

EE324 CONTROL SYSTEMS LAB

Problem Sheet 7

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Question 1: Gain and Phase Margin

$$G_s = \frac{1}{s(s^2 + 4s + 8)}$$

Part A)

In this part, we have to find gain K such that the Gain margin and phase margin of the closed-loop characteristic function of G_s is 0

We have closed-loop characteristics function as

$$P_s = K * G_s$$

$$P_s = \frac{k}{s(s^2 + 4s + 8)}$$

$$P_s = \frac{k}{s^3 + 4s^2 + 8s}$$

$$s = j\omega$$

$$P_s = \frac{k}{(-4\omega^2) + j(8\omega - \omega^3)}$$

For GM and PM equal to 0, $\omega_{gcf} = \omega_{pcf} = \omega$

The imaginary part will be 0

$$\omega^2 = 8$$

$$f = 0.45 \text{ Hz}$$

magnitude of P_s should be one and phase should be -180°

hence $P_s = -1$

$$P_s = \frac{k}{-4\omega^2} = -1$$

$$k = 4\omega^2$$

$$\mathbf{k = 32}$$

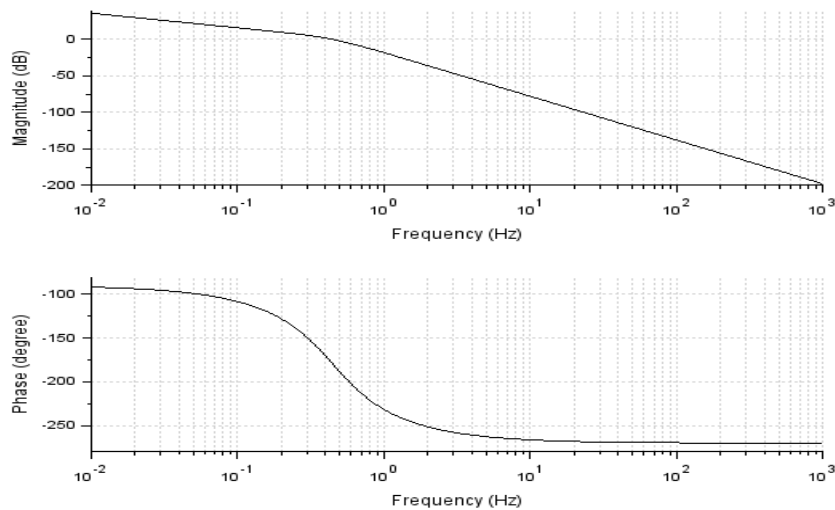


Fig. Bode Plot of Characteristic function

Code for the same:

```
s=%s;
Gs=syslin('c',1/(s*(s^2+4*s+8)));
CharEq=32*Gs;
bode(CharEq,0.01,1000);
```

Part B)

It is not possible to have a non zero gain margin and zero phase margin or vice versa. If the gain margin is zero, then from its definition, we know that at -180° , we have a gain equal to 0 dB.

But this statement also implies a phase margin equal to zero.

We also know that GM and PM decrease monotonically for increasing value of k . Both of them intersect at a point where both are zero. Hence mathematically, it won't be possible to have PM zero and GM non zero.

Part C)

