## Model Order Reduction

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## 1 Introduction by A Mechanical System

Suppose a four-mass mechanical system is described by the following dynamics:

$$\dot{x} = \begin{bmatrix} 0 & 1 \\ -M^{-1}K & -M^{-1}G \end{bmatrix} x + \begin{bmatrix} 0 \\ M^{-1}D \end{bmatrix} u$$

$$y = \begin{bmatrix} P & Q \end{bmatrix} x$$

where

$$M = \operatorname{diag}(m_1, m_2, m_3, m_4)$$

$$G = \operatorname{diag}(b_1, 0, 0, b_5)$$

$$K = \begin{bmatrix} k_1 + k_2 & -k_2 & 0 & 0 \\ -k_2 & k_2 + k_3 & -k_3 & 0 \\ 0 & -k_3 & k_3 + k_4 & -k_4 \\ 0 & 0 & -k_4 & k_4 + k_5 \end{bmatrix}$$

$$D = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix}^T$$

$$P = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & k_4/m_4 & -(k_4 + k_5)/m_4 \end{bmatrix}$$

$$Q = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -b_5/m_4 \end{bmatrix}$$

$$x = (q^T, \dot{q}^T)^T \in \mathbb{R}^8$$

$$y = (q_1, \ddot{q}_2)^T$$

this is a two-input, **eight**-state, two-output system model. For real case, for example an airplane, a system could be **too complicate** because of **too many state variables**.

## 2 Model Order Reduction Problem

Given a model (A, B, C), with order(state dimension) n, find a model  $(A_r, B_r, C_r)$  with order r < n whose transfer function satisfies:

$$C_r (sl - A_r)^{-1} B_r \simeq C(sl - A)^{-1} B$$
 CT-case  $C_r (zl - A_r)^{-1} B_r \simeq C(zl - A)^{-1} B$  DT-case

To determine if two transfer functions are **close** to each other, given the same input u, they should produce **similar** outputs y and  $y_r$ . Note that:

- similarity between y and  $y_r$  is quantified as  $||y y_r||$  using some norm on the vector space of all output signals
- since y and  $y_r$  are linear in u,  $||y y_r||$  can be very large due to large u
- ullet evaluate system by looking for largest output difference under u with bounded energy:

$$\sup_{\|u\|=1} \|y - y_r\|$$

where ||u|| is **a**(sometimes may not be  $\mathcal{L}_2$ ) norm on the vector space of all input signals

## 3 Naive Attempt to Achieve Order Reduction

3 intuitive ways of reducing system order are given and later we will focus on how to make this process systematic rather than relying on intuition.

## 3.1 Kalman Approach

In Kalman form:

$$\tilde{A} = T^{-1}AT = \begin{bmatrix} \tilde{A}_{11} & \tilde{A}_{12} \\ 0 & \tilde{A}_{22} \end{bmatrix}, \tilde{B} = T^{-1}B = \begin{bmatrix} \tilde{B}_{1} \\ 0 \end{bmatrix}, \tilde{C} = CT = \begin{bmatrix} \tilde{C}_{1} & \tilde{C}_{2} \end{bmatrix}$$

- if (A, B) is not controllable, the controllable subsystem  $(\tilde{A}_{11}, \tilde{B}_1, \tilde{C}_1)$  realizes the same transfer function as (A, B, C) but with a lower order.
- if (C, A) is not observable, then the observable subsystem realizes the same transfer function with a lower order.

The problem is that most systems are both controllable and observable, meaning that this method won't work.

#### 3.2 Drop Method

Given a DT system:

$$A = \begin{bmatrix} 0.7 & 0 \\ 0 & 0.8 \end{bmatrix}, B = \begin{bmatrix} 10 \\ 0.1 \end{bmatrix}, C = \begin{bmatrix} 10 & 0.1 \end{bmatrix}$$

Mode associated with  $\lambda_1=0.7$  is much more controllable and observable compared to mode associated with  $\lambda_2=0.8$ . Discarding mode 0.8 results in  $A_r=0.7, B_r=10, C_r=10$ , which lead to:

$$C_r (zl - A_r)^{-1} B_r = \frac{100}{z - 0.7} \simeq C(zl - A)^{-1} B = \frac{100}{z - 0.7} + \frac{0.01}{z - 0.8}$$

Note that 0.01 is quiet small compare to 100.

