

**Lecture 8**  
*of*  
**EEE307**

# Electronics for Communications

**Department of Electrical & Electronic Engineering**  
**Xi'an Jiaotong-Liverpool University (XJTLU)**

Friday, 8<sup>th</sup> November 2019

- ❑ Positive Feedback for Oscillation
- ❑ Ring Oscillator & LC Oscillator
- ❑ **Voltage-Controlled Oscillator (VCO)**
  - use of varactors
- ❑ Phase Noise



Xi'an Jiaotong-Liverpool University  
**西交利物浦大学**

# Oscillators for Signal Generation

(applications)

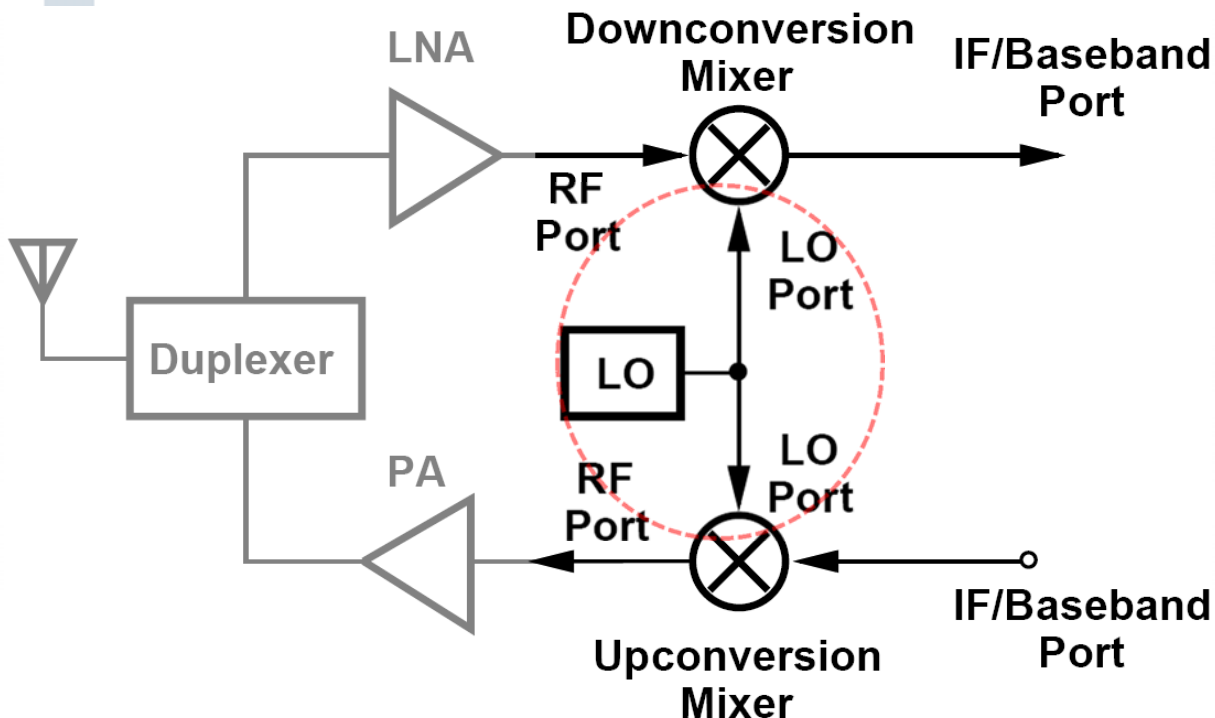
- ❑ **Oscillators** are used extensively for **signal generation** in various electronic systems. Their applications range from clock generation in microprocessors to synthesis of carrier signals in wireless communication systems.
  - The oscillator topologies and performance consideration can vary considerably depending on the applications.
  - Common types of oscillators include **ring oscillators** and **LC oscillators** in generating **periodic** electrical signals.
  - Usually, oscillators are embedded in phase-locked systems.

# Oscillators for Signal Generation

(radio communication system)

- ❑ In a wireless communication system, a **periodic local oscillator (LO)** signal is needed to drive one input of the mixers in the transmit and receive paths.

From: Behzad Razavi, *RF Microelectronics*, © 2012 Pearson, USA.

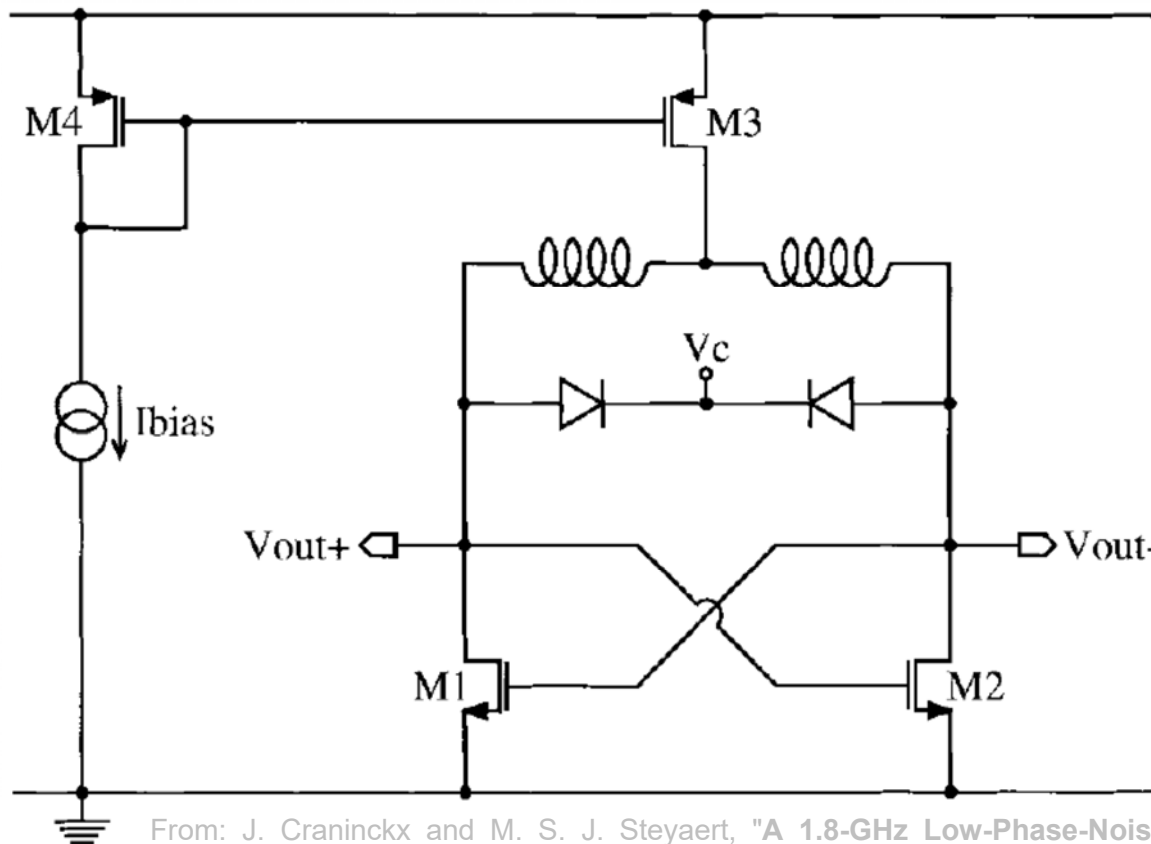


➤ **Oscillators**, in particular, **tuneable oscillators** are indispensable in radio communication and optical communication systems.

# CMOS VCO Example

(using spiral inductors & varactors)

- ❑ A 1.8-GHz low-phase-noise CMOS VCO using optimised hollow spiral inductors



- How can we understand such a **voltage-controlled oscillator (VCO)** circuit from the basic concepts?
- Why is it designed in such a way? What topology is it?

From: J. Craninckx and M. S. J. Steyaert, "A 1.8-GHz Low-Phase-Noise CMOS VCO Using Optimized Hollow Spiral Inductors," *IEEE Journal of Solid-state Circuits*, vol. 32, no. 5, May 1997 (pp. 736-744).

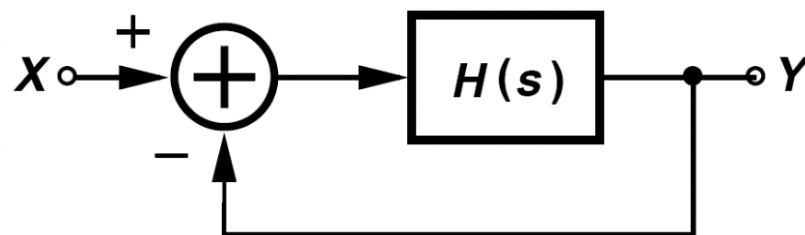


Xi'an Jiaotong-Liverpool University  
西交利物浦大学

# Oscillators

(feedback system)

- ❑ An **oscillator** can be described by a positive (or **regenerative**) feedback system.
  - In **regenerative feedback**, a portion of the output signal is fed back to the input and it is in phase with the input signal.
- ❑ Consider a negative feedback system,



$$\frac{V_{out}(s)}{V_{in}(s)} = \frac{V_Y(s)}{V_X(s)} = \frac{H(s)}{1 + H(s)}$$

From: Behzad Razavi, *RF Microelectronics*, © 2012 Pearson, USA.

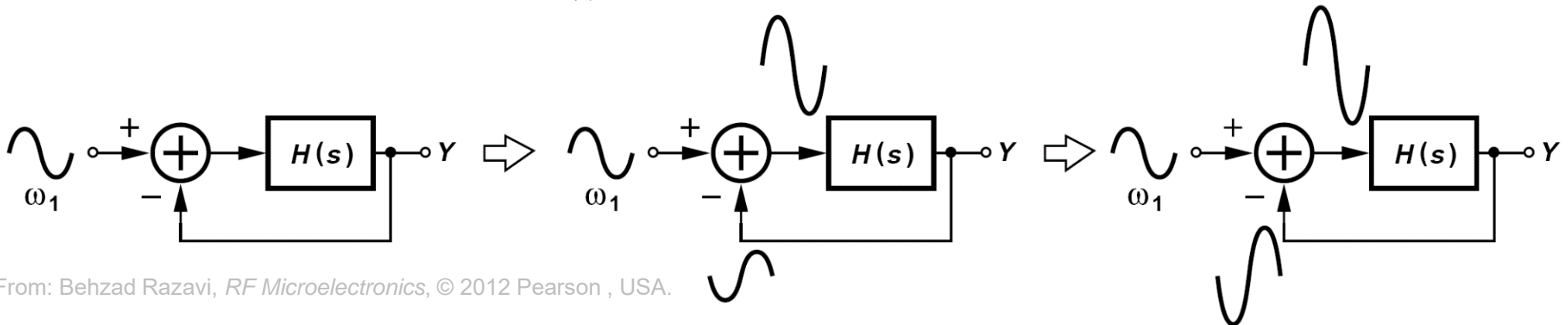
# Oscillation in Feedback System

(at a particular frequency)

- ❑ In a negative feedback system, if for  $s = j\omega_1$ , the open-loop transfer function  $H(j\omega_1) = -1$ , then the closed-loop gain approaches infinity at  $\omega_1$ .

- The system can amplify its own noise component at  $\omega_1$  indefinitely.

$$\frac{V_{out}(j\omega_1)}{V_{in}(j\omega_1)} = \frac{H(j\omega_1)}{1 + H(j\omega_1)} \rightarrow \frac{-1}{1 + (-1)} \rightarrow \infty$$



From: Behzad Razavi, *RF Microelectronics*, © 2012 Pearson, USA.

- Will the output get to infinity?  
Why not?