We have a system transfer function for $k=32$

$$T_s = \frac{32}{s^3 + 4s^2 + 8s + 32}$$

Poles of this transfer function are

$$\begin{aligned} & -4 \\ & + j2.83 \\ & - j2.83 \end{aligned}$$

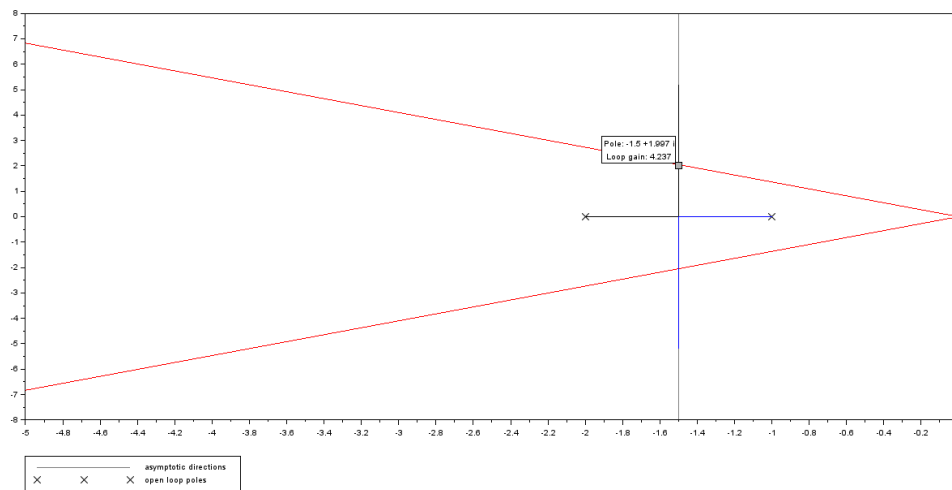
As we can see, the dominant poles of the System are on an imaginary axis; the System becomes unstable

Question 2: Lag Compensator

Part A)

$$G_s = \frac{1}{s^2 + 3s + 2}$$

For this open-loop transfer function G_s , we have to find gain K such that the %OS=10. We can solve this using the Root Locus Method in Scilab



The desired value of gain $K=4.297$

Code for the same:

```
s=%s;  
Gs=syslin('c',1,s^2+3*s+2);  
OS=0.11;  
slope=%pi/2.30;  
x=-5:0.01:0;  
OS_line1=slope.*x;  
OS_line2=-1*slope.*x;  
plot(x,OS_line1,'r');  
plot(x,OS_line2,'r');  
evans(Gs,kpure(Gs));
```

Part B)

Steady state error for unity feedback loop is

$$e(\infty) = \frac{1}{1 + kG(0)}$$

$$e(\infty) = \frac{1}{1 + \frac{4.297}{2}}$$

$$e(\infty) = 0.317$$

Now we will introduce the Lag compensator of z/p ratio 20

Let $z=-0.2$ and $p=-0.01$

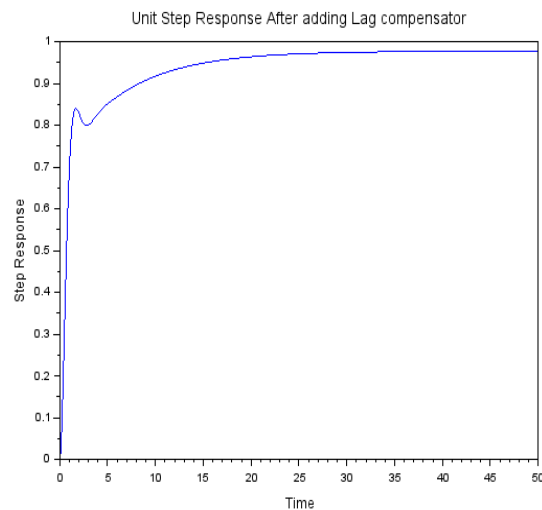
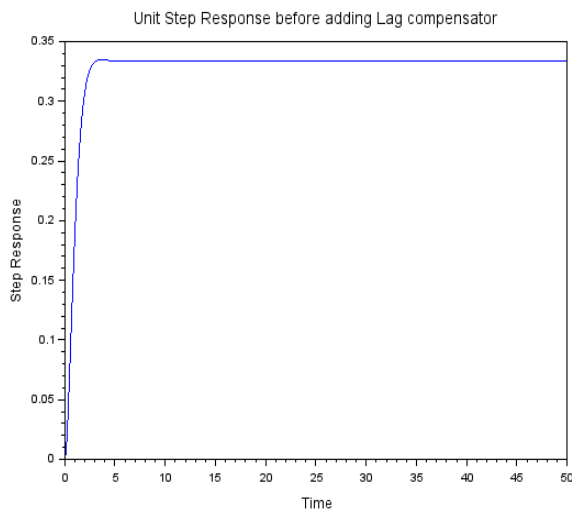
Our new Plant becomes

