

# 势涡的共振和非共振输运与 $E \times B$ 台阶

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## 1 研究背景

## 2 研究路线

## 3 湍流-剖面演化系统

## 4 $E \times B$ 台阶

## 5 总结

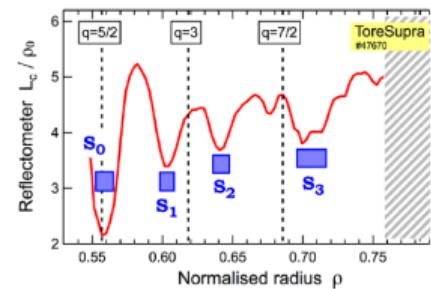
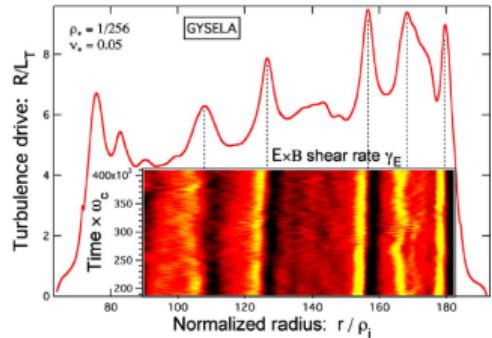


Fig. 1: 模拟中出现的平均温度分布褶皱和  $E \times B$  剪切流的位置[Dif-Pradalier et al., 2010]; ToreSupra 中, 反射计测量得到的相关长度[Dif-Pradalier et al., 2015]

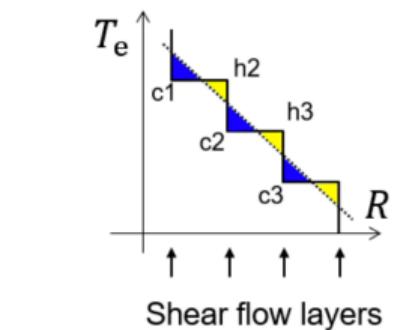
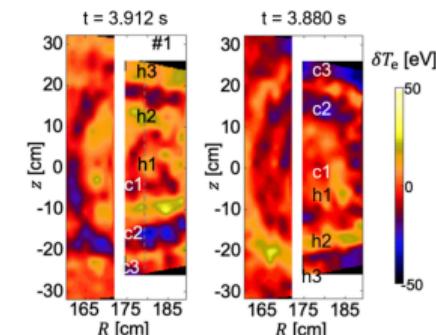


Fig. 2: KSTAR 中 ECEI 测量得到温度褶皱[Choi et al., 2019]

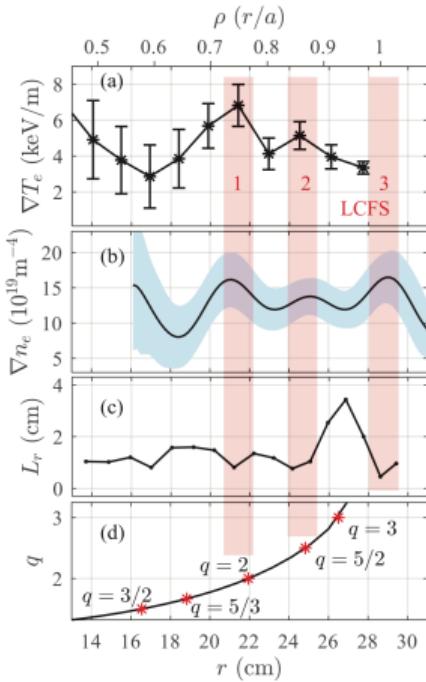


Fig. 3: HL-2A 中 ECE 和反射计测量得到温度台阶[Liu et al., 2021]

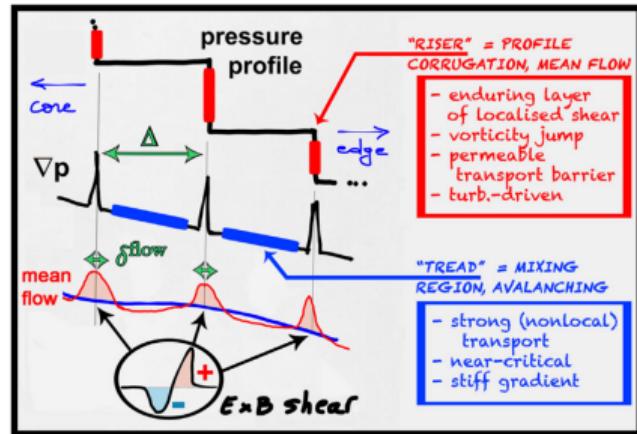


Fig. 4:  $E \times B$  台阶示意图 [Dif-Pradalier et al., 2017]

- 台面尺寸给出了一个 **有效的混合长度**  
?  
⇒ gyro-Bohm 定标的失效;
- 微输运垒融合为内输运垒? 多级输运垒优于单级输运垒? [Ashourvan et al., 2019]

## $E \times B$ 台阶: 剪切层和剖面褶皱的准规则模式 (pattern)

- $E \times B$  台阶中微输运垒 ( $E \times B$  剪切层) 将 DW 湍流的活跃区分隔 (台面)
- 台面区为类雪崩输运
- 台面宽度大约  $20 - 40 \rho_i$
- 剪切层位置和有理面没有明显关联
- 部分模拟中观察到台阶融合

## 研究意义

- 提高等离子体约束
- 先进运行模式
- 大规模回旋动力学模拟的简化



## 1、初值问题

任何热通量中的“惯性”都可能导致时间延迟

[Kosuga et al., 2014, Kosuga et al., 2013],

$$\partial_t Q = -\frac{1}{\tau} (Q - Q_0[\delta T]) \quad (1)$$

=====

Large  $\tau \implies v_0 \sim \lambda \delta T_0 > v_{ph} \sim \sqrt{\frac{\chi_2}{\tau}} \implies$  Jam Inst.

## 2、边值问题

基于 Hasegawa-Wakatani 模型, 认为存在一个依赖于梯度的混合长度  $\implies$  双稳定 (Bistable)

[Ashourvan & Diamond, 2016, Ashourvan & Diamond, 2017].

$$l_{mix} = \frac{l_0}{1 + l_0^2 [\partial_x(n - u)]^2 / \mathcal{E}} \quad (2)$$

## 3、其他

- 剖面耦合

[Leconte & Kobayashi, 2021, Singh & Diamond, 2021]

- Wave Trapping [Garbet et al., 2021]

## 现有理论的主要不足

- 模型大多偏唯象、多讨论密度剖面、解释能力有限
- 没有从动理学出发给出的理论, 缺少微观效应的讨论

如何理解台阶尺度的涌现 (emergence) ?

$E \times B$  台阶需要更细致的理论研究



1 研究背景

2 研究路线

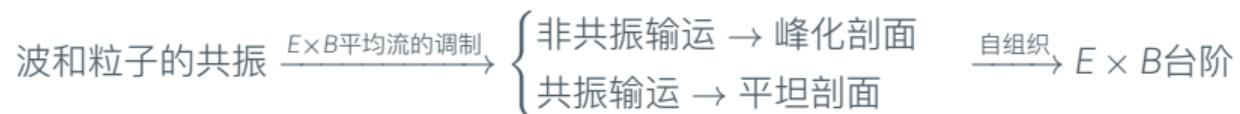
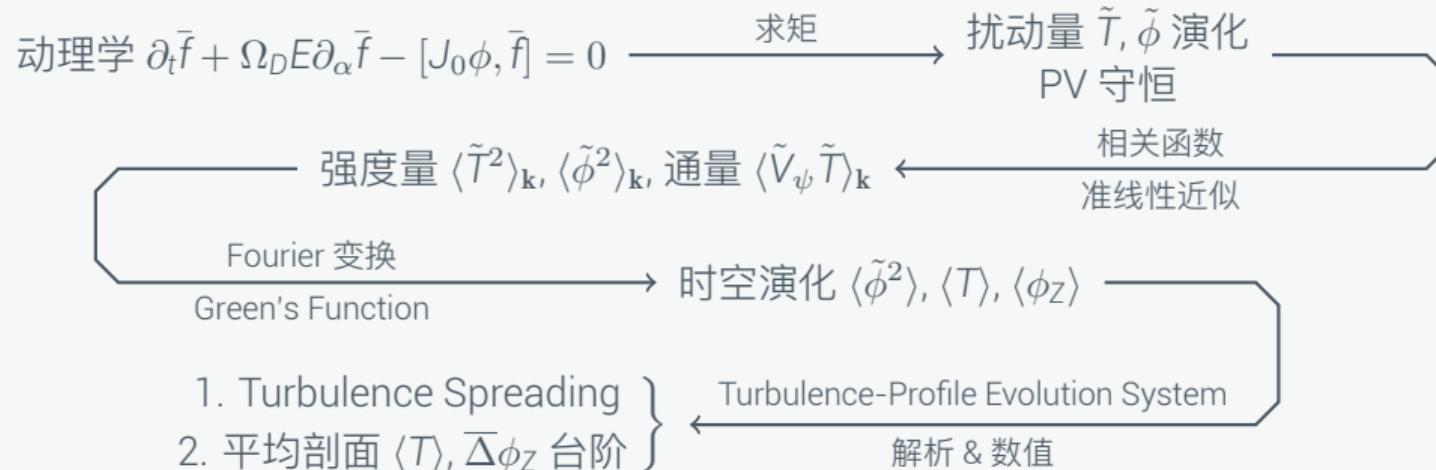
3 湍流-剖面演化系统

4  $E \times B$  台阶

5 总结



## 关于 $E \times B$ 台阶的一个理论：





1 研究背景

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- 势涡守恒系统
- 剖面演化

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对托卡马克中的低频湍流 ( $\omega < \omega_b$ , 回弹频率):  $f(\vec{r}, \vec{p}, t) \xrightarrow[\text{Bounce-average}]{\text{Gyro-average}} \bar{f}(\psi, \alpha, E, t)$ . 其中  $\psi$  磁面坐标,  $\alpha$  环向,  $E$  是能量 [Depret et al., 2000].

$$\begin{cases} \partial_t \bar{f} + \Omega_D E \partial_\alpha \bar{f} - [J_0 \phi, \bar{f}] = 0 \\ n_i = n_e \end{cases} \quad (3)$$

+

其中,  $[F, G] = \partial_\alpha F \partial_\psi G - \partial_\psi F \partial_\alpha G$ .

