

# Vector Field Mid Review

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November 2023

## 1 Coordinate

There are three commonly used coordinates: rectangular (Cartesian), cylindrical, and spherical coordinates. You need to know their conversions.

**Proposition 1.1.** *Conversion of coordinates*

Conversion	Formulae		
$(r, \theta, z) \rightarrow (x, y, z)$	$x = r \cos \theta$	$y = r \sin \theta$	$z = z$
$(x, y, z) \rightarrow (r, \theta, z)$	$r = \sqrt{x^2 + y^2}$	$\tan \theta = y/x$	$z = z$
$(\rho, \phi, \theta) \rightarrow (r, \theta, z)$	$r = \rho \sin \theta$	$\theta = \theta$	$z = \rho \cos \phi$
$(r, \theta, z) \rightarrow (\rho, \phi, \theta)$	$\rho = \sqrt{r^2 + z^2}$	$\tan \phi = r/z$	$\theta = \theta$
$(\rho, \phi, \theta) \rightarrow (x, y, z)$	$x = \rho \sin \phi \cos \theta$	$y = \rho \sin \phi \sin \theta$	$z = \rho \cos \phi$
$(x, y, z) \rightarrow (\rho, \phi, \theta)$	$\rho = \sqrt{x^2 + y^2 + z^2}$	$\cos \phi = \frac{z}{\sqrt{x^2 + y^2 + z^2}}$	$\tan \theta = \frac{y}{x}$

There is another thing that is important for the conversion of coordinates. When we integrate along a curve, we may need to know the "element" of arc length,  $ds$ . In addition, we also need to consider the "element" of the area of a surface or that of volume. Thanks to Renjing and Prof. Andrew, they brought me a fabulous way to think about the element, div and curl.

Consider the conversion of coordinate  $(x^1, \dots, x^n) \rightarrow (u^1, \dots, u^n)$ . Then the position can be written as

$$\vec{r}(u^1, \dots, u^n) = x^1 \hat{e}_{x^1} + \dots + x^n \hat{e}_{x^n}$$

Take the differentiation, we get

$$d\vec{r}(u^1, \dots, u^n) = \sum_{i=1}^n \frac{\partial \vec{r}}{\partial u^i} du^i.$$

We hope that  $\{\frac{\partial \vec{r}}{\partial u^i}\}$  forms a basis. To check whether the new coordinate system  $(u^1, \dots, u^n)$  is acceptable (the vectors above is a basis), we need to check the determinant

$$\begin{vmatrix} \frac{\partial \vec{r}}{\partial u^1} & \dots & \frac{\partial \vec{r}}{\partial u^n} \end{vmatrix}$$

If the determinant is not 0, then the conversion is bijective. The determinant above is called Jacobian, denoted by

$$J(u^1, \dots, u^n) = \begin{vmatrix} \frac{\partial x^1}{\partial u^1} & \dots & \frac{\partial x^1}{\partial u^n} \\ \vdots & \ddots & \vdots \\ \frac{\partial x^n}{\partial u^1} & \dots & \frac{\partial x^n}{\partial u^n} \end{vmatrix}$$

However, one may find that  $\{\frac{\partial \vec{r}}{\partial u^1}, \dots, \frac{\partial \vec{r}}{\partial u^n}\}$  may not be unit vectors, thus we need to normalize them.

$$\vec{e}_1 = \frac{1}{h_1} \frac{\partial \vec{r}}{\partial u^1}, \dots, \vec{e}_n = \frac{1}{h_n} \frac{\partial \vec{r}}{\partial u^n}$$

$$h_1 = \left\| \frac{\partial \vec{r}}{\partial u^1} \right\|, \dots, h_n = \left\| \frac{\partial \vec{r}}{\partial u^n} \right\|$$

For an orthogonal coordiante system,  $d\vec{r}$  can be rewritten as

$$d\vec{r} = \frac{\partial \vec{r}}{\partial u_1} du_1 + \frac{\partial \vec{r}}{\partial u_2} du_2 + \dots + \frac{\partial \vec{r}}{\partial u_n} du_n = h_1 du_1 \vec{e}_1 + \dots + h_n du_n \vec{e}_n. \quad (1)$$

Then the element of square of arc length can be written as

$$ds^2 = d\vec{r} \cdot d\vec{r} = h_1^2 du_1^2 + \dots + h_n^2 du_n^2 \quad (2)$$

and

$$dV = dx_1 dx_2 dx_3 = \frac{\partial(x_1, x_2, \dots, x_n)}{\partial(u_1, u_2, \dots, u_n)} du_1 du_2 du_3.$$

The statements above might be abstract, so an example is given below.