$$G_s' = \frac{s + 0.2}{(s + 0.01)(s^2 + 3s + 2)}$$

The new value of steady-state error is

$$e(\infty) = \frac{1}{1 + \frac{4.297 * 20}{2}}$$

$$e(\infty) = 0.0227$$



Code for the same:

```
s=%s;
k=4.297;
Gs1=syslin('c',1,s^2+3*s+2);
Gs2=syslin('c',(s+0.2),(s+0.01)*(s^2+3*s+2));
time=0:0.01:100;
```

```

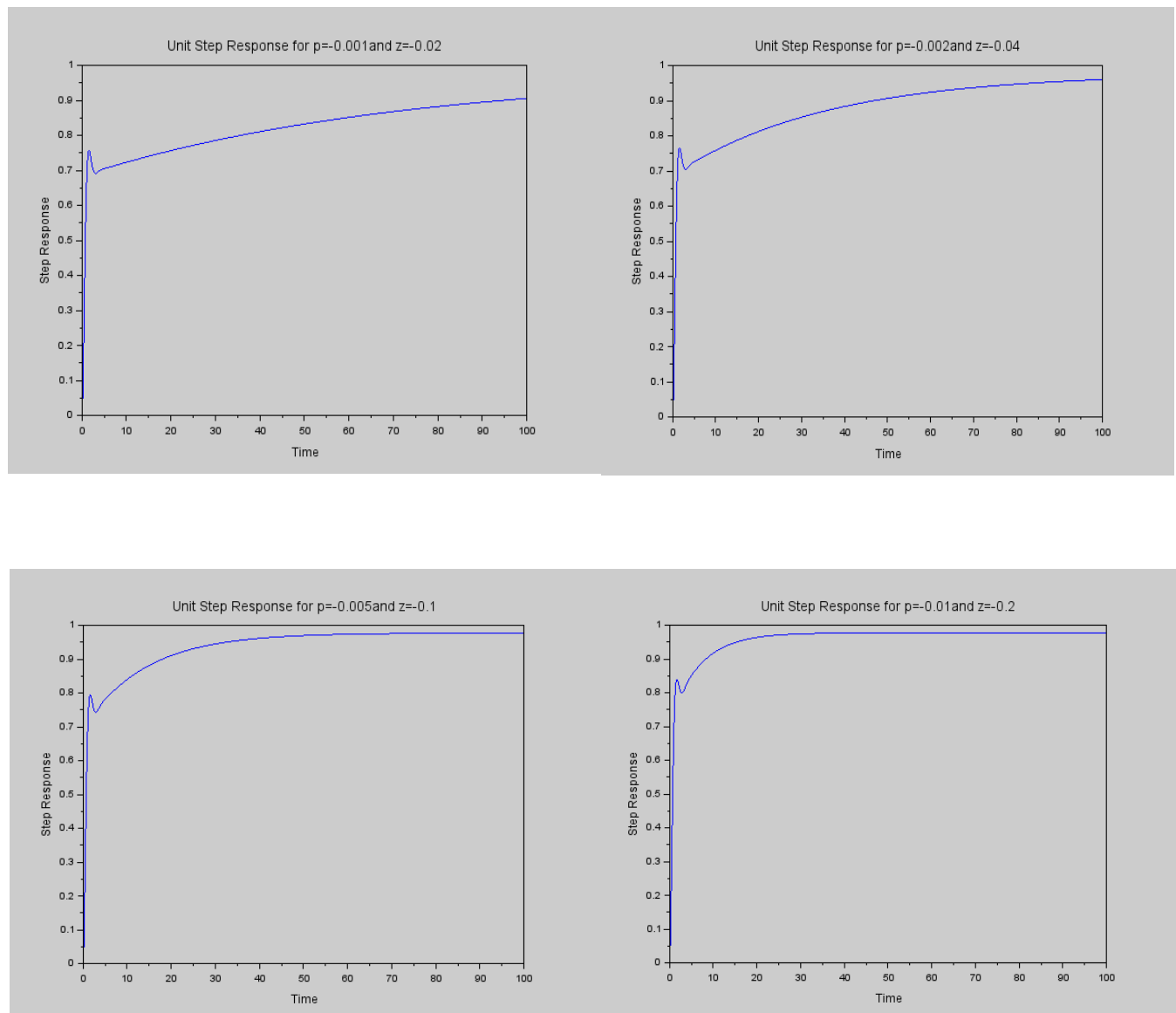