#### 3.3 Compromise Approximation

Given a DT system which is slightly different for C:

$$A = \begin{bmatrix} 0.7 & 0 \\ 0 & 0.8 \end{bmatrix}, B = \begin{bmatrix} 10 \\ 0.1 \end{bmatrix}, C = \begin{bmatrix} 0.1 & 10 \end{bmatrix}$$

Mode for  $\lambda_1 = 0.7$  is still much more controllable, but now much less observable, than mode for  $\lambda_2 = 0.8$ . Discarding either mode will result in a large error for approximating

$$H(z) = C(zl - A)^{-1}B = \frac{1}{z - 0.7} + \frac{1}{s - 0.8}$$

Noting that the two poles of H(z) are very close to each other, we can first approximate H(z) by

$$H_r(z) = \frac{2}{z - 0.75} \simeq H(z)$$

and then find a first-order realization of  $H_r(z)$ , say,  $A_r = 0.75, B_r = 2, C_r = 1$ , as the reduced-order model.

# 4 Lower-Rank(by SVD) Approximation of Matrix

A matrix  $A \in \mathbb{R}^{m \times n}$  viewed as a map  $A : \mathbb{R}^n \to \mathbb{R}^m$  with rank p. The problem is to find a matrix  $A_r \in \mathbb{R}^{m \times n}$  with rank r < p to

$$\text{minimize } \sup_{u \in \mathbb{R}^n, \|u\| = 1} \|Au - A_r u\|$$

- $\bullet$   $\|\cdot\|$  represent Euclidean norm
- Function to be minimized is equal to the  $\mathcal{L}_2$ -norm of matrix  $A A_r$

Suppose A has singular value decomposition(SVD)

$$A = U \left[ \begin{array}{cc} \Sigma + & 0 \\ 0 & 0 \end{array} \right] V^T$$

with

$$\Sigma_{+} = \operatorname{diag}\left(\sigma_{1}, \ldots, \sigma_{p}\right), \sigma_{1} \geq \cdots \geq \sigma_{p} > 0$$

then

$$A_r^* = U \begin{bmatrix} \operatorname{diag}(\sigma_1, \dots, \sigma_r, 0, \dots, 0) & 0 \\ 0 & 0 \end{bmatrix} V^T$$

with the approximation error

$$||A_r - A_r^*|| = \sigma_{r+1}$$

This can be extended to linear systems.

## 4.1 LTI System as Linear Operator

Consider the discrete-time LTI system

$$x[k+1] = Ax[k] + Bu[k]$$
$$y[k] = Cx[k]$$

If x[0] = 0(for convenience), the system maps the input sequence to the output sequence:

$$\underbrace{ \begin{bmatrix} y[0] \\ y[1] \\ y[2] \\ y[3] \\ \vdots \end{bmatrix} }_{Y} = \underbrace{ \begin{bmatrix} 0 \\ CB & 0 \\ CAB & CB & 0 \\ CA^2B & CAB & CB & 0 \\ \vdots & & \ddots \end{bmatrix} }_{G} \underbrace{ \begin{bmatrix} u[0] \\ u[1] \\ u[2] \\ u[3] \\ \vdots \end{bmatrix} }_{Y}$$

- G is a **Toeplitz matrix** (constant along diagonal direction) because the system is time-invariant
- ullet G is lower triangular matrix because the system is causal
- $\bullet$  G is unchanged under coordinate transformation

## 4.2 $\ell_2$ -Gain

The  $\ell_2$ -gain of the system is the induced norm of G:

$$||G||_2 = \sup_{\mathbf{U} \neq 0} \frac{||G\mathbf{U}||}{||\mathbf{U}||}$$

- maximal energy magnification from input to output
- useful in robust control (**U** is the perturbation)