**Example 1.1.** Consider the cylindrical coordinate, we know that a point in the space can be written as  $\vec{r} = (r \cos \theta, r \sin \theta, z)$ . Then we have

$$h_1 = h_r = \left\| \frac{\partial \vec{r}}{\partial r} \right\| = \|(\cos \theta, \sin \theta, 0)\| = 1$$

$$h_2 = h_\theta = \left\| \frac{\partial \vec{r}}{\partial \theta} \right\| = \|(-r \sin \theta, r \cos \theta, 0)\| = r$$

$$h_3 = h_z = \left\| \frac{\partial \vec{r}}{\partial z} \right\| = \|(0, 0, 1)\| = 1$$

thus we have

$$\vec{e}_r = (\cos \theta, \sin \theta, 0)$$

$$\vec{e}_\theta = (-\sin \theta, \cos \theta, 0)$$

$$\vec{e}_z = (0, 0, 1)$$

One can check that they are orthogonal and satisfy the right-hand rule. It also explains that it is  $r d\theta$  in  $d\vec{r} = dr \vec{e}_r + r d\theta \vec{e}_\theta + dz \vec{e}_z$  instead of  $d\theta$  itself.

*Remark:* You can also use dimension (unit) analysis to check that there should be an  $r$  in the coefficient of  $e_\theta$ .

## 2 Gradient, Divergence and Curl

### 2.1 Directional Derivative

Before we introduce the gradient, we need to know what is the directional derivative.

**Definition 2.1.** *Given a scalar field  $f$  (in fact it is just a scalar function) and a vector  $v$ , the directional derivative of  $f$  in the direction  $\vec{v} = v_1, \dots, v_n$  at point  $p$  is defined to be*

$$\left. \frac{\partial f}{\partial v} \right|_p = \lim_{t \rightarrow 0} \frac{f(p + tv)}{t}.$$

One may check that  $\frac{\partial f}{\partial v} = (\frac{\partial f}{\partial x_1}, \dots, \frac{\partial f}{\partial x_n}) \cdot \vec{v}$

If we restrict  $\|\vec{v}\| = 1$ , we may find that

$$\left| \frac{\partial f}{\partial v} \right| \leq \|(\frac{\partial f}{\partial x_1}, \dots, \frac{\partial f}{\partial x_n})\|, \quad (3)$$

the equal holds when  $\vec{v}$  is parallel to  $(\frac{\partial f}{\partial x_1}, \dots, \frac{\partial f}{\partial x_n})$ .

Note that here scalar field and vector field can be regarded as functions  $f : \mathbb{R}^n \rightarrow \mathbb{R}$  and  $\vec{A} : \mathbb{R}^n \rightarrow \mathbb{R}^n$ , respectively.

### 2.2 Gradient

From the inequality(3), it is quite nature to define the vector  $(\frac{\partial f}{\partial x_1}, \dots, \frac{\partial f}{\partial x_n})$ .

**Definition 2.2.** *Gradient*

*Given a scalar field  $f$ , the gradient of  $f$  is defined to be*

$$\nabla f = (\frac{\partial f}{\partial x_1}, \dots, \frac{\partial f}{\partial x_n}). \quad (4)$$

The gradient indicates the direction the the scalar field increases the most rapidly. In addition, its norm is the rate of the maximum increase.

