using the transistor's **switching action** for power amplification is the class E power amplifier and it is called a “**switching power amplifier**”.
- It is a type of **nonlinear amplifiers** that achieve efficiency approaching 100% while delivering full power to the antenna.
- The perfect efficiency is based on the reasoning that an ideal switch dissipates no power: there is either zero voltage across it or zero current through it.
- The **switching amplifier** version of the **push-pull output stage** is the class D PA.



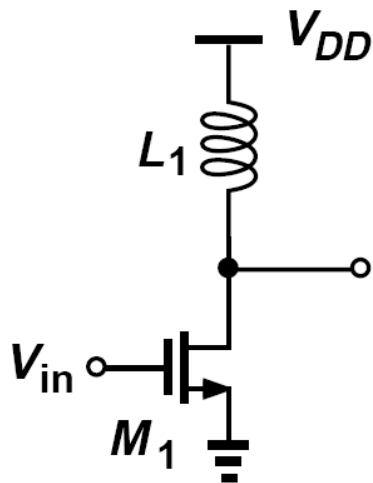
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Class E RF Power Amplifier

(switching RF PA)

- Such a “**switching power amplifier**” topology achieves a high efficiency if:

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1. the output transistor M_1 sustains a small voltage V_{DS} when it carries current;
2. M_1 carries a small current when it sustains a finite voltage;
3. the transition times between the on- and off-states are minimised.

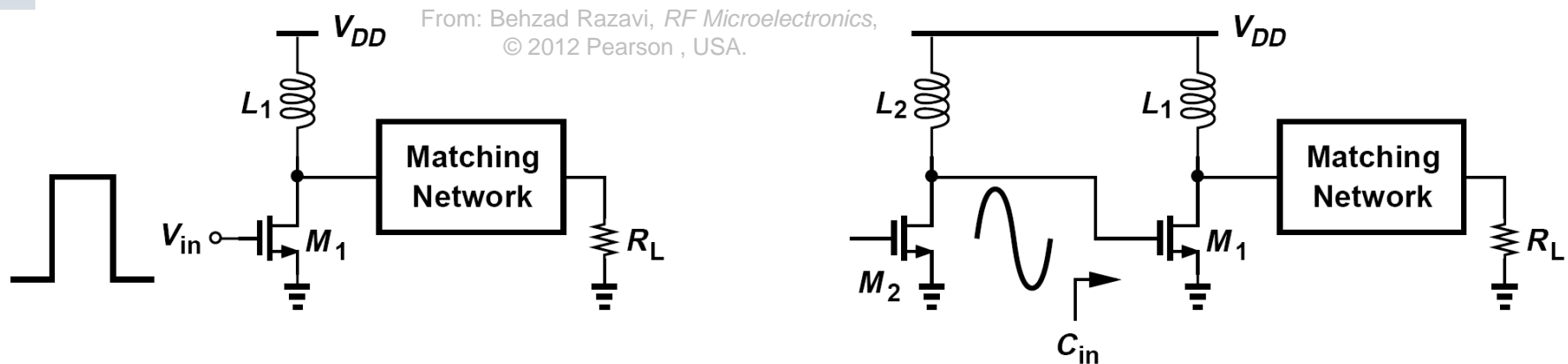
➤ It is like minimising power dissipation in the CMOS inverter.

- The input signal V_{in} for **switching** the transistor should approximate a rectangular waveform.

Class E RF Power Amplifier

(switching RF PA)

- While the gate of the output MOSFET must be **switched** as abruptly as possible to maximise the **efficiency**, its typically large transistor size (W/L) in RF PA makes resonance necessary at the input.
 - This inevitably gives rise a nearly sinusoidal waveform.

