

Homework 6 Classification of differential equations and shock tube due march

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Task 1: Classification

a)

$$\begin{aligned} \underline{\underline{A}} \frac{\partial \underline{u}}{\partial x} + \underline{\underline{B}} \frac{\partial \underline{u}}{\partial y} &= 0 \\ \begin{bmatrix} 1 & 0 & 0 \\ u & 0 & 1 \\ 0 & u & 0 \end{bmatrix} \begin{bmatrix} \frac{\partial u}{\partial x} \\ \frac{\partial v}{\partial x} \\ \frac{\partial p}{\partial x} \end{bmatrix} + \begin{bmatrix} 0 & 1 & 0 \\ v & 0 & 0 \\ 0 & v & 1 \end{bmatrix} \begin{bmatrix} \frac{\partial u}{\partial y} \\ \frac{\partial v}{\partial y} \\ \frac{\partial p}{\partial y} \end{bmatrix} &= 0 \end{aligned} \quad (0.1)$$

$$\underline{\underline{A}} = \begin{bmatrix} 1 & 0 & 0 \\ u & 0 & 1 \\ 0 & u & 0 \end{bmatrix}$$

$$\underline{\underline{B}} = \begin{bmatrix} 0 & 1 & 0 \\ v & 0 & 0 \\ 0 & v & 1 \end{bmatrix}$$

b)

$$\begin{aligned} \underline{\underline{B}} - \lambda \underline{\underline{A}} &= \begin{bmatrix} -\lambda & 1 & 0 \\ v - \lambda u & 0 & -\lambda \\ 0 & v - \lambda u & 1 \end{bmatrix} = 0 \\ &= -\lambda \times \lambda \times (v - \lambda u) - (v - \lambda u) \\ &= (v - \lambda u)(1 + \lambda^2) \end{aligned} \quad (0.2)$$

$$\lambda_1 = i$$

$$\lambda_2 = -i$$

$$\lambda_3 = \frac{v}{u}$$

Since eigenvalues are both real and complex, it is the mixed PDEs type. The results could be expected as marching properties. And all boundary should be know to solve this kind of equations.

Task 2: Shock tube

a)

$$\square u_t + f_x = 0 \quad f = au \quad (0.3)$$

$$\begin{aligned}
u_j^* &= u_j^n - \lambda(f(u_{j+1}^n) - f(u_j^n)) \\
u_j^{n+1} &= \frac{1}{2}(u_j^n + u_j^*) - \frac{1}{2}\lambda(f(u_j^*) - f(u_{j-1}^*)) \\
\sigma &= \left| a \frac{\Delta t}{\Delta x} \right| \leq 1
\end{aligned} \tag{0.4}$$

For the linear advection equation, or this advection equation, the MacCormach scheme is identical to the Lax-Wendroff scheme, second order scheme in time and space.

b)

$$\begin{aligned}
\begin{pmatrix} \rho \\ u \end{pmatrix}_t + \begin{pmatrix} u & \rho \\ K\gamma\rho^{\gamma-2} & u \end{pmatrix} \begin{pmatrix} \rho \\ u \end{pmatrix}_x &= 0 \\
\Rightarrow \begin{pmatrix} u & \rho \\ K\gamma\rho^{\gamma-2} & u \end{pmatrix} - \lambda \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} &= 0 \Rightarrow \begin{pmatrix} u-\lambda & \rho \\ \frac{c^2}{\rho} & u-\lambda \end{pmatrix} = 0 \\
(u-\lambda)^2 - c^2 = 0 &\Rightarrow \lambda = u \pm c
\end{aligned} \tag{0.5}$$

c)

analytical shock speed s is

$$s = \frac{\rho_L u_L - \rho_R u_R}{\rho_L - \rho_R} = \frac{0.5336 * 249 - 0.2233 * 0.4162}{0.5336 - 0.2233} = 427.8 \text{ m/s} \tag{0.6}$$

All the values are taken from the figure 1. While for the measured shock speed:

$t = 50 \text{ time steps} * dt = 50 * 6.1307e-5 = 3.0653e-3 \text{ s}$

$x = 2.775 - 1.5 = 1.275 \text{ m}$

$v = 415 \text{ m/s}$

These two shock speeds are nearly the same.