### 2.3 Divergence

**Definition 2.3.** *Divergence*

*The divergence of a vector field  $\vec{A} = (f_1, f_2, \dots, f_n)$  is defined to be*

$$\text{div } \vec{A} = \nabla \cdot \vec{A} = (\frac{\partial}{\partial x_1}, \dots, \frac{\partial}{\partial x_n}) \cdot \vec{A} = \sum_{i=1}^n \frac{\partial f_i}{\partial x_i} \quad (5)$$

We can not get anything intuitively from the definition. To have a better understanding, we may start with the Gauss theorem

$$\iiint_V \text{div } \vec{A} dV = \iint_S \vec{A} \cdot \vec{n} ds \quad (6)$$

divide each side by  $\|V\|$  and let  $\|V\| \rightarrow 0$ , we get

$$\operatorname{div} \vec{A} = \lim_{\|V\| \rightarrow 0} \frac{1}{\|V\|} \iint_S \vec{A} \cdot \vec{n} \, ds \quad (7)$$

One may find that the divergence is the flux of the vector field on an element of volume.

## 2.4 Curl

**Definition 2.4.** For a vector field  $\vec{A} = (f, g, h)$ , we may define its curl as

$$\operatorname{curl} \vec{A} = \begin{vmatrix} i & j & k \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ f & g & h \end{vmatrix} \quad (8)$$

It is also hard to understand what is curl from the definition. Hence one can try to use Stokes' theorem which contains curl for help.

$$\oint_C \vec{A} \cdot d\vec{r} = \iint_S \operatorname{curl} \vec{A} \cdot \vec{n} \, dS.$$

Divide each side by  $\|S\|$  (the area of surface) and let  $\|S\| \rightarrow 0$ , then we get

$$\operatorname{curl} \vec{A} \cdot \vec{n} = \lim_{\|S\| \rightarrow 0} \frac{1}{\|S\|} \oint_C \vec{A} \cdot d\vec{r} \quad (9)$$

Since  $\|\operatorname{curl} \vec{A}\| \geq |\operatorname{curl} \vec{A} \cdot \vec{n}|$ , one may find that the curl of a vector space can be regarded as the maximum of circulating flow on an element of area.

## 3 Some Basic Method for Integration

### 3.1 Line Integral

**Integrate on Scalar Field** Let  $f$  be a scalar function and  $C$  a curve. Then we may have a parametric representation  $s : I \rightarrow \mathbb{R}^n$ ,  $s = s(t)$  for the curve  $C$ .

The integral of  $f$  along  $C$  can be written as

$$\int_C f(s) \, ds = \lim_{\delta_{s_i} \rightarrow 0} \sum_{i=1}^N f(s_i) \delta_{s_i}$$

By equation(2), we know that the integral can be written as

$$\int_I f(s(t)) \sqrt{h_1^2 \left(\frac{ds_1}{dt}\right)^2 + \dots + h_n^2 \left(\frac{ds_n}{dt}\right)^2} \, dt \quad (10)$$

For rectangular coordinates, equation(10) is

$$\int_I f(s(t)) \sqrt{\left(\frac{dx_1}{dt}\right)^2 + \dots + \left(\frac{dx_n}{dt}\right)^2} dt$$

For cylindrical coordinates, equation(10) is

$$\int_I f(s(t)) \sqrt{\left(\frac{dr}{dt}\right)^2 + r^2 \left(\frac{d\theta}{dt}\right)^2 + \left(\frac{dz}{dt}\right)^2} dt$$

In this case, the line integral is transformed into proper integral.

**Integral on Vector Field** Let  $\vec{F}(x, y, z) = (f(x, y, z), g(x, y, z), h(x, y, z))$  a vector field,  $C$  a curve in  $\mathbb{R}^3$  with representation  $\vec{r}(t)$ . Then the line integral of  $\vec{F}$  along  $C$  is

$$\int_C \vec{F}(x, y, z) \cdot d\vec{r} = \int_C f(x, y, z) dx + g(x, y, z) dy + h(x, y, z) dz$$

To calculate the integral, one could use  $d\vec{r} = \frac{d\vec{r}(t)}{dt} dt$  and compute the inner product  $\vec{F} \cdot \frac{d\vec{r}(t)}{dt}$  first and integral along  $I$ . It would not be so hard.

