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LAB 2. SECOND-ORDER SYSTEM IDENTIFICATION AND ANALYSIS

ASSIGNED DATA

For easily referencing it, the Assigned Data has been placed at the start of this document.

On your pre-lab and post-lab submissions, always include this page at the beginning of the document.

Select your lab session:		<input type="checkbox"/> morning lab; <input checked="" type="checkbox"/> afternoon lab; <input checked="" type="checkbox"/> Tue; <input type="checkbox"/> Wed; <input type="checkbox"/> Thu
CourseBook Group Number		45
Assigned plant number ($Plant\ i = CourseBook\ GroupNumber\ i$)		45
Plant parameters:	a	2
	b	5
	T	100
	K _i	330

The green highlighting present in this document is meant to draw your attention to things that need to be done.

Section 4.1

$T_p(s)$	c_{max} (V)	$c_{ss}(V)$	$T_r(s)$	$T_s(s)$
8.22E-003	1.48	1	3.01E-003	3.364E-002

Table 1: Response specifications - experimental values



Figure 1: Second order underdamped

$T_p(s)$	c_{max} (V)	$c_{ss}(V)$	OS(%)	ζ	$\omega_n(\text{rad/s})$
8.22E-003	1.48	1	48	0.2275	435.68

Table 2: System identification data and results

Calculations for table 2:

Using the formula for overshoot

$$\begin{aligned}
 OS &= e^{\frac{-\zeta\pi}{\sqrt{1-\zeta^2}}} \\
 0.48 &= e^{\frac{-\zeta\pi}{\sqrt{1-\zeta^2}}} \\
 \ln 0.48 &= \frac{-\zeta\pi}{\sqrt{1-\zeta^2}} \\
 \ln^2 0.48 &= \frac{\zeta^2\pi^2}{1-\zeta^2} \\
 \ln^2 0.48 \times (1-\zeta^2) &= \zeta^2\pi^2 \\
 \ln^2 0.48 &= \zeta^2 \times (\pi^2 + \ln^2 0.48) \\
 \zeta &= \sqrt{\frac{\ln^2 0.48}{\pi^2 + \ln^2 0.48}} \\
 \zeta &= 0.2275
 \end{aligned}$$

Using the formula for peak time

$$\begin{aligned}
 T_p &= \frac{\pi}{\omega_n \sqrt{1-\zeta^2}} \\
 \omega_n &= \frac{\pi}{T_p \sqrt{1-\zeta^2}} \\
 \omega_n &= \frac{\pi}{0.00822 \sqrt{1-\zeta^2}} \\
 \omega_n &= \frac{382.93}{\sqrt{1-\zeta^2}} \\
 \omega_n &= \frac{382.93}{\sqrt{1-0.2275}} \\
 \omega_n &= 435.68
 \end{aligned}$$

Discussing Table 2

Prelab values: $\zeta = 0.2462$ $\omega = 406.20$

Experimental values: $\zeta = 0.2275$ $\omega = 435.68$

The experimental values differed from the theoretical values calculated in the prelab by around 8%. Errors may have stemmed from inaccurate graph reading when recording experimental values, or by small rounding errors during mathematical calculations for experimental and theoretical values.

Section 4.2



Figure 2: Open-loop step response with $K=1$

K_p	$T_p(s)$	$y_{max}(V)$	$y_{ss}(V)$	OS(%)
1	8.2E-003	1.48	1	48
1.3	8.17E-003	1.98	1.33	49
1.66	8.27E-003	2.47	1.66	49
2	8.17E-003	2.93	2	47

Table 3: Open-loop step response values for K_p =variable

Discussing Table 3

Peak Value: This increased with K_p . This fits control theory as the peak value is the highest oscillation above the steady state value, since the steady state value is increasing without ζ changing this value should rise as well.

Steady state: As K_p increases the steady state value increases to match the K_p value. This fits with control theory as the output for $G(S)$ has a steady state value of 1, experimentally verified. For the open loop system the output should be equal to $G(S) \times K \times K_p$ (as they are all in series) and since K stayed at 1 for all experiments the output increase was proportional to K_p .

