

# A precipitation-hardened high-entropy alloy with outstanding tensile properties

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## ARTICLE INFO

### Article history:

Received 11 August 2015

Received in revised form

29 August 2015

Accepted 29 August 2015

Available online 29 September 2015

### Keywords:

High-entropy alloys

Precipitation hardening

Strengthening mechanisms

Mechanical properties

3 dimensional atom probe tomography

## ABSTRACT

Recent studies indicated that high-entropy alloys (HEAs) possess unusual structural and thermal features, which could greatly affect dislocation motion and contribute to the mechanical performance, however, a HEA matrix alone is insufficiently strong for engineering applications and other strengthening mechanisms are urgently needed to be incorporated. In this work, we demonstrate the possibility to precipitate nanosized coherent reinforcing phase, i.e., L1<sub>2</sub>-Ni<sub>3</sub>(Ti,Al), in a fcc-FeCoNiCr HEA matrix using minor additions of Ti and Al. Through thermomechanical processing and microstructure controlling, extraordinary balanced tensile properties at room temperature were achieved, which is due to a well combination of various hardening mechanisms, particularly precipitation hardening. The applicability and validity of the conventional strengthening theories are also discussed. The current work is a successful demonstration of using integrated strengthening approaches to manipulate the properties of fcc-HEA systems, and the resulting findings are important not only for understanding the strengthening mechanisms of metallic materials in general, but also for the future development of high-performance HEAs for industrial applications.

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## 1. Introduction

Conventional alloy design strategy, which is usually based on one principal constituent and adds other minor elements for further optimization of properties and performances, has created a variety of metallic materials for our daily life. Recently, a revolutionary alloy design concept, namely, high-entropy alloy (HEAs) concept, was proposed and the basic idea is to simultaneously alloy multiple principal elements in equimolar or near equimolar ratios to increase the configuration entropy to stabilize the structures. Since its inception, this new family of alloys has been attracted extensive attention due to their unique properties and the related scientific importance [1–5]. Due to their high mixing entropy, these alloys tend to form single-phase structures with a high symmetry, such as fcc (face-centered cubic), bcc (body-centered cubic), and hcp (hexagonal close-packed) [4,6–8]. They have been

demonstrated to exhibit several special intrinsic characteristics, for example, high configuration entropy [9], sluggish atomic diffusion [10], and large lattice distortion [3,11]. These features are anticipated to enhance formation and stabilization of solid solution phases and impede dislocation motion, thereby improving the mechanical strength, particularly at high temperatures. Nevertheless, recent studies [12–14] indicate that a HEA matrix alone, especially single-phase fcc structure, is insufficiently strong for practical applications. In other words, other strengthening mechanisms are needed so that desirable mechanical properties can be obtained. While, qualitative descriptions and equations of strengthening mechanisms for traditional solid solution alloys are well established, such theories are missing for the highly concentrated HEAs because it is difficult to clearly identify their “solvent” and “solutes”. Therefore, strengthening mechanisms in these emerging metallic materials must be carefully investigated so that reliable theories can be established.

FeCoNiCrMn is generally recognized as a “model” HEA with a simple fcc structure, and exhibits both outstanding ductility and

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fracture toughness property [12], even at the liquid nitrogen temperature. However, its strength is relatively low, only around 200 MPa in the as-cast state [13,14], which is far from practical structural applications. To make it useful, additional strengthening methods, without sacrificing its ductility, must be induced in the alloy and, the underlying mechanisms need to be scrutinized so that general understanding of the strengthening of HEAs can be achieved.

Along this line, Otto et al. made attempts to enhance the strength of this fcc-FeCrNiCoMn by grain refinement and found that the room-temperature yield strength of the alloy increased from 200 to 350 MPa when the grain size was reduced from 144 to 4.4  $\mu\text{m}$  [13]. This work suggests grain boundary hardening can be induced in the fcc-FeCrNiCoMn alloy, but the hardening is seemingly not extraordinary. To further improve the strength without losing plastic stability, one must, therefore, rely on other mechanisms, such as precipitation hardening, which would require a modification of the chemical composition of the alloy.

In terms of precipitation hardening in HEAs, published results appear somewhat sketchy. A few publications reported the observation of precipitation behavior in HEAs, e.g., in a mixed fcc + bcc CuCr<sub>2</sub>Fe<sub>2</sub>NiMn [15], a mixed fcc + bcc Al<sub>0.3</sub>CrFe<sub>1.5</sub>MnNi<sub>0.5</sub> and single-phase bcc-Al<sub>0.5</sub>CrFe<sub>1.5</sub>MnNi<sub>0.5</sub> [16]. The precipitates in these HEAs were relatively bulky (generally, larger than  $\mu\text{m}$  in size), significantly different from the distribution of fine precipitates ( $\sim\text{nm}$ ) commonly observed in traditional precipitation-hardened alloys. Nevertheless, Yeh et al. have reported the presence of nano-scale precipitates in some HEAs [5]. In this case, a distribution of extremely tiny precipitates (diameter  $\sim 3\text{--}7\text{ nm}$ ) was observed in a CuCoNiCrAlFe HEA with a modulated structure. Tensile properties and possible strengthening of the alloy were unfortunately not evaluated. However, these observations are quite encouraging and suggest that proper selection of the chemical composition combined with appropriate thermomechanical treatment may offer the opportunity to manipulate precipitation strengthening of HEAs.

In the present paper, we demonstrate that minor alloy additions of Ti and Al to a single-phase fcc-FeCoNiCr HEA can induce the formation of L<sub>1</sub><sub>2</sub> coherent nano-size precipitates in the alloy matrix. Subsequently, both yield and ultimate tensile strengths of the alloys are drastically increased. The strengthening efficacies from various strengthening mechanisms are evaluated based on the resulting microstructure in the current highly concentrated HEA matrix.

## 2. Experimental

Two HEA compositions were prepared by vacuum arc melting: the base alloy, FeCoNiCr (in equimolar ratio) for comparison, and another with the nominal composition of (FeCoNiCr)<sub>94</sub>Ti<sub>2</sub>Al<sub>4</sub> (at.%). The alloy ingots were prepared by arc-melting a mixture of pure metals (purity larger than 99.9%), and re-melted at least four times to ensure homogeneity. The master ingots were then drop-casted into a copper mold with a dimension of  $10 \times 10 \times 60\text{ mm}^3$ , and subsequently tube-sealed and homogenized at 1473 K for 4 h.

Two thermomechanical procedures were conducted on the alloyed HEA to obtain fine structures. The first treatment, P1, includes an initial cold rolling of 30%, subsequent annealing at 1273 K for 2 h, aging at 1073 K for 18 h, and followed by water quenching. The second process, P2, includes an initial cold rolling of 70%, and then aging at 923 K for 4 h, followed by water quenching. Therefore, four different HEA samples were prepared, i.e., the as-homogenized FeCoNiCr (alloy A), as-homogenized (FeCoNiCr)<sub>94</sub>Ti<sub>2</sub>Al<sub>4</sub> (alloy B), P1 and P2.