- $q\phi/T_{eq} \ll 1$ , 平均、绝热和非绝热:

$$\bar{f} = \langle f \rangle - \frac{q_{i,e}\phi}{T_{i,e}} \langle f \rangle + h_{i,e}.$$

- 扰动不响应带状电势:

$$\tilde{n}_{i,e}/n_0 = -q_{i,e}(\phi - \langle \phi \rangle_\alpha)/T_{i,e}$$

非绝热扰动分布函数  $h_i$  和准中性方程如下 (Darmet 模型 [Darmet et al., 2008, Sarazin et al., 2005]):

$$\partial_t h_i + \Omega_D E \partial_\alpha h_i - \left[ \bar{\phi}, -\frac{q}{T_i} (\phi - \langle \phi \rangle_\alpha) \langle f_i \rangle + h_i \right] = \partial_t \left( \frac{q}{T_i} (\phi - \langle \phi \rangle_\alpha) \langle f_i \rangle \right) + \partial_\alpha (\overline{\phi - \langle \phi \rangle_\alpha}) \partial_\psi \langle f_i \rangle \quad (4)$$

$$C_{ad} (\phi - \langle \phi \rangle_\alpha) - C_i \overline{\Delta_{i+e} \phi} = \frac{2}{n_0 \sqrt{\pi}} \int_0^\infty J h_i \sqrt{E} dE - \frac{2}{n_0 \sqrt{\pi}} \int_0^\infty J h_e \sqrt{E} dE \quad (5)$$

其中  $C_i = q/T_i$ ,  $C_{ad} = C_i(1+\tau)/\sqrt{2\varepsilon_0}$ ,  $\tau = T_i/T_{e0}$ ,  $\overline{\Delta_s} = \rho_{0s}^2 \partial_\alpha^2 + \delta_{bs}^2 \partial_\psi^2$ . 可能是 DW 湍流的最小化动理学系统!



涡度演化:

$$\left( \frac{\partial}{\partial t} + \tilde{\mathbf{V}} \cdot \nabla + \Omega_Z \cdot \nabla \right) (C_i \bar{\Delta} \tilde{\phi}) = \frac{3}{2} \Omega_D \partial_y \tilde{T}_i - i C_e (\omega - \omega_E + \frac{\omega_{*n}^i}{\tau}) \tilde{\phi} - C_i \tilde{V}_x \partial_x (\bar{\Delta} \phi_Z) \quad (6)$$

$$\frac{\partial}{\partial t} [C_i \bar{\Delta} \phi_Z] = -C_i \partial_x \langle \tilde{V}_x \bar{\Delta} \tilde{\phi} \rangle_y \quad (7)$$

温度演化:

$$\sqrt{2\varepsilon_0} \left( \partial_t + \tilde{\mathbf{V}} \cdot \nabla + \Omega_Z \cdot \nabla \right) \tilde{T}_i = -i(\omega - \omega_E - \omega_{*n}^i - \omega_{*T}^i) \langle T_i \rangle C_i \tilde{\phi} \quad (8)$$

$$\frac{\partial}{\partial t} (\langle T_i \rangle + \langle T_i \rangle \ln \langle n_i \rangle) = -\sqrt{2\varepsilon_0} \partial_x \langle \tilde{V}_x \tilde{T}_i \rangle_y \quad (9)$$

Notation changed  $(\psi, \alpha) \rightarrow (x, y)$ 

Eq. (6)-(9) 等价于一个势涡 (Potential Vorticity, PV) 演化系统 (忽略密度梯度的贡献)  
 [Yan & Diamond, 2021]:

$$\partial_t \langle q \rangle = -\partial_x \langle \tilde{V}_x \delta q \rangle_y \quad (10)$$

$$\frac{d}{dt} \delta q = -\frac{3}{2} \Omega_D \partial_y \tilde{T}_i - \tilde{\mathbf{V}} \cdot \nabla \langle q \rangle \quad (11)$$

PV  $\langle q \rangle + \delta q$ ,  $\Omega_Z \equiv \partial_x \phi_Z$ .

$$\langle q \rangle = \frac{\tau}{\sqrt{2\varepsilon_0}} \ln \langle T_i \rangle - C_i \bar{\Delta} \phi_Z,$$

$$\delta q = \tau \frac{\tilde{T}_i}{\langle T_i \rangle} - C_i \bar{\Delta} \tilde{\phi}$$

$$\frac{d}{dt} = \frac{\partial}{\partial t} + \tilde{\mathbf{V}} \cdot \nabla + \Omega_Z \cdot \nabla$$

可类比于 Hasegawa-Wakatani 模型。



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$$\begin{aligned}
 \partial_t \ln \langle T \rangle &= -\sqrt{2\varepsilon_0} \partial_x \langle \tilde{V}_x \tilde{T} \rangle_y + \chi_{\text{neo}} \partial_x^2 \ln \langle T \rangle \\
 &\downarrow \\
 \langle \tilde{V}_x \tilde{T} \rangle_k & \\
 &\downarrow \\
 \sim R(\omega - k_y \Omega_Z - b_k \bar{\Omega}_D) \langle \tilde{V}_x^2 \rangle_k [\partial_x \bar{\Delta}\phi_Z(\dots) - \partial_x \ln \langle T \rangle(\dots)] & \\
 &\downarrow \\
 (\chi_4^{\text{non-res}} + \chi_4^{\text{res}}) \partial_x \bar{\Delta}\phi_Z - (\chi_3^{\text{non-res}} + \chi_3^{\text{res}}) \partial_x \ln \langle T \rangle & \\
 &\chi \text{ model} \downarrow \\
 &\text{Equation (22)}
 \end{aligned}$$

$$\begin{aligned}
 \partial_t [\bar{\Delta}\phi_Z] &= -\underbrace{\partial_x \langle \tilde{V}_x \bar{\Delta}\tilde{\phi} \rangle_y}_{\langle \tilde{V}_x \bar{\Delta}\tilde{\phi} \rangle_k} + \nu_c \partial_x^2 \bar{\Delta}\phi_Z \\
 &\downarrow \\
 \langle \tilde{V}_x \bar{\Delta}\tilde{\phi} \rangle_k &= -\langle \tilde{V}_x \delta q \rangle_k + \langle \tilde{V}_x \tilde{T} \rangle_k \\
 &\downarrow \\
 R(\omega - k_y \Omega_Z) R(\omega - k_y \Omega_Z - k_y b_k \bar{\Omega}_D) \langle \tilde{V}_x^2 \rangle_k \partial_x \ln \langle T \rangle(\dots) & \\
 -R(\omega - k_y \Omega_Z - k_y b_k \bar{\Omega}_D) \langle \tilde{V}_x^2 \rangle_k \partial_x \bar{\Delta}\phi_Z(\dots) & \\
 &\downarrow \\
 \chi_1^{\text{non-res}} \frac{\partial_x \ln \langle T \rangle}{\sqrt{2\varepsilon_0}} - (\chi_2^{\text{non-res}} + \chi_2^{\text{res}}) \partial_x \bar{\Delta}\phi_Z & \\
 &\chi \text{ model} \downarrow \\
 &\text{Equation (21)}
 \end{aligned}$$

$$\tilde{T}_k = R(\dots) [\partial_x \bar{\Delta}\phi_Z(\dots) - \partial_x \ln \langle T \rangle(\dots)] \tilde{V}_x(k)$$

$$\delta q_k = R(\omega - k_y \Omega_Z) [\tilde{T}_k(\dots) - \partial_x \langle q \rangle(\dots)] \tilde{V}_x(k)$$

$$C_i \bar{\Delta}\tilde{\phi} = \tau \tilde{T} - \delta q$$

$$\chi_3 = \Re \sum_k [\tilde{V}_x(k)]^2 \frac{i}{\omega - k_y (\Omega_Z + b_k \bar{\Omega}_D)}$$

- 温度 and 涡度 梯度同时出现在热通量和涡量通量中<sup>2</sup>

- $\omega = \omega_R + i\gamma \Rightarrow$  分离共振和非共振贡献
- 共振输运只出现在涡量通量中

<sup>2</sup>Connections to Ref. [Heinonen & Diamond, 2020]



数值求解色散函数并近似:  $\omega_R = \frac{R_1 k_y \Omega_D}{1 + R_2(\rho^2 k_y^2 + \delta^2 k_x^2)} \simeq R k_y \Omega_D$ ,  $R \approx 2.36$ .

$$\chi_3^{\text{res}} = \sum_k \left[ \tilde{V}_x(k) \right]^2 \pi \delta(\dots) \leftarrow \delta \left( \omega_R - k_y \Omega_Z - \frac{C_i \bar{\Omega}_D k_y}{\tau + \sqrt{2\epsilon_0} (\delta^2 k_x^2 + \rho^2 k_y^2)} \right) \quad (12)$$

共振发生:  $\omega_R$  (TIM),  $E \times B$  mean flow  $\Omega_Z$ , trapped ion precession  $\Omega_D$ . "Wave=Particle+Flow"

$$\Theta_{\text{res}} \equiv \delta^2 k_{x,\text{res}}^2 + \rho^2 k_{y,\text{res}}^2 \quad (13)$$

$$\Theta_{\text{max}} \equiv \delta^2 k_{x,\text{max}}^2 + \rho^2 k_{y,\text{max}}^2 \lesssim 1 \quad (14)$$

其中  $C_i \bar{\Omega}_D = 3\Omega_D/2$ ,  $\Omega_Z = \partial_x \phi_Z$ .

$$\Theta_{\text{res}} = \frac{\Omega_D(R\tau - 1.5) - \tau \Omega_Z}{\sqrt{2\epsilon_0} (\Omega_Z - R\Omega_D)} \quad (15)$$

只需  $\Omega_Z/\Omega_D \sim 1 - 1.5$ , 则存在  $k_x, k_y$  满足共振条件!