plot(time,csim('step',time,syslin('c',Gs1/(1+Gs1))));
xlabel("Time");
ylabel("Step Response");
xtitle("Unit Step Response before adding Lag compensator");
scf(2);
plot(time,csim('step',time,syslin('c',k*Gs2/(1+k*Gs2))));
xlabel("Time");
ylabel("Step Response");
xtitle("Unit Step Response After adding Lag compensator");

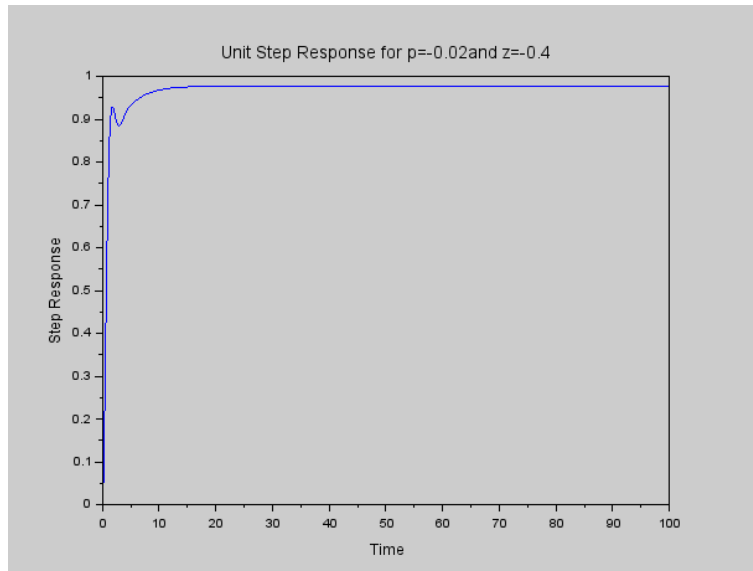
```