A CMT4105 universal electronic tensile testing machine was employed for tensile tests at room temperature with a nominal

strain rate of  $1 \times 10^{-3}\text{ s}^{-1}$ . The dog bone-shaped tensile samples had a gauge length of 20 mm, a width of 5 mm and a thickness of 1.3 mm. The surface of test samples was polished down to a 2000-grit SiC paper to eliminate scratches.

Considering the relative low accuracy of X-ray diffraction (XRD) in nano-precipitates detection, phase identification in this study was conducted by neutron diffraction, at the VULCAN instrument, beam line 7, Oak Ridge National Laboratory Spallation Neutron Source (ORNL, SNS), USA, at room temperature. The microstructure was characterized by a Zeiss Supra55 scanning electron microscope (SEM) and a JEOL ARM200 transmission electron microscope (TEM) equipped with an objective lens corrector and a thermal field-emission gun (FEG). SEM specimens were initially polished to 2000-grit SiC paper and, subsequently, electrochemically polished for the final surface clarification using a HClO<sub>4</sub>:C<sub>2</sub>H<sub>6</sub>O = 1:9 solution with a direct voltage of 30 V at room temperature. TEM samples were primarily punched to  $\Phi 3\text{ mm}$  circle sheets and then ground to about 50  $\mu\text{m}$ , followed by twin-jet electro-polishing using a mixed solution of HNO<sub>3</sub>:CH<sub>4</sub>O = 1:4 with a direct voltage of 28 V and a current of 60 mA at a temperature around 233 K.

Sharp tip specimens for atom probe tomography (APT) were made by a two-step electrochemical polishing. The 0.3 mm  $\times$  0.3 mm blanks were cut by low speed diamond saw, followed by electrochemical polishing using 10% perchloric acid at a direct voltage of 15 V, the tips were then polished by using weaker electrolyte (2%) of perchloric acid at a direct voltage of 8 V. Data acquisition was performed by using a local electrode atom probe (LEAP 4000HR) equipped with an energy-compensated reflectron by which the mass resolution can be greatly improved. The APT acquisition temperature was set at  $\sim 60\text{ K}$  and the pulse frequency and pulse fractions were 200 kHz and 20%, respectively. CAMECA Integrated Visualization and Analysis Software (IVAS 3.6.8) package was used for the data processing and three-dimensional (3D) atomic reconstruction.

Shear modulus and Poisson's ratio of polished specimens with a dimension of 5.5  $\times$  5.5  $\times$  2.5 mm<sup>3</sup> were measured using RUSpec resonant ultrasound spectrometer, Teclab, USA. To determine the dislocation density using the Williamson-Hall method, XRD tests were conducted using CuK $\alpha$  radiation (Rigaku Dmax 2500 V) with a scanning 2 $\theta$  range of 40°–100° and a step of 0.02°. Annealed single crystal Si powder was also tested to define the instrument peak broadening in this method.

## 3. Results

### 3.1. Neutron diffraction and SEM results

Neutron diffraction patterns of the four HEA specimens, i.e., the homogenized FeCoNiCr (Alloy A) and (FeCoNiCr)<sub>94</sub>Ti<sub>2</sub>Al<sub>4</sub> (Alloy B), and two thermomechanically processed (FeCoNiCr)<sub>94</sub>Ti<sub>2</sub>Al<sub>4</sub> alloys P1 and P2, respectively, are presented in Fig. 1. A single family of fcc peaks are clearly observed for alloy A and B. By contrast, extra series of minor peaks identified as L<sub>1</sub><sub>2</sub>-Ni<sub>3</sub>(Ti, Al) are detected in P1 and P2 samples, indicating the precipitation of secondary phases. It should also be noticed that, there are still two weak peaks at  $\sim 1.4\text{ \AA}$  in alloy A and B and another one at  $\sim 1.1\text{ \AA}$  in alloy P1 and P2 being unknown. Due to the relative low intensity and limited amount of peaks, one can hardly determine the exact phase structure they belong to. Nevertheless, the matrix of the four alloys is mainly composed of an fcc structure.

Fig. 2 shows the corresponding SEM micrographs of the four kinds of HEA samples. As can be seen, both A and B alloys appear to be single-phase structure in Fig. 2a and b, respectively, with only few dirt on the surface probably introduced during the electro-polishing process. In accordance with the neutron diffraction

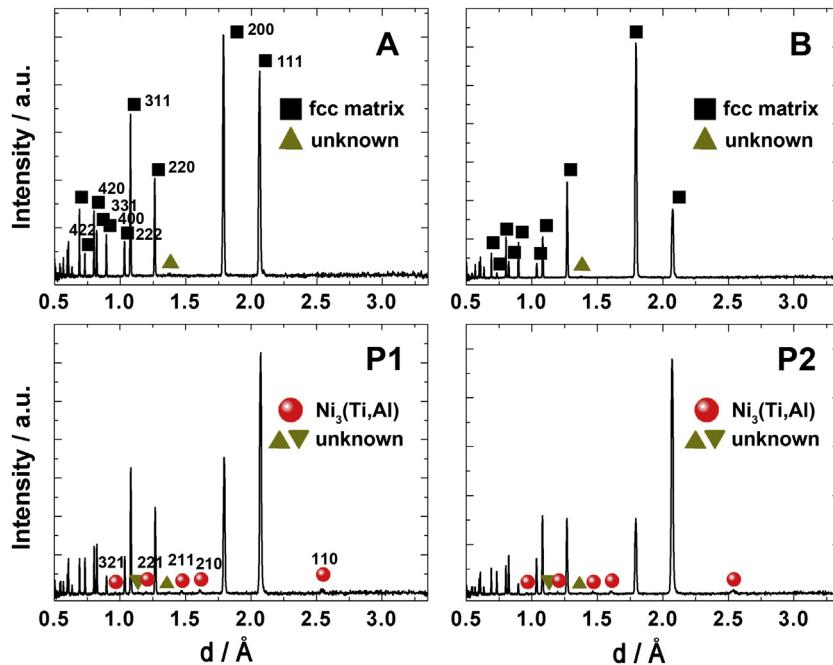


Fig. 1. Neutron diffraction patterns of the four HEA samples.

results, however, both P1 (Fig. 2c) and P2 (Fig. 2d) show a significant amount of fine precipitates. In addition to these fine precipitates, a few blocky particles at the micro-scale were observed to form near the grain boundary region in P1 (marked by arrows in Fig. 2c). Additional study of these large particles using TEM-EDX indicates that they are enriched in Ni, Al and Ti, and the corresponding TEM selected area electron diffraction (SAED) patterns (not shown) identify it as the Ni<sub>2</sub>AlTi phase; the results are summarized in Table 1. According to a recent work by Choudhuri et al. [17], this phase has a L<sub>2</sub><sub>1</sub> Heusler-like structure (strong but brittle at room temperature), and is incoherent with the fcc HEA matrix. An enlarged view of the precipitate morphology is presented in Fig. 2e and f for P1 and P2, respectively. In P1 (Fig. 2e), two regions with distinct precipitate morphologies are observed (as marked). Region I consists of spherical particles with a size less than 40 nm and homogeneously distributed inside the grain, whilst Region II consists of plate-like precipitates with a width larger than 70 nm. In P2 (Fig. 2f), however, precipitates appear to be more uniform throughout the entire matrix, with a diameter ranging from 20 to 100 nm. The L<sub>2</sub><sub>1</sub> Ni<sub>2</sub>AlTi particles are also found, but in a finer scale of ~100 nm and they appear as irregular blocks, as arrowed in Fig. 2f. Further detailed structure description and strengthening mechanism analysis of this L<sub>2</sub><sub>1</sub> phase are considered not important, because of the relative low volume fraction in both P1 and P2.