共振条件转化为要求  $1 \lesssim \Omega_Z/\Omega_D \lesssim 1.5 \implies$  共振条件!

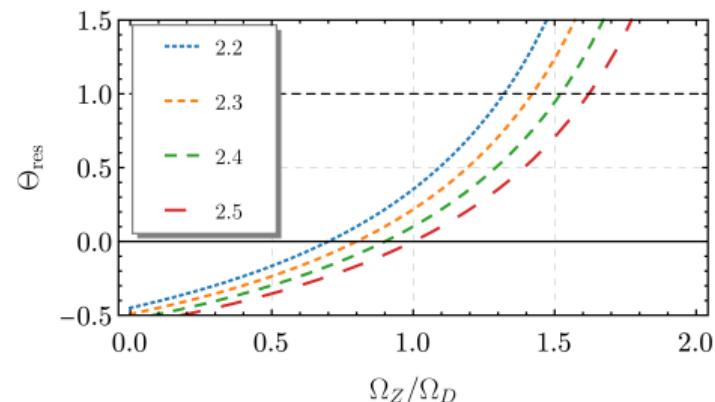


Fig. 5:  $\Theta_{\text{res}}$  和  $\Omega_Z$  的关系。 $\Theta_{\text{res}}$  的定义决定其取值在 0 和 1 之间, 这对应  $\Omega_Z/\Omega_D$  需要在大概 1 到 1.5 之间。不同线对应的  $R$  略有不同。



色散关系模型:

$$\omega_R = R k_y \Omega_D, \quad \gamma = \gamma_0 R \Omega_D k_y (k_{y,\max} - k_y) \quad (16)$$

其中实频率正比于  $k_y$ ; 增长率近似模型中参数  $\Lambda \sim \rho/\sigma, k_{y,\max} = 1/(\mu_y \rho), \mu_y^2 \sigma^2 \sim 10$

$$\chi_3^{\text{non-res}} = \sum_k \frac{[\tilde{V}_x(k)]^2 |\gamma|}{|\omega - k_y \Omega_Z - k_y b_k \bar{\Omega}_D|^2} \sim \frac{|\tilde{\phi}_0|^2 \mu^2 \sigma^2}{\Omega_D \rho [(\mu^2 \sigma^2 + 1 + \beta^2)^2]} \quad (18)$$

$$\chi_3^{\text{res}} = \sum_k [\tilde{V}_x(k)]^2 \pi \delta(\omega_R - k_y \Omega_Z - k_y b_k \bar{\Omega}_D) \sim \frac{|\tilde{\phi}_0|^2 k_{y,\text{res}}^2 \beta^2}{\beta^2 + \mu^2 \Theta_{\text{res}}} \frac{\mu_y \rho}{|\beta_y (\Omega_Z + \Omega_D)|} \quad (19)$$

$$\chi^r / \chi^n \sim \frac{(\mu^2 \sigma^2 + 1 + \beta^2)^2}{\mu^2 \sigma^2} \sim \mathcal{O}(10) - \mathcal{O}(10^2)$$

$$\sim \frac{1}{\Lambda^2 k_{y,\max}^2} \sim \frac{\Omega_D^2}{\Lambda^2 \Omega_D^2 k_{y,\max}^2} \sim \frac{\omega_R^2}{\gamma^2} \quad (20)$$

设谱分布函数满足 Lorentz 分布 [Diamond et al., 2010]:

$$|\tilde{\phi}|_{k_x, k_y}^2 = \frac{|\tilde{\phi}_0|^2}{\pi^2 \Delta k_x \Delta k_y} \frac{1}{\left[1 + \left(\frac{k_x - k_{x0}}{\Delta k_x}\right)^2\right] \left[1 + \left(\frac{k_y - k_{y0}}{\Delta k_y}\right)^2\right]} \quad (17)$$

Define

- $\chi_3^{\text{non-res}} \equiv \chi^n |\tilde{\phi}_0|^2$
- $\chi_3^{\text{res}} \equiv \chi^r |\tilde{\phi}_0|^2$

共振和非共振输运之间的比例大概为实频率和增长率之比的平方。构造一个关于  $\Omega_Z$  的分段函数模型  $\chi \equiv (\chi^n + \chi^r) |\tilde{\phi}_0|^2$ 。

$$\text{Eq.(6): } \tilde{U} \equiv \tilde{\phi} - \overline{\Delta} \tilde{\phi} \rightarrow \text{Eq.(36): } \partial_t \langle \tilde{U}^2 \rangle \xrightarrow{\text{Green's function}} \langle \tilde{\phi}^2 \rangle \sim |\tilde{\phi}_0|^2$$



$$\frac{\partial}{\partial t} (\bar{\Delta}\phi_Z) = -\frac{\partial}{\partial x} \left( \frac{1}{C_i} \vartheta \chi^n \frac{\partial}{\partial x} \frac{\ln \langle T \rangle}{\sqrt{2\varepsilon_0}} \right) + \frac{\partial}{\partial x} \left[ \vartheta \chi \frac{\partial}{\partial x} (\bar{\Delta}\phi_Z) \right] + \nu \frac{\partial^2}{\partial x^2} \bar{\Delta}\phi_Z \quad (21)$$

$$\frac{\partial}{\partial t} \ln \langle T \rangle = -\frac{\partial}{\partial x} \left[ C_i \sqrt{2\varepsilon_0} (1 - \vartheta) \chi \frac{\partial}{\partial x} (\bar{\Delta}\phi_Z) \right] + \frac{\partial}{\partial x} \left[ \chi \frac{\partial}{\partial x} \ln \langle T \rangle \right] + \chi_{\text{neo}} \frac{\partial^2 \ln \langle T \rangle}{\partial x^2} \quad (22)$$

边界条件

$$\frac{\partial}{\partial x} \bar{\Delta}\phi_Z \Big|_B = 0 \quad (23)$$

$$\frac{\partial}{\partial x} \ln \langle T \rangle \Big|_B \equiv \kappa_T^B = \text{Const.} \quad (24)$$

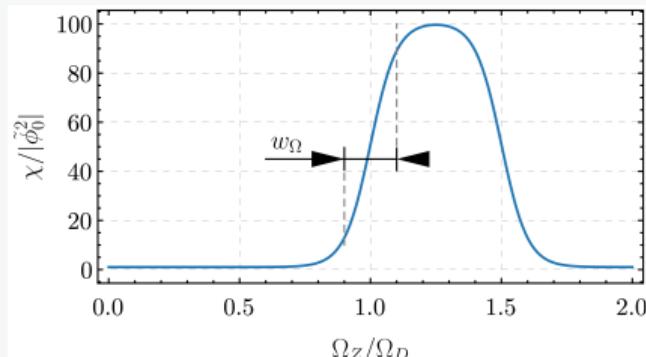
$$\frac{\partial}{\partial x} \langle \tilde{U}^2 \rangle \Big|_B = 0, \quad \text{or} \quad \frac{\partial}{\partial x} \langle \tilde{\phi}^2 \rangle \Big|_B = 0 \quad (25)$$

And:  $\Omega_Z = \partial_x \phi_Z$ , set B.C. for  $\Omega_Z$  as:

$$\Omega_Z \Big|_B = 0 \quad (26)$$

Flux-driven System

分段输运系数模型  $\chi \equiv (\chi^n + \chi^r)|\tilde{\phi}_0|^2$



Eq. (21), (22), (36) + 边界条件 (23-26) + 输运系数模型  $\Longrightarrow E \times B$   
台阶演化系统