# Oscillation in Feedback System

(Barkhausen criteria)

- ❑ Called “**Barkhausen criteria**”, two conditions are necessary (but not sufficient) for a negative feedback system to oscillate:

$$|H(j\omega_1)| \geq 1 \text{ and } \angle H(j\omega_1) = 180^\circ$$

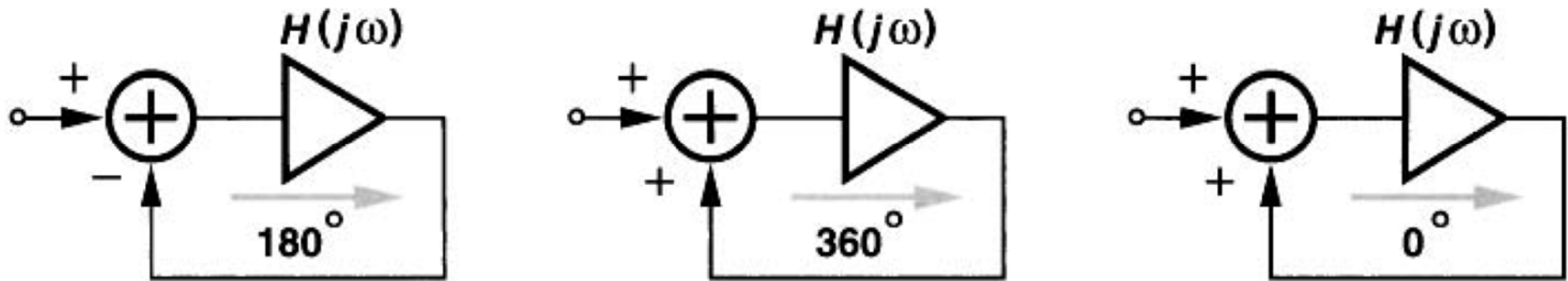
- These two criteria state that the phase shift at  $\omega_1$  around the feedback loop must be  $0^\circ$  or  $360^\circ$  (i.e. positive feedback) and the loop gain must be no less than unity.
- ❑ To ensure oscillation due to temperature or process variations, a loop gain of at least twice or three times the required value is needed.



# Oscillation in Feedback System

(phase shift condition)

- ❑ The second “**Barkhausen criterion**”  $\angle H(j\omega_1) = 180^\circ$  can be stated in two other equivalent ways:



From: Behzad Razavi, *Design of Integrated Circuits for Optical Communications*, 2e © 2012 Wiley, USA.

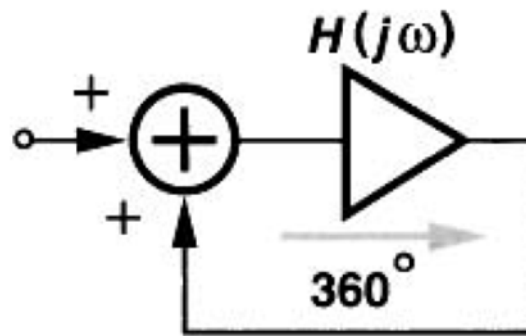
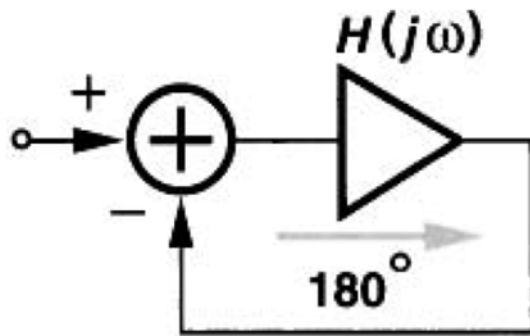
- Note that in a negative feedback system, the **phase shift** is already  $180^\circ$  in the signal travelling around the loop (as represented by the subtraction sign). This is called the DC or low-frequency phase shift of  $180^\circ$ .
- $\angle H(j\omega_1) = 180^\circ$  refers to the **frequency-dependent phase shift**.



# Oscillation in Feedback System

(360° phase shift)

- ❑ The second “**Barkhausen criterion**”  $\angle H(j\omega_1) = 180^\circ$  can be stated in two other equivalent ways:



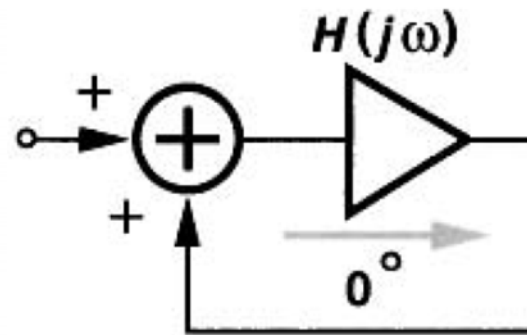
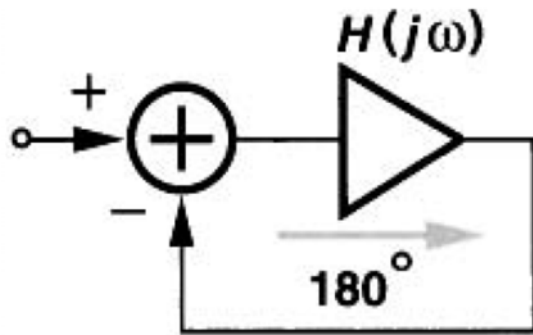
From: Behzad Razavi,  
*Design of Integrated  
Circuits for Optical  
Communications*, 2e  
© 2012 Wiley, USA.

- The total phase shift is  $360^\circ$  at particular frequencies in the whole feedback system. This can be achieved by having enough stages with proper polarities to provide the total phase shift of  $360^\circ$ .  
⇒ ring oscillators

# Oscillation in Feedback System

(0° phase shift)

- ❑ The second “**Barkhausen criterion**”  $\angle H(j\omega_1) = 180^\circ$  can be stated in two other equivalent ways:



From: Behzad Razavi,  
*Design of Integrated  
Circuits for Optical  
Communications*, 2e  
© 2012 Wiley, USA.

- The whole feedback system produces no phase shift (i.e.  $0^\circ$ ) at a particular frequency  $\omega$ . This implies very few gain stages  $\Rightarrow$  cross-coupled stages.

# Positive Feedback for Oscillation

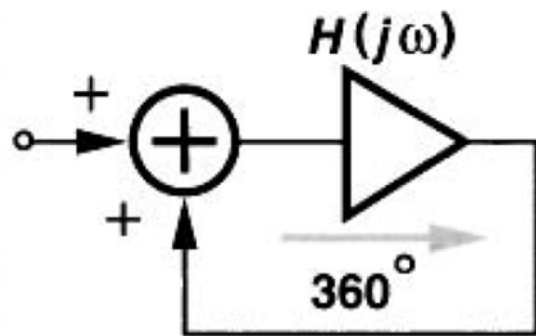
(oscillators built from op amp)

- ❑ The main idea of constructing an oscillatory electronic circuit is **positive feedback** using certain gain stages.
- ❑ In principle, **operational amplifiers (op amp)** can be used to build oscillators. They are not commonly used in RF circuits.
  - Op-amp-based oscillators can be used to generate signals with frequencies of up to approximately one-half of the gain-bandwidth product ( $\omega_{GX}$ ) of the op amp.
  - Oscillators designed with transistors and inductors and capacitors can generate signals with frequencies limited only by the cut-off frequency of the individual transistors.

# Oscillation in Feedback System

(360° phase shift)

- ❑ To achieve oscillation, we may cascade multiple gain stages so that the phase shift of individual gain stages would add up to 360°.



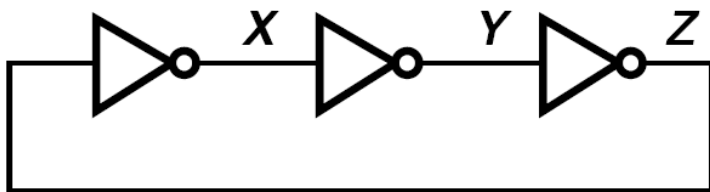
- Note that in op amp design, cascading “too many” gain stages for a very large signal gain is undesirable because this would cause instability.

- ❑ This is the **ring oscillator** design approach.
- ❑ A **ring oscillator** consists of a number of **gain stages in a loop**.

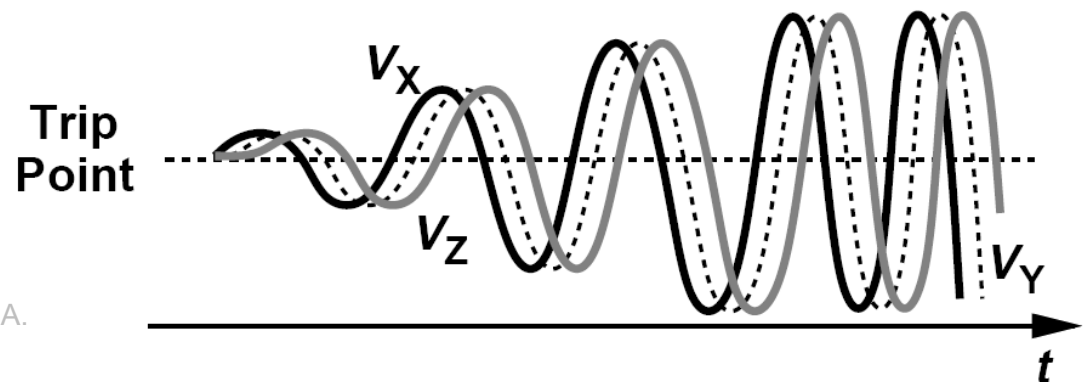
# Ring Oscillators

(cascading odd number of inverters)

- ❑ A simple implementation of a **ring oscillator** is cascading an odd number of the inverter logic gates in a loop.
  - Why odd number (typically no less than three)?
  - Such a ring oscillator is helpful in determining the maximum speed of the logic gates in an IC technology.



From: Behzad Razavi, *RF Microelectronics*, © 2012 Pearson, USA.

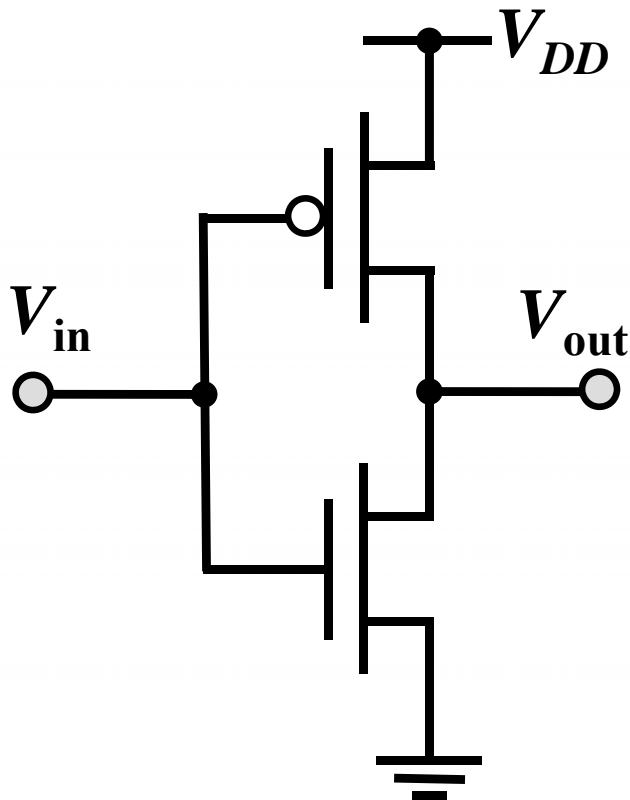
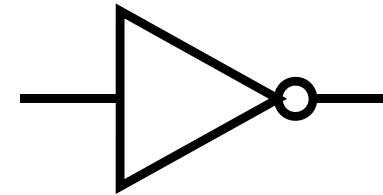


- How to estimate the oscillation frequency from the inverter delay?

# Ring Oscillators

(CMOS inverter)

- ❑ In CMOS technology, an efficient **inverter** logic gate can be constructed with one *n*-channel MOSFET and one *p*-channel MOSFET.



- ❑ Do you still remember what you learned in EEE112 & EEE201 in designing W/L and estimating the **delay time** of a CMOS inverter?
  - If the delay of an inverter is 0.2 ns, what is the oscillation frequency of a 5-inverter ring oscillator?