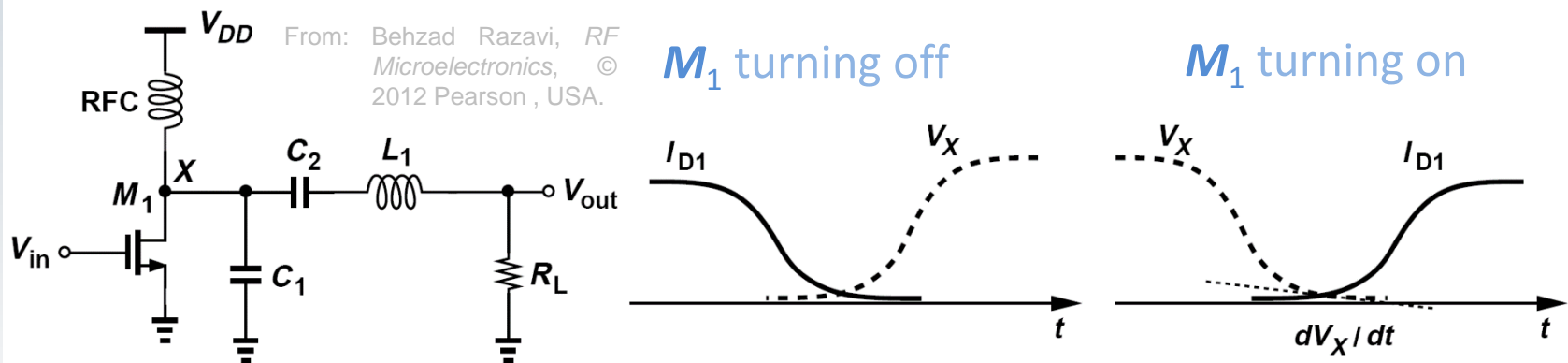


- As a result, the **switching** transistor is driven by a *gradual* waveform.

Class E RF Power Amplifier

(finite input & output transition)

- ❑ The operation of class E power amplifiers in reality never has the perfect **rectangular waveform** to **switch** on and off the transistor **abruptly**.
- ❑ The finite input and output transition times in class E amplifiers can be handled by proper load design.



- The passive output network is designed such that I_{D1} drops to zero when V_X rises and vice versa.

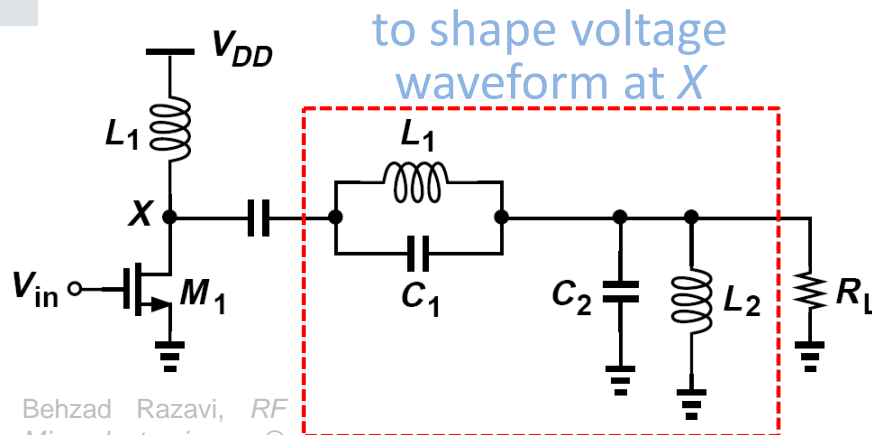


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Class F RF Power Amplifier

(overcome issues of class E PA)

- ❑ The class E power amplifier has quite poor **power handling capability** as it results in a large peak current and voltage.
- ❑ Besides, the large drain current can degrade the **efficiency** as the transistor used as a **switch** has a non-zero on-resistance R_{on} .
- ❑ The **harmonic enhancement** technique for high-efficiency class A power amplifiers can be used in class E amplifiers.

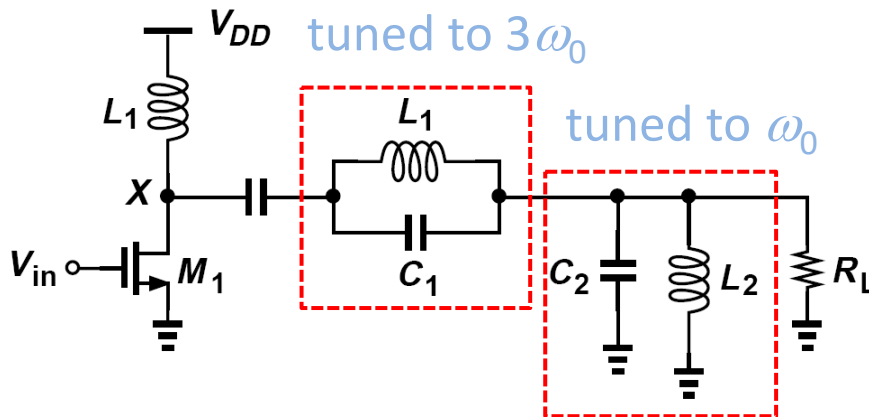


- ❑ The output **matching network** can be used to **shape** the waveform at the drain. This is the class F PA.