### 3.2. TEM characterization

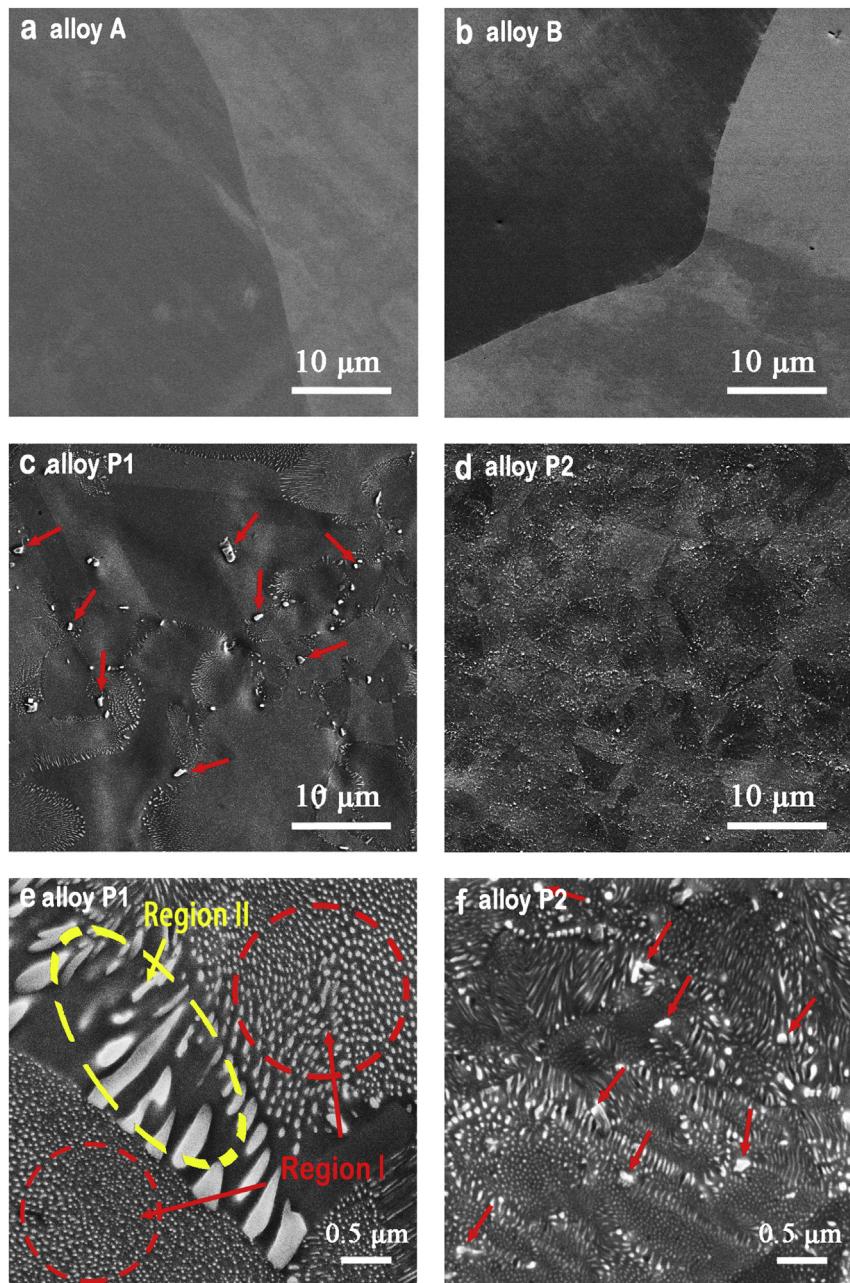
Since the precipitation sequence in alloy P1 and P2 are expected to be similar with only some minor differences, for simplicity and clarity, we mainly focus on the discussion of the microstructure in P1. A representative bright field (BF) TEM image taken from P1 is presented in Fig. 3a, which gives a general view of two regions of nano-precipitates. In the right insets of Fig. 3a, three SAED patterns along different Z-axes taken from Region I are shown. The main diffraction spots confirm that the matrix is indeed fcc, whilst additional weak spots observed in all the images affirm the presence of precipitates which has a superlattice L<sub>1</sub><sub>2</sub> structure. Together with the neutron diffraction results, we can eventually identify the

L<sub>1</sub><sub>2</sub> phase as Ni<sub>3</sub>(Ti, Al) type  $\gamma'$  phase (hereafter denoted as  $\gamma'$  phase). Similar diffraction patterns were also obtained in Region II (e.g., the image along Z-[1 1 0] shown in the left inset of Fig. 3a), suggesting that precipitates in both regions are the same, although their morphologies are obviously different. The lattice parameter of both the disordered fcc matrix and precipitates were measured to be 0.358 nm. The lattice mismatch appears to be extremely small, revealing a coherent interface between them.

Further, two corresponding bright and dark field images are shown in Fig. 3b and c. With a upper region boundary and a under twin boundary, a group of spherical  $\gamma'$  phase particles dispersed in the Region I matrix is demonstrated. To reveal the interfacial coherence, a high resolution TEM picture showing the interface between a particle and the fcc matrix is presented in Fig. 3d. The fast Fourier transformation (FFT) images indicate a (1 1 1) atomic plane, for both matrix and particle. In the figure, two groups of atoms across the interface are selected, and labeled with different colors, to conveniently distinguish each other: pink for atoms belonging to the particle and green for those of the matrix (seen in Fig. 3d). In this manner, the transition of atomic arrangement across the particle-matrix interface is directly shown. The corresponding lattice sketches are also inserted, exhibiting the typical (1 1 1) plane of atoms of the A1 crystal structure (i.e., the basic fcc structure) and L<sub>1</sub><sub>2</sub> crystal structure, for green and pink regions respectively. The blue balls represent small constituent atoms (here are Ni, Fe, Co or Cr) which compose of the A1 matrix lattice, while the orange ones stand for the large atoms of Al or Ti, occupying the face centered position in the superlattice. These results provide us with a visual understanding of the particle-matrix interface structure in detail.

