- 1. Read the attached Chapter 4 and use the experimental results from Table 4.4(a), (b) to
- (a) re-calculate the surface defect and thickness SN ratios using only Test Wafer 1 and Test Wafer 3 data.

計算Defect的S/N ratio可從下列公式得到:

$$\eta = -10\log_{10}(\frac{1}{n}\sum_{i=1}^{n}y^{2})$$

根據wafer 1與wafer 3的結果可得到:

| expt no. | | test wafer 1 | | | SN-1&3 | | |
|----------|------|--------------|--------|------|--------|--------|---------|
| слрі по. | top | center | bottom | top | center | bottom | |
| 1 | 1 | 0 | 1 | 1 | 1 | 0 | 1.76091 |
| 2 | 1 | 2 | 8 | 126 | 3 | 1 | -34.247 |
| 3 | 3 | 35 | 106 | 315 | 50 | 180 | -43.88 |
| 4 | 6 | 15 | 6 | 15 | 40 | 18 | -26.103 |
| 5 | 1720 | 1980 | 2000 | 2020 | 360 | 13 | -64.005 |
| 6 | 135 | 360 | 1620 | 2500 | 270 | 35 | -61.807 |
| 7 | 360 | 810 | 1215 | 1800 | 720 | 315 | -60.086 |
| 8 | 270 | 2730 | 5000 | 9999 | 225 | 1 | -73.442 |
| 9 | 5000 | 1000 | 1000 | 3000 | 2800 | 2000 | -69.016 |
| 10 | 3 | 0 | 0 | 1 | 0 | 1 | -2.6324 |
| 11 | 1 | 0 | 1 | 1 | 0 | 1 | 1.76091 |
| 12 | 3 | 1620 | 90 | 270 | 8 | 3 | -56.541 |
| 13 | 1 | 25 | 270 | 225 | 3 | 0 | -43.158 |
| 14 | 3 | 21 | 162 | 63 | 15 | 39 | -37.325 |
| 15 | 450 | 1200 | 1800 | 1890 | 180 | 25 | -61.506 |
| 16 | 5 | 6 | 40 | 14 | 1 | 1 | -24.911 |
| 17 | 1200 | 3500 | 3500 | 9999 | 600 | 8 | -73.232 |
| 18 | 8000 | 2500 | 3500 | 5000 | 2000 | 2000 | -72.844 |

計算thickness的S/N ratio可從下列公式可先求出兩個wafer中每個測量點得到的值的平均數與標準差。其中n為測量點總各數:

$$\mu = \frac{1}{n} \sum_{i=1}^{n} \tau_i$$

$$\sigma^2 = \frac{1}{n-1} \sum_{i=1}^{n} (\tau_i - \mu)^2$$

根據wafer 1與wafer 3的結果可得到對thickness的S/N ratio為:

| evnt no | t | est wafer | 1 | t | est wafer | 3 | mu | var | SN |
|----------|------|-----------|--------|------|-----------|--------|---------|---------|---------|
| expt no. | top | center | bottom | top | center | bottom | | | |
| 1 | 2029 | 1975 | 1961 | 1952 | 1941 | 1949 | 1967.83 | 1032.97 | 35.7389 |
| 2 | 5375 | 5191 | 5242 | 5323 | 5307 | 5091 | 5254.83 | 10577.8 | 34.1672 |
| 3 | 5989 | 5894 | 5874 | 6077 | 5943 | 5962 | 5956.5 | 5300.3 | 38.2568 |
| 4 | 2118 | 2109 | 2099 | 2149 | 2130 | 2111 | 2119.33 | 317.067 | 41.5125 |
| 5 | 4102 | 4152 | 4174 | 5031 | 5040 | 5032 | 4588.5 | 239075 | 19.4481 |
| 6 | 3022 | 2932 | 2913 | 2934 | 2875 | 2841 | 2919.5 | 3811.5 | 33.4952 |
| 7 | 3030 | 3042 | 3028 | 3709 | 3671 | 3687 | 3361.17 | 129138 | 19.4193 |
| 8 | 4707 | 4472 | 4336 | 5073 | 4898 | 4599 | 4680.83 | 74171.8 | 24.7041 |
| 9 | 3859 | 3822 | 3850 | 4110 | 4067 | 4110 | 3969.67 | 19446.7 | 29.0866 |
| 10 | 3227 | 3205 | 3242 | 3599 | 3591 | 3535 | 3399.83 | 37445 | 24.8952 |
| 11 | 2521 | 2499 | 2499 | 2551 | 2552 | 2570 | 2532 | 900.8 | 38.523 |
| 12 | 5921 | 5766 | 5844 | 5691 | 5777 | 5743 | 5790.33 | 6566.27 | 37.0809 |
| 13 | 2792 | 2752 | 2716 | 2765 | 2786 | 2773 | 2764 | 759.6 | 40.0249 |
| 14 | 2863 | 2835 | 2859 | 2891 | 2844 | 2841 | 2855.5 | 418.3 | 42.8988 |
| 15 | 3218 | 3149 | 3124 | 3241 | 3189 | 3197 | 3186.33 | 1878.27 | 37.3283 |
| 16 | 3020 | 3008 | 3016 | 3235 | 3162 | 3140 | 3096.83 | 9105.77 | 30.2252 |
| 17 | 4277 | 4150 | 3992 | 4593 | 4298 | 4219 | 4254.83 | 39613.4 | 26.5992 |
| 18 | 3125 | 3119 | 3127 | 4120 | 4088 | 4138 | 3619.5 | 295284 | 16.4706 |

(b) Plot the surface defect and thickness SN ratio effect plots using only Test Wafer 1 and Test Wafer 3 data.

透過直交表,將六個變數進行三種水準的表現進行交錯實驗,共可得到實驗數據18組。將每個變數的水準表現對應到的實驗組別所對應到的S/N ratio取平均後,根據平均繪出主因素分析圖。

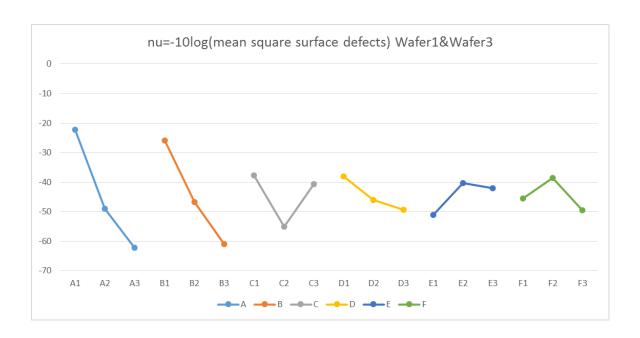
Defect的六個參數在三個水準之下的運作狀態平均S/N ratio如下表:

| A1 | | A2 | | A3 | | B1 | | B2 | | B3 | | C1 | | C2 | | C3 | |
|---------------------------|-----------------------------|------------------------------------|--|------------------------------------|------------------------------|---------------------------|-------------------------------|--|---|------------------------------------|--|------------------------------------|---|------------------------------------|--|------------------------------------|--|
| 1.000 | 1.761 | 4.000 | -26.103 | 7.000 | -60.086 | 1.000 | 1.761 | 2.000 | -34.247 | 3.000 | -43.880 | 1.000 | 1.761 | 2.000 | -34.247 | 3.000 | -43.880 |
| 2.000 | -34.247 | 5.000 | -64.005 | 8.000 | -73.442 | 4.000 | -26.103 | 5.000 | -64.005 | 6.000 | -61.807 | 4.000 | -26.103 | 5.000 | -64.005 | 6.000 | -61.807 |
| 3.000 | -43.880 | 6.000 | -61.807 | 9.000 | -69.016 | 7.000 | -60.086 | 8.000 | -73.442 | 9.000 | -69.016 | 9.000 | -69.016 | 7.000 | -60.086 | 8.000 | -73.442 |
| 10.000 | -2.632 | 13.000 | -43.158 | 16.000 | -24.911 | 10.000 | -2.632 | 11.000 | 1.761 | 12.000 | -56.541 | 11.000 | 1.761 | 12.000 | -56.541 | 10.000 | -2.632 |
| 11.000 | 1.761 | 14.000 | -37.325 | 17.000 | -73.232 | 13.000 | -43.158 | 14.000 | -37.325 | 15.000 | -61.506 | 15.000 | -61.506 | 13.000 | -43.158 | 14.000 | -37.325 |
| 12.000 | -56.541 | 15.000 | -61.506 | 18.000 | -72.844 | 16.000 | -24.911 | 17.000 | -73.232 | 18.000 | -72.844 | 17.000 | -73.232 | 18.000 | -72.844 | 16.000 | -24.911 |
| | -22.296 | | -48.984 | | -62.255 | | -25.855 | | -46.749 | | -60.932 | | -37.723 | | -55.147 | | -40.666 |
| D1 | | D2 | | D3 | | E1 | | E2 | | E3 | | F1 | | F2 | | F3 | |
| 1.000 | 1.761 | 2,000 | -34.247 | 3.000 | -43,880 | 1.000 | 1.761 | 2,000 | -34.247 | 3.000 | -43.880 | 1.000 | 1.761 | 2.000 | -34.247 | 3,000 | -43.880 |
| | | | | | | | | | | 3.000 | | | | | 34.247 | 5.000 | |
| 6.000 | -61.807 | 4.000 | -26.103 | 5.000 | -64.005 | 6.000 | -61.807 | 4.000 | -26.103 | 5.000 | -64.005 | 5.000 | -64.005 | 6.000 | -61.807 | 4.000 | -26.103 |
| 7.000 | -61.807 -60.086 | | | | -64.005 -69.016 | 6.000 8.000 | -61.807 -73.442 | | | | | | | | | | |
| | | 4.000 | -26.103 | 5.000 | | | | 4.000 | -26.103 | 5.000 | -64.005 | 5.000 | -64.005 | 6.000 | -61.807 | 4.000 | -26.103 |
| 7.000 | -60.086 | 4.000 8.000 | -26.103 -73.442 | 5.000 9.000 | -69.016 | 8.000 | -73.442 | 4.000 9.000 | -26.103 -69.016 | 5.000 7.000 | -64.005 -60.086 | 5.000 8.000 | -64.005 -73.442 | 6.000 9.000 | -61.807 -69.016 | 4.000 7.000 | -26.103 -60.086 |
| 7.000 11.000 | -60.086 1.761 | 4.000 8.000 12.000 | -26.103 -73.442 -56.541 | 5.000 9.000 10.000 | -69.016 -2.632 | 8.000 12.000 | -73.442 -56.541 | 4.000 9.000 10.000 | -26.103 -69.016 -2.632 | 5.000 7.000 11.000 | -64.005 -60.086 1.761 | 5.000 8.000 10.000 | -64.005 -73.442 -2.632 | 6.000 9.000 11.000 | -61.807 -69.016 1.761 | 4.000 7.000 12.000 | -26.103 -60.086 -56.541 |
| 7.000 11.000 14.000 | -60.086 1.761 -37.325 | 4.000 8.000 12.000 15.000 | -26.103 -73.442 -56.541 -61.506 | 5.000 9.000 10.000 13.000 | -69.016 -2.632 -43.158 | 8.000 12.000 13.000 | -73.442 -56.541 -43.158 | 4.000 9.000 10.000 14.000 18.000 | -26.103 -69.016 -2.632 -37.325 | 5.000 7.000 11.000 15.000 | -64.005 -60.086 1.761 -61.506 | 5.000 8.000 10.000 15.000 | -64.005 -73.442 -2.632 -61.506 | 6.000 9.000 11.000 13.000 | -61.807 -69.016 1.761 -43.158 | 4.000 7.000 12.000 14.000 | -26.103 -60.086 -56.541 -37.325 |

