

Section 4

* Amplitude Modulation - Single Side band [SSB]: [passband B.W = B].

→ It only Sends one Sideband [Either the upper or the lower].

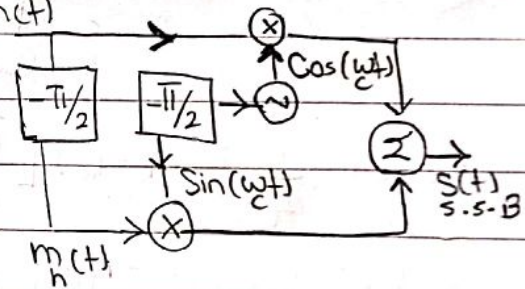
Modulators: ① Selective filtering method: It uses a filter that selects the transmitted sideband.

② phase shift method: It changes the phase of $s(t)$ using Hilbert transform

$$S(t) = m(t) \cos \omega_c t \pm m_h(t) \sin(\omega_c t)$$

→ If the ~~two~~ two terms are added → LSB

→ If the two terms are subtracted → USB.



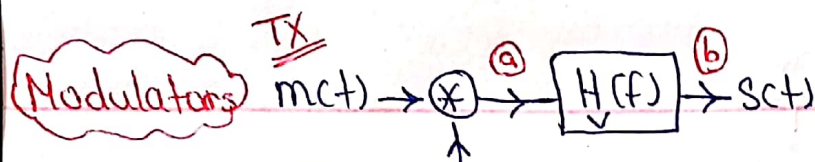
* Amplitude Modulation: Vestigial Sideband: [VSB]:

* It Compromises between SSB & DSB in spectrum & power.

SSB → Difficult to realize the modulators but power efficient.

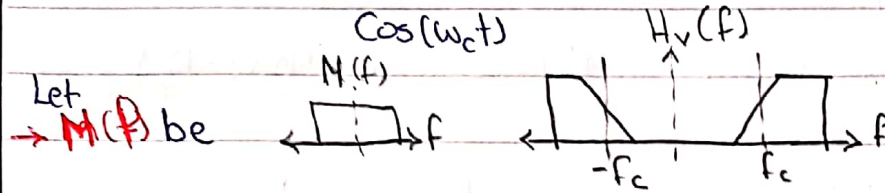
DSB → Easier to realize the modulators but power inefficient.

* Instead of sending only one sideband [SSB] or sending ~~both~~ the two sidebands [DSB], VSB passes one sideband along with a part of the other sideband.



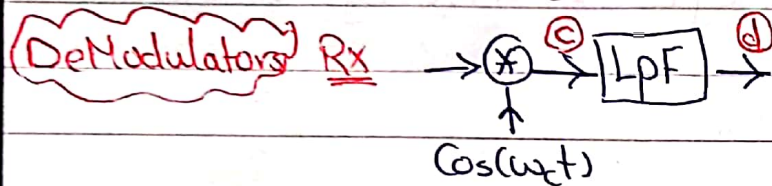
Recall: $x(t) \xrightarrow{h(t)} y(t)$
 $y(t) = x(t) \otimes h(t)$
 (Conv.)

$y(f) = x(f) \cdot H(f)$
 (Mult.)



→ @a: $\frac{1}{2} [M(f-f_c) + M(f+f_c)]$

→ @b: $\frac{1}{2} H_v(f) [M(f-f_c) + M(f+f_c)]$



→ @c: $\frac{1}{4} H_v(f-f_c) [M(f-2f_c) + \underline{M(f)}] + \frac{1}{4} H_v(f+f_c) [\underline{M(f)} + M(f+2f_c)]$

→ @d: $\frac{1}{4} M(f) [H_v(f-f_c) + H_v(f+f_c)]$

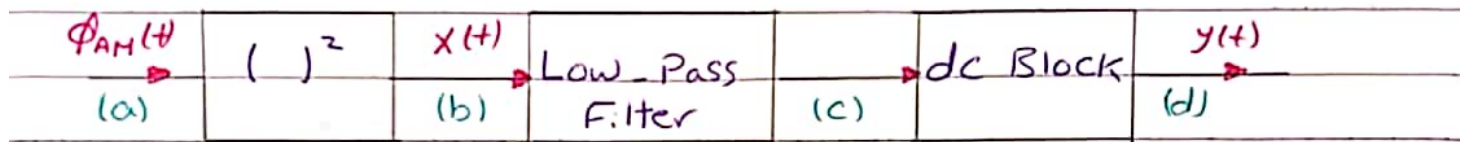
* $H_v(f-f_c) + H_v(f+f_c) \rightarrow$ must be constant so that the message does not get distorted.

If $[H_v(f-f_c) + H_v(f+f_c)]$ is not constant, an **equalizer** should be used. It reverses the effect of the $H_v(f)$ [filter].