## 5 Hankel Operator

The operator G typically has rank infinity, hence difficult to study. Instead, look at the map from past into future output:

$$\underbrace{ \begin{bmatrix} y[0] \\ y[1] \\ y[2] \\ \vdots \end{bmatrix}}_{Y_{L}} = \underbrace{ \begin{bmatrix} CB & CAB & CA^{2}B & \dots \\ CAB & CA^{2}B & CA^{3}B & \dots \\ CA^{2}B & CA^{3}B & CA^{4} & \dots \\ \vdots & \vdots & \vdots & \ddots \end{bmatrix}}_{\Gamma} \underbrace{ \begin{bmatrix} u[-1] \\ u[-2] \\ u[-3] \\ \vdots \end{bmatrix}}_{U_{L}}$$

- $\Gamma$  is a **Hankel matrix**(constant along anti-diagonal direction)
- Each column represents the impulse response w.r.t.  $u_j[-k]$  at time k < 0, hence  $\Gamma$  can be constructed from experimental data
- $\bullet$   $\Gamma$  unchanged under coordinate changes
- $\Gamma$  has finite rank!

## 5.1 Decomposition of Hankel Operator

Since state x[0] summarizes contributions of past input, we have

$$\mathbf{U}_{-} \underbrace{\overset{\Psi_{c}}{\longrightarrow} x[0] \overset{\Psi_{o}}{\longrightarrow}}_{\Gamma} \mathbf{Y}_{+}$$

In other words(VIP):

$$\Gamma = \Psi_o \Psi_c = \begin{bmatrix} C \\ CA \\ CA^2 \\ \vdots \end{bmatrix} \cdot \underbrace{\begin{bmatrix} B & AB & A^2B & \cdots \end{bmatrix}}_{\Psi_c}$$

After coordinate transformation:

$$\begin{split} x &= T\tilde{x} \\ \tilde{\Psi}_c &= T^{-1}\Psi_c \\ \tilde{\Psi}_o &= \Psi_o T \\ \tilde{\Gamma} &= \Gamma \end{split}$$

Rank of  $\Gamma$  is **at most**  $n = \dim(x)$ 

### 5.2 Rank of Hankel Operator

- Controllability operator  $\Psi_c$  is full rank if (A, B) is controllable
- Observability operator  $\Psi_o$  is full rank if (C, A) is observable

The Hankel operator  $\Gamma$  has rank  $n = \dim(x)$  if and only if the system (A, B, C) is minimal.

**Proof**: Use the two Sylvester rank inequalities for  $\Gamma = \Psi_o \Psi_c$ :

$$\begin{aligned} \operatorname{rank}(\Gamma) &\leq \min \left\{ \operatorname{rank} \left( \Psi_c \right), \operatorname{rank} \left( \Psi_o \right) \right\} \\ \operatorname{rank}(\Gamma) &\geq \operatorname{rank} \left( \Psi_c \right) + \operatorname{rank} \left( \Psi_o \right) - n \end{aligned}$$

## 5.3 McMillan Degree

- For a transfer function (or matrix) H(s), the state dimension of its minimal realization is called its **Mcmillan degree**
- McMillan degree is the rank of the Hankel operator  $\Gamma$

## 5.4 Hankel Singular Values

Suppose A is stable and system (A, B, C) is minimal. Then both controllability and observability gramians exist and are positive definite:

$$W_c = \Psi_c \Psi_c^T = \sum_{k=0}^{\infty} A^k B B^T (A^T)^k, \quad W_o = \Psi_o^T \Psi_o = \sum_{k=0}^{\infty} (A^T)^k C^T C A^k$$

 $W_oW_c$  is diagonalizable with positive eigenvalues:

- this is because  $W_oW_c$  is similar to  $W_c^{1/2}W_oW_c^{1/2}\succeq 0$
- eigenvalues of  $W_oW_c$  unchanged under coordinate change  $x=T\widetilde{x}$ :

$$\widetilde{W}_{o} = T^{T}W_{o}T, \widetilde{W}_{c} = T^{-1}W_{c}\left(T^{-1}\right)^{T} \Rightarrow \widetilde{W}_{o}\widetilde{W}_{c} = T^{T}W_{o}W_{c}\left(T^{-1}\right)^{T}$$

Hankel singular values (VIP) of the system are (nonzero) singular values of  $\Gamma$  or equivalently, the square roots of the eigenvalues of  $W_oW_c$ .