Overshoot and Peak time: These values did not change much. This fits control theory as the equations for overshoot and peak time are proportional to ζ and ω_n which do not vary with K or K_p in the open-loop system.



Figure 3: Closed-loop step response with $K=1$

K_p	$T_p(s)$	$y_{max}(V)$	$y_{ss}(V)$	e_{ss}	OS(%)
1	5.6E-003	0.82	0.5	0.5	64
1.3	5.2E-003	0.93	0.57	0.565	63
1.66	4.92E-003	1.03	0.64	0.615	62
2	4.5E-003	1.12	0.68	0.667	65

Table 4: Closed-loop step response values for K_p =variable

Discussing Table 4

Peak Value and Steady State value: These values are increasing with K_p . Due to control theory our system output with the increase of K_p from 1 is:

$$Y(S) = \frac{K_p H(S)}{1 + K_p H(S)}$$

As K_p increases in the above equation the output will also increase is what causes the increase in the peak value and the steady state value.

Overshoot: The overshoot does not change much. This is due to the steady state and peak value increasing by the same ratio. We can also see that this value will not change because it is related to ζ which has not changed.

Peak Time: The peak time is decreasing as K_p increases. This is due to the peak time being inversely proportional to the natural frequency. In this system the natural frequency was proportional to K_p , so when K_p increases the natural frequency increases which causes the peak time to decrease.

Zeta and Omega Calculations

The new transfer function for the system is:

$$\begin{aligned} H(S) &= \frac{K_i b T K K_p}{s^2 + a T s + K_i b T + K_i b T K_p K} \\ K_p &= 1 \text{ and } K = 1 \\ &= \frac{K_i b T}{s^2 + a T s + 2 K_i b T} \\ &= \frac{1}{2} \times \frac{2 K_i b T}{s^2 + a T s + 2 K_i b T} \end{aligned}$$

This is a standard second order system with a coefficient. Since coefficients carry over during a Laplace transform we can use the equations for a standard second order system with the coefficient.

Based on the definition of standard second order system:

$$\begin{aligned} \omega_n^2 &= 2 K_i b T K K_p \\ \omega_n &= \sqrt{2 K_i b T K K_p} \\ &= \sqrt{2 * 330 * 5 * 100} \\ &= \sqrt{2 * 330 * 5 * 100} \\ &= 574.45 \end{aligned}$$

$$\begin{aligned} a T &= 2 \zeta \omega_n \\ \zeta &= \frac{a T}{2 \omega_n} \\ &= \frac{2 * 100}{2 * 574.45} \\ &= 0.35 \end{aligned}$$

Using the formula for overshoot

$$\begin{aligned} OS &= \frac{1}{2} e^{\frac{-\zeta \pi}{\sqrt{1-\zeta^2}}} \\ \zeta &= \sqrt{\frac{\ln^2 \frac{OS}{2}}{\pi^2 + \ln^2 \frac{OS}{2}}} \\ \zeta &= \sqrt{\frac{\ln^2 \frac{0.64}{2}}{\pi^2 + \ln^2 \frac{0.64}{2}}} \\ \zeta &= 0.34 \end{aligned}$$

Since the peak time formula is found by taking the sinusoidal function is highest, it is not influenced by the added

coefficient so we can use the same function for calculating ω_n . Using the formula for peak time

$$T_p = \frac{\pi}{\omega_n \sqrt{1 - \zeta^2}}$$

$$\omega_n = \frac{\pi}{T_p \sqrt{1 - \zeta^2}}$$

$$\omega_n = \frac{\pi}{0.0056 \sqrt{1 - 0.34^2}}$$

$$\omega_n = 596.76$$

Experimental Open-loop: $\zeta = 0.2275$ $\omega_n = 435.68$

Experimental Closed-loop: $\zeta = 0.34$ $\omega_n = 596.76$

Theoretical Open-loop: $\zeta = 0.2462$ $\omega = 406.20$

Theoretical Closed-loop: $\zeta = 0.35$ $\omega_n = 575.45$

The dampening ratio increased when the loop was closed due to the stabilizing nature of a closed loop. The output is dampened by the subtraction of itself from the input. The transfer function multiplied to natural frequency by 2 which resulted in it increasing by a factor of $\sqrt{2}$.