Part C)

In this part, we have to vary the pole-zero Location by keeping the z/p ratio constant to 20

Using Scilab we get following Step response for the pole value=[0.001,0.002,0.005,0.01,0.02]





Code for the same:

```
s=%s;
pole_value=[0.001,0.002,0.005,0.01,0.02];
time=0:0.01:100;
k=4.297
for p=pole_value
    z=p*20;
    Gs1=syslin('c',(s+z),(s+p)*(s^2+3*s+2));
    Ts1=syslin('c',k*Gs1/(1+k*Gs1));
    figure,plot(time,csim('step',time,Ts1));
    xlabel("Time");
    ylabel("Step Response");
    xtitle("Unit Step Response for p="+string(-p)+"and z="+string(-
z));
end;
```

Question 3: Lead Compensator

Part A)

In this part, we have to design a lead compensator such that Closed-loop step response has 10% OS and half the settling time than non compensated System

$$G_s = \frac{1}{s^2 + 3s + 2}$$

Pole location for 10% OS calculated using intersection 10%OS line with RL

$$\text{Pole location} \rightarrow -1.5 \pm j2.01$$

$$\zeta \omega_n = 1.5$$

$$\text{Settling time} = T_s = \frac{4}{\zeta \omega_n} = 2.66 \text{ sec}$$

Now we have to design the PD controller such that settling time becomes half

$$\text{The desired value of } T_s = 1.33 \text{ sec}$$

$$\zeta \omega_n = 3$$

$$\text{The real part of poles} = -3$$

Our %OS is the same, so by extrapolating, we get desired root locations as

$$\text{Pole Location} \rightarrow -3 \pm j4.02$$

Original Poles of G_s are -1 and -2

Let zero of lead compensator be at -4

Now after summing angle extended at pole location by poles and zero, we get

$$\text{Sum of angles} = -144.39^\circ$$

Angle extended by the pole of the lead compensator

$$= 180 - 144.39$$

$$= 35.61^\circ$$

$$\text{Pole location of lead compensator} = -3 - \frac{4.02}{\tan(35.61)}$$

$$= -8.613$$

Our new Plant Gs' becomes

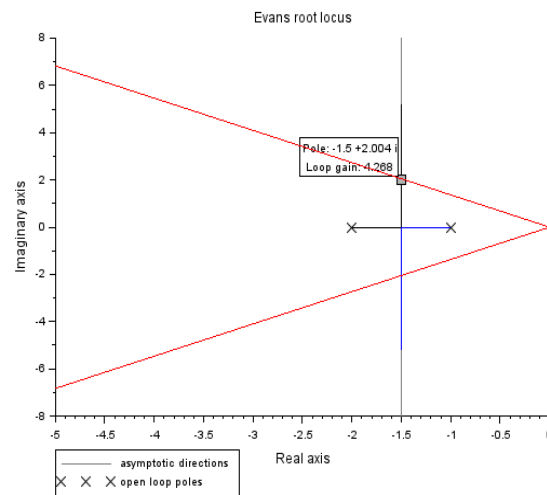
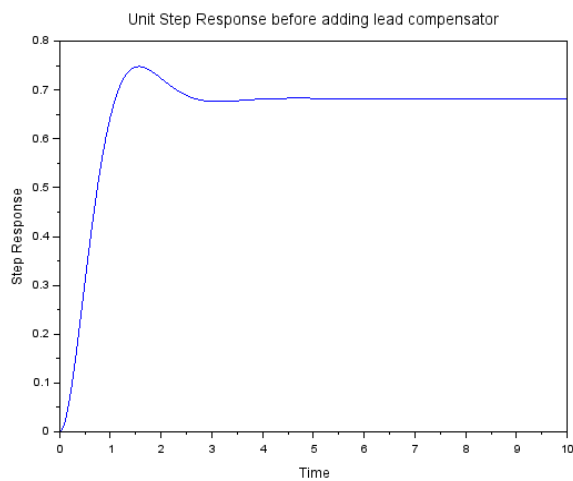
$$Gs' = \frac{k(s + 4)}{(s + 8.613)(s^2 + 3s + 2)}$$

Using Scilab, we get

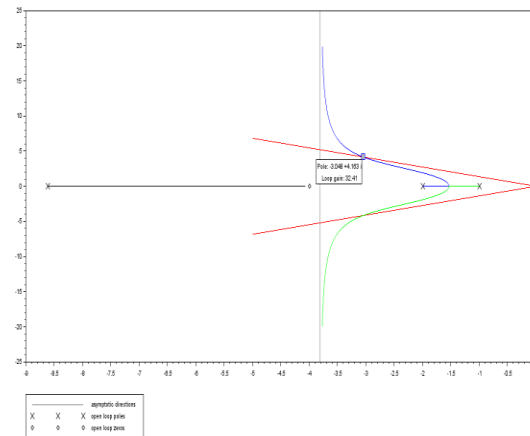
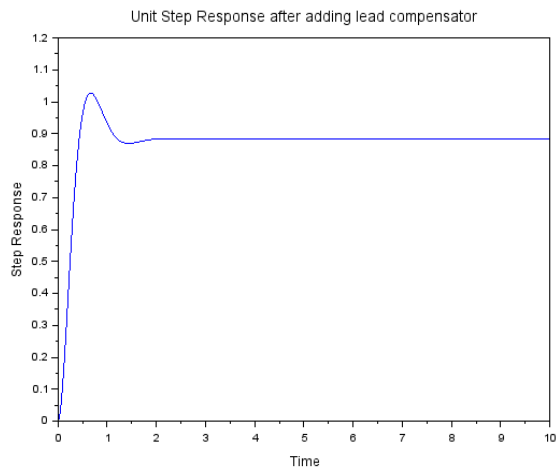
$$K = 32.41$$