### 3.3. Atom probe tomography (APT) analysis

To obtain the chemical distribution of the constituent atoms, we employed 3D-APT reconstruction of alloy P1. Atom maps in Region I in P1 with Fe, Co, Cr and Ni, Al, Ti color-coded and resolved in two boxes are given in Fig. 4a. Generally, many visible particles enriched with Ni, Al, Ti in a size of tens of nanometers are embedded in the homogeneous matrix. A 35% Ni iso-concentration map is further

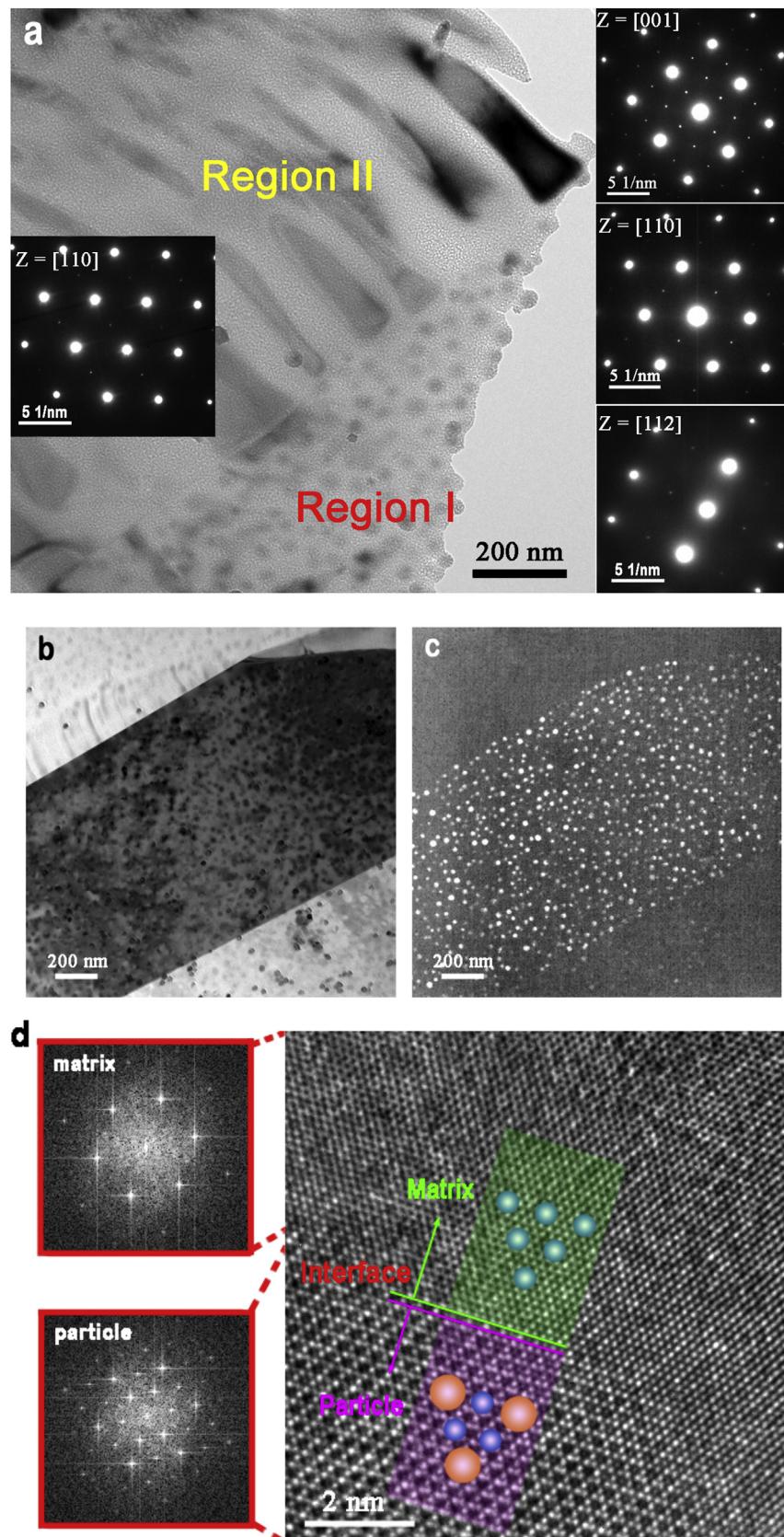


**Fig. 2.** SEM micrographs of electrochemical polished HEAs; (a) alloy A, (b) alloy B, (c) alloy P1 and (d) alloy P2 at low magnification. An enlarged view of the precipitate morphology is given in (e) and (f) for alloy P1 and P2, respectively.

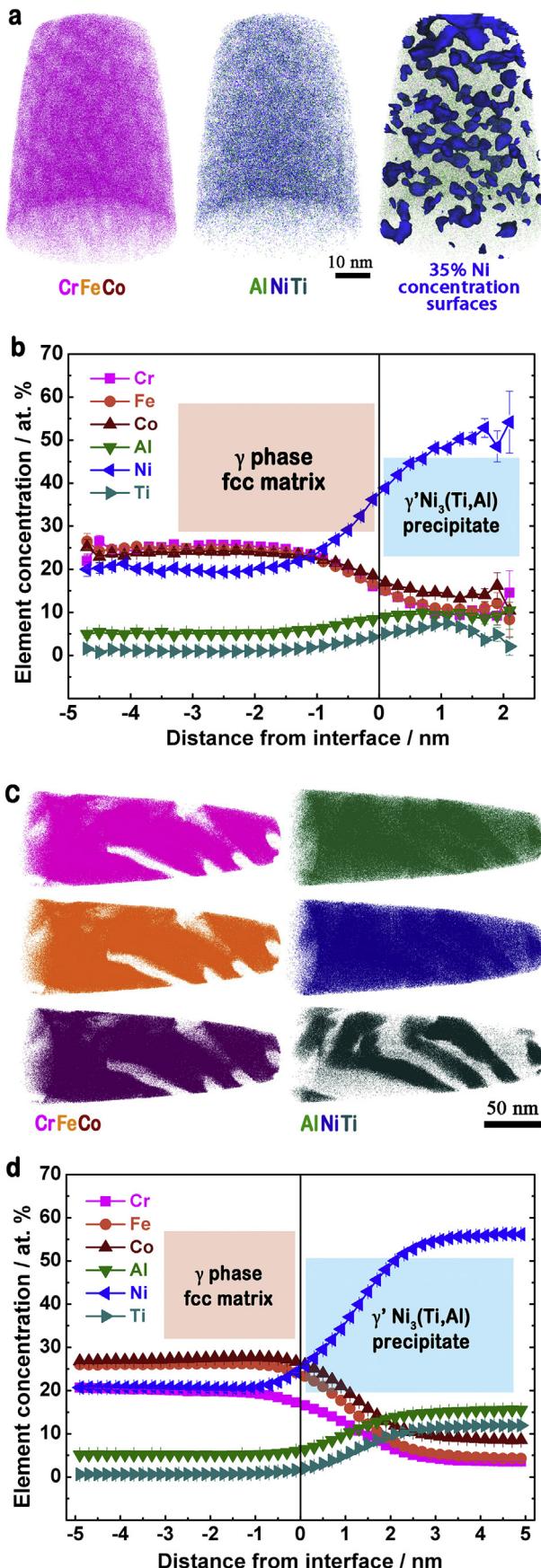
**Table 1**

Chemical compositions of different phases in high-entropy alloys A, B, P1 and P2 by TEM-EDX measurements (at.%).