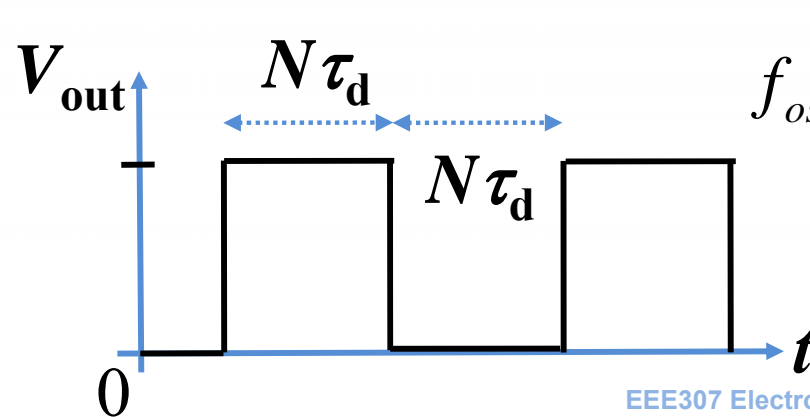
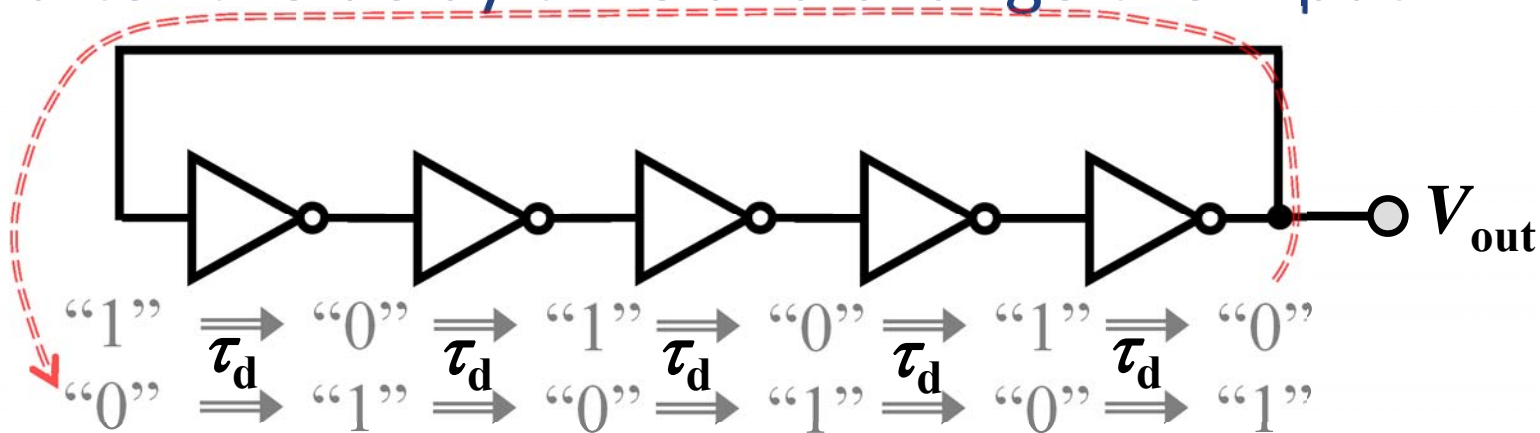
Xi'an Jiaotong-Liverpool University  
西交利物浦大学



# Ring Oscillators

(inverter delay & oscillation frequency)

- With the odd number of the inverter logic gates in a loop, the output would be fed back to the input after the delay time and change the input:



$$f_{osc} = \frac{1}{T} = \frac{1}{2N\tau_d}$$

$\tau_d$ : inverter delay  
 $N$ : odd number of inverters

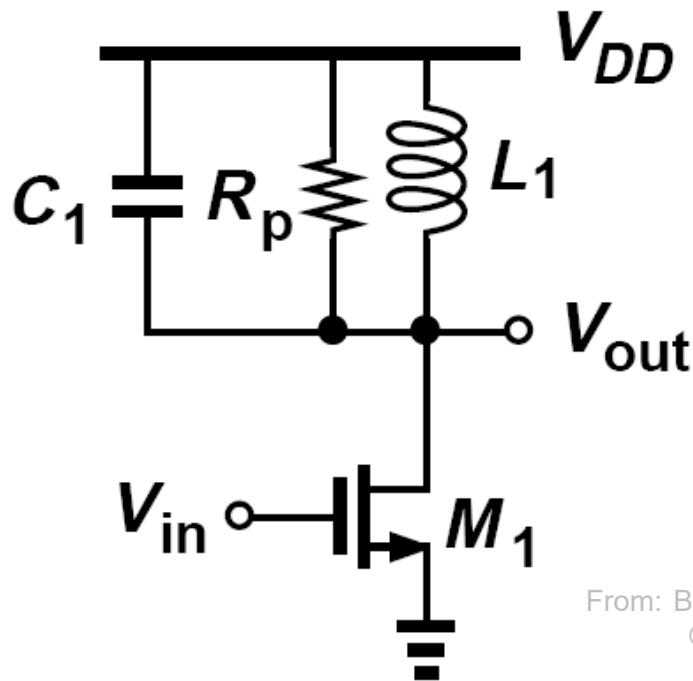


# Oscillators from Tuned Amplifiers

(using inductors & capacitors)

- ❑ In RF circuits, it is more common to construct an **oscillator** circuit from a **tuned amplifier** using inductors and capacitors.

➤ In a common-source amplifier,  $\frac{V_{out}}{V_{in}} = -g_m (X_C // R_p // X_L // r_{o1})$



➤ At low frequencies,  $\frac{V_{out}(s)}{V_{in}(s)} \approx -g_m s L_1$

➤ At  $\omega_0$ ,  $\frac{V_{out}(j\omega_0)}{V_{in}(j\omega_0)} \approx -g_m R_p$

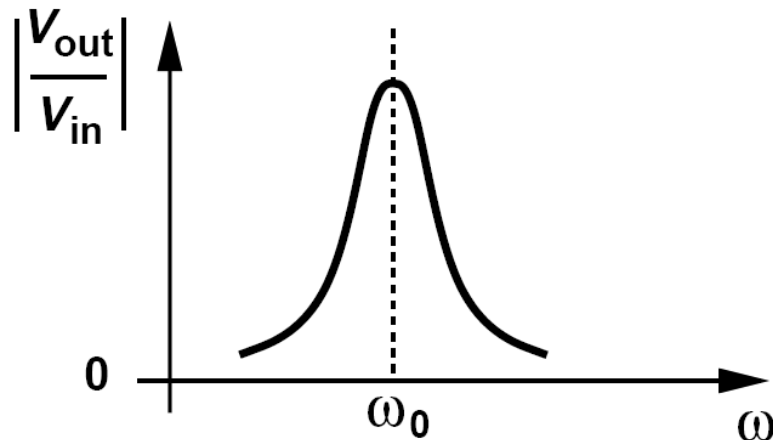
➤ At high frequencies,  $\frac{V_{out}(s)}{V_{in}(s)} \approx -\frac{g_m}{s C_1}$

From: Behzad Razavi, *RF Microelectronics*,  
© 2012 Pearson, USA.

# LC-Tuned Amplifier

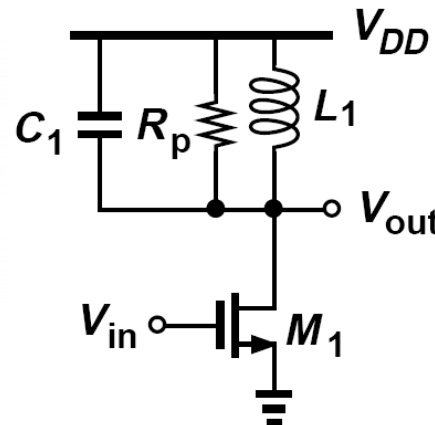
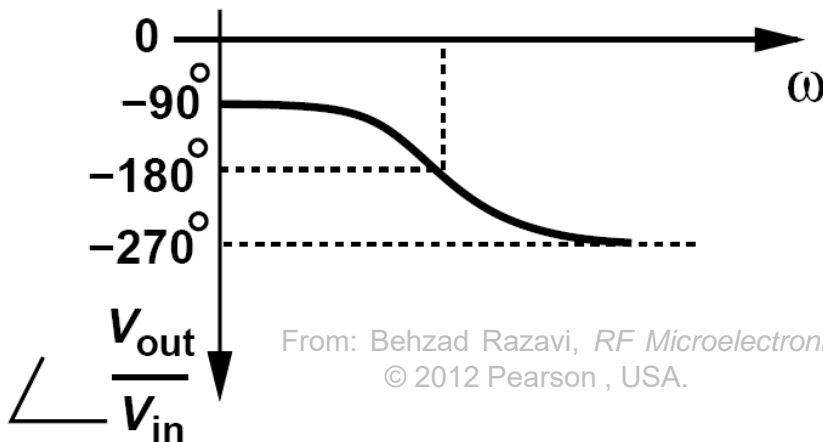
(phase shift at different frequencies)

- ❑ The LC-tuned amplifier can achieve the required phase shift for oscillation at a particular frequency.



- At low frequencies, the phase shift is  $\angle(V_{out}/V_{in}) \approx -90^\circ$ . (Why?)
- At very high frequencies, the phase shift is  $\angle(V_{out}/V_{in}) \approx +90^\circ$ . (Why?)
- At the resonance frequency  $\omega_0$ ,

the phase shift from the input to the output is  $180^\circ$ .



From: Behzad Razavi, *RF Microelectronics*,  
© 2012 Pearson, USA.

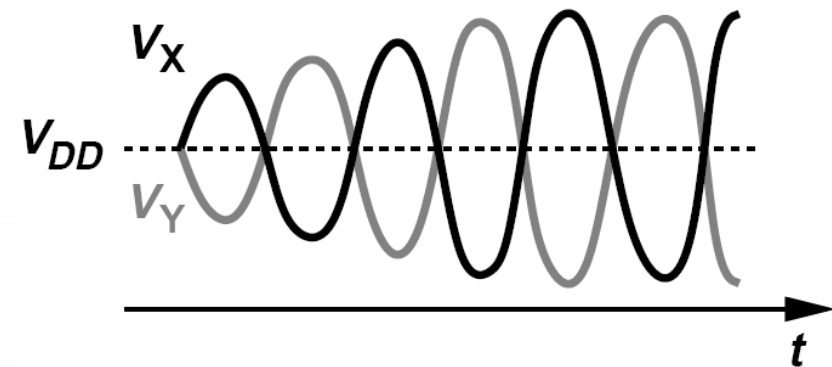
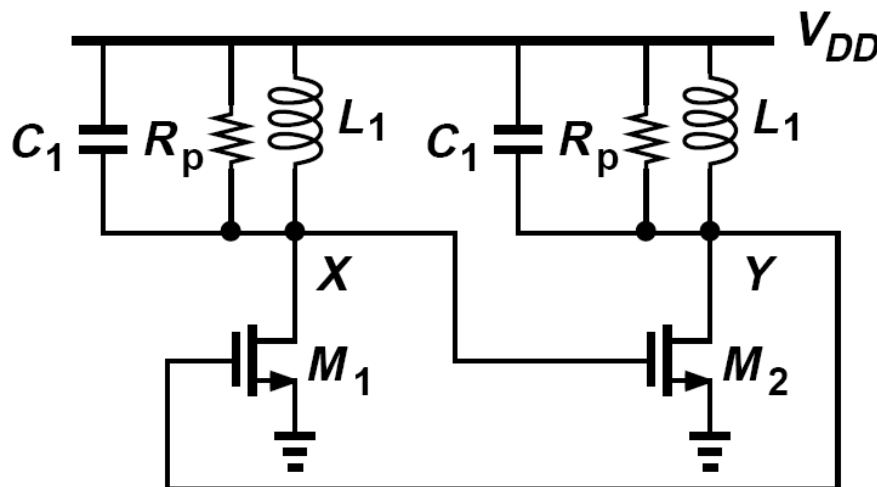
# LC-Tuned Amplifier

(cascading two CS amplifiers)

- ❑ With the  $180^\circ$  phase shift at the resonance frequency  $\omega_0$  of the LC-tuned amplifier, **cascading** two **common-source amplifier** in a loop will form an **oscillator** with the positive (regenerative) feedback.