## 1 研究背景

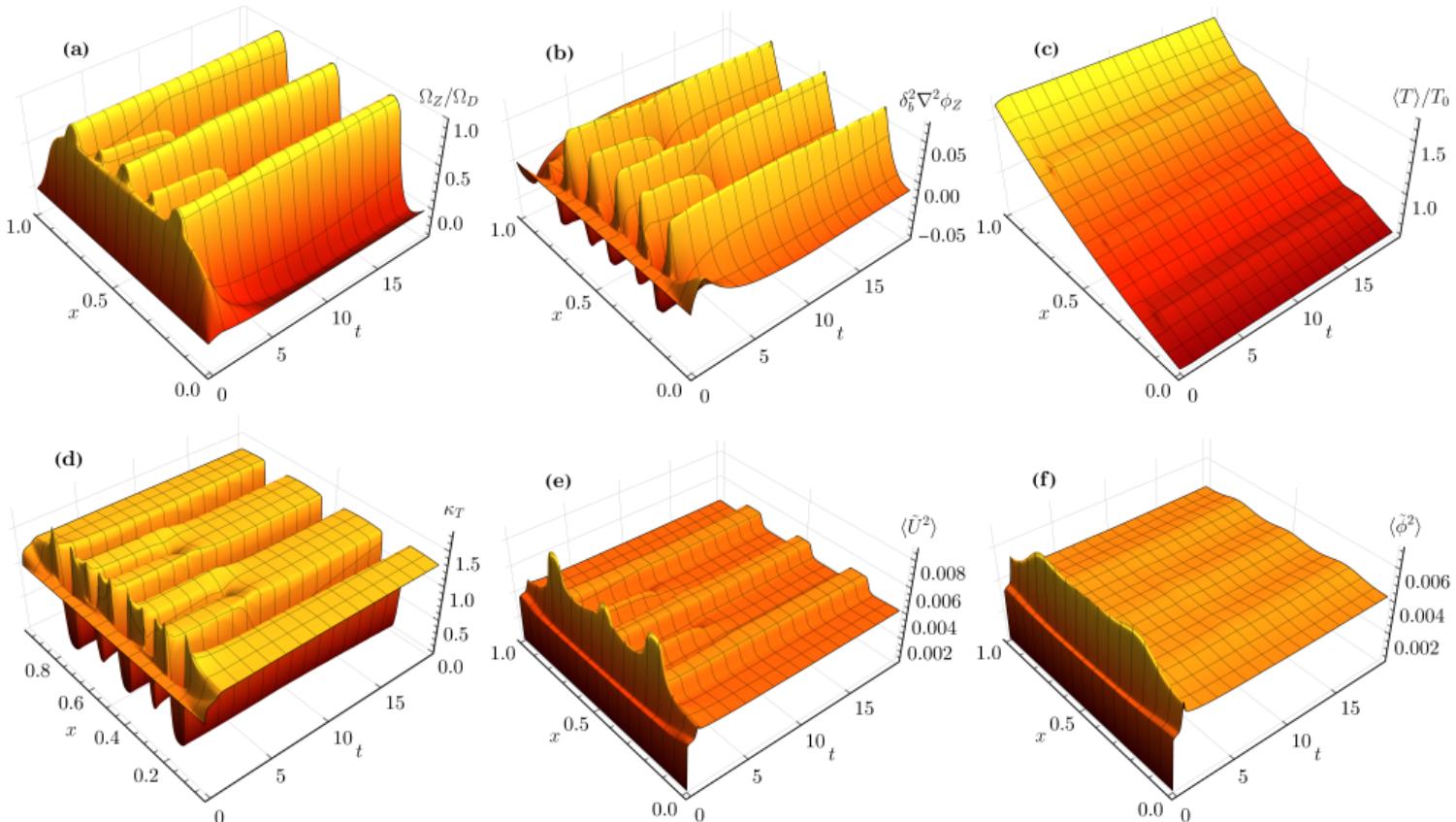
## 2 研究路线

## 3 湍流-剖面演化系统

## 4 $E \times B$ 台阶

- 数值结果
- 两种状态和两种反馈循环
- 台阶的触发
- 台阶宽度

## 5 总结



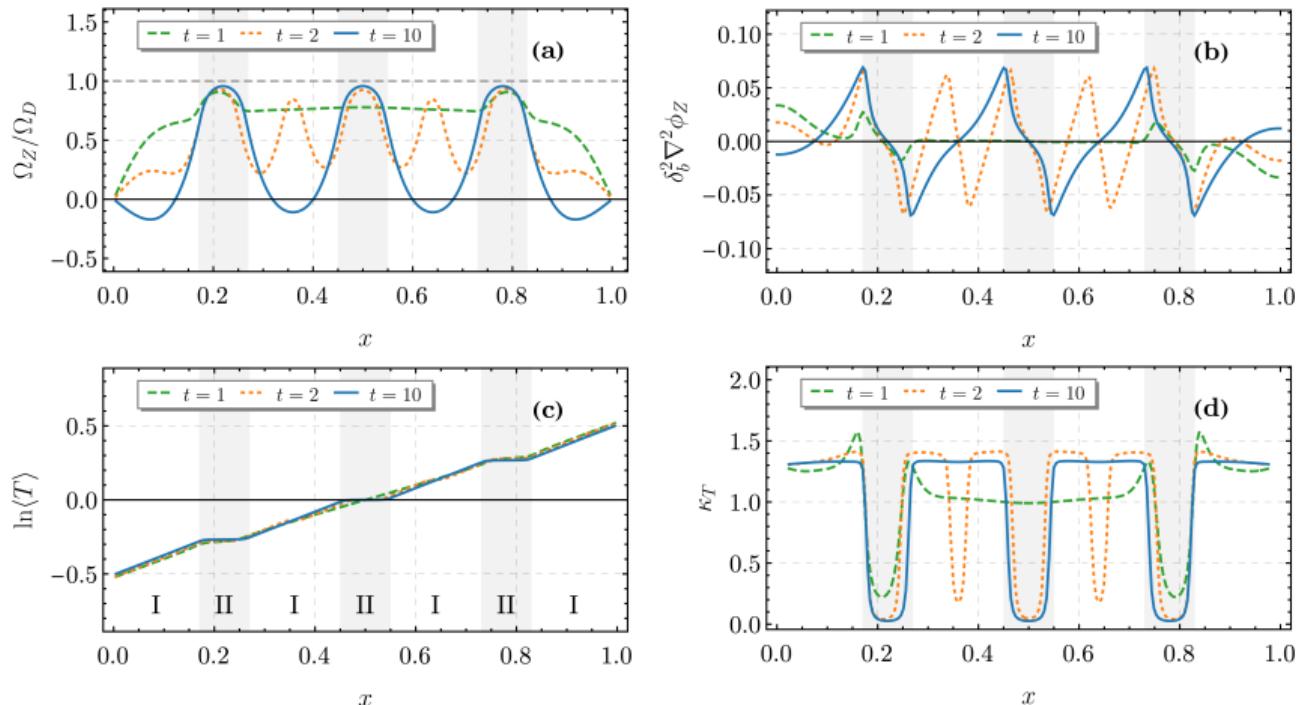


Fig. 6: 剖面演化。如 (c) 所示, 将温度剖面几乎平坦的这些区域命名为 II-区, 区域内平均涡量的剖面较平, 同时由图 (a) 可知这些区域对应的  $\Omega/\Omega_D$  高于了共振输运所需的阈值。所以在 II-区, 共振输运占主导; 与此同时在 I-区, 剖面较为陡峭, 非共振输运占主导。



$$\frac{\partial}{\partial t} (\delta_b^2 \Omega_Z) = -\frac{1}{C_i} \vartheta \chi^n \frac{\partial}{\partial x} \frac{\ln \langle T \rangle}{\sqrt{2\varepsilon_0}} + \underbrace{\frac{1}{C_i} \left( \vartheta \chi^n \frac{\partial}{\partial x} \frac{\ln \langle T \rangle}{\sqrt{2\varepsilon_0}} \right)}_{\text{Drive Source}} \Big|_B + \vartheta \chi(\Omega_Z) \delta_b^2 \frac{\partial^2}{\partial x^2} \Omega_Z + \nu_c \delta_b^2 \frac{\partial^2}{\partial x^2} \Omega_Z$$

I: Local Gradient Balanced      II: Resonant Dissipation Balanced

2 feedback loops  
 ↓  
 2 profile states emergent in space  
 ↓  
 Staircase involving resonant transport!

准稳态  $\Omega_Z \rightarrow$  需平衡边界驱动  $\kappa_T^B$ :

### I 局域梯度 $\kappa_T(t, x) \equiv \partial_x \ln \langle T \rangle$

- $\Omega_Z / \Omega_D < 1$ , 通常的湍流输运
- $C_i = q\omega_0 L_\psi / T_{i, eq} \ll 1$ ,  $\kappa_T$  起主要作用, 且
$$\kappa_T|_{(t,x)} \sim (1 - e^{-t/\tau_{\nabla T}}) \kappa_T^B, \quad \tau_{\nabla T} \sim 1/(\pi^2 \chi^n m^2)$$
- $\kappa_T^B - \kappa_T(t, x)$  残余部分由  $\chi^n + \nu_c$  平衡
- 陡峭的温度剖面

### II $\Omega_Z$ 的共振输运

- $\Omega_Z \gtrsim \Omega_D$  触发 Eq.(22) 和 (21) 中的共振输运
- 温度梯度仅有非共振贡献  $\chi^n$
- $\kappa_T^B \rightleftharpoons \Omega_Z$  的共振输运
- $\kappa_T(x, t) \Rightarrow$  平坦  $\Rightarrow$  Near Marginal (Hypothesis)

$$\frac{\partial}{\partial t} (\delta_b^2 \Omega_Z) = -\frac{1}{C_i} \vartheta \chi^n \frac{\partial}{\partial x} \frac{\ln \langle T \rangle}{\sqrt{2\varepsilon_0}} + \left. \frac{1}{C_i} \left( \vartheta \chi^n \frac{\partial}{\partial x} \frac{\ln \langle T \rangle}{\sqrt{2\varepsilon_0}} \right) \right|_B + \vartheta \chi \delta_b^2 \frac{\partial^2}{\partial x^2} \Omega_Z + \nu_c \delta_b^2 \frac{\partial^2}{\partial x^2} \Omega_Z$$

$$\frac{\partial}{\partial t} \ln \langle T \rangle = -\frac{\partial}{\partial x} \left[ \sqrt{2\varepsilon_0} C_i (1 - \vartheta) \chi \frac{\partial}{\partial x} (\Delta \phi_Z) \right] + \frac{\partial}{\partial x} \left[ \chi \frac{\partial}{\partial x} \ln \langle T \rangle \right] + \chi_{\text{neo}} \frac{\partial^2}{\partial x^2} \ln \langle T \rangle$$

Main Balance

①   ⑤  
④   ②  
③

台阶模式如何涌现?