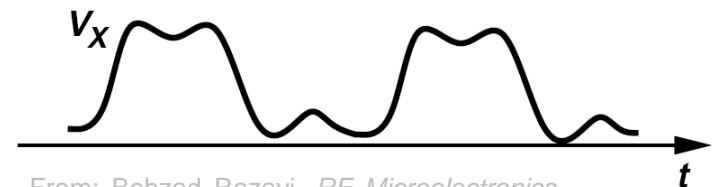
Class F RF Power Amplifier

(harmonic enhancement)

- ❑ In the generic **switching stage**, the passive output network can be designed (with LC tanks) to provide a high termination impedance for the second or third harmonics. The **voltage waveform** across the transistor as a **switch** then exhibits sharper edges than a sinusoid \Rightarrow square wave.



sharper edges with **harmonic enhancement of V_x**



From: Behzad Razavi, *RF Microelectronics*,
© 2012 Pearson, USA.

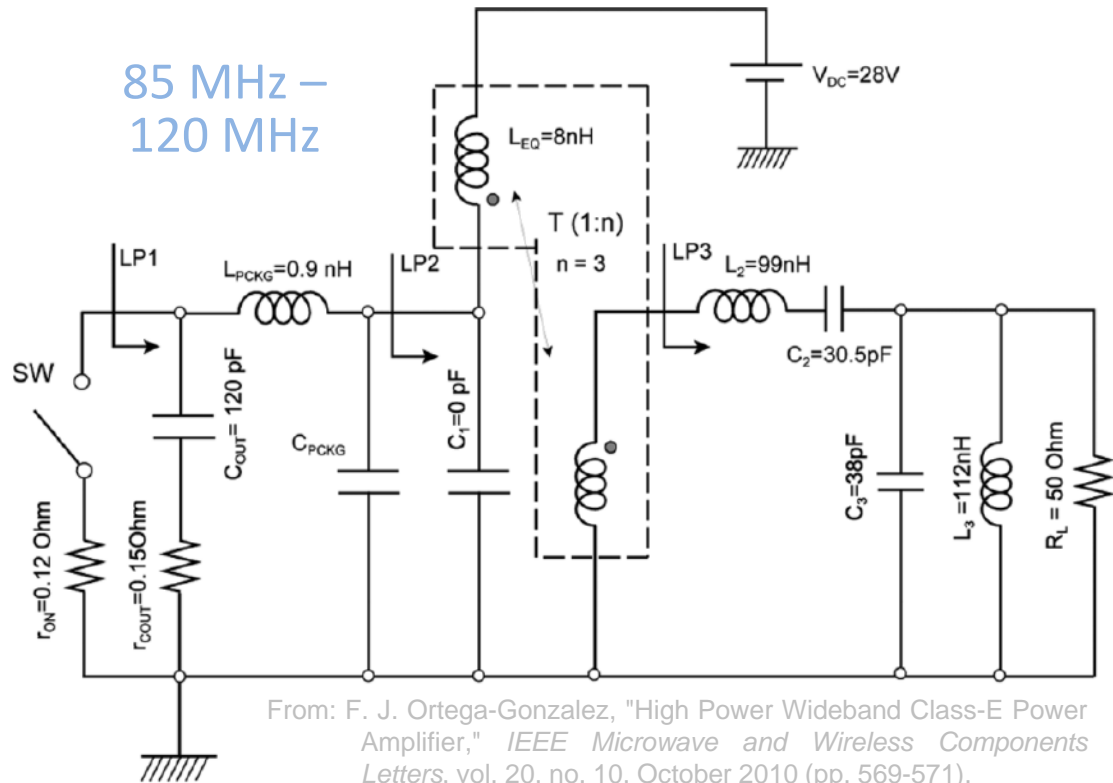
- This reduces the power loss in the **switching** transistor.
- Note the impedance is still seen from X as R_L at the fundamental frequency ω_0 .



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Wideband RF Power Amplifier

(passive output network)



- ❑ It can be seen about the importance of passive **matching network** in RF power amplifier design.
- ❑ In fact, passive **LC circuits** can be used for making an RF power amplifier for **wideband** amplification.