From: Behzad Razavi, *RF Microelectronics*, © 2012 Pearson, USA.

- The circuit oscillates if the loop gain  $(g_m R_p)^2 \geq 1$ .

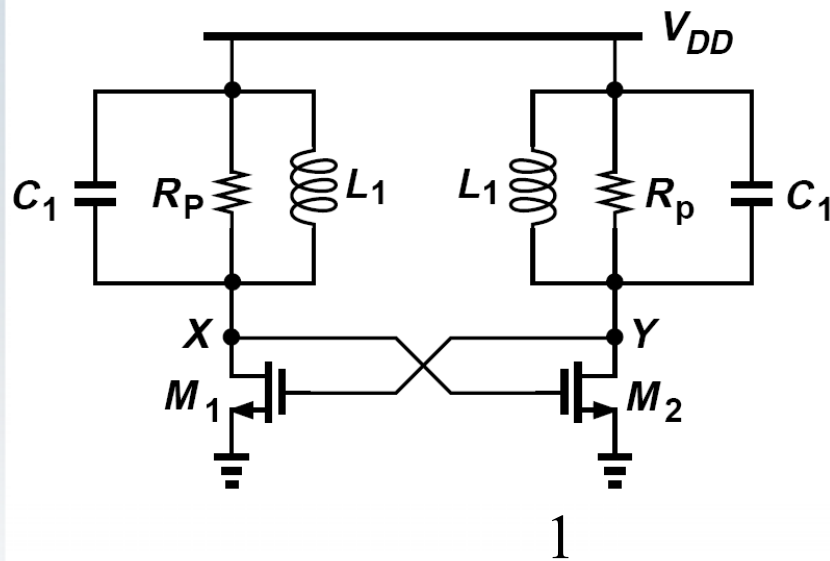


# Cross-Coupled LC Oscillators

(two amplifiers with positive feedback)

- ❑ The **oscillator** circuit with two common-source amplifiers **cascaded** in a **loop** can be represented in a different form.
- ❑ This is the dominant **cross-coupled LC oscillator** design for RF applications due to its robust operation.

From: Behzad Razavi, *RF Microelectronics*, © 2012 Pearson, USA.



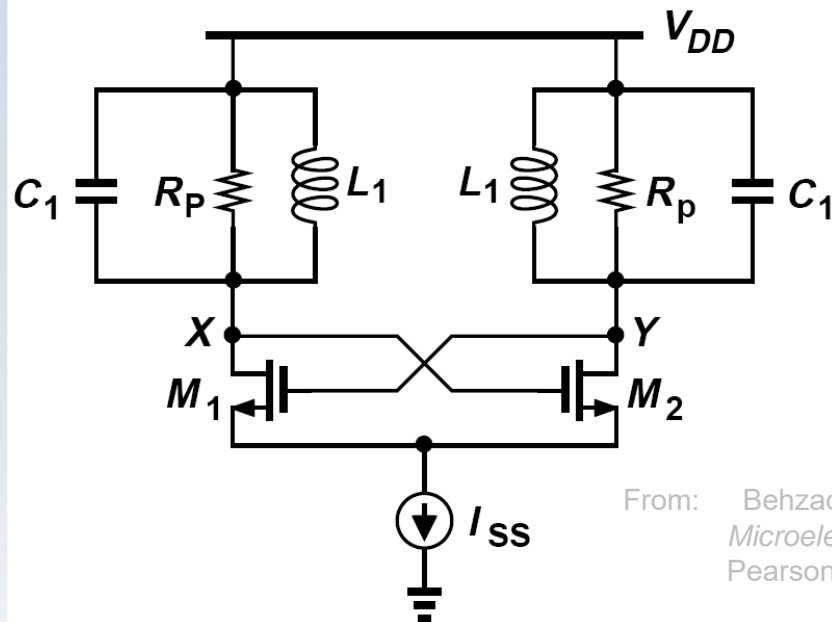
- It is like a differential amplifier with the outputs fed into the inputs in phase.
- Note that resonance frequency  $\omega_{osc}$  can include the parasitic capacitances of the transistors.

$$\omega_{osc} = \frac{1}{\sqrt{L_1(C_{GS2} + C_{DB1} + 4C_{GD} + C_1)}}$$

# Cross-Coupled LC Oscillators

(two amplifiers with positive feedback)

- ❑ The **cross-coupled LC oscillator** design can have the differential pair of transistors biased with a certain DC current  $I_{SS}$ .



- Then the DC offset voltage  $V_{XY}$  at the differential output can be set at such a value so that the output **voltage swing** can be maximised.

$$V_{XY} \approx \frac{4}{\pi} I_{SS} R_p$$

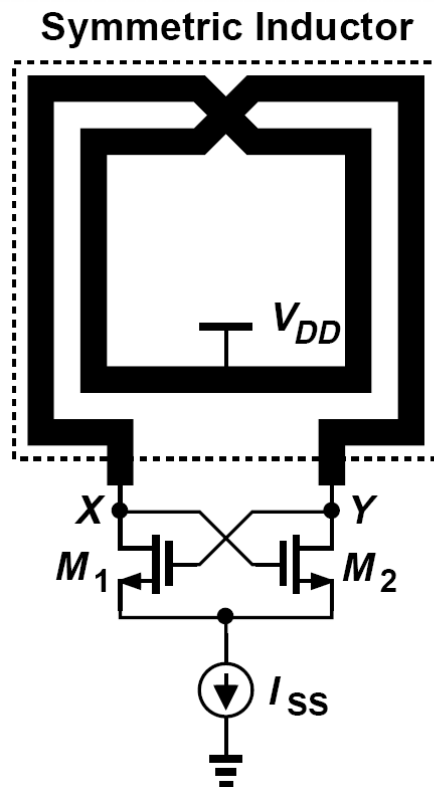
$$\omega_{osc} = \frac{1}{\sqrt{L_1 (C_{GS2} + C_{DB1} + 4C_{GD} + C_1)}}$$

From: Behzad Razavi, *RF Microelectronics*, © 2012 Pearson, USA.

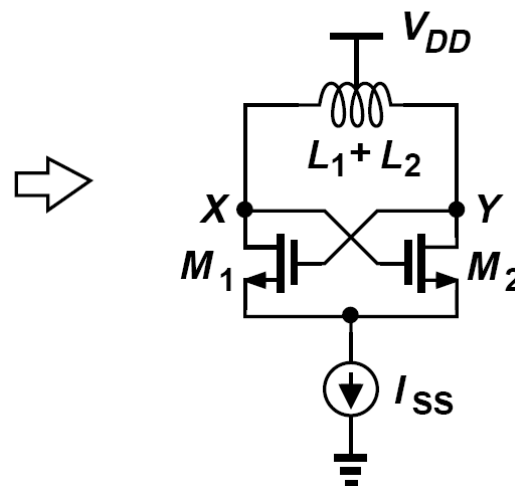
# Cross-Coupled LC Oscillators

(symmetric spiral inductors)

- ❑ The **cross-coupled LC oscillator** gives a differential output. A symmetric planar spiral inductor can be used in RFIC design for improved performance.



From: Behzad Razavi, *RF Microelectronics*, © 2012 Pearson, USA.

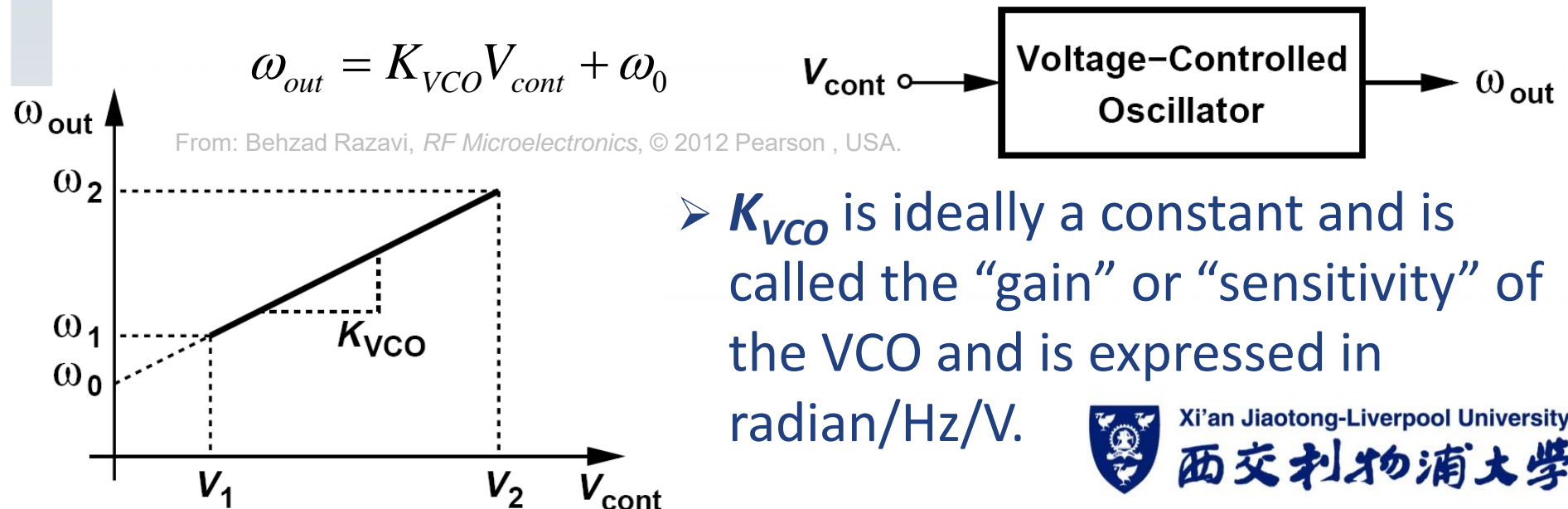


- The point of symmetry of the planar spiral inductors, namely the “centre tap” is connected to  $V_{DD}$ .

# Voltage-Controlled Oscillator

(varying frequency by voltage)

- ❑ In most applications, **oscillators** need to be tuned over a certain frequency range.
- ❑ Typically, the frequency is varied electronically by a controlling voltage. Such an oscillator is called **voltage-controlled oscillator (VCO)**.