- The singular values are typically sorted as  $\sigma_1 \geq \sigma_2 \geq \cdots \sigma_n > 0$
- Singular values do not depend on state coordinates

#### 5.5 Proof of Properties of Hankel Singular Values

Singular values of  $\Gamma$  are sequare roots of nonzero enginvalues of

$$\Gamma^{T}\Gamma = (\Psi_{o}\Psi_{c})^{T}(\Psi_{o}\Psi_{c}) = \Psi_{c}^{T}W_{o}\Psi_{c} = (W_{o}^{1/2}\Psi_{c})^{T}(W_{o}^{1/2}\Psi_{c})$$

which has the same nonzero eigenvalues as those of

$$(W_o^{1/2}\Psi_c)(W_o^{1/2}\Psi_c)^T=W_0^{1/2}W_cW_o^{1/2}$$

which in turn is similar to  $W_oW_c$  (hence have identical eigenvalues).

#### 5.6 Hankel Norm

Suppose A is stable and system (A, B, C) is minimal. Then  $\Gamma$  maps finite energy input  $\mathbf{U}_{-}$  to finite energy output  $\mathbf{Y}_{+}$ , **Hankel norm** of system is

$$\|\Gamma\| := \sup_{\mathbf{U}_{-} \neq 0} \frac{\|\Gamma \mathbf{U}_{-}\|}{\|\mathbf{U}_{-}\|} = \sigma_1(\Gamma)$$

It is the maximum energy amplification from past input to future output.

#### 5.7 Lower-Rank Hankel Operator Approximation

Given a Hankel operator  $\Gamma$  with rank n, for r < n, find a Hankel operator  $\Gamma_r$  to

minimize 
$$\|\Gamma - \Gamma_r\|$$
  
s.t.  $\operatorname{rank}(\Gamma_r) = r$ 

- $\Gamma$  corresponds to a minimal system (A, B, C) with state dimension n
- $\Gamma_r$  corresponds to a minimal system  $(A_r, B_r, C_r)$  with state dimension r whose I/O operator is **closest** to that of (A, B, C)
- recall lower-rank approximation of matrices using SVD truncation

The optimal solution  $\Gamma_r^*$  satisfies  $\|\Gamma - \Gamma_r^*\| \ge \sigma_{r+1}$ , where  $\sigma_{r+1}$  is the (r+1)-th largest sigular value of  $\Gamma$ . Lower bound may not be tight due to the Hankel constraint on  $\Gamma_r^*$ .

## 6 Balanced Realization

Given a minimal system (A, B, C) with A stable, there exists a coordinate transformation  $x = T\tilde{x}$  such that in the new coordinates, the controllability and observability Gramians are equal and diagonal:

$$\widetilde{W}_c = \widetilde{W}_o = \Sigma = \operatorname{diag}(\sigma_1, \dots, \sigma_n)$$

where  $\sigma_1 \geq \cdots \geq \sigma_n$  are the Hankel singular values of the system.

- state space model with the above properties are called balanced
- trongly controllable states are also strongly observable!