### 3.2 Fundamental Theorem of Line Integral

**Theorem 3.1.** If  $\vec{F} = \nabla\phi$  for some scalar field  $\phi$ , then

$$\int_C \vec{F} \cdot d\vec{r} = \phi(p_1) - \phi(p_0)$$

where  $p_1$  and  $p_0$  are the end point and starting point, correspondingly.

*Proof.*

$$\begin{aligned} \int_C \vec{F} \cdot d\vec{r} &= \int_C \frac{\partial\phi}{\partial x} dx + \frac{\partial\phi}{\partial y} dy + \frac{\partial\phi}{\partial z} dz \\ &= \int_a^b \left( \frac{\partial\phi}{\partial x} \frac{dx}{dt} + \frac{\partial\phi}{\partial y} \frac{dy}{dt} + \frac{\partial\phi}{\partial z} \frac{dz}{dt} \right) dt \\ &= \int_a^b \frac{d}{dt} \phi(x(t), y(t), z(t)) dt \\ &= \phi(x(t), y(t), z(t)) \Big|_{t=a}^{t=b} = \phi(p_1) - \phi(p_0) \end{aligned}$$

□

**Theorem 3.2.** Let  $\vec{F}(x, y) = (f(x, y), g(x, y))$  where  $f$  and  $g$  have continuous first partial derivatives in an open simple connected region, then

$$\exists \phi(\nabla\phi = \vec{F}) \Leftrightarrow \left( \frac{\partial f}{\partial y} = \frac{\partial g}{\partial x} \right)$$

at each point of the region.

### 3.3 Green's Theorem

**Theorem 3.3.** *Let  $R$  be a simply connected plane region whose boundary is a piecewise smooth closed curve  $C$  oriented counterclockwise. If  $f$  and  $g$  have continuous first derivatives on some open set containing the region  $R$ , then*

$$\int_C f(x, y) dx + g(x, y) dy = \iint_R \left( \frac{\partial g}{\partial x} - \frac{\partial f}{\partial y} \right) dA \quad (11)$$

*Proof.* The proof is on pages 47-50 of the note for Chapter 3.  $\square$

In fact, one can regard it as the 2 – dim version of Stokes' theorem.

## 4 Surface Integration

Before we step into the surface integration, we may introduce the orientation first. For a curve, the orientation is the direction of the derivative of the representation  $\vec{r}(t)$ . However, the surface would have two normal vectors, so we need to define its orientation.

**Definition 4.1.** *Oriented Surface*

*Let  $S(u, v) : D \rightarrow \mathbb{R}^3$  be a parametric representation of the surface  $S$ . Define  $\vec{n} : S(D) \rightarrow S^2$  mapping each point on the surface to the unit sphere. We say that  $S$  is oriented by  $\vec{n}$  if for any curve  $\alpha(t)$  on the surface,  $\vec{n} \circ \alpha$  is continuous.*

*Intuitively, one could think that the normal vector changes continuously on the surface.*

*In addition, if there is  $\vec{n}$  such that the surface  $S$  is oriented, we say  $S$  is orientable, and  $\vec{n}$  an orientation of  $S$ . Otherwise,  $S$  is not orientable.*

*Notice:* The Möbius strip is an example of non-orientable surfaces.

**Definition 4.2.** *Surface Integrals*

*Let  $S$  be surface,  $g$  a scalar field. Then the integral of  $g$  on  $S$  is defined to be*

$$\iint_S g dS = \lim_{m \rightarrow \infty} \sum_{i=1}^m g_i \delta S_i \quad (12)$$

*where  $m$  is the (supremum) area of  $\delta S_i$ .*

The definition is not so convenient to compute the integral, so we need a further theorem.

**Theorem 4.1.** *If we can project the surface injectively onto the subset  $R$  of the  $x - y$  plane, we have*

$$\iint_S g dS = \iint_R g \frac{dx dy}{|\vec{n} \cdot \vec{k}|}$$

*where  $\vec{n}$  is the unit orientation of surface and  $\vec{k} = (0, 0, 1)$ .*

**Remark:** the inner product of  $\vec{n}$  and  $\vec{k}$  should be always  $> 0$  or  $< 0$  since it is also continuous and the denominator should not be 0.