Adjusted value is $k=1.04$

	Low-freq gain (dB)	Experimental bw (rad/s)	Theor or sim bw (rad/s)	Error (%)
Open-loop	0.5	589	603	2.4
Closed-loop	-5.8	850	869	2.2

Table 5: Bandwidth (bw) measurement results

Closing the loop dramatically increased the measured bandwidth. Bandwidth is defined as the range of frequencies over which the output is relatively close to the input. We want to be able to change bandwidth in order to lessen the amount of disturbance.

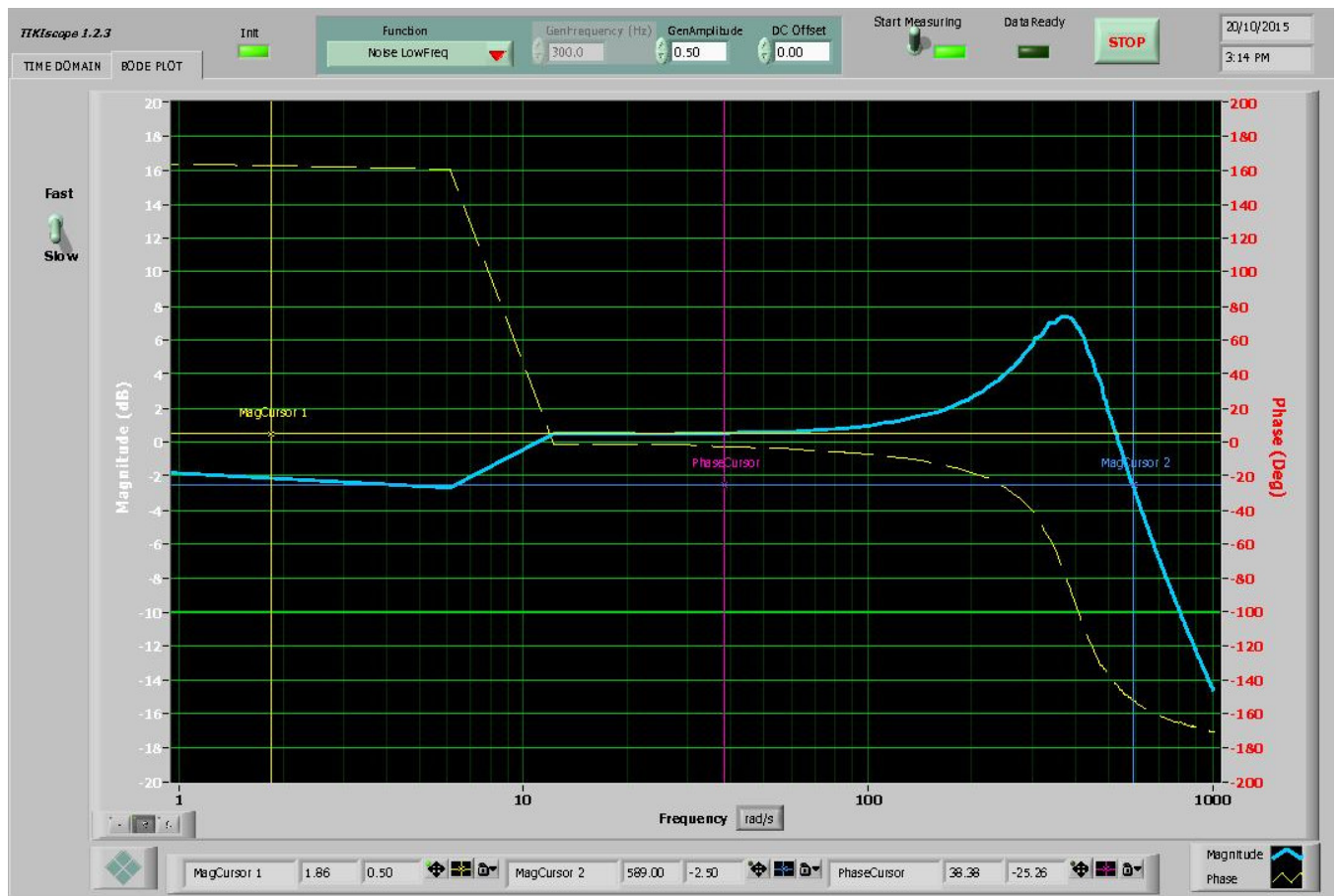


Figure 4: Open-loop frequency response