Tip:note that  $W_c^{1/2}W_oW_c^{1/2}=U\Sigma^2U^T$  for some orthogonal U and diagonal  $\Sigma$ . By choosing  $T=W_c^{1/2}U\Sigma^{-1/2}$  we have

$$\widetilde{W}_o = T^T W_0 T = \Sigma, \quad \widetilde{W}_c = T^{-1} W_c \left( T^{-1} \right)^T = \Sigma$$

## 7 Balanced Truncation

Given a minimal system (A, B, C) with stable A, first do a coordinate change  $x = T\widetilde{x}$  so that  $(\widetilde{A}, \widetilde{B}, \widetilde{C})$  is a balanced realization:

- $\widetilde{W}_c = \widetilde{W}_o = \operatorname{diag}(\sigma_1, \dots, \sigma_n)$
- states  $\tilde{x}_1, \dots, \tilde{x}_n$  have decreasing controllability and observability

To find a reduced-order model of order r < n, keep only the first r states:

$$\begin{bmatrix} \tilde{A}_{11} & \tilde{A}_{12} & \tilde{B}_1 \\ \tilde{A}_{21} & \tilde{A}_{22} & \tilde{B}_2 \\ \tilde{C}_1 & \tilde{C}_2 & 0 \end{bmatrix} \stackrel{(\tilde{x}_1, \dots, \tilde{x}_n) \to (\tilde{x}_1, \dots, \tilde{x}_r)}{\overset{(\tilde{x}_1, \dots, \tilde{x}_r)}{\longleftrightarrow}} \begin{bmatrix} \tilde{A}_{11} & \tilde{B}_1 \\ \tilde{C}_1 & 0 \end{bmatrix}$$

Reduced-order model  $(\tilde{A}_{11}, \tilde{B}_1, \tilde{C}_1)$  is called the r-th order **balanced truncation** of (the transfer function of) the model (A, B, C), and  $(\tilde{A}_{11}, \tilde{B}_1, \tilde{C}_1)$  is also balanced and  $\tilde{A}_{11}$  is stable

## 8 Example

Again, given system:  $A = \begin{bmatrix} 0.7 & 0 \\ 0 & 0.8 \end{bmatrix}, B = \begin{bmatrix} 10 \\ 0.1 \end{bmatrix}, C = \begin{bmatrix} 0.1 & 10 \end{bmatrix}$ , find first-order reduction.

1. controllability and observability gramians are

$$W_c = \begin{bmatrix} 196.0784 & 2.2727 \\ 2.2727 & 0.0278 \end{bmatrix}, \quad W_o = \begin{bmatrix} 0.0196 & 2.2727 \\ 2.2727 & 277.7778 \end{bmatrix}$$

so

$$W_oW_c = \left[ \begin{array}{cc} 9.01 & 0.10769 \\ 1076.9 & 12.881 \end{array} \right]$$

2.  $W_oW_c$  has two eigenvalues  $\lambda_1=21.888, \lambda_2=0.0036161$ , whose square roots yield the Hankel singular values:

$$\sigma_1 = 4.6784 \quad \sigma_2 = 0.060134$$

alternatively, Matlab command hsvd can be used

- 3. As  $\sigma_1$  is much larger than  $\sigma_2$ , a first order system can approximate the original system very well.
- 4. Apply the linear transform  $x = T\tilde{x} = \begin{bmatrix} -6.4152 & 7.671 \\ -0.076711 & -0.064152 \end{bmatrix} \tilde{x}$
- 5. A balanced realization is resulted:

$$\tilde{A} = T^{-1}AT = \begin{bmatrix} 0.75885 & 0.049211 \\ 0.049211 & 0.74115 \end{bmatrix}, \tilde{B} = T^{-1}B = \begin{bmatrix} -1.4086 \\ 0.12559 \end{bmatrix}$$

$$\tilde{C} = CT = \begin{bmatrix} -1.4086 & 0.12559 \end{bmatrix}$$

whose controllability and observability gramians are diag $(\sigma_1, \sigma_2)$ 

6. A 1st-order balanced truncation is as follows

$$\tilde{A}_{11} = 0.75885, \quad \tilde{B}_1 = -1.4086, \quad \tilde{C}_1 = -1.4086$$

whose transfer function is  $\frac{1.9842}{z-0.75885},$  alternatively, Matlab command balred can be used