Alloys	Phases	Chemical compositions (at.%)					
		Al	Ti	Cr	Fe	Co	Ni
A	matrix	—	—	23.1 ± 0.4	25.9 ± 0.7	24.3 ± 0.9	24.7 ± 1.0
B	matrix	4.4 ± 0.1	2.1 ± 0.1	22.0 ± 0.2	24.1 ± 0.2	23.3 ± 0.2	24.1 ± 0.3
P1	matrix	1.3 ± 0.1	0.8 ± 0.1	25.8 ± 0.1	24.4 ± 0.2	26.1 ± 0.2	21.6 ± 0.2
	γ'	8.4 ± 0.1	2.1 ± 0.2	11.6 ± 0.2	13.3 ± 0.2	17.4 ± 0.3	47.1 ± 0.4
P2	Ni <sub>2</sub> AlTi	22.3 ± 0.2	17.4 ± 0.2	3.4 ± 0.1	5.0 ± 0.2	22.2 ± 0.3	31.7 ± 0.4
	matrix	2.2 ± 0.1	0.2 ± 0.1	26.8 ± 0.4	26.7 ± 0.4	25.1 ± 0.4	19.0 ± 0.4
	γ'	6.3 ± 0.1	2.7 ± 0.1	19.2 ± 0.3	20.2 ± 0.3	21.2 ± 0.3	30.4 ± 0.4
	Ni <sub>2</sub> AlTi	18.6 ± 0.2	14.5 ± 0.2	3.1 ± 0.1	6.2 ± 0.2	19.3 ± 0.3	38.3 ± 0.4



**Fig. 3.** Bright TEM field image of Region I and II (a); (b) and (c) are the corresponding bright and dark field images showing the particles distribution in Region I, (d) high-resolution TEM image showing the interface between one single nano-particle and fcc matrix, with relative FFT patterns are shown in the left; the atomic arrangement are directly distinguished.



displayed to delineate the outline of particles. In Fig. 4b, the elemental partitioning is shown in a proximity histogram constructed across the interface between the matrix and precipitates. It is noted that, in  $\gamma'$  phase particles, despite up to 50% Ni concentration, some of the Ni sites are still taken by substitutional atoms, such as Fe, Co and Cr (~30% in total). In Region II, separate plots of each element are shown in Fig. 4c. The depletion or enrichment of each element in some regions easily reveals the plate-like precipitation morphology and its accompanied compositional separation, just as shown in the corresponding proximity histogram of elemental concentration in Fig. 4d. In the precipitates side (on the right-hand-side of the figure), Ni concentration almost reaches 60 at.%, whilst Fe and Cr are largely depleted. Also, the concentration difference between the precipitate and matrix is larger, which means being more close to the components of Ni<sub>3</sub>Al compounds than the spherical particles in Region I. From the above observations, we can tentatively conclude that Region II may have initially evolved from Region I during the long aging process. Additional work to identify the kinetic path for precipitate formation is currently underway.

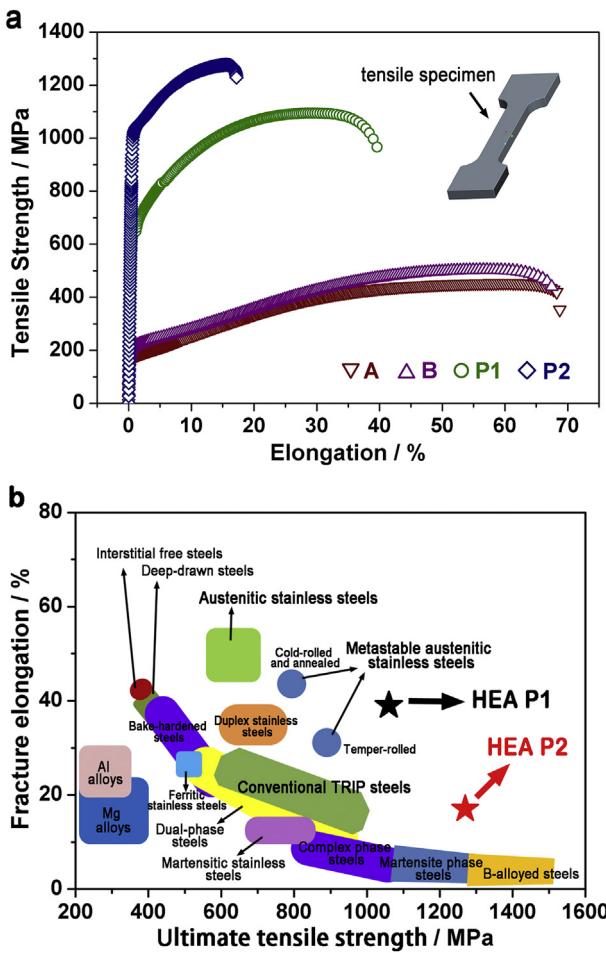
### 3.4. Tensile properties at room temperature

Representative tensile stress-strain curves of the four specimens are shown in Fig. 5a. The ultimate strengths of A and B samples are noted to be 453 and 503 MPa, respectively. Since there is essentially no second phase in these two alloys, the slight strength increase in the homogenized sample B (~50 MPa) is probably attributable to the solid-solution effect caused by the Ti and Al additions. After thermomechanical treatments, strengths of both P1 and P2 alloys are noted to dramatically increase, and specifically the yield and ultimate tensile strengths of P1 become 645 and 1094 MPa, respectively, without significant loss in plasticity (~39%). For the P2 sample, yield and ultimate tensile strengths are even higher at 1005 and 1273 MPa, respectively, whilst the elongation still remains at a respectable value of 17%. The yield strength of over 1 GPa is particularly noteworthy since, to the authors' knowledge, such high yield strength has not been reported in fcc-HEAs before. We can further estimate the toughness of these alloys and compare it with that of other conventional alloys. The product of strength and elongation for P1 reaches a value of 42,600 MPa%, which well exceeds the level of many TRIP steels (only about 15,000–30,000 MPa%) [18–21]. A direct comparison of the tensile strength and elongation of the current HEAs with those of several advanced steels (data from Ref. [19]) is presented in Fig. 5b. The current P1 and P2 HEAs are located at the upper-right above the general curve for the conventional alloys, clearly indicating that they outperform most advanced steels.