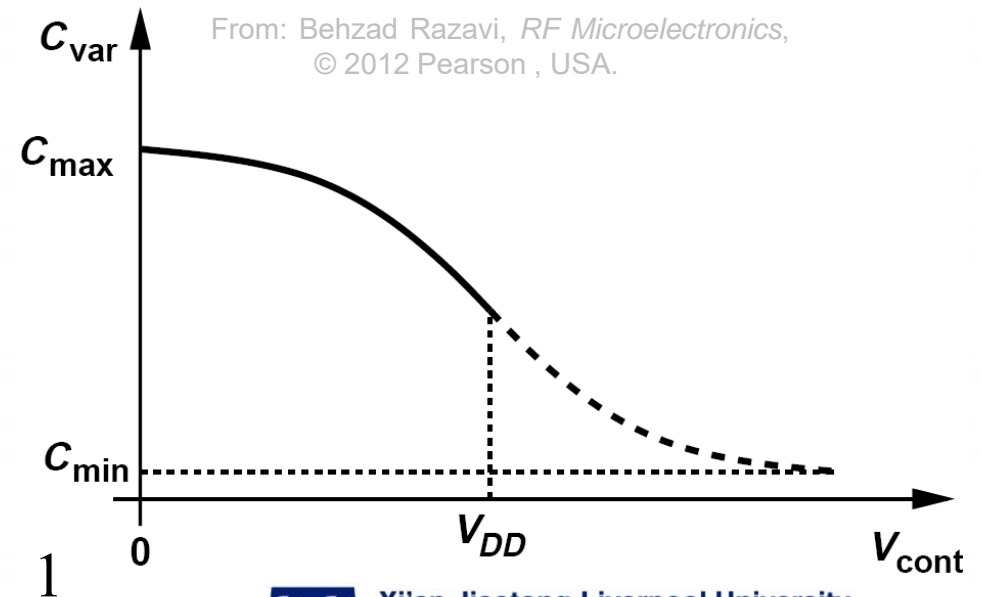
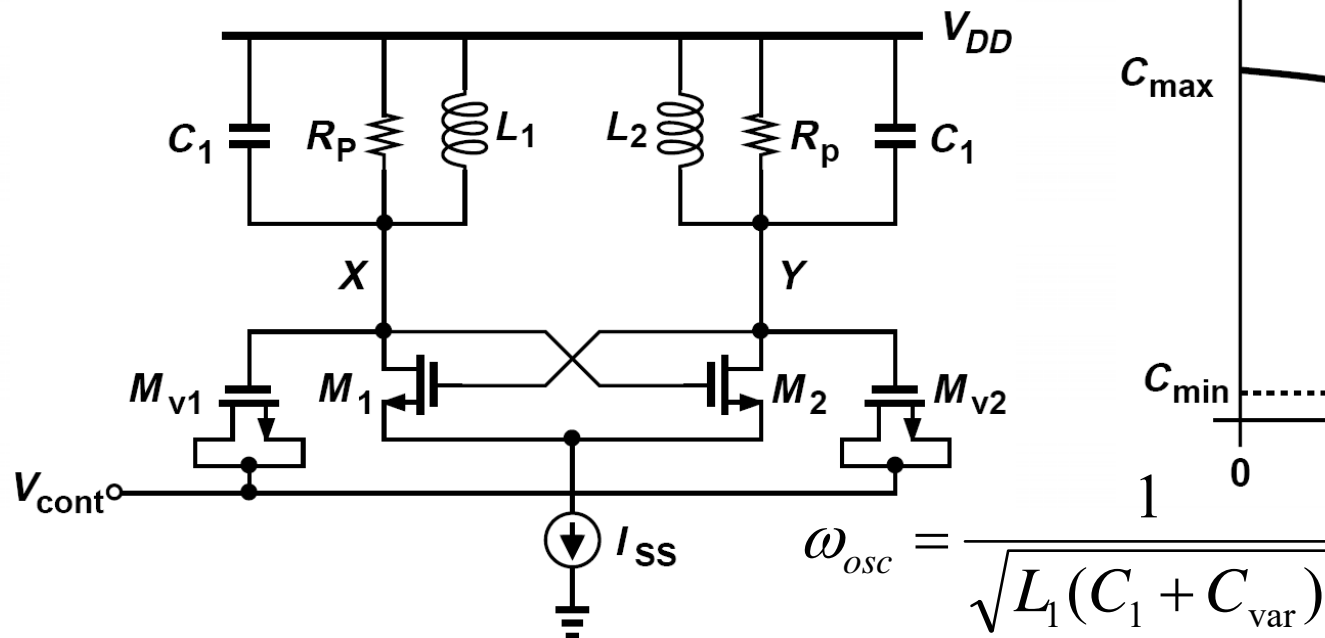
➤  $K_{VCO}$  is ideally a constant and is called the “gain” or “sensitivity” of the VCO and is expressed in radian/Hz/V.



# Voltage-Controlled Oscillator

(use of varactors)

- ❑ The **cross-coupled LC oscillator** can be made into a VCO easily by adding a device called **varactor**.
  - A **varactor** changes its capacitance with an applied voltage. A **MOS capacitor** can serve as a **varactor** by tying the source and drain.



Xi'an Jiaotong-Liverpool University  
西交利物浦大学

# Voltage-Controlled Oscillator

(frequency tuning range)

- With the varactor's capacitance included in the resonance frequency, the oscillator's frequency

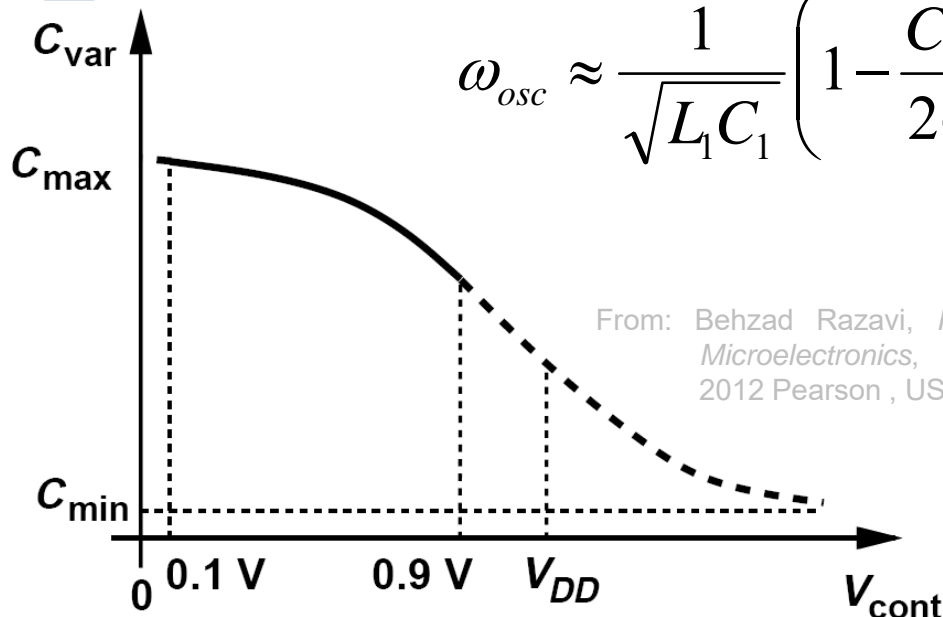
$\omega_{osc}$  becomes:

$$\omega_{osc} = \frac{1}{\sqrt{L_1 C_1 (1 + C_{var} / C_1)}} = \frac{1}{\sqrt{L_1 C_1}} \left( 1 + \frac{C_{var}}{C_1} \right)^{-\frac{1}{2}}$$

$$\omega_{osc} \approx \frac{1}{\sqrt{L_1 C_1}} \left( 1 - \frac{C_{var}}{2C_1} \right)$$

- The frequency tuning range of the VCO is

$$\Delta\omega_{osc} \approx \frac{1}{\sqrt{L_1 C_1}} \left( \frac{C_{var2} - C_{var1}}{2C_1} \right)$$



From: Behzad Razavi, *RF Microelectronics*, © 2012 Pearson, USA.

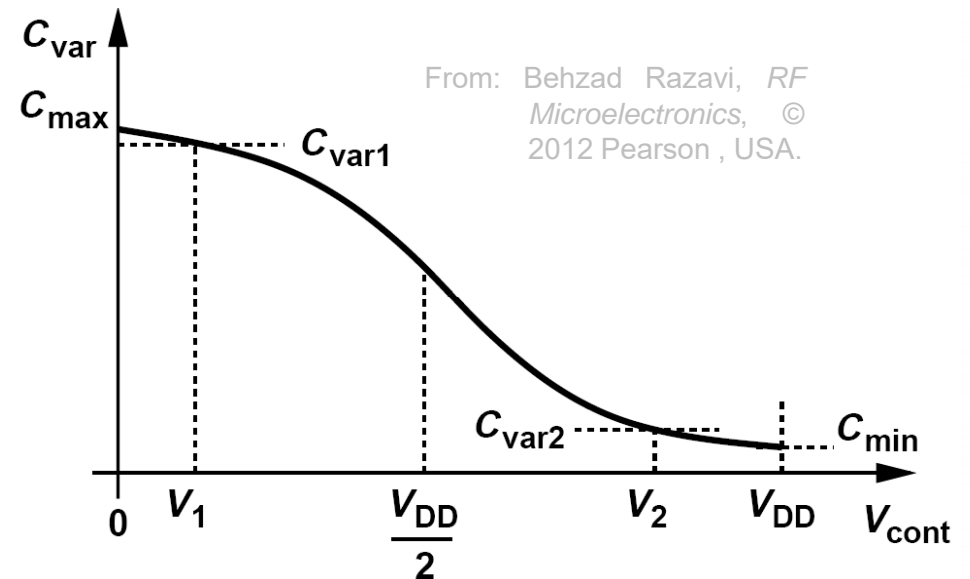
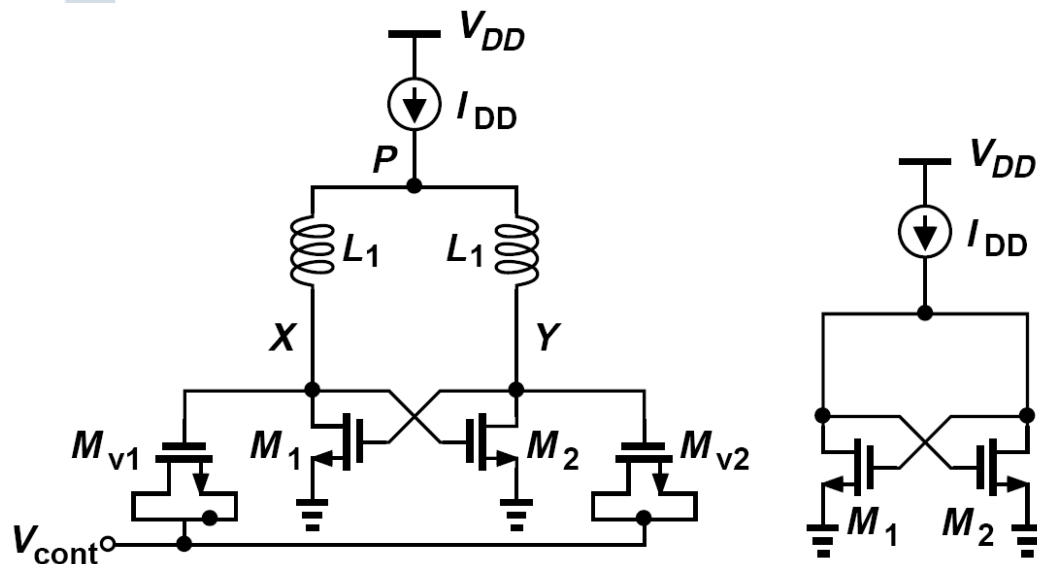


Xi'an Jiaotong-Liverpool University  
西交利物浦大学

# Voltage-Controlled Oscillator

(frequency tuning range improvement)

- ❑ In using the MOS capacitor as a varactor in the **cross-coupled LC oscillator**, the frequency tuning range can be increased by using a top current source (compared with the tail-biased circuit).

