

# Unit 5: Negative Feedback and Operational Amplifiers

Xueqi Li\*  
(Dated: Apr 14, 2018)

## INTRODUCTION

An operational amplifier (opamp) can amplify the input voltage by a large factor. Since it has a large gain, it might not be stable in many cases and the output is very uncontrollable, we usually build up a circuit with it to achieve a much more stable circuit.

An opamp, other than power-supply pins ( $V_{CC}$  and  $V_{EE}$ ), has two input and one output, where the inputs are known as non-inverting input (+) and inverting input (-). The output is given as:

$$v_{out} = A_0(v_+ - v_-) \quad (1)$$

where  $A_0$  is a very large number. Usually it is higher than  $10^5$ . The impedance of the opamp can be thought of as ideal.

## Negative Feedback

A negative feedback is such that the output of the opamp connects to the inverting input. That is to say,  $v_- = v_{out}$ . This leads to the following equation:

$$v_+ = v_- \quad (2a)$$

$$i_+ = i_- = 0 \quad (2b)$$

## Follower

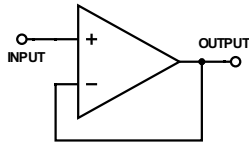


FIG. 1: A follower

The simplest negative feedback circuit is a follower, so as in Figure 1. From Equation 2a, we see that

$$V_{out} = V_{in} \quad (3)$$

## Inverting Amplifier

An operational amplifier has to be able to be an amplifier! An Inverting Amplifier is presented as Figure 2.

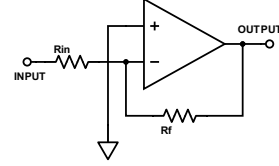


FIG. 2: An Inverting Amplifier

Since the non-inverting input is grounded, we must have  $v_+ = v_- = 0V$ . Thus, we can find the current in the input side as given as

$$I_{in} = \frac{V_{in}}{R_{in}}$$

Following Equation 2b, this current has to be also going through  $R_f$ , where the voltage drop on  $R_f$  just so happened to be the output voltage ( $v_- - V_{out}$ ):

$$V_{out} = -IR_f = -V_{in} \frac{R_f}{R_{in}} \quad (4)$$

where we see that the gain is just given as:

$$\text{Gain} = -\frac{R_f}{R_{in}}$$

Notice that for the inverting amplifier, the input impedance is given as:

$$Z_{in} = \frac{dV_{in}}{dI_{in}} = R_{in}$$

which is not a very high input impedance. In the other hand, easy to see the output impedance is ideal.

## Non-inverting Amplifier

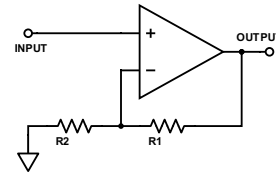


FIG. 3: A non-inverting Amplifier

It is nice to have a non-inverting amplifier. A non-inverting amplifier is shown as Figure 3. Since the input

is directly connect to the non-inverting input, we have  $V_{\text{input}} = v_+ = v_-$ . In the end of  $R_2$ , we must have 0V since it is grounded. Thus we have:

$$I_2 = \frac{V_{\text{in}}}{R_2}$$

From Equation 2b, this current have to go through  $R_1$ :

$$V_1 = IR_1 = V_{\text{in}} \frac{R_1}{R_2}$$

where the other end of  $R_2$  just so happened to be the output:

$$V_{\text{output}} = V_{\text{in}} + V_1 = V_{\text{in}} \left(1 + \frac{R_1}{R_2}\right) \quad (5)$$

which give as a gain as:

$$\text{Gain} = \left(1 + \frac{R_1}{R_2}\right)$$

### Integrator

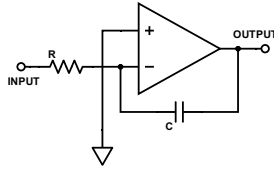


FIG. 4: An Integrator

The circuit presented in Figure 4 is an integrator. Since the non-inverting input is grounded, we have  $v_- = v_+ = 0V$ . Thus we can find the current in the capacitor is the same as the current go through the resistor:

$$I = -C \frac{dV_{\text{out}}}{dt} = \frac{V_{\text{in}}}{R}$$

solve the equation, we have:

$$V_{\text{out}} = -\frac{1}{RC} \int V_{\text{in}} dt \quad (6)$$

However, there is a problem for the integrator. Usually, the input might have an offset. That is to say, there is a constant term in the input voltage. This will give us a growing or falling output after integration. To solve it, one can parallel a resistor with the capacitor.

### T Network

To achieve a large parallel resistor, one can use a T network, so as in Figure 5. Ignore the capacitor, we can

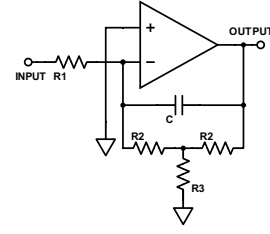


FIG. 5: An Integrator with T network

just calculate the effect of the T network. First, we still have the current on the  $R_1$  will go through the left  $R_2$ :

$$I_1 = \frac{V_{\text{in}}}{R_1} = I_{2L} = I_{2R} + I_3$$

On the other hand, the voltage between  $R_1$  and  $R_{2L}$  is 0V. Thus we can find the voltage between two  $R_2$ :

$$V_2 = 0 - I_1 R_2 = -V_{\text{in}} \frac{R_2}{R_1}$$

And this voltage will drop to zero once it go through  $R_3$ :

$$I_3 = \frac{V_2}{R_3} = -V_{\text{in}} \frac{R_2}{R_1 R_3}$$

In the output end, we can write the current go through  $R_2$  as following:

$$I_2 = \frac{V_2 - V_{\text{out}}}{R_2} = -\frac{V_{\text{in}}}{R_1} - \frac{V_{\text{out}}}{R_2}$$

This relate the output voltage to the current. Now we have  $I_1 = I_2 + I_3$ :

$$\frac{V_{\text{in}}}{R_1} = -V_{\text{in}} \frac{R_2}{R_1 R_3} - \frac{V_{\text{in}}}{R_1} - \frac{V_{\text{out}}}{R_2}$$

Solve the equation, we find

$$V_{\text{out}} = -V_{\text{in}} \frac{R_2}{R_1} \left(2 + \frac{R_2}{R_3}\right)$$

This give us the impedance of the T network:

$$Z_f = R_2 \left(2 + \frac{R_2}{R_3}\right)$$

Thus, we can achieve a high impedance if we just chose two two small resistor with a large ratio.

### Differentiator

By interchange the resistor and capacitor of integrator, one can achieve a differentiator, as in Figure 6. Since the non-inverting input is grounded, we have to have 0V on  $v_-$ . This means the current go through the capacitor and the resistor are the same:

$$V_{\text{out}} = -IR = -RC \frac{dV_{\text{in}}}{dt} \quad (7)$$

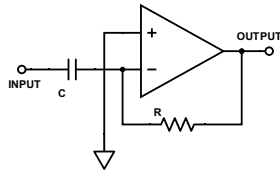


FIG. 6: An Differentiator

### Limit of the Opamp

A realistic opamp are not ideal. There are a few important things we have to consider when use it:

1. The voltage gain ( $A_0$ ) will drop linearly to the frequency in logarithm scale;
2. There might be a phase shift in the output;
3. For the feedback loop, Equation 2b is approximate, i.e.,  $i_+$ ,  $i_- \approx 0$ ;

4. For the feedback loop, Equation 2a is approximate, i.e.,  $v_+ \approx v_-$ ;
5. There is a small delay to the output. When input voltage change suddenly, the output voltage will learly increase and reach the theoretical value. This is called slew rate.

### DATA AND CALCULATION

#### ANALYSIS

#### CONCLUSION

---

\* Partner: Tianming Hai