$(x_1, x_2) \in \text{Feedback loop II} \Rightarrow \text{Heat flux } \uparrow$



$(x_1, x_2)$  的邻域:  $\kappa_T(t, x) > \kappa_T^B$



邻域  $\in \text{Feedback loop I}$



触发共振输运  $\rightarrow$  台阶模式自发形成

## II-区中的反馈循环

- ①  $\partial_x \ln \langle T \rangle|_B$  驱动  $\Omega_Z$  增长
- 若  $\Omega_Z \gtrsim \Omega_D$ , 共振输运触发  $\chi^r$ ,  
② 流的输运和③ 局域温度的输运  
都被增强
- ④ 局域温度梯度变缓 flattened +  
非共振输运。 $\kappa_T(t, x) \downarrow$
- 边界热流驱动的作用更强  
 $(\kappa_T^B - \kappa_T(t, x)) \uparrow$
- ⑤ 在第②步中增强的  $\Omega_Z$  的输运  
可以平衡驱动的增长
- 最终,  $\Omega_Z$  达到准稳态

$$\frac{\partial}{\partial t} (\delta_b^2 \Omega_Z) = -\frac{1}{C_i} \vartheta \chi^n \frac{\partial}{\partial x} \frac{\ln \langle T \rangle}{\sqrt{2\varepsilon_0}} + \frac{1}{C_i} \left( \vartheta \chi^n \frac{\partial}{\partial x} \frac{\ln \langle T \rangle}{\sqrt{2\varepsilon_0}} \right) \Big|_B + \vartheta \chi \delta_b^2 \frac{\partial^2}{\partial x^2} \Omega_Z + \nu_c \delta_b^2 \frac{\partial^2}{\partial x^2} \Omega_Z$$

Main Balance

①   ⑤

④   ②

③

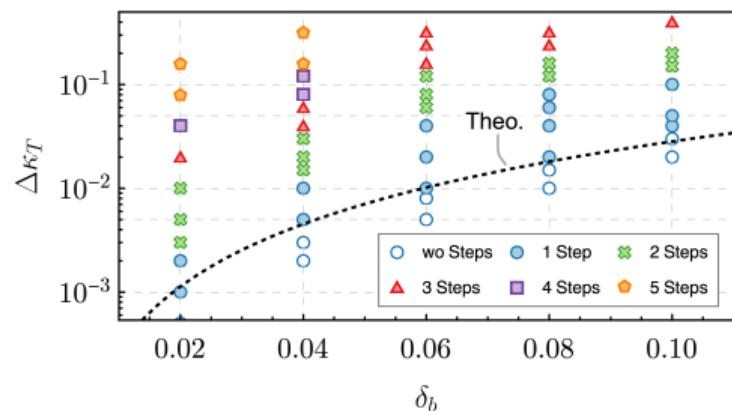
$$\frac{\partial}{\partial t} \ln \langle T \rangle = -\frac{\partial}{\partial x} \left[ \sqrt{2\varepsilon_0} C_i (1 - \vartheta) \chi \frac{\partial}{\partial x} (\bar{\Delta} \phi_Z) \right] + \frac{\partial}{\partial x} \left[ \chi \frac{\partial}{\partial x} \ln \langle T \rangle \right] + \chi_{\text{neo}} \frac{\partial^2}{\partial x^2} \ln \langle T \rangle$$

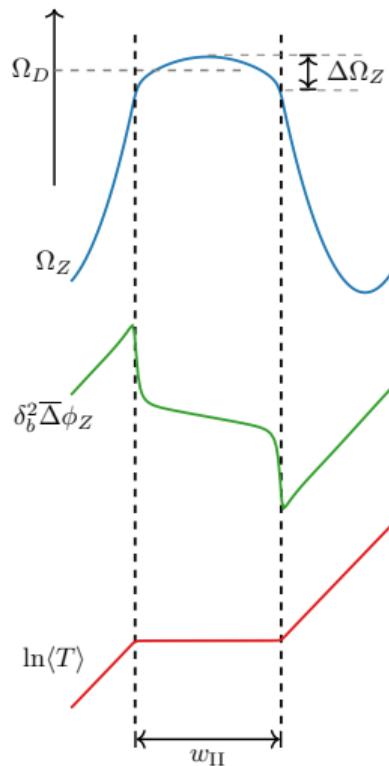
### 影响台阶模式的因素

- 触发所需的边界热通量阈值  $\Delta \kappa_T^{\text{crit}}$
- 对我们的系统做数值扫描，结果显示符合理论给出的阈值
- 更小的  $\delta_b$ , 更小的触发临界值
- 相同参数下, 更强的净驱动  $\Rightarrow$  更多台阶

需要边界热流  $\kappa_T^B$  足够强  $\rightarrow$  在局域温度梯度达到边界值之前,  $\Omega_Z$  抵达共振阈值条件!

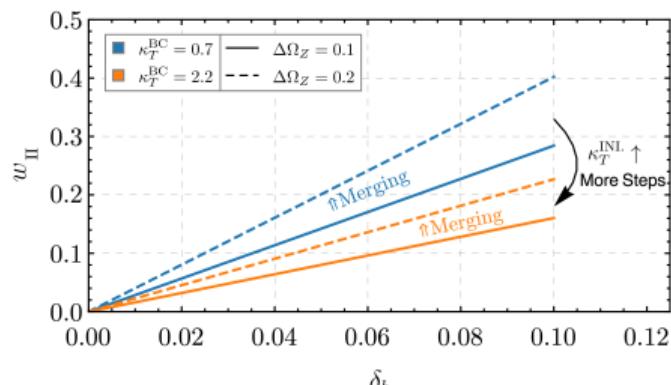
$$\kappa_T \Big|_B - \kappa_T \Big|_I > \Delta \kappa_T^{\text{crit}} \equiv C_i \Omega_D \frac{8 \delta_b^2 \sqrt{2\varepsilon_0}}{\vartheta} \quad (27)$$





基于  $\Omega_Z$  在 II-区的平衡:  $\left( \frac{1}{C_i} \chi^n \frac{\partial}{\partial x} \frac{\ln\langle T \rangle}{\sqrt{2\varepsilon_0}} \right) \Big|_B \sim \chi \delta_b^2 \frac{\partial^2}{\partial x^2} \Omega_Z$ 。定义了  $\Omega_Z^{\text{Max}} - \Omega_Z^{\text{Crit}}$  为  $\Delta\Omega_Z$ 。台阶宽度的估计为:

$$w_{II} \sim 2 \sqrt{\frac{\Delta\Omega_Z}{K_{II}}} \sim 2\delta_b \sqrt{\Delta\Omega_Z \frac{\chi^r}{\chi^n} \frac{C_i \sqrt{2\varepsilon_0}}{\kappa_T^B}} \quad (28)$$

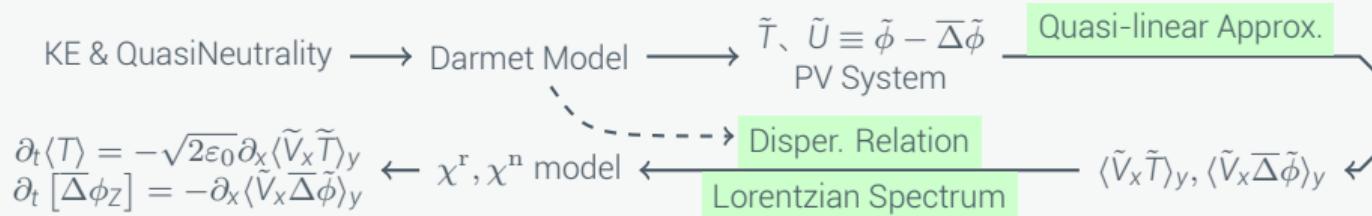


台阶宽度决定于:

- $\propto \delta_b$
- $\chi^r / \chi^n \sim \mathcal{O}(10) - \mathcal{O}(100)$
- 边界梯度 (通量), 越陡峭越窄
- 宽度越窄, 台阶数量上限越高
- 更强的驱动, 更多的台阶