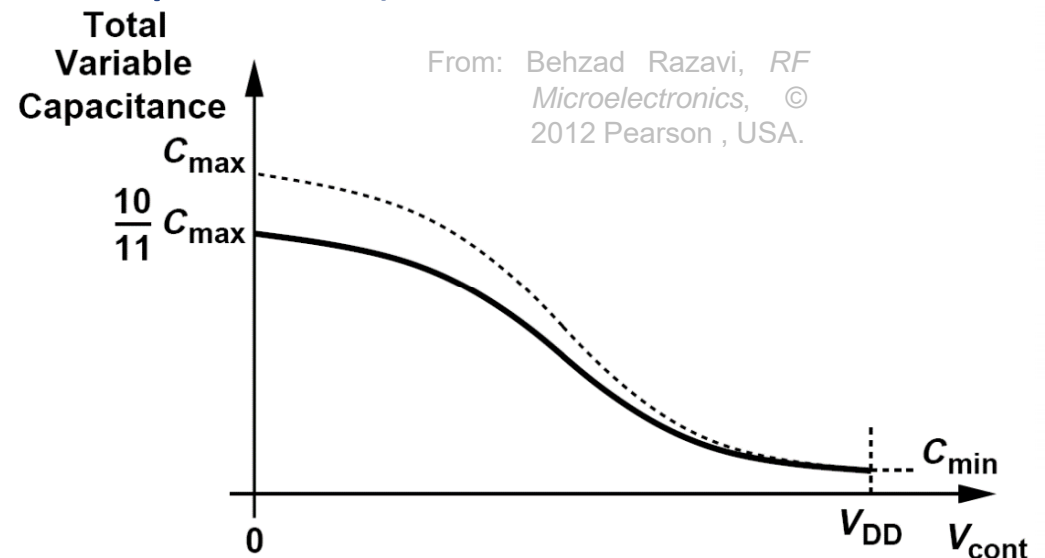
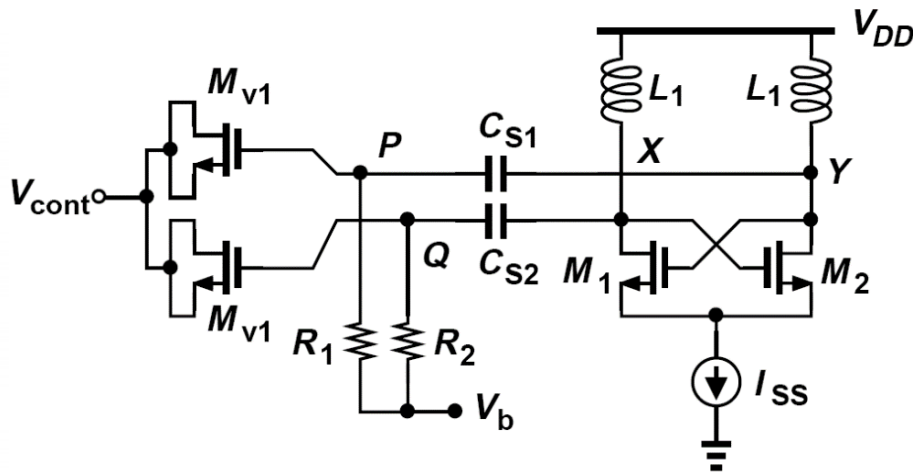


- This however suffers from worse phase noise.

# Voltage-Controlled Oscillator

(varactor AC coupling)

- ❑ There can be varactor modulation in the **cross-coupled LC oscillator** due to the noise of the bias current source.
- ❑ This can be avoided by using AC coupling between the varactors and the core (i.e. connecting the varactors to the transistor core through linear capacitors).



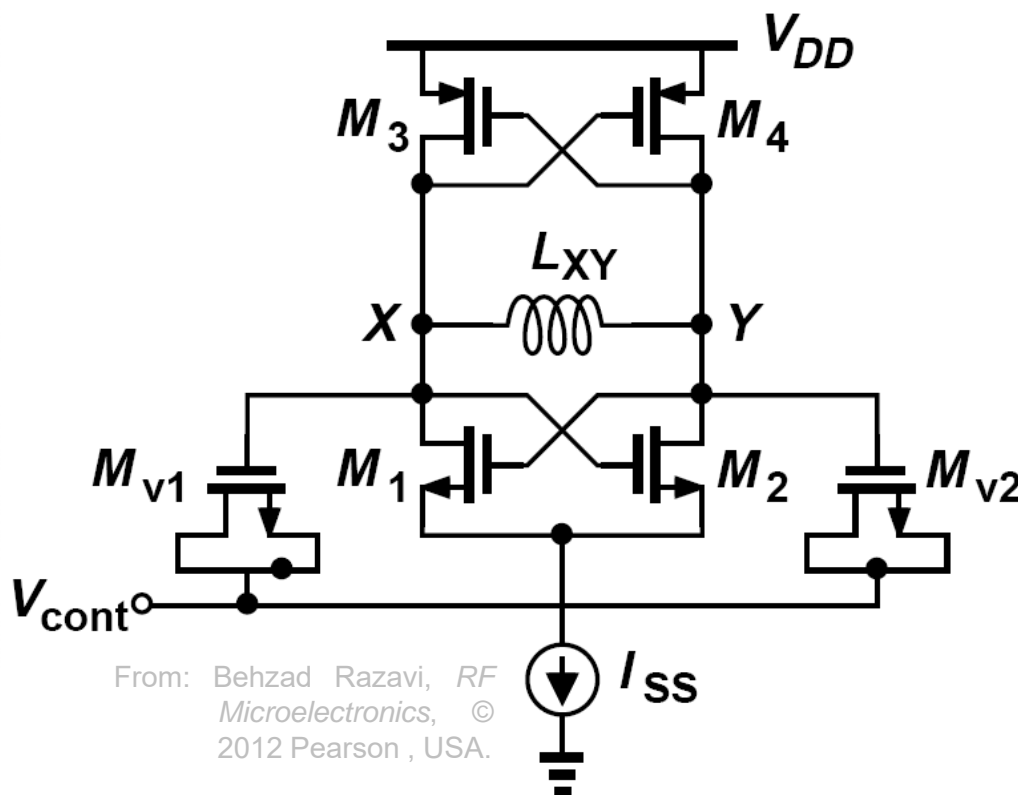
➤ Disadvantage: less tuning range

# Voltage-Controlled Oscillator

(cross-coupled PMOS transistor)

- ❑ Another improvement of the **cross-coupled LC oscillator** is the use of cross-coupled PMOS transistors to replace the resistors.

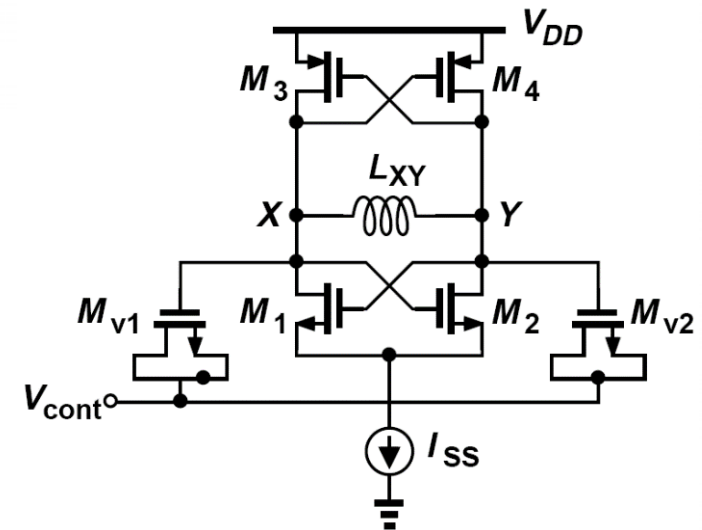
- With proper choices of the MOSFET size (i.e.  $W/L$ ) and the biasing current  $I_{SS}$ , the common mode voltage at nodes  $X$  and  $Y$  can be set at  $V_{DD}/2$  and hence increasing the VCO output voltage swing, specifically doubled.



From: Behzad Razavi, *RF Microelectronics*, © 2012 Pearson, USA.

(operation)

- 1<sup>st</sup> half cycle

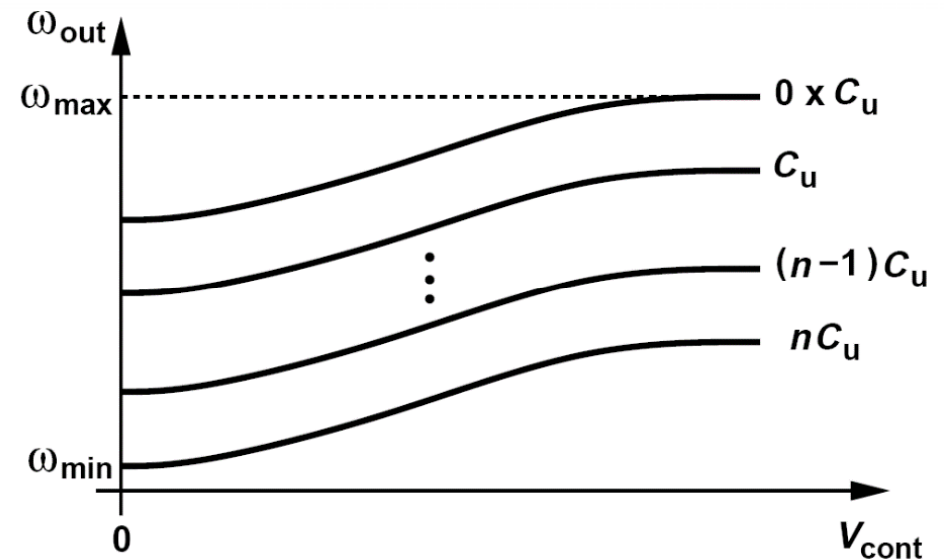
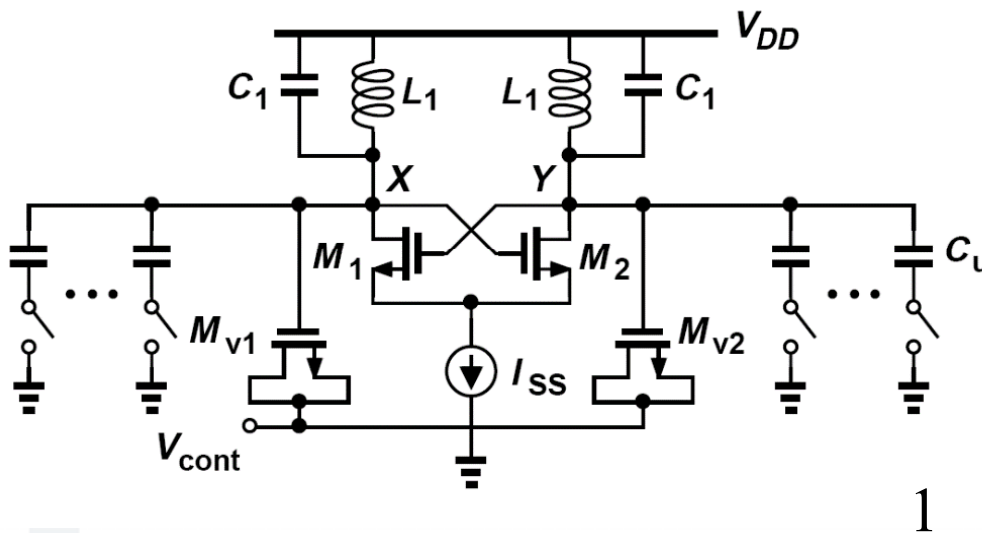


Xi'an Jiaotong-Liverpool University  
西交利物浦大學

# Voltage-Controlled Oscillator

(discrete tuning)

- ❑ In the **cross-coupled LC oscillator** design, discrete tuning range is possible by adding a bank of small capacitors (e.g. parallel-plate capacitors) in parallel to the LC tanks.
  - The capacitors can be switched in or out to adjust the resonance frequency  $\omega_{osc}$ .



$$\omega_{osc} = \frac{1}{\sqrt{L_1 C_1 (1 + C_{var} / C_1)}}$$

From: Behzad Razavi, *RF Microelectronics*, © 2012 Pearson, USA.