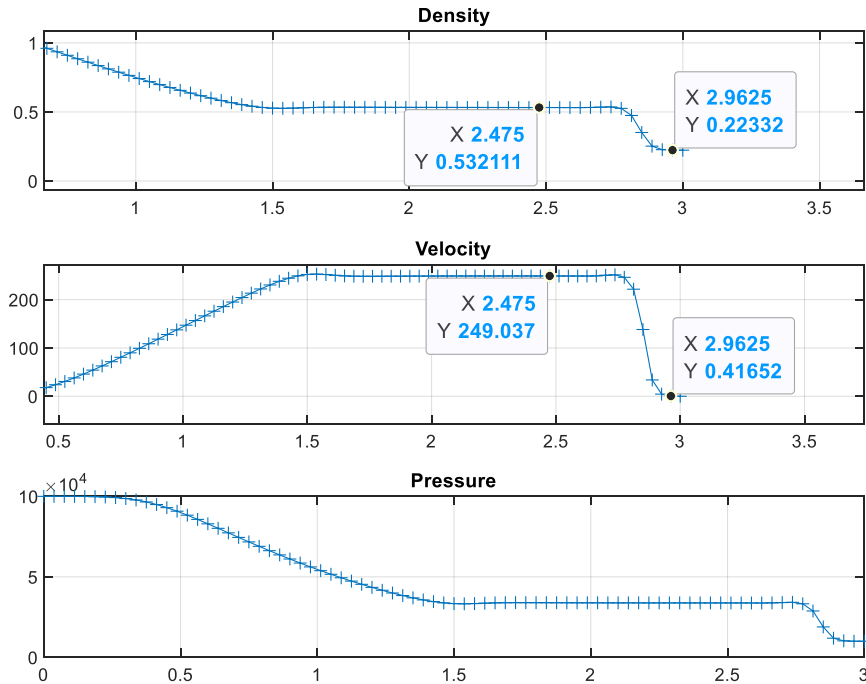


Figure 1 Computed states of shock, where are density and speed comes from to calculate the analytical shock speed.