## 湍流-剖面演化系统



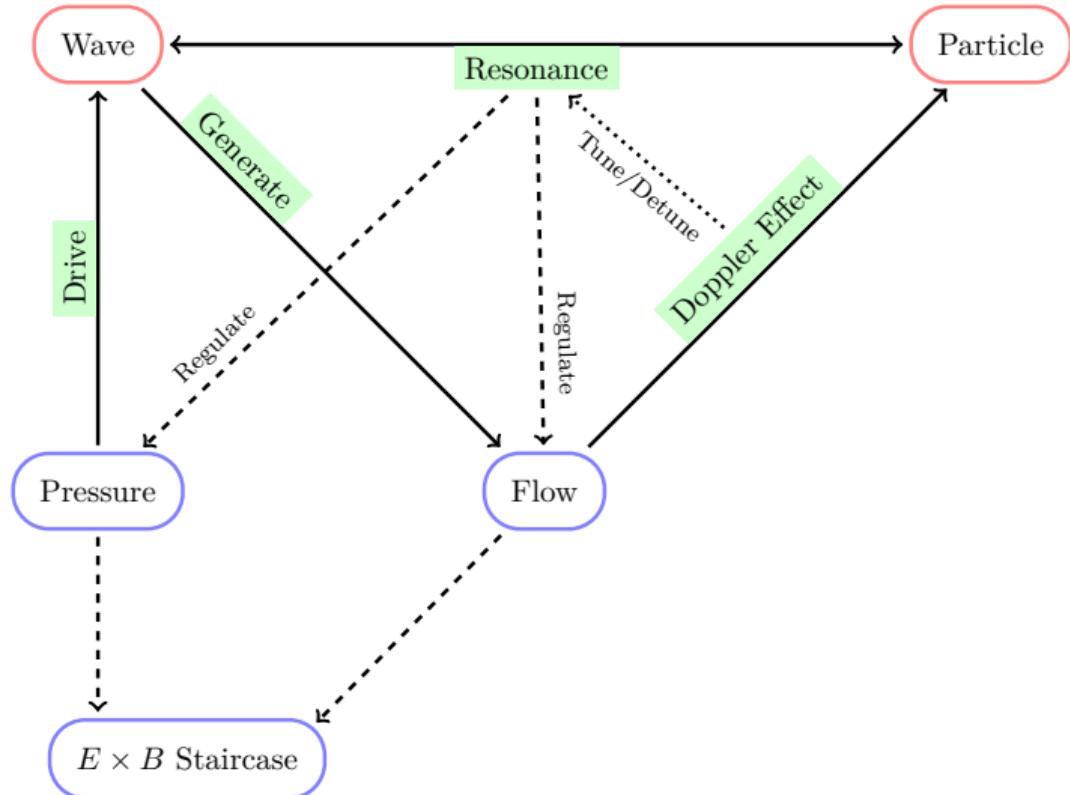
## 剖面模式 (pattern) – $E \times B$ 台阶

- 共振: “Wave + Particle + Flow”
- 涡度通量中仅温度梯度的非共振贡献
- 流结构  $\Omega_Z$  调制剖面状态:
  - 非共振态: 陡峭的温度剖面
  - 共振态: (hypothesized) Near-marginal 温度剖面
- 触发台阶的边界热通量条件  $\Delta\kappa_T^{\text{crit}}$
- 台阶宽度决定于:  $\delta_b, \chi^r/\chi^n, \kappa_T^B$

## 可能的应用

- ZF 的无碰撞饱和 [Li & Diamond, 2018]
- 模型推广到快离子和湍流相互作用
- ITB, F-ATB?
- kinetic DW 湍流中自组织和模式形成的范式?

[Yan & Diamond, 2022]





Thank You!  
Thank You!



## 1 研究背景

## 2 研究路线

## 3 湍流-剖面演化系统

- 势涡守恒系统
- 剖面演化

## 4 $E \times B$ 台阶

- 数值结果
- 两种状态和两种反馈循环
- 台阶的触发
- 台阶宽度

## 5 总结



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Quasi-linear expressions for Fluctuation quantities.

$$\left( \frac{\partial}{\partial t} + \Omega_Z \cdot \nabla \right) \left( A \tilde{\phi} - \bar{\Delta} \tilde{\phi} \right) - \tilde{V} \cdot \nabla \left( \bar{\Delta} \tilde{\phi} \right) = -\bar{\Omega}_D \partial_y \tilde{T} + \delta_b^2 \tilde{V}_x \partial_x^3 \phi_Z \quad (29)$$

$$\left( \frac{\partial}{\partial t} + ik_y \Omega_Z \right) \tilde{\phi}_k = \frac{1}{A + \bar{k}_\perp^2} \sum_{\mathbf{k} + \mathbf{p} + \mathbf{q} = \mathbf{0}} \hat{z} \cdot \mathbf{p} \times \mathbf{q} (q^2 - p^2) \tilde{\phi}_{\mathbf{p}} \tilde{\phi}_{\mathbf{q}} - \frac{\bar{\Omega}_D}{A + \bar{k}_\perp^2} ik_y \tilde{T}_k - \frac{\delta_b^2 \partial_x^3 \phi_Z}{A + \bar{k}_\perp^2} ik_y \tilde{\phi}_k \quad (30)$$

The second equation above is a direct Fourier transformation of Eq.(29). Similarly for  $\tilde{T}_k$  applying the Fourier Transformation and replacing  $-i(\omega - \omega_Z)\tilde{\phi}$  with fluctuation vorticity equation.

$$\sqrt{2\varepsilon_0} \left( \partial_t + \tilde{\mathbf{V}} \cdot \nabla + \Omega_Z \cdot \nabla \right) \tilde{T}_i = -i(\omega - \omega_Z - \omega_{*n}^i - \omega_{*T}^i) \langle T_i \rangle \frac{q \tilde{\phi}}{\tilde{T}_i} \quad (31)$$

$$\begin{aligned} \frac{\partial}{\partial t} \tilde{T}_k &= \sum_{\mathbf{p} + \mathbf{q} + \mathbf{k} = \mathbf{0}} \hat{z} \cdot \mathbf{p} \times \mathbf{q} \left( \tilde{\phi}_{\mathbf{p}} \tilde{T}_{\mathbf{q}} - \tilde{\phi}_{\mathbf{q}} \tilde{T}_{\mathbf{p}} \right) + \frac{C_i}{\sqrt{2\varepsilon_0}} \frac{1}{A + \bar{k}_\perp^2} \sum_{\mathbf{p} + \mathbf{q} + \mathbf{k} = \mathbf{0}} \hat{z} \cdot \mathbf{p} \times \mathbf{q} (q^2 - p^2) \tilde{\phi}_{\mathbf{p}} \tilde{\phi}_{\mathbf{q}} \\ &\quad - ik_y \tilde{T}_k \left( \Omega_Z + \frac{C_i}{\sqrt{2\varepsilon_0}} \frac{\bar{\Omega}_D}{A + \bar{k}_\perp^2} \right) - \frac{ik_y \tilde{\phi}_k}{\sqrt{2\varepsilon_0}} \left( C_i \frac{\delta_b^2 \partial_x^3 \phi_Z}{A + \bar{k}_\perp^2} - \partial_x \ln \langle T \rangle \right) \end{aligned} \quad (32)$$



QL for fluctuation PV:

$$\delta q_k = \frac{C_i \bar{\Omega}_D k_y}{\omega - k_y \Omega_Z} \tilde{T}_k - \frac{i \partial_x \langle q \rangle}{\omega - k_y \Omega_Z} \tilde{V}_x(k)$$

Then,

$$\begin{aligned} \langle \tilde{V}_x \delta q \rangle_k &\sim \tilde{V}_x(-k) \delta q_k \\ &= \frac{C_i \bar{\Omega}_D k_y}{\omega - k_y \Omega_Z} \tilde{V}_x(-k) \tilde{T}_k - \frac{i \partial_x \langle q \rangle}{\omega - k_y \Omega_Z} \tilde{V}_x(-k) \tilde{V}_x(k) \\ &= \frac{k_y}{\omega - k_y \Omega_Z} C_i \bar{\Omega}_D \langle \tilde{V}_x \tilde{T} \rangle_k - \frac{i}{\omega - k_y \Omega_Z} \langle \tilde{V}_x^2 \rangle_k \partial_x \langle q \rangle \\ &= \frac{k_y}{\omega - k_y \Omega_Z} C_i \bar{\Omega}_D \langle \tilde{V}_x \tilde{T} \rangle_k - \frac{i}{\omega - k_y \Omega_Z} \langle \tilde{V}_x^2 \rangle_k \left( \frac{1}{\sqrt{2\varepsilon_0}} \partial_x \ln \langle T \rangle - C_i \delta_b^2 \partial_x^3 \phi_z \right) \end{aligned}$$



$$\delta q = \tau \tilde{T} - C_i \bar{\Delta} \tilde{\phi}$$

$$\langle \tilde{V}_x \bar{\Delta} \tilde{\phi} \rangle =$$

$$\begin{aligned} \langle \tilde{V}_x \tilde{T} \rangle_k - \langle \tilde{V}_x \delta q \rangle_k &= \left(1 - \frac{k_y}{\omega - k_y \Omega_Z} C_i \bar{\Omega}_D\right) \langle \tilde{V}_x \tilde{T} \rangle_k + \frac{i}{\omega - k_y \Omega_Z} \langle \tilde{V}_x^2 \rangle_k \left(\frac{1}{\sqrt{2\varepsilon_0}} \partial_x \ln \langle T \rangle - C_i \delta_b^2 \partial_x^3 \phi_Z\right) \\ &= \frac{\omega - k_y \Omega_Z - k_y C_i \bar{\Omega}_D}{\omega - k_y \Omega_Z} \frac{i}{\omega - k_y \left(\Omega_Z + \frac{C_i}{\sqrt{2\varepsilon_0}} \frac{\bar{\Omega}_D}{A + \bar{k}_\perp^2}\right)} \langle \tilde{V}_x^2 \rangle_k \left(\frac{C_i}{\sqrt{2\varepsilon_0}} \frac{\delta_b^2 \partial_x^3 \phi_Z}{A + \bar{k}_\perp^2} - \frac{1}{\sqrt{2\varepsilon_0}} \partial_x \ln \langle T \rangle\right) \\ &\quad + \frac{i}{\omega - k_y \Omega_Z} \langle \tilde{V}_x^2 \rangle_k \left(\frac{1}{\sqrt{2\varepsilon_0}} \partial_x \ln \langle T \rangle - C_i \delta_b^2 \partial_x^3 \phi_Z\right) \\ &= \frac{\partial_x \ln \langle T \rangle}{\sqrt{2\varepsilon_0}} \frac{i k_y \bar{\Omega}_D a_k \langle \tilde{V}_x^2 \rangle_k}{(\omega - k_y \Omega_Z)(\omega - k_y \Omega_Z - k_y b_k \bar{\Omega}_D)} - \delta_b^2 \partial_x^3 \phi_Z \frac{i a_k \langle \tilde{V}_x^2 \rangle_k}{\omega - k_y \Omega_Z - k_y b_k \bar{\Omega}_D} \end{aligned}$$

here,

$$a_k \equiv 1 - \frac{1}{\sqrt{2\varepsilon_0}} \frac{1}{A + \bar{k}_\perp^2} = 1 - \frac{1}{\sqrt{2\varepsilon_0}} \frac{1}{\frac{\tau}{\sqrt{2\varepsilon_0}} + \bar{k}_\perp^2} > 0, \quad b_k \equiv \frac{C_i}{\sqrt{2\varepsilon_0}} \frac{1}{A + \bar{k}_\perp^2}$$