Xi'an Jiaotong-Liverpool University  
西交利物浦大学

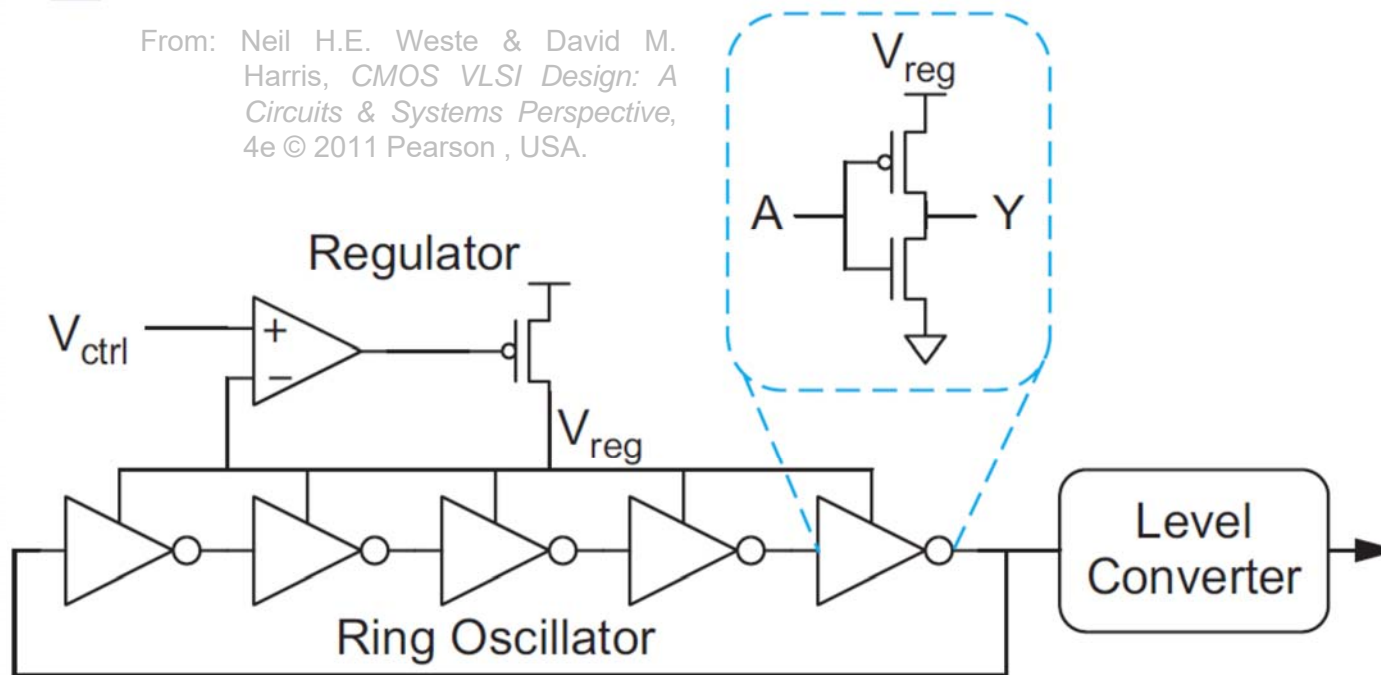


# Voltage-Controlled Oscillator

(ring oscillator)

- ❑ The **ring oscillator** design can also be made as a VCO.
- ❑ The oscillation frequency can be controlled by the **delay** of each inverter stage.

From: Neil H.E. Weste & David M. Harris, *CMOS VLSI Design: A Circuits & Systems Perspective*, 4e © 2011 Pearson, USA.



➤ The delay of each inverter stage can be controlled by the supply voltage hence the dynamic current.

➤ A level converter restores the output to the full swing of the supply voltage.

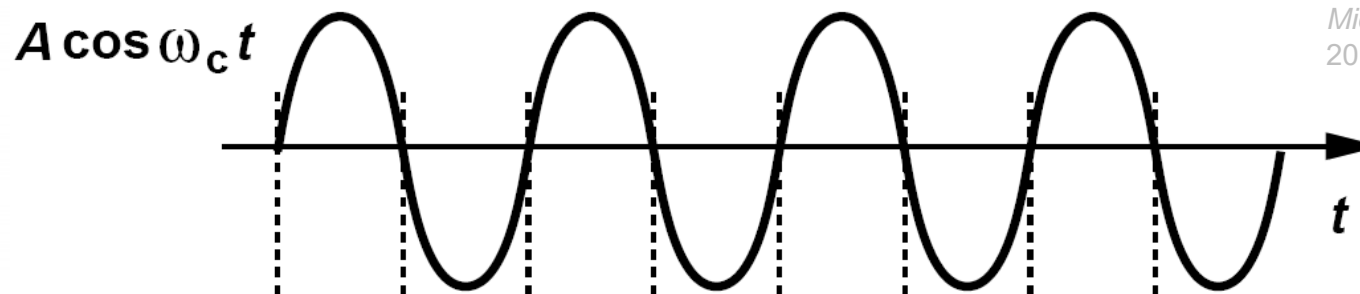


Xi'an Jiaotong-Liverpool University  
西交利物浦大学

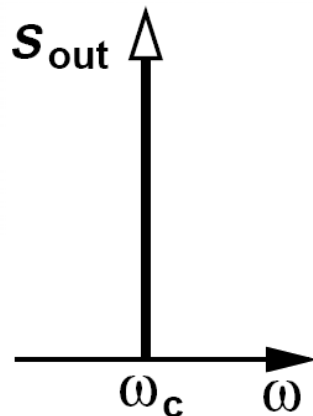
# Phase Noise of VCO

(ideal oscillator)

- ❑ An ideal **oscillator** produces a perfectly periodic output of the form  $v(t) = A\cos(\omega_c t)$ .
- ❑ The zero crossings occur at exact multiples of the period ( $T_c = 2\pi/\omega_c$ ) of the waveform.



From: Behzad Razavi, *RF Microelectronics*, © 2012 Pearson, USA.



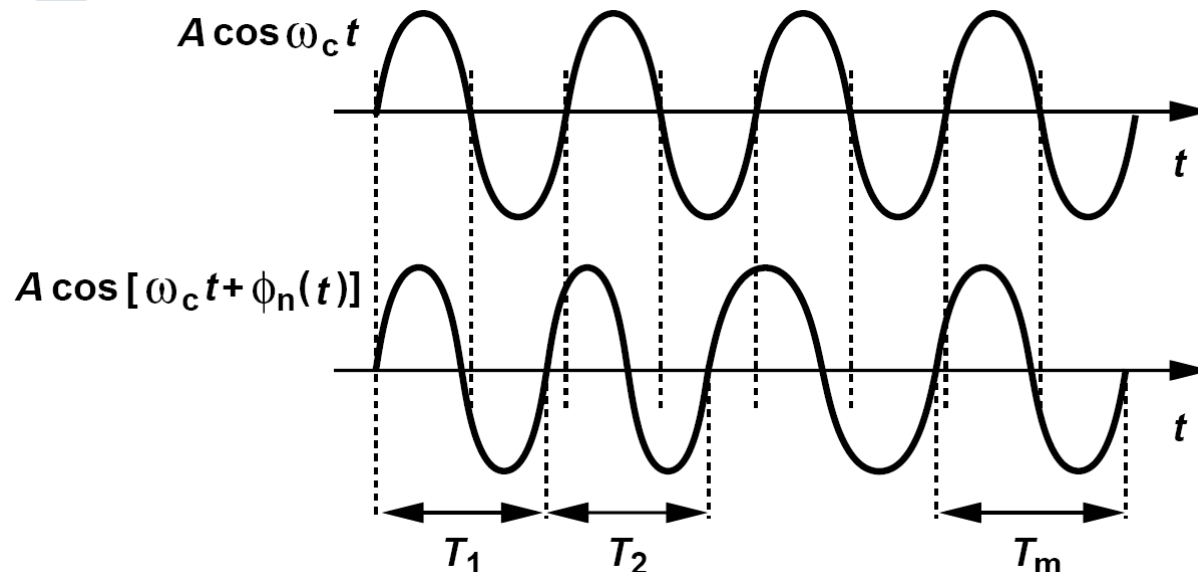
- In the frequency spectrum, it would ideally consist of one impulse at  $\omega_c$ .

# Phase Noise of VCO

(perturbed zero crossings)

- ❑ In reality however, the noise of the oscillator randomly **perturbs** the **zero crossings**.
  - To model this perturbation, we can write  $v(t) = A\cos(\omega_c t + \phi_n(t))$ , where  $\phi_n(t)$  is a small **random phase** quantity that **deviates** the **zero crossings** from integer multiples of  $T_c$ .

From: Behzad Razavi, *RF Microelectronics*, © 2012 Pearson, USA.



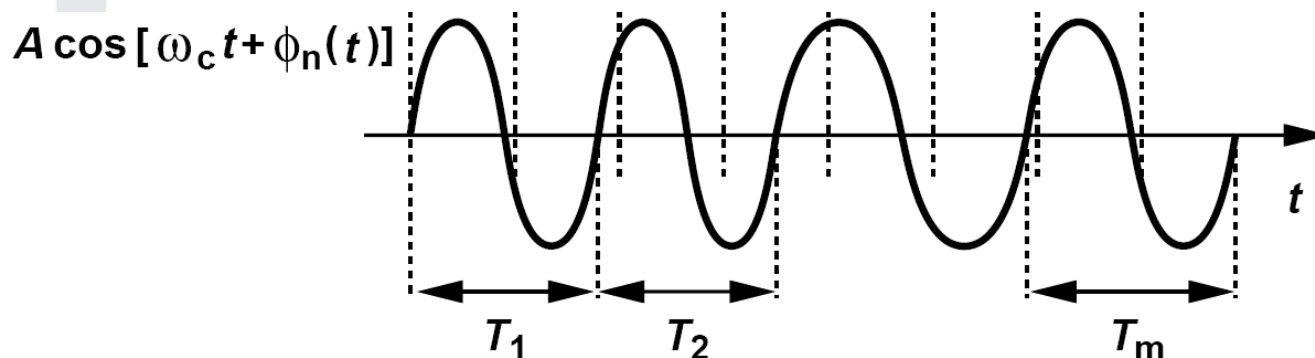
- $\phi_n(t)$  is called the **phase noise** of the oscillator. This is viewed in the time domain.

# Phase Noise of VCO

(frequency deviations)

- ❑ The **perturbation** of the **zero crossings** can be viewed as the **period** of the waveform **deviates** randomly from the constant  $T_c$  of a **perfectly periodic** signal.
- ❑ In other words, the waveform has a distribution of **periods** (i.e.  $T_1, T_2, \dots, T_m$ ) and hence a distribution of **frequencies** (i.e.  $1/T_1, 1/T_2, \dots, 1/T_m$ ).

From: Behzad Razavi, *RF Microelectronics*, © 2012 Pearson, USA.



➤ Note  $f_1 = 1/T_1$ ;  
 $\omega_1 = 2\pi/T_1$ .

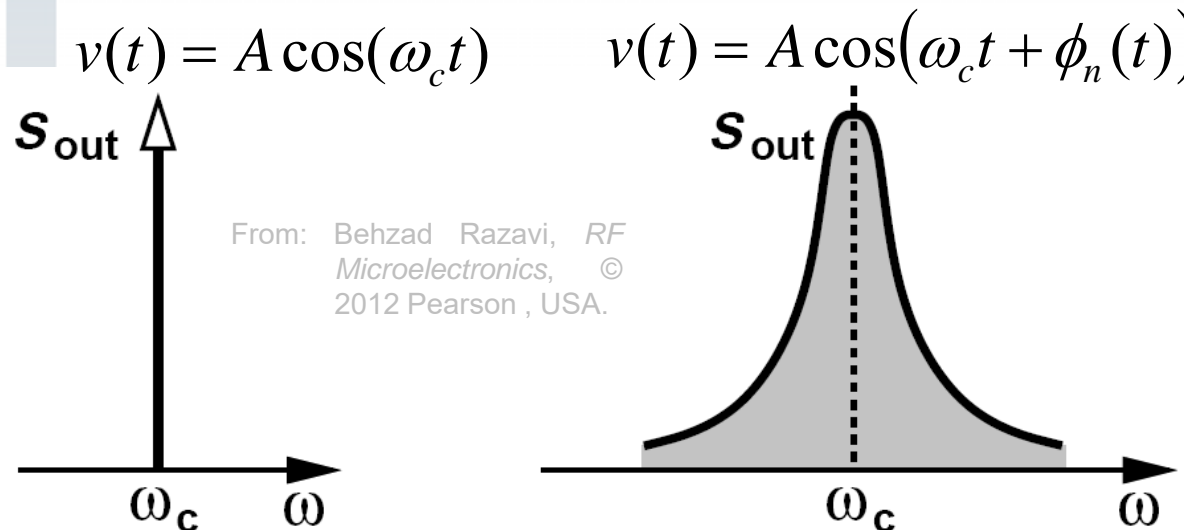


Xi'an Jiaotong-Liverpool University  
西交利物浦大学

# Phase Noise of VCO

(distribution in frequency spectrum)

- ❑ In the frequency domain, the **random deviation** from the constant  $T_c$  of a **perfectly periodic** signal can be represented by a “broadened” impulse around  $\omega_c$ .
  - The spectrum of the oscillator output has a distribution of **frequencies** ( $\omega_1, \omega_2, \dots, \omega_m$ ) around  $\omega_c$ .