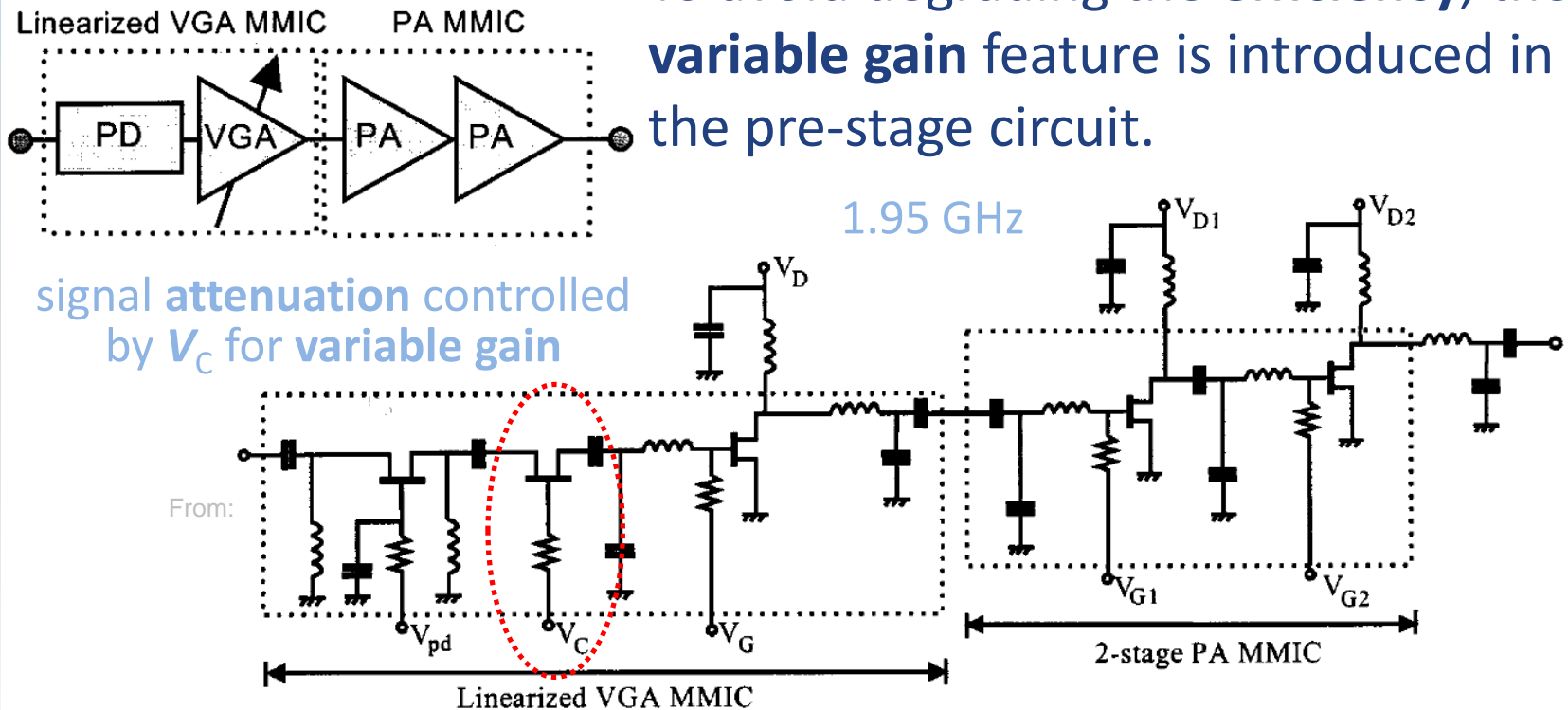
- Do you know where the output transistor is?
- What type is the RF power amplifier?

RF PA with Variable Gain

(pre-stage circuit driving output transistors)

□ RF power amplifiers can also be made with **variable gain**.

➤ To avoid degrading the **efficiency**, the **variable gain** feature is introduced in the pre-stage circuit.



From: Gary Hau, Takeshi B. Nishimura, and Naotaka Iwata, "High Efficiency, Wide Dynamic Range Variable Gain and Power Amplifier MMICs for Wide-Band CDMA Handsets," *IEEE Microwave and Wireless Components Letters*, vol. 11, no. 1, January 2001 (pp. 13-15).