Define:

$$\chi_1 = \Re \sum_k \left[ \tilde{V}_x(k) \right]^2 \frac{i k_y \bar{\Omega}_D a_k}{(\omega - k_y \Omega_Z)(\omega - k_y \Omega_Z - k_y b_k \bar{\Omega}_D)}, \quad \chi_2 = \Re \sum_k \left[ \tilde{V}_x(k) \right]^2 \frac{i a_k}{\omega - k_y \Omega_Z - k_y b_k \bar{\Omega}_D}$$

$\Re$  represents the real part. By decomposition  $\omega = \omega_R + i\gamma$ , we have,

$$\begin{aligned} \chi_1^{\text{non-res}} &= \sum_k \left[ \tilde{V}_x(k) \right]^2 a_k \frac{|\gamma| k_y \bar{\Omega}_D (2\omega_R - 2k_y \Omega_Z - k_y b_k \bar{\Omega}_D)}{|\omega - k_y \Omega_Z|^2 |\omega - k_y \Omega_Z - k_y b_k \bar{\Omega}_D|^2} \\ \chi_1^{\text{res}} &= \sum_k \left[ \tilde{V}_x(k) \right]^2 a_k \frac{k_y \bar{\Omega}_D \pi \delta(\omega - k_y \Omega_Z - k_y b_k \bar{\Omega}_D)}{\omega - k_y \Omega_Z} + \sum_k \left[ \tilde{V}_x(k) \right]^2 a_k \frac{k_y \bar{\Omega}_D \pi \delta(\omega - k_y \Omega_Z)}{\omega - k_y \Omega_Z - k_y b_k \bar{\Omega}_D} \sim 0 \\ \chi_2^{\text{non-res}} &= \sum_k \left[ \tilde{V}_x(k) \right]^2 a_k \frac{|\gamma|}{|\omega - k_y \Omega_Z - k_y b_k \bar{\Omega}_D|^2}, \quad \chi_2^{\text{res}} = \sum_k \left[ \tilde{V}_x(k) \right]^2 a_k \pi \delta(\omega - k_y \Omega_Z - k_y b_k \bar{\Omega}_D) \end{aligned}$$

QL for vorticity flux is:

$$\langle \tilde{V}_x \bar{\Delta} \tilde{\phi} \rangle_y = \chi_1^{\text{non-res}} \frac{\partial_x \ln \langle T \rangle}{\sqrt{2\varepsilon_0}} - (\chi_2^{\text{non-res}} + \chi_2^{\text{res}}) \delta_b^2 \partial_x^3 \phi_Z \quad (33)$$

No temperature gradient contribution in the vorticity flux!

Backing to the profiles evolution, putting all those quasi-linear expression of fluxes, obtains

$$\frac{\partial}{\partial t} (\bar{\Delta}\phi_Z) = -\frac{\partial}{\partial x} \left( \frac{1}{C_i} \chi_1^{\text{non-res}} \frac{\partial}{\partial x} \frac{\ln \langle T \rangle}{\sqrt{2\varepsilon_0}} \right) + \frac{\partial}{\partial x} \left[ (\chi_2^{\text{non-res}} + \chi_2^{\text{res}}) \delta_b^2 \frac{\partial^3}{\partial x^3} \phi_Z \right] + \nu \frac{\partial^2}{\partial x^2} \bar{\Delta}\phi_Z \quad (34)$$

$$\frac{\partial}{\partial t} \ln \langle T \rangle = -\frac{\partial}{\partial x} \left[ C_i (\chi_4^{\text{non-res}} + \chi_4^{\text{res}}) \frac{\partial}{\partial x} (\bar{\Delta}\phi_Z) \right] + \frac{\partial}{\partial x} \left[ (\chi_3^{\text{non-res}} + \chi_3^{\text{res}}) \frac{\partial}{\partial x} \ln \langle T \rangle \right] \quad (35)$$

$$\begin{aligned} \frac{1}{2} \frac{\partial}{\partial t} \langle \tilde{U}^2 \rangle &= \frac{\partial}{\partial x} D_U \frac{\partial}{\partial x} \langle \tilde{U}^2 \rangle - \frac{\bar{\Omega}_D}{\sqrt{2\varepsilon_0}} C_i (\chi_3^{\text{non-res}} + \chi_3^{\text{res}}) \frac{\partial}{\partial x} (\bar{\Delta}\phi_Z) + \frac{\bar{\Omega}_D}{\sqrt{2\varepsilon_0}} (\chi_5^{\text{non-res}} + \chi_5^{\text{res}}) \frac{\partial}{\partial x} \langle T \rangle \\ &\quad - \frac{1}{C_i} \chi_1^{\text{non-res}} \left( \frac{\partial}{\partial x} \frac{\ln \langle T \rangle}{\sqrt{2\varepsilon_0}} \right) \left[ \frac{\partial}{\partial x} (\bar{\Delta}\phi_Z) \right] + (\chi_2^{\text{non-res}} + \chi_2^{\text{res}}) \left[ \frac{\partial}{\partial x} (\bar{\Delta}\phi_Z) \right]^2 - \frac{\nu_{\text{NL}}}{l_x^2} \langle \tilde{U}^2 \rangle^2 \end{aligned} \quad (36)$$

To analyze the evolution, we need further simplification fo coefficients. Take  $\chi_3$  as an example:

$$\chi_3^{\text{non-res}} = \sum_k \left[ \tilde{V}_x(k) \right]^2 \frac{|\gamma|}{|\omega - k_y \Omega_Z - k_y b_k \bar{\Omega}_D|^2}, \quad \chi_3^{\text{res}} = \sum_k \left[ \tilde{V}_x(k) \right]^2 \pi \delta(\omega_R - k_y \Omega_Z - k_y b_k \bar{\Omega}_D)$$

Directing calculating the integral above! Need dispersion relation  $\omega(k)$  and turbulence spectrum  $[\tilde{V}_x(k)]^2$ .



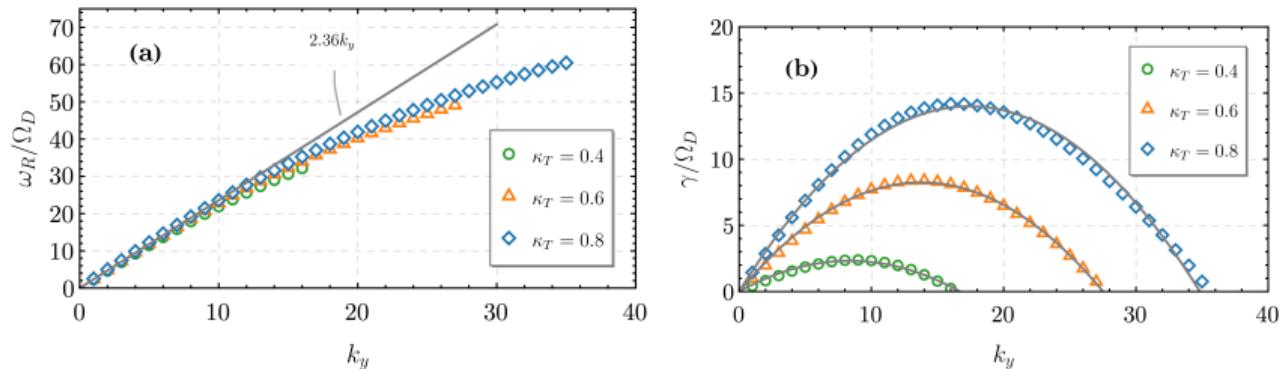
$$\langle \tilde{\phi}^2 \rangle = \int_{-\infty}^{\infty} G_2(x - x') \langle \tilde{U}^2 \rangle(x') dx' \quad (37)$$

here the Green's function is defined as:

$$\begin{aligned} G_2(x) &= \mathcal{F}^{-1} \left\{ \frac{1}{(A + k^2)^2} \right\} \\ &= \frac{1}{2} \sqrt{\frac{\pi}{2A^3}} \left( e^{-\sqrt{A}|x|} + \sqrt{A}|x|e^{-\sqrt{A}|x|} \right) \end{aligned} \quad (38)$$



$$D(k, z \equiv \frac{\omega}{k_y \Omega_D}) = (C_{ad}/C_i) + \rho_{i0}^2 k_y^2 + \delta_{b0}^2 k_x^2 + 2 \left[ z - \frac{\kappa_n}{C_i \Omega_D} \left( 1 - \frac{3\eta_i}{2} \right) \right] [1 + \sqrt{z} Z_p(\sqrt{z})] - \frac{\kappa_T}{C_i \Omega_D} \left[ 1 + 2z + 2z^{3/2} Z_p(\sqrt{z}) \right] \quad (39)$$



Real frequency can be well fit by:

$$\omega_R = \frac{R_1 k_y \Omega_D}{1 + R_2 (\rho^2 k_y^2 + \delta^2 k_x^2)} \quad (40)$$

where  $R_1 \simeq 2.3675$ ,  $R_2 \simeq 0.16 \ll 1$ , so there is  $\omega_R \simeq R k_y \omega_D = 2.36 k_y \omega_D$ . Growth rate can be approximated as:

$$\gamma = \gamma_0 R \Omega_D k_y (k_{y,\max} - k_y) \quad (41)$$

Here  $k_{y,\max}$  varies with  $k_x$ . It can be written as  $k_{y,\max} = 1/(\mu_y \rho)$ . Because  $\Theta_{\max} \lesssim 1$ ,  $\mu_y > 1$ .  $\gamma_0$  varies with  $k_x$  and  $\kappa_T$ . We define  $\sigma = \rho/\sigma$ . Numerical results show that  $\sigma > 1$ .