$$Gs' = \frac{32.41(s + 4)}{(s + 8.613)(s^2 + 3s + 2)}$$

Before adding Lead Compensator



After adding Lead Compensator



Code for the same:

```
s=%s;
k=32.41;
Gs1=syslin('c',1,s^2+3*s+2);
Gs2=syslin('c',(s+4),(s+8.613)*(s^2+3*s+2));
time=0:0.01:10;
plot(time,csim('step',time,syslin('c',4.297*Gs1/(1+4.297*Gs1))));
xlabel("Time");
ylabel("Step Response");
xtitle("Unit Step Response before adding PD controller");
scf(2);
plot(time,csim('step',time,syslin('c',k*Gs2/(1+k*Gs2))));
xlabel("Time");
ylabel("Step Response");
xtitle("Unit Step Response after adding PD controller");
scf(3);
evans(Gs1,kpure(Gs1));
slope=%pi/2.30;
x=-5:0.01:0;
OS_line1=slope.*x;
OS_line2=-1*slope.*x;
plot(x,OS_line1,'r');
plot(x,OS_line2,'r');
scf(4);
slope=%pi/2.30;
x=-5:0.01:0;
OS_line1=slope.*x;
OS_line2=-1*slope.*x;
plot(x,OS_line1,'r');
plot(x,OS_line2,'r');
evans(Gs2,kpure(Gs2));
```

Part B)

In this part, we have to design a PD controller

First of all, an uncompensated system is

$$G_s = \frac{1}{s^2 + 3s + 2}$$

Pole location for 10% OS calculated using intersection 10%OS line with RL

Pole location → $-1.5 \pm j2.01$

$$\zeta\omega_n=1.5$$

$$\text{Settling time} = T_s = \frac{4}{\zeta\omega_n} = 2.66 \text{ sec}$$

Now we have to design the PD controller such that settling time becomes half

$$\text{The desired value of } T_s = 1.33 \text{ sec}$$

$$\zeta\omega_n=3$$

$$\text{The real part of poles} = -3$$

Our %OS is the same, so by extrapolating, we get desired root locations as

$$\text{Pole Location} \rightarrow -3 \pm j4.02$$

$$\text{Original Poles of } G_s \text{ are } -1 \text{ and } -2$$

We will now measure the angle extended by these poles at the new pole location

$$\text{Sum of angles} = -220.45^\circ$$

$$\text{Angle contribution from zero} = 220.45^\circ - 180^\circ$$

$$= 40.45^\circ$$

$$\text{Now Location of zero} = -3 - \left(\frac{4.02}{\tan(40.45)} \right)$$

$$= -7.83$$

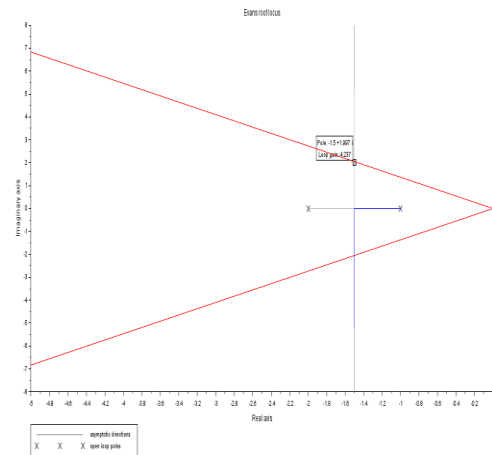
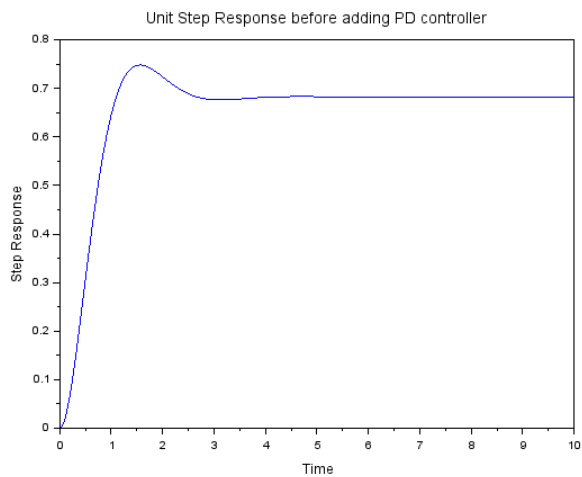
Our new Plant becomes