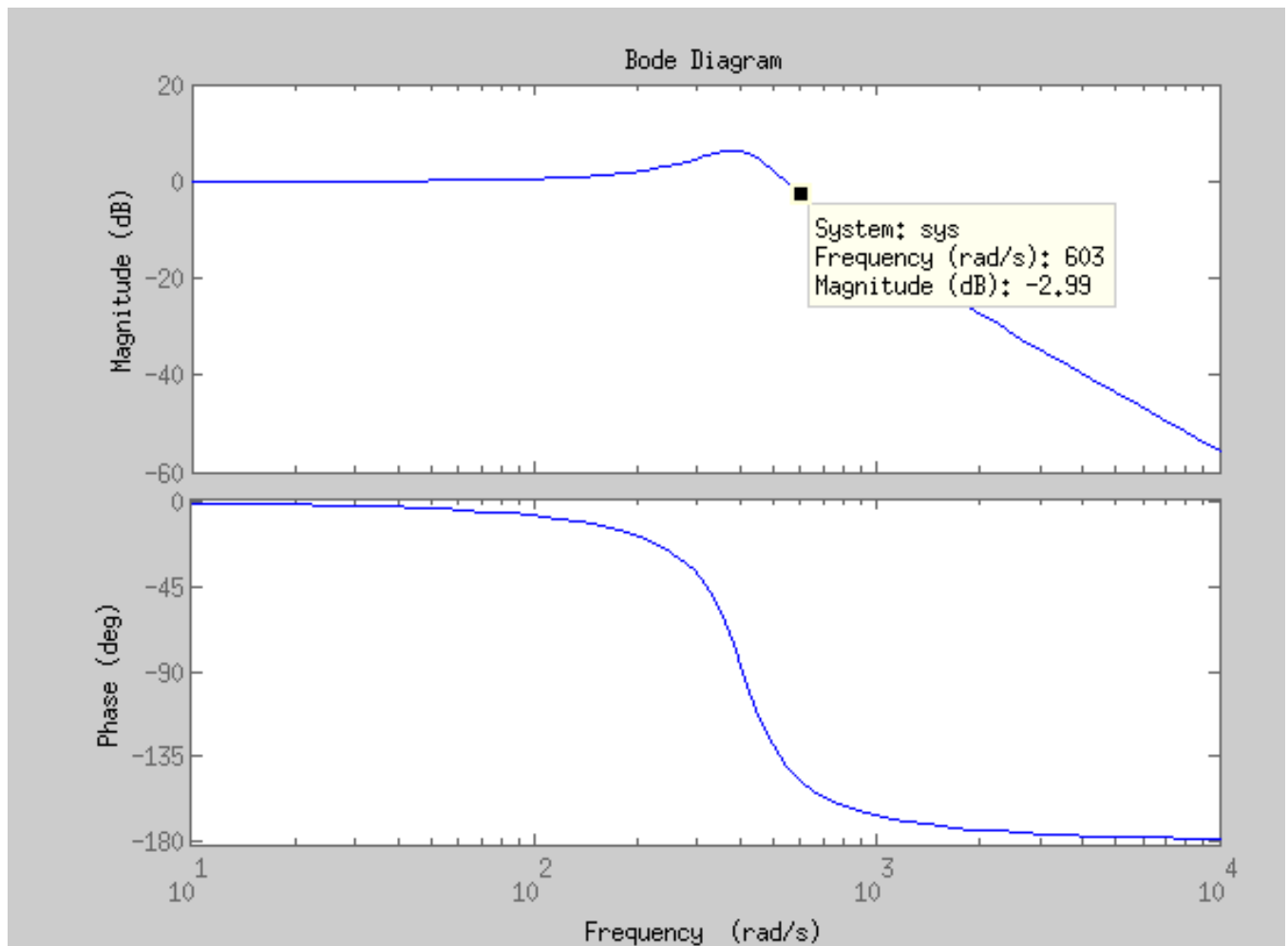


Figure 5: Matlab open-loop frequency response

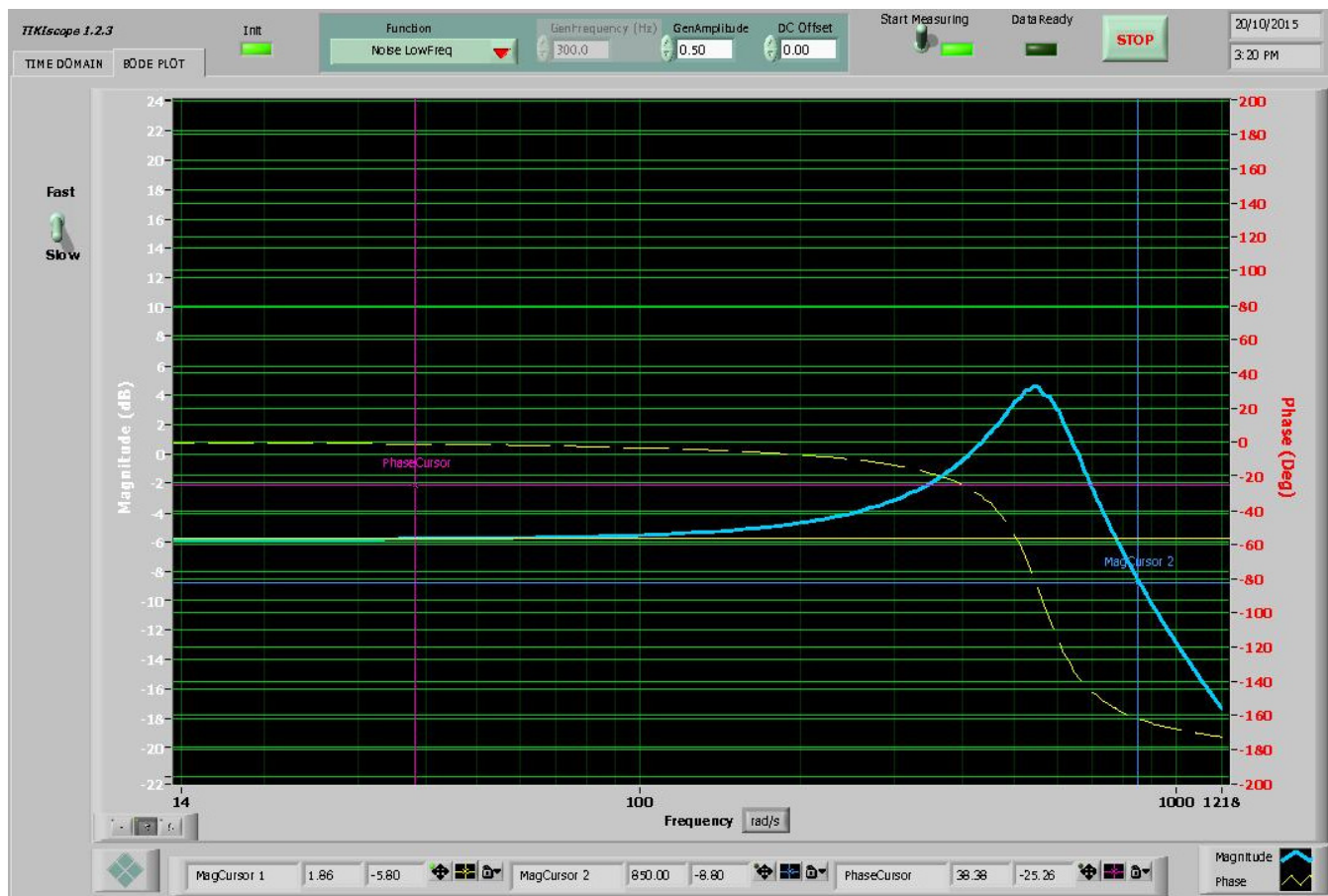


Figure 6: Closed-loop frequency response

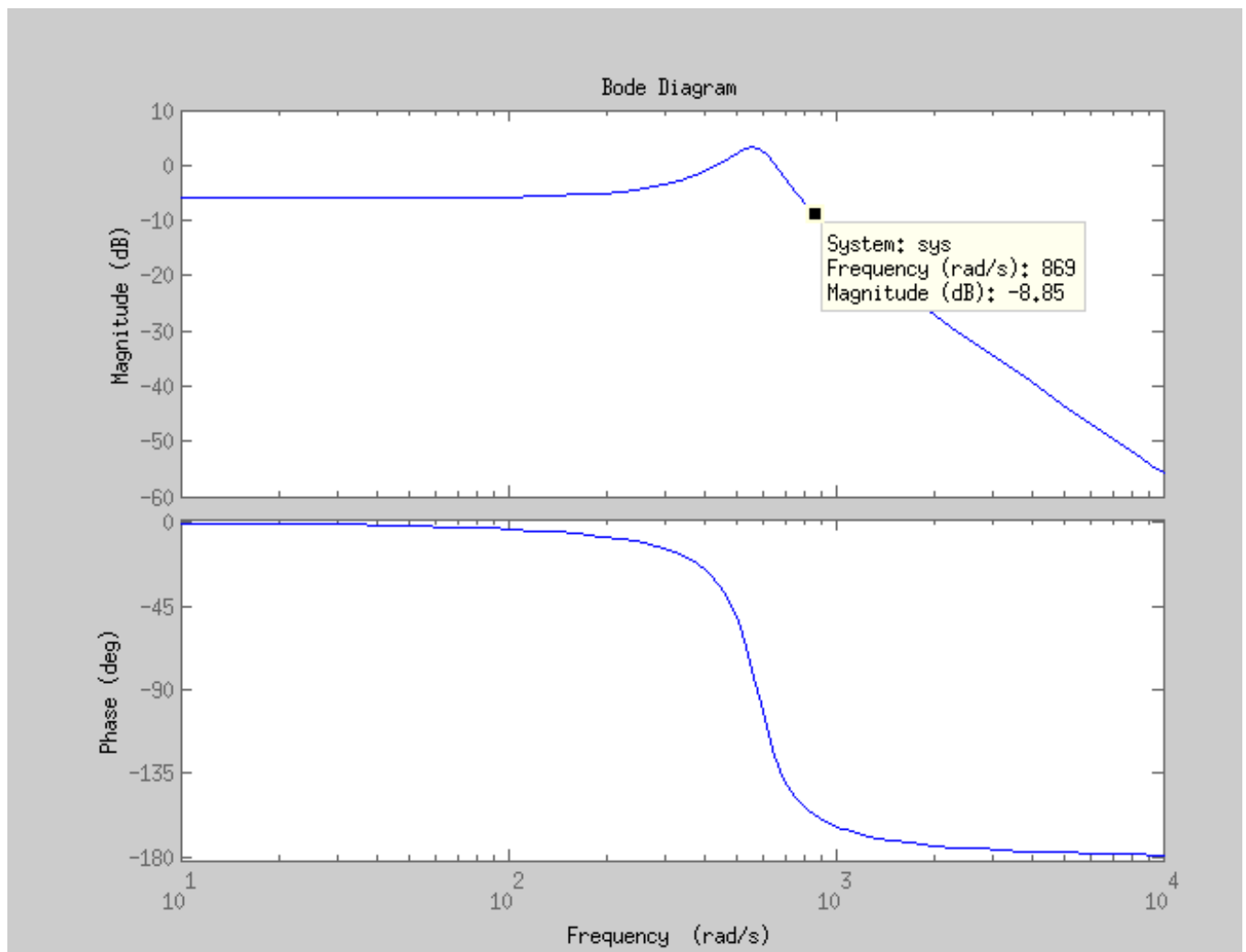


Figure 7: Matlab closed-loop frequency response

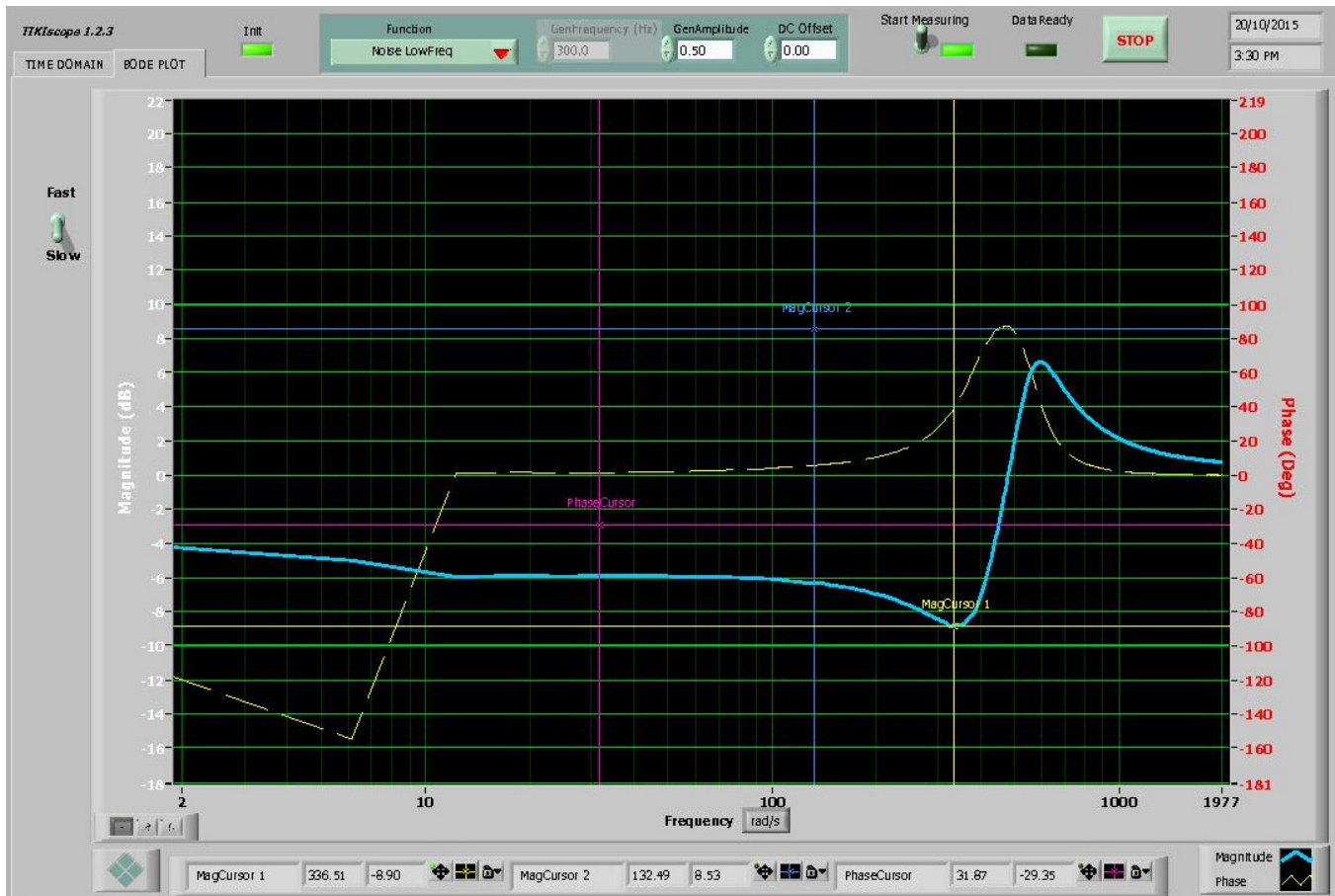


Figure 8: Frequency response response with disturbance

Section 4.3

The equation for the system with input at $D(S)$ is:

As shown in Figure 8 frequencies below 336.51 rad/s show little disturbance and frequencies after that show wild changes in response to the disturbances.

In the open-loop system there is no disturbance rejection since nothing is piped back in. The disturbance is directly added to our output. Due to the closed nature of the closed-loop system there is disturbance rejection by subtracting the output from the input.