## 4. Discussion

Strengthening mechanisms in polycrystalline materials are traditionally summarized into four categories: solid-solution hardening, grain-boundary hardening, dislocation hardening, and precipitation hardening. As the four mechanisms are operating independently, yield strength is a simple summation of the four

**Fig. 4.** APT results in P1. For Region I; two boxes of atom maps with Fe, Co, Cr and Al, Ni, Ti separately and one box with 35% Ni iso-concentration surface showing the outline of particles (a), and (b) the proximity histogram constructed across the interface between the matrix and precipitates. For Region II; atom map of each component showing a plate-like structure (c), and (d) the proximity histogram indicating a larger difference of element distribution.



**Fig. 5.** Tensile properties of alloys A, B, P1 and P2 at room temperature (a), and the map of ultimate tensile strength–ductility combinations of various advanced steels including P1 and P2 HEAs (b), showing great advantage of the current HEAs.

individual contributions and can be expressed as [22]:

$$\sigma_{0.2} = \sigma_A + \Delta\sigma_S + \Delta\sigma_G + \Delta\sigma_D + \Delta\sigma_P \quad (1)$$

where  $\sigma_A = 165 \text{ MPa}$  is the yield strength of alloy A, which is the intrinsic strength, or the so-called lattice friction strength, and  $\Delta\sigma_S$ ,  $\Delta\sigma_G$ ,  $\Delta\sigma_D$  and  $\Delta\sigma_P$  are strengthening contributions from solid solution, grain boundary, dislocations, and precipitates, respectively. In the following, we will focus on these mechanisms and evaluate their contributions to the overall strength in the current HEA individually.

#### 4.1. Solid solution hardening

Traditional approaches of measuring the effect of solid-solution hardening are all based on dilute solution alloys, especially for binary systems [23,24]. However, for HEAs, generally known as “concentrated solid-solution” systems, the terms “solute” and “solvent” lose their conventional meanings. How to evaluate, or just define, the precise contribution of solid-solution strengthening in HEAs, remains a challenge. Recently, Toda-Caraballo et al. [25] made special efforts to extend the traditional solid solution hardening theories to include concentrated multicomponent alloys such as HEAs, however, the model still has difficulties to describe materials with complex chemical structures (for example, precipitates, a mixed fcc plus bcc structure). Fortunately, the current HEA can be

simply treated as a FeCoNiCr solvent matrix containing Ti + Al solutes, and a standard model for substitutional solid solution strengthening based on dislocation-solute elastic interactions can be directly applied to evaluate the potency of solution strengthening caused by Ti and Al [26,27], namely,

$$\Delta\sigma_S = M \cdot \frac{G \cdot \varepsilon_s^{3/2} \cdot c^{1/2}}{700} \quad (2)$$

where G is the shear modulus for the Ti<sub>2</sub>Al<sub>4</sub> system (78.5 GPa). c is the total molar ratio of Ti + Al in the simple fcc matrix, which is listed in Table 1. M = 3.06 is the Taylor factor, a factor that converts shear stress to normal stress for a fcc polycrystalline matrix. The interaction parameter  $\varepsilon_s$  is expressed as:

$$\varepsilon_s = \left| \frac{\varepsilon_G}{1 + 0.5\varepsilon_G} - 3 \cdot \varepsilon_a \right| \quad (3)$$

which combines the effects of elastic and atomic size mismatches, i.e.,  $\varepsilon_G$  and  $\varepsilon_a$ , and they are defined as:

$$\varepsilon_G = \frac{1}{G} \frac{\partial G}{\partial c} \quad (4)$$

$$\varepsilon_a = \frac{1}{a} \frac{\partial a}{\partial c} \quad (5)$$

where a is the lattice constant of the FeCoNiCr base alloy matrix.

The parameter  $\varepsilon_a$  can be readily obtained from refined XRD patterns (lattice parameters are: 0.3578, 0.3594 and 0.3590 nm for A, P1 and P2, respectively), while the parameter  $\varepsilon_G$  is usually negligible compared to  $\varepsilon_a$ . In this case, the value of  $\varepsilon_s$  and thus  $\Delta\sigma$  can be properly estimated. The strength enhancement caused by solid-solution hardening in P1 and P2 (as compared to the base alloy A) can be subsequently calculated to be  $\Delta\sigma_{S1} = 25.4 \text{ MPa}$  and  $\Delta\sigma_{S2} = 14.4 \text{ MPa}$ , respectively. These values are obviously too small to account for the strength difference, suggesting that solid solution hardening is not the dominant mechanism.

#### 4.2. Grain-boundary hardening

It is also known that grain-size refinement can improve the strength of an alloy. Smaller grain size offers a higher volume fraction of grain-boundaries, which could impede dislocation motion. The relationship between yield strength and grain size can be well described by the classical Hall-Petch equation [28,29]:

$$\sigma_y = \sigma_0 + k_y / d^{1/2} \quad (6)$$

where  $\sigma_y$  is the yield stress,  $\sigma_0$  is again the lattice friction stress,  $k_y$  is the strengthening coefficient and d is the average grain diameter. According to Eq. (6), yield strength increase caused by grain size difference ( $\Delta\sigma_G$ ) can be expressed as:

$$\Delta\sigma_G = k_y (d_p^{-1/2} - d_A^{-1/2}) \quad (7)$$

where  $d_p$  represent the grain size of the thermomechanically processed materials. In this work, we adopt the value of  $k_y$  from the FeCoNiCrMn system, that is,  $226 \text{ MPa} \cdot \mu\text{m}^{1/2}$  according to the study of Liu et al. [30]. The average grain sizes of alloys A, P1 and P2 measured from using SEM and TEM are  $d_A = 289.7 \mu\text{m}$ ,  $d_{P1} = 15.7 \mu\text{m}$ , and  $d_{P2} = 2.8 \mu\text{m}$ , respectively. The current alloys are noted to contain only a few twins. Even including these twin boundaries in the calculations, we obtain  $\Delta\sigma_{G1} = 43.7 \text{ MPa}$  and  $\Delta\sigma_{G2} = 122.6 \text{ MPa}$ . The grain boundary contribution in P2

alloy is almost three times as much as that in the P1 alloy. However, both values are relatively small to account for the total strength increase.

### 4.3. Dislocation hardening

Plastic deformation results from the movement of mobile dislocations, and these dislocations interact with each other, then impede their own motion. In general, a higher dislocation density leads to a higher yield strength. A Bailey–Hirsch formula [31] is applied here to describe the relationship as:

$$\Delta\sigma_D = M\alpha Gb\rho^{1/2} \quad (8)$$

where  $\alpha = 0.2$  is a constant for fcc metals,  $\rho$  stands for the dislocation density, and  $b$  is the burger vector, for a fcc structure,  $b = \sqrt{2}/2 \times a_{Ti2Al4} = 0.255 \text{ nm}$  (see Ref. [32]).