d)
different Cn

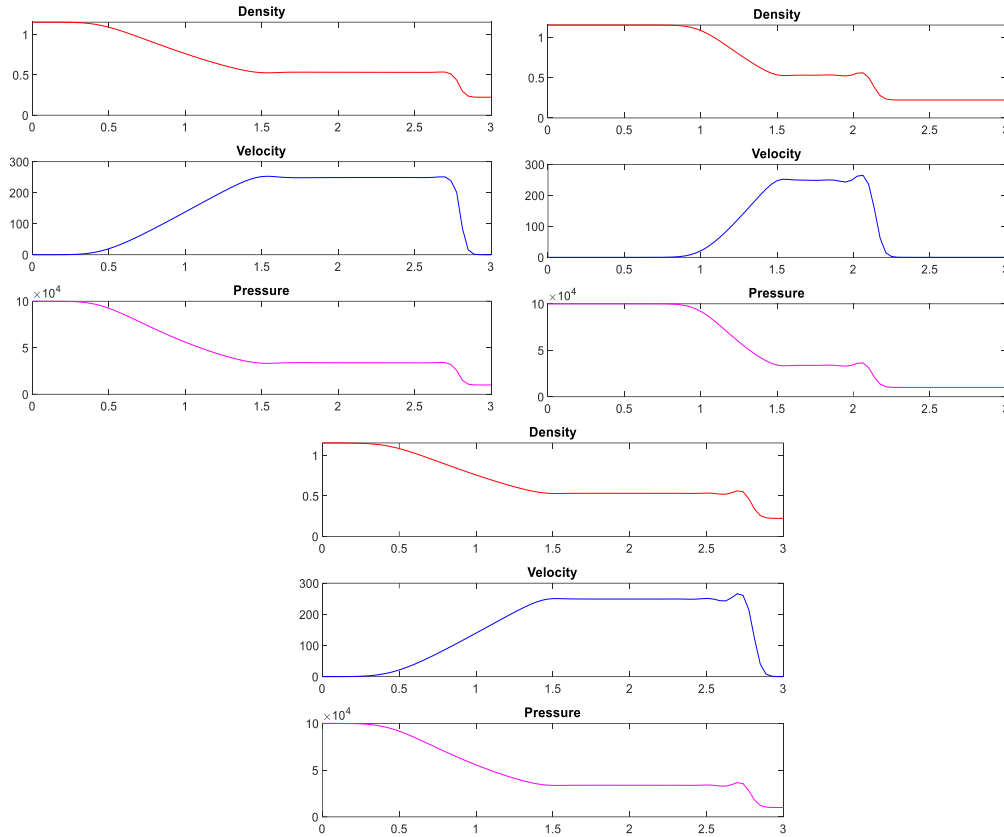


Figure 2 a: $C_n=0.9$ $N_{stp}=50$ b) $C_n=0.45$ $N_{stp}=50$ c) $C_n=0.45$ $N_{stp}=100$

As shown in figure 2 is different C_n . The final time t_f is nearly 0.003 s. For case b, $C_n=0.45$ and $N_{stp}=50$, the final time t_f is 0.0015 s. The reason is C_n decreased to half so the dt decreased to half, thus the total final time is half of 0.003s. As shown in case 3, when the N_{stp} increase 2 times to 100, the final time t_f is 0.003s and the shock is the nearly the same. But for case c, in the edge of the shock, there is small bump, since the dt is smaller than case a, the result in case c is more accurate. We could say small C_n means high accurate.

Different C_0 and C_2 $C_n=0.9$ $N_{stp}=50$

As show in figure 3, different C_0 and C_2 . Through the comparison of $C_0=0.05$ $C_2=0.05$ and $C_0=0.45$, $C_2=0.05$, it could be concluded that when C_0 is small, the shock shape is sharp in the edge, while C_0 is large could induce a smooth edge of shock. The reason is C_0 is a background diffusion parameter, large C_0 means large artificial viscosity and the shock pressure diffusion faster, so no large difference of velocity and pressure in the shock edges.

As for the C_2 , it seems there are not very significant influence on the shock shape. While for the large density filed, it could damp the oscillations. As shown in $C_0=0.05$ $C_2=0.4$ and $C_0=0.05$ $C_2=0.05$, for the velocity, in the large density derivative area, large C_2 has smooth velocity. **Above all, the $C_0=0.05$, $C_2=0.25$ is the best case.**

As for the $t_f=0.01$ for the last case, after the shock is reflected, it could see that at the large density derivative area, the oscillations increase which could be seen as a large bump compares with previous $t_f=0.003$.