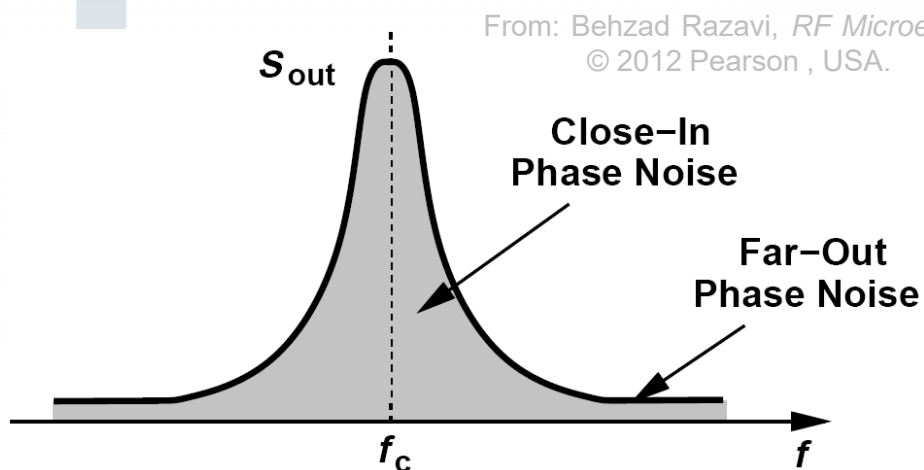


- The frequency deviation from  $\omega_c$  is due to the random variations of  $\phi_n(t)$ .

# Phase Noise of VCO

(linkage to time domain)

- ❑ The spectrum of the **oscillator** output has declining skirts from the peak at  $\omega_c$ .
  - The **phase noise** is more significant when it is close to  $\omega_c$  while it reaches almost a constant floor when the frequency is far away from  $\omega_c$ .
  - Such behaviour in the frequency domain can be related to the **phase noise**  $\phi_n(t)$  in the time domain.



$$\begin{aligned}v(t) &= A \cos(\omega_c t + \phi_n(t)) \\&\approx A \cos(\omega_c t) - A \sin(\omega_c t) \sin(\phi_n(t)) \\&\approx A \cos(\omega_c t) - \phi_n(t) A \sin(\omega_c t)\end{aligned}$$

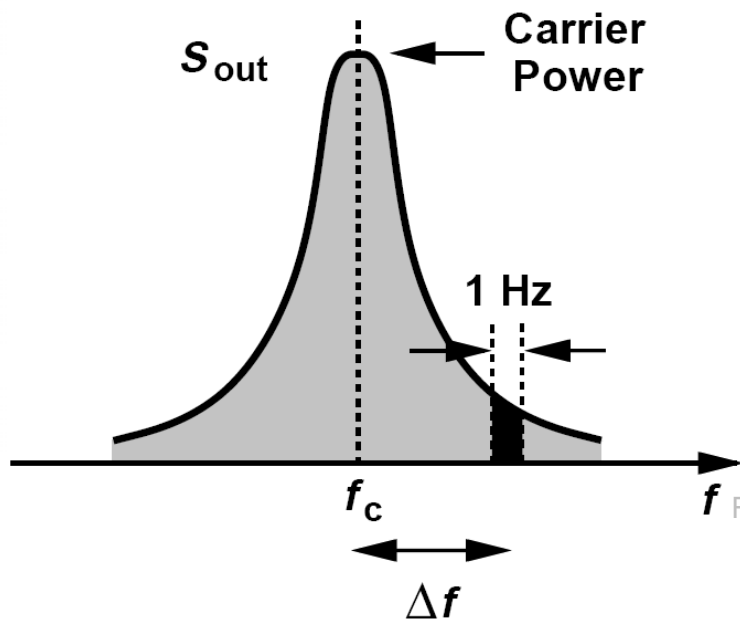
$$\cos(\theta_1 + \theta_2) = \cos \theta_1 \cos \theta_2 - \sin \theta_1 \sin \theta_2$$

$$|\phi_n(t)| \ll 1 \text{ radian}$$

# Phase Noise of VCO

(specifying at offset frequency)

- ❑ As the **phase noise** in the frequency domain falls at frequencies farther away from  $f_c$ , the **phase noise performance** of an oscillator can be quantified by specifying at a certain **frequency offset** (i.e. a certain difference with respect to  $f_c$ ).



- We can consider a 1-Hz bandwidth of the spectrum at an offset of  $\Delta f$  and then measure the power in this bandwidth, and finally normalise the power to the “carrier power” (i.e. the peak of the spectrum).

From: Behzad Razavi, *RF Microelectronics*,  
© 2012 Pearson, USA.



Xi'an Jiaotong-Liverpool University  
西交利物浦大学

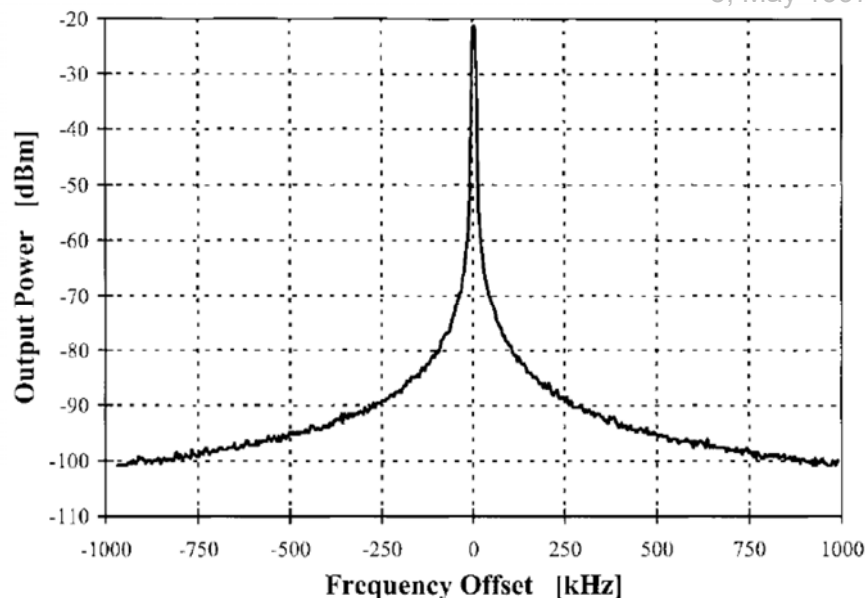


# Phase Noise of VCO

(dBc - dB with respect to the carrier)

- ❑ As an example in specifying the **phase noise** of an oscillator, the requirement in GSM applications is below **-115 dBc/Hz** at 600-kHz offset.
- The unit **dBc** is called “**dB with respect to the carrier**” and signifies normalization of the noise power to the carrier power.

From: J. Craninckx and M. S. J. Steyaert, "A 1.8-GHz Low-Phase-Noise CMOS VCO Using Optimized Hollow Spiral Inductors," *IEEE Journal of Solid-state Circuits*, vol. 32, no. 5, May 1997 (pp. 736-744).



- Can you read the VCO's phase noise here to see if it meets the GSM requirement?
- The phase noise performance is -80 dBc/Hz at 1-MHz offset here.



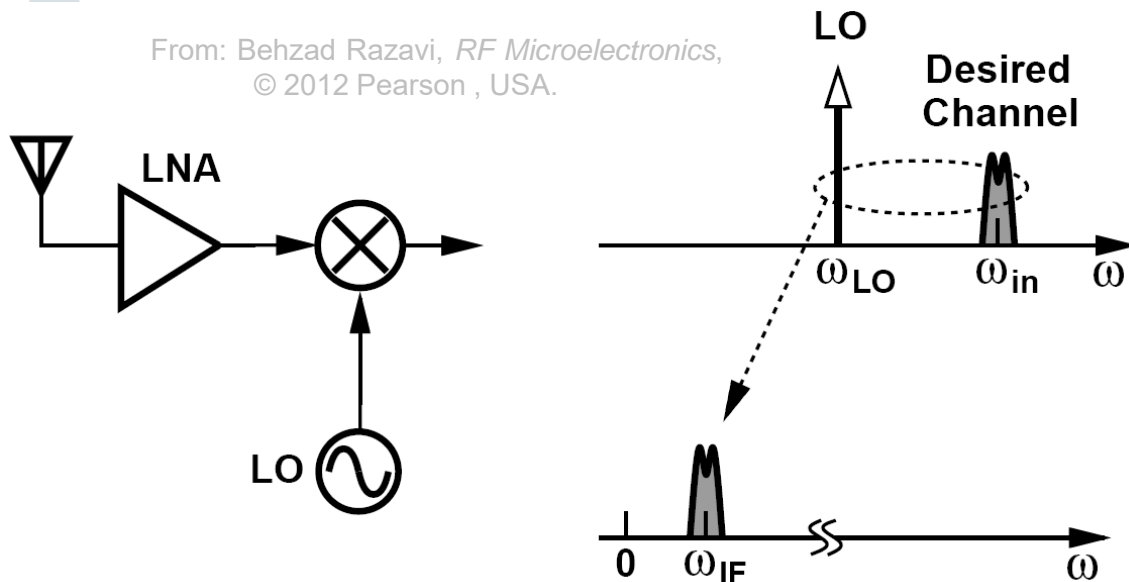
Xi'an Jiaotong-Liverpool University  
西交利物浦大学

# Phase Noise of VCO

(effect in downconversion)

- ❑ The effect of phase noise can be understood in an RF front-end receiver in which the RF signal is downconverted by a mixer driven by a **local oscillator** (LO) signal.
  - With the downconversion mixing, the desired channel is convolved with the impulse at  $\omega_{LO}$ , producing an intermediate frequency (IF) signal at  $\omega_{IF} = | \omega_{in} - \omega_{LO} |$ .

From: Behzad Razavi, *RF Microelectronics*,  
© 2012 Pearson, USA.

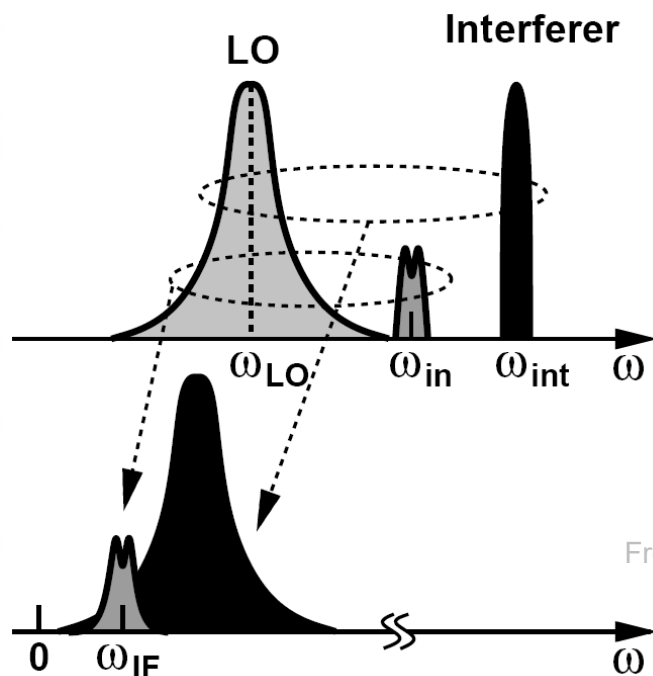


- No problem is caused in the downconversion if the LO signal is **perfectly periodic** (i.e. has no phase noise).

# Phase Noise of VCO

(effect of downconverted interferer signal)

- ❑ It is not uncommon that the desired RF signal is accompanied by a strong interferer signal (and they are close to each other in the frequency spectrum).
- ❑ The interferer signal is also downconverted together with the desired RF signal.



- If the LO signal has considerable phase noise, the downconverted interferer would have its noise skirt corrupting the desired IF signal.
- This phenomenon is called “reciprocal mixing”.

From: Behzad Razavi, *RF Microelectronics*,  
© 2012 Pearson, USA.



Xi'an Jiaotong-Liverpool University  
西交利物浦大学