We roughly estimated the dislocation density through the Williamson-Hall method, a widely used first approximation to assess the effects of micro strain and crystallite size [33,34]. In this approach, the true XRD peak broadening  $\beta$  (the observed peak broadening deducting the instrument broadening) consists of two parts: the crystallite size broadening  $\beta_G$  and the strain broadening  $\beta_S$  [35,36], and based on the assumption of Cauchy-type function, they are:

$$\beta = \beta_G + \beta_S \quad (9)$$

$$\beta_G = K\lambda/(D \cdot \cos\theta) \quad (10)$$

$$\beta_S = 4\epsilon \cdot \tan\theta \quad (11)$$

where  $K \sim 0.9$  is a constant,  $\lambda = 0.15405 \text{ nm}$  is the wavelength of Cu Ka radiation,  $D$  is the crystallite size,  $\epsilon$  is the micro strain, and  $\theta$  is the Bragg angle of the certain peak. Focusing on the micro strain  $\epsilon$  only, Eq. (9) can be rewritten as:

$$\beta \cos\theta = K\lambda/D + (4\sin\theta) \cdot \epsilon \quad (12)$$

The slope of the linear fit of the  $\beta \cos\theta - 4\sin\theta$  plot determines the parameter  $\epsilon$ . Such plots for P1 and P2 are shown in Fig. 6. It is seen that, the micro strain of P2, i.e.,  $\epsilon_2 = 0.102$ , with a relative small positive intercept of 0.03 resulting from the experimental errors. However, the micro strain for P1, i.e., the  $\epsilon_1$  value, is nearly zero ( $\sim -0.002$ ). This kind of phenomenon has also been observed in

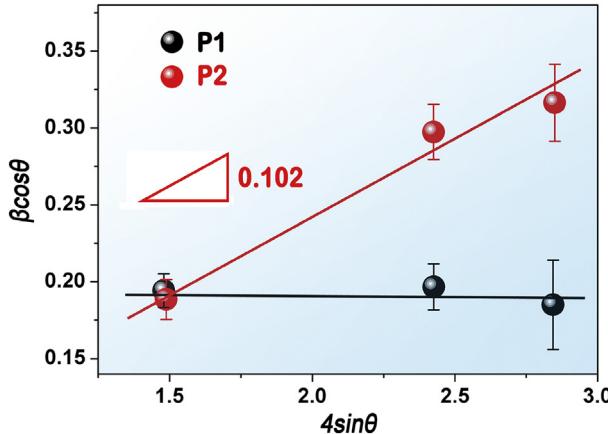


Fig. 6. The peak broadening  $\beta$  as a function of  $4\tan\theta$ ; the slope of the linear fit shows the value of micro strain  $\epsilon$ .

another alloy system [37] in which it was suggested to be caused by the fact that the fully annealed structure has few dislocations. Here, we believe the occurrence of a similar situation in P1, which was heat-treated 2 h at a relatively high temperature of 1273 K (above 0.75 Tm). Considering the data and pattern refinement error, it is reasonable to treat the micro strain in P1 as  $\epsilon_1 = 0$ .

The dislocation density, can then be derived from the micro strain above [34,38]:

$$\rho = 2\sqrt{3} \cdot \epsilon / (Db) \quad (13)$$

from which, the dislocation density in P1 and P2 can be determined as  $\rho_1 \approx 0$  and  $\rho_2 = 5.02 \times 10^{14} \text{ m}^{-2}$ . Inserting these values into Eq. (8), the yield strength increment from dislocation strengthening is evaluated as  $\Delta\sigma_{D1} = 0$  and  $\Delta\sigma_{D2} = 274.5 \text{ MPa}$ , in P1 and P2, respectively. The result indicates that dislocation hardening plays a somewhat important role on the strength of P2. It also suggests that annealing at the intermediate temperature of 923 K is insufficient to annihilate the large amount of dislocations created during the heavy cold work (70%).

### 4.4. Precipitation hardening

As shown in Fig 2, both P1 and P2 are full of fine precipitates and these precipitates are expected to produce hardening, either through a dislocation by-pass mechanism (Orowan-type) or particle shearing mechanism. Generally, Orowan mechanism occurs when the radius of particles exceeds a critical value or is incoherent with the matrix, however, shearing mechanism would dominate when precipitates are sufficiently small and coherent. Based on the current precipitate morphology, particle shearing is expected to take the control. We will, therefore, focus our discussion on this mechanism in the following.

As discussed earlier, the microstructure of P1 consists of two different regions each with its own precipitate size and distribution. In this case, a simple composite model is applicable to estimate the strength, namely,

$$\sigma_{P1} = \sigma_I \cdot C_I + \sigma_{II} \cdot C_{II} \quad (14)$$

where  $\sigma_{P1}$  is the overall strength,  $\sigma_I$  and  $\sigma_{II}$  represent the intrinsic strength of Region I and II, respectively, and  $C_I$  and  $C_{II}$  are the volume fractions of Region I and II, respectively. Many of the precipitates in Region II are noted to be actually plate-like, but to simplify our analysis, we will treat these particles as spherical. The fraction, size and spacing of precipitates are evaluated from the microstructural observation and summarized in Table 2.

In the calculation of the effect of particles sheared by dislocations, three contributing factors are considered and they are particle-matrix coherency ( $\Delta\sigma_{CS}$ ), modulus mismatch ( $\Delta\sigma_{MS}$ ) and atomic ordering ( $\Delta\sigma_{OS}$ ) [39–41]. The former two make contributions prior to the shearing, while the latter one contributes during the shearing. In principle, the larger one of  $\Delta\sigma_{CS} + \Delta\sigma_{MS}$  and  $\Delta\sigma_{OS}$  determines the resultant contribution in these sequential processes. The equations for these contributions are [42].

$$\Delta\sigma_{CS} = M \cdot \alpha_e (G \cdot \epsilon)^{3/2} \left( \frac{rf}{0.5Gb} \right)^{1/2} \quad (15)$$

$$\Delta\sigma_{MS} = M \cdot 0.0055 (\Delta G)^{3/2} \left( \frac{2f}{G} \right)^{1/2} \left( \frac{r}{b} \right)^{3m/2-1} \quad (16)$$

**Table 2**

Fraction, size and spacing data of precipitates in P1 and P2 alloys. Specially, in Region II of alloy P1, the spacing and radius data are calculated in width direction of the plates. The strengthening effect of the Ni<sub>2</sub>AlTi phase is negligible due to its low volume fraction.