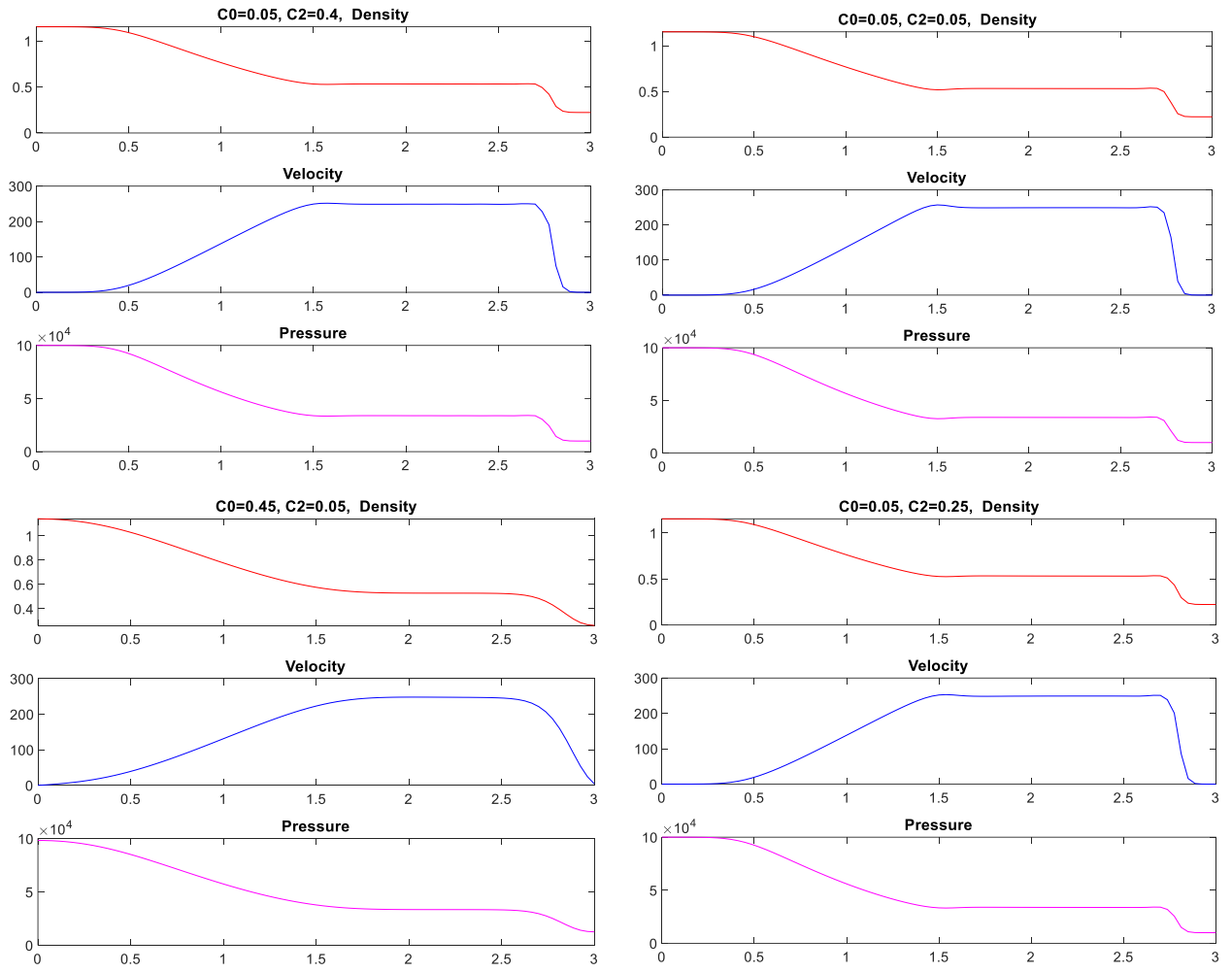


Figure 3 Different C_0 and C_2

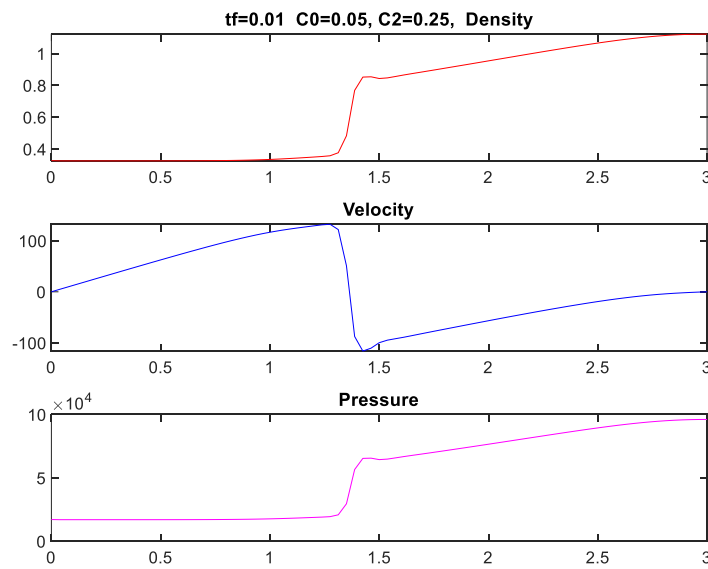


Figure 4 $T_f = 0.01$ for $C_0 = 0.05$ $C_2 = 0.25$