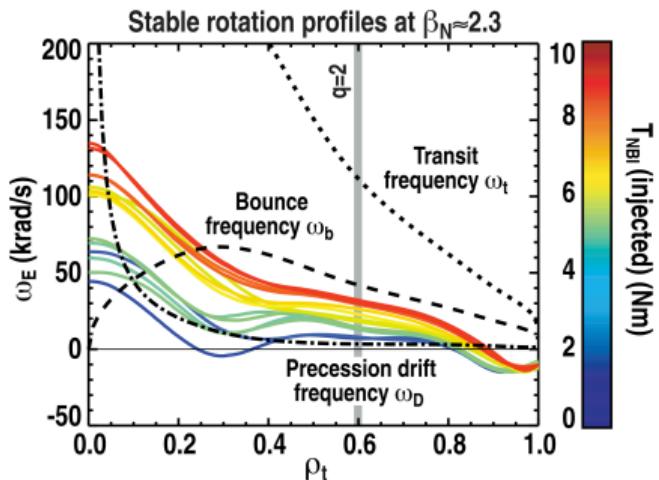


Fig. 7: Trapped ion precession frequency in DIII-D  
[Reimerdes et al., 2011]

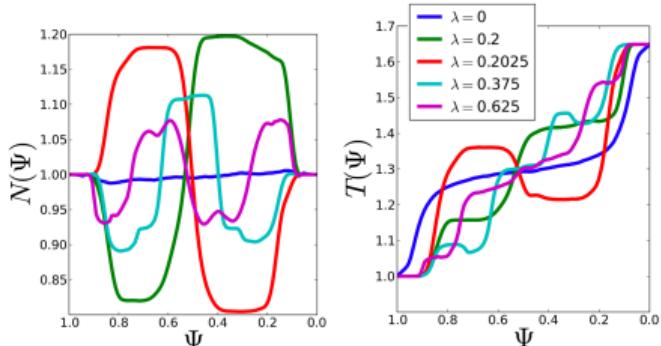


Fig. 8: Cartier-Michaud et al. obtained  $E \times B$  staircase using TERESA [Cartier-Michaud et al., 2014]

Though the Darmet model is simple, it contains the physics for staircase formation.  
Corollary: So does the PV conserving system derived from the Darmet model!

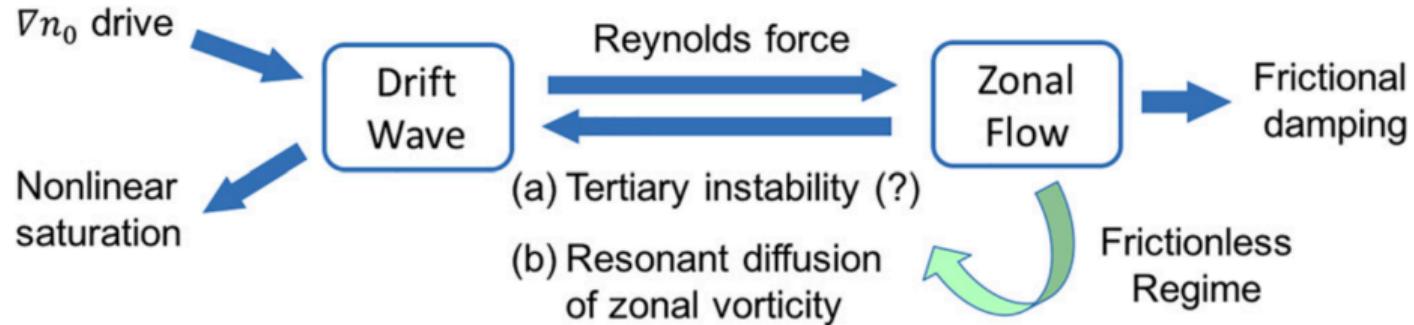
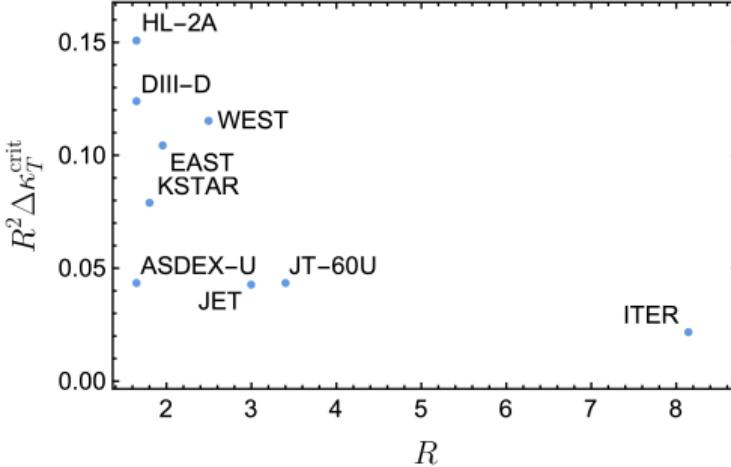
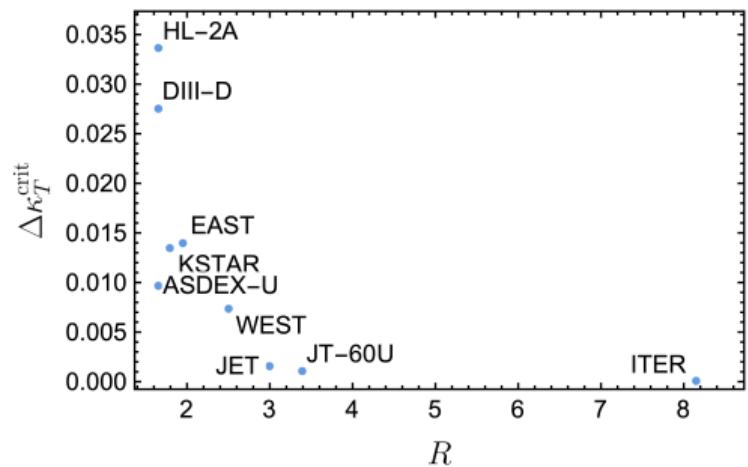


Fig. 9: [Li &amp; Diamond, 2018]



$$\left. \frac{1}{L_T} \right|_{\text{B}} - \left. \frac{1}{L_T} \right|_{\text{I}} < -\frac{8\sqrt{2}}{\vartheta} \frac{1}{R_0} \sqrt{\frac{a}{R_0}} \left( \frac{\delta_b}{a} \right)^2 \quad (42)$$

Assuming  $kT_i = 10 \text{ keV}$ ,



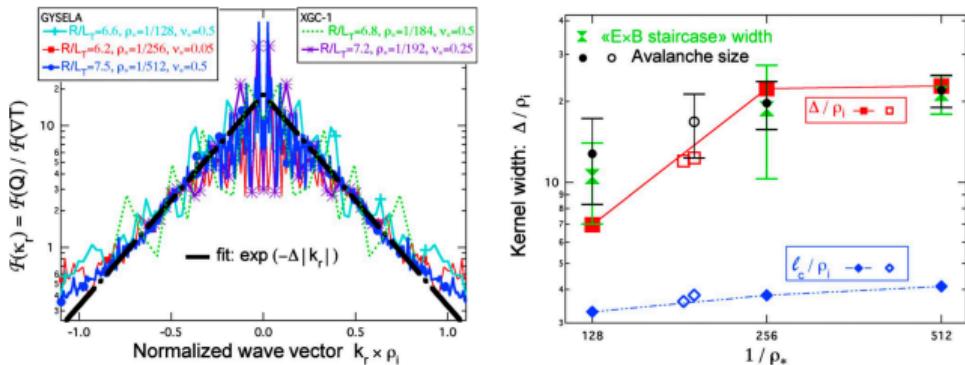
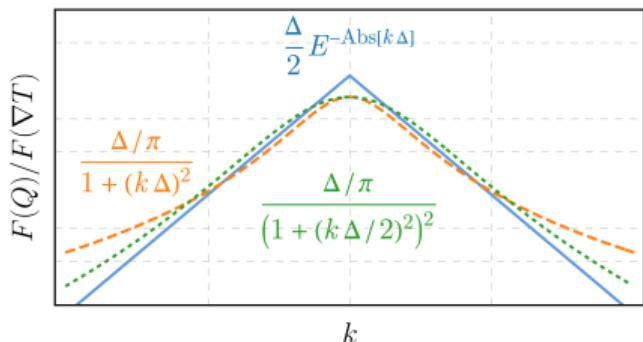


Fig. 10: [Dif-Pradalier et al., 2010]



$$\begin{cases} \mathcal{F}(Q) / \mathcal{F}(\nabla T) \sim \frac{1}{1 + (k\Delta)^2} \\ \mathcal{K}(r, r') = e^{-|r-r'|/\Delta} \end{cases}$$

$$Q(r) = - \int \mathcal{K}(r, r') \nabla T(r') dr'$$

$$\begin{cases} \mathcal{F}(Q) / \mathcal{F}(\nabla T) \sim e^{-\Delta |k|} \\ \mathcal{K}(r, r') = \frac{\Lambda}{\pi} \frac{\Delta/2}{(\Delta/2)^2 + (r - r')^2} \end{cases}$$