$$G_s' = \frac{k(s + 7.83)}{s^2 + 3s + 2}$$

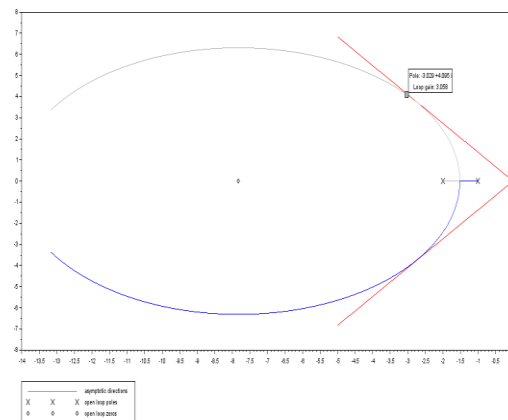
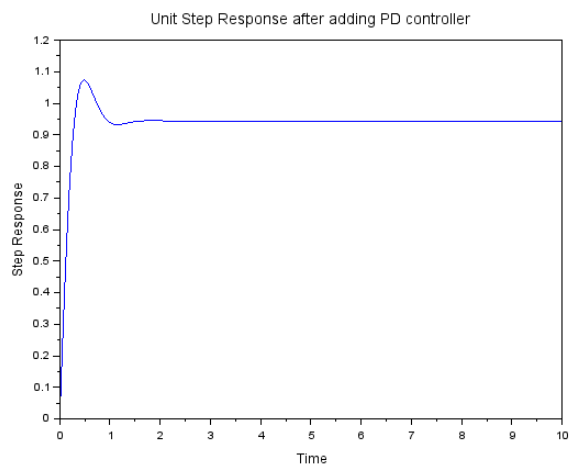
Using Scilab, we get $k = 3.008$

$$G_s' = \frac{3(s + 7.83)}{s^2 + 3s + 2}$$

Before Adding PD controller



After Adding PD controller



Code for the same:

```
s=%s;
k=3;
Gs1=syslin('c',1,s^2+3*s+2);
Gs2=syslin('c',(s+7.83),(s^2+3*s+2));
time=0:0.01:10;
plot(time,csim('step',time,syslin('c',4.297*Gs1/(1+4.297*Gs1))));
xlabel("Time");
ylabel("Step Response");
xtitle("Unit Step Response before adding PD controller");
scf(2);
plot(time,csim('step',time,syslin('c',k*Gs2/(1+k*Gs2))));
xlabel("Time");
ylabel("Step Response");
```

```
xtitle("Unit Step Response after adding PD controller");  
scf(3);  
evans(Gs1, kpure(Gs1));  
slope=%pi/2.30;  
x=-5:0.01:0;  
OS_line1=slope.*x;  
OS_line2=-1*slope.*x;  
plot(x, OS_line1, 'r');  
plot(x, OS_line2, 'r');  
scf(4);  
slope=%pi/2.30;  
x=-5:0.01:0;  
OS_line1=slope.*x;  
OS_line2=-1*slope.*x;  
plot(x, OS_line1, 'r');  
plot(x, OS_line2, 'r');  
evans(Gs2, kpure(Gs2));
```