So, $H_{\text{Reverse}}(f) = \frac{1}{H_v(f-f_c) + H_v(f+f_c)}$ ← Frequency response of the equalizer

Sheet Two Solution

110 In The early days of radio, AM signals were demodulated by a crystal detector followed by a low-pass filter and a dc blocker as shown in the Figure. Assume a crystal detector to be basically a squaring device. Determine the signals at Point a, b, c and d. Point out the distortion term in the output $y(t)$. Show that if $A \gg |m(t)|$ the distortion is small



Solution

at Point (a) $\rightarrow \phi_{AM}(t) = [A + m(t)] \cos(\omega_c t)$

at Point (b) $\rightarrow (\phi_{AM}(t))^2 = [A^2 + 2Am(t) + m^2(t)] * \frac{1}{2} * (1 + \cos 2\omega_c t)$

at Point (c) $\rightarrow \frac{1}{2} [A^2 + 2Am(t) + m^2(t)]$

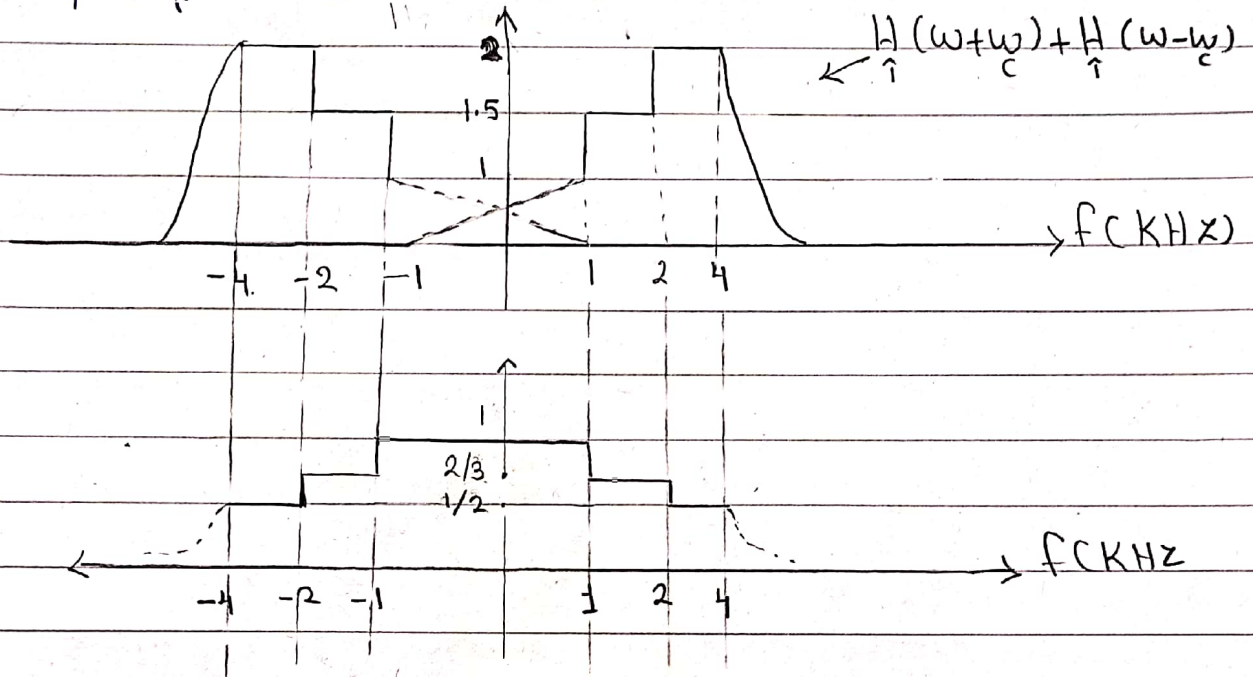
at Point (d) $\rightarrow y(t) = \frac{1}{2} [2Am(t) + m^2(t)] = \left[m(t) + \frac{m^2(t)}{2A} \right]$

$\therefore A \gg |m(t)| \Rightarrow \frac{|m(t)|}{A} \ll 1$

$\therefore y(t) \approx Am(t)$

\rightarrow We see that the distortion component $\frac{m^2(t)}{2A}$

$$H_0(\omega) = \frac{1}{\text{LPF} \{ \hat{H}_1(\omega + \omega_c) + \hat{H}_1(\omega - \omega_c) \}}$$
 where $|\omega| \leq 2\pi B$



∴ Message Baseband BW = 4 kHz.

∴ Insert LPF after the equalizer with $f_c = 4$ kHz

Note To make sure that you successfully obtained $H_0(\omega)$, Multiply $H_0(\omega)$ by $[\hat{H}_1(\omega + \omega_c) + \hat{H}_1(\omega - \omega_c)]$. It should give 1 [Constant].