Alloys	Regions or particles	Region fraction C (%)	Precipitates fraction f (%)	Precipitates radius r (nm)	Particle spacing L <sub>p</sub> (nm)
P1	I	68.1	23.3	12.6	17.2
	II	31.9	16.2	46.3	90.9
P2	γ'	—	26.8	9.7	11.3
	Ni <sub>2</sub> AlTi	—	2.77	25.9	182.9

$$\Delta\sigma_{OS} = M \cdot 0.81 \frac{\gamma_{APB}}{2b} \left( \frac{3\pi f}{8} \right)^{1/2} \quad (17)$$

where  $\alpha_e = 2.6$  for fcc structure,  $m = 0.85$ ,  $\varepsilon \approx 2/3 \cdot (\Delta a/a)$  is the constrained lattice parameter mismatch, with  $(\Delta a/a) = 0.0026$  in this work, where  $\Delta a$  is the difference of lattice constant between Ni<sub>3</sub>(Ti,Al) phase and the fcc matrix of P1 and P2 calculated from the XRD results;  $f$  is the volume fraction of the precipitates,  $\Delta G$  is the shear modulus mismatch between precipitates and matrix, and  $\gamma_{APB}$  is the anti-phase boundary energy of the precipitates,  $\Delta G = 81 - 77 = 4 \text{ GPa}$ ,  $\gamma_{APB} = 0.12 \text{ J/m}^2$  are adopted from the corresponding data of Ni<sub>3</sub>Al precipitates in Ni-based superalloys [43]. The calculated individual values of  $\Delta\sigma_{CS}$ ,  $\Delta\sigma_{MS}$  and  $\Delta\sigma_{OS}$  are listed in Table 3, and the final strength increment from shearing  $\Delta\sigma_{SH}$  is determined to be  $\Delta\sigma_{SH1-I} = 305.6 \text{ MPa}$  and  $\Delta\sigma_{SH1-II} = 371.9 \text{ MPa}$  for Regions I and II in sample P1, respectively, and  $\Delta\sigma_{SH2-Ni3(Ti,Al)} = 327.7 \text{ MPa}$  in sample P2. Consequently, the overall hardening contributed by precipitates in samples P1 and P2 are  $\Delta\sigma_{P1} = 326.7 \text{ MPa}$  and  $\Delta\sigma_{P2} = 327.7 \text{ MPa}$ , respectively. This result shows that the two alloys actually have a similar strengthening effect from precipitation.

Based on the discussion above, the yield strengths of P1 and P2 HEAs are calculated as  $\sigma_1 = 560.8 \text{ MPa}$  and  $\sigma_2 = 904.2 \text{ MPa}$ . For clarity, we summarize a column chart (Fig. 7) to directly show the strength contributions from the four individual mechanisms as well as the overall contributions (right column). It is apparent that the predicted data are in reasonable agreement with the experimental values (marked by the black and red dots). The small discrepancy may be attributable to a couple of reasons. First, the precipitates in Region II of P1, are considered to be spherical in the models to simplify calculations, however, many of them are actually in plate-like shape. Irregular plate-shaped particles are expected to produce more resistance to plastic flow as compared to smooth spherical particles. Secondly, texture difference actually exists, according to the Neutron diffraction results before. It could be developed during the cold-rolling and recrystallization process in present HEAs, according to the reported results by Dan recently [44], which can to some degree affect the overall strength of the materials. Furthermore, in our calculations, several intrinsic parameters (e.g.,  $\Delta G$  and  $\gamma_{APB}$ ) are borrowed from Ni-based superalloys. Nevertheless, the agreement between experiments and calculations is quite satisfactory. It is especially noted that, in the thermomechanically processed P1 and P2, precipitation hardening offers the largest strength increment. The P2 alloy, in particular, shows a much higher strength yet still keeps a respectable ductility,

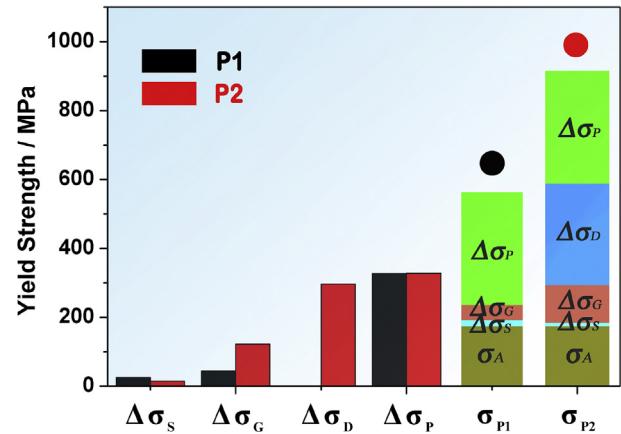


Fig. 7. The strength contributions from different hardening mechanisms. The calculation values agree well with the experimental data.

due to a good utilization of various hardening mechanisms: grain boundary hardening, dislocation hardening, and most importantly, the precipitation hardening.

## 5. Conclusion

As elaborated above, for the first time, we demonstrate that a minor Ti and Al alloying addition can produce a fine dispersion of L<sub>12</sub> coherent nano-precipitates in a fcc HEA alloy by proper thermomechanical treatments. These nano-precipitates can drastically enhance the strength of the alloy without compromising its tensile ductility.

We have presented two examples to illustrate the strengthening effects. The first example is a HEA (alloy P1), whose structure is composed of a mixture of two precipitate morphologies: Region I consists of nano-precipitates less than 40 nm in size, while Region II consists of particles coarser than 100 nm. All of these nano-scaled precipitates are identified to be the L<sub>12</sub> Ni<sub>3</sub>(Ti, Al)-type γ' phase. This simple composites structure results in a 645 MPa yield strength with an outstanding 39% elongation. Precipitation hardening is the dominant strengthening mechanism in this alloy, which contributes a strength increment of about 326.7 MPa. In the second example (alloy P2), the alloy consists of very fine dispersion of nano-precipitates, main the coherent γ' phase, although there are also minor nano-scale Ni<sub>2</sub>AlTi particles. This alloy exhibits even higher yield strength of over 1 GPa, but still keeps a reliable 17%

**Table 3**

Strength contributions during shearing process, showing the total strength increment derived from the shearing mechanism.

Alloys	Regions or particles	Δσ <sub>CS</sub> (MPa)	Δσ <sub>MS</sub> (MPa)	Δσ <sub>OS</sub> (MPa)	Δσ <sub>CS</sub> + Δσ <sub>MS</sub> (MPa)	Δσ <sub>SH</sub> (MPa)
P1	I	216.8	29.8	305.6	246.6	305.6
	II	346.5	35.6	254.8	382.1	382.1
P2	—	204.0	29.8	327.7	233.8	327.7

tensile ductility. The exceptionally high yield strength results from contributions of precipitation hardening (327.7 MPa), dislocation hardening (274.5 MPa), and grain boundary hardening (122.6 MPa).

In summary, we have shown a successful exploration to find a way for effectively strengthening fcc-HEA systems using a controllable thermomechanical procedure. The resultant microstructure consists of precipitates with an L1<sub>2</sub>-structure and structurally coherent with their fcc alloy matrices. It bears great resemblance to that of γ'-γ Ni superalloys, which are the cornerstone of high-temperature gas turbine engine materials. Our findings open a new door for the future development of HEAs for high-temperature structural applications.

## Acknowledgments

This research was supported by National Natural Science Foundation of China (51531001, 51422101 and 51271212, 51371003), 111 Project (B07003), International S&T Cooperation Program of China (2015DFG52600) and Program for Changjiang Scholars and Innovative Research Team in University (IRT\_14R05). TGN acknowledges the support of US National Science Foundation under Contract DMR-1408722. The portion of this research at ORNL's Spallation Neutron Source was sponsored by the Scientific User Facilities Division, Office of Basic Energy Sciences, US Department of Energy.

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