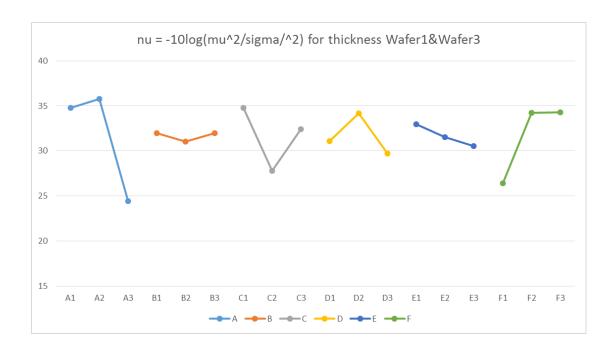
Thickness的六個參數在三個水準之下的運作狀態平均S/N ratio如下表:

| A1 | | A2 | | A3 | | B1 | | B2 | | В3 | | C1 | | C2 | | C3 | |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 1.000 | 35.739 | 4.000 | 41.512 | 7.000 | 19.419 | 1.000 | 35.739 | 2.000 | 34.167 | 3.000 | 38.257 | 1.000 | 35.739 | 2.000 | 34.167 | 3.000 | 38.257 |
| 2.000 | 34.167 | 5.000 | 19.448 | 8.000 | 24.704 | 4.000 | 41.512 | 5.000 | 19.448 | 6.000 | 33.495 | 4.000 | 41.512 | 5.000 | 19.448 | 6.000 | 33.495 |
| 3.000 | 38.257 | 6.000 | 33.495 | 9.000 | 29.087 | 7.000 | 19.419 | 8.000 | 24.704 | 9.000 | 29.087 | 9.000 | 29.087 | 7.000 | 19.419 | 8.000 | 24.704 |
| 10.000 | 24.895 | 13.000 | 40.025 | 16.000 | 30.225 | 10.000 | 24.895 | 11.000 | 38.523 | 12.000 | 37.081 | 11.000 | 38.523 | 12.000 | 37.081 | 10.000 | 24.895 |
| 11.000 | 38.523 | 14.000 | 42.899 | 17.000 | 26.599 | 13.000 | 40.025 | 14.000 | 42.899 | 15.000 | 37.328 | 15.000 | 37.328 | 13.000 | 40.025 | 14.000 | 42.899 |
| 12.000 | 37.081 | 15.000 | 37.328 | 18.000 | 16.471 | 16.000 | 30.225 | 17.000 | 26.599 | 18.000 | 16.471 | 17.000 | 26.599 | 18.000 | 16.471 | 16.000 | 30.225 |
| | 34.777 | | 35.785 | | 24.417 | | 31.969 | | 31.057 | | 31.953 | | 34.798 | | 27.768 | | 32.413 |
| D1 | | D2 | | D3 | | E1 | | E2 | | E3 | | F1 | | F2 | | F3 | |
| 1.000 | 35.739 | 2.000 | 34.167 | 3.000 | 38.257 | 1.000 | 35.739 | 2.000 | 34.167 | 3.000 | 38.257 | 1.000 | 35.739 | 2.000 | 34.167 | 3.000 | 38.257 |
| 6.000 | 33.495 | 4.000 | 41.512 | 5.000 | 19.448 | 6.000 | 33.495 | 4.000 | 41.512 | 5.000 | 19.448 | 5.000 | 19.448 | 6.000 | 33.495 | 4.000 | 41.512 |
| 7.000 | 19.419 | 8.000 | 24.704 | 9.000 | 29.087 | 8.000 | 24.704 | 9.000 | 29.087 | 7.000 | 19.419 | 8.000 | 24.704 | 9.000 | 29.087 | 7.000 | 19.419 |
| 11.000 | 38.523 | 12.000 | 37.081 | 10.000 | 24.895 | 12.000 | 37.081 | 10.000 | 24.895 | 11.000 | 38.523 | 10.000 | 24.895 | 11.000 | 38.523 | 12.000 | 37.081 |
| 14.000 | 42,899 | 15.000 | 37.328 | 13.000 | 40.025 | 13.000 | 40.025 | 14.000 | 42.899 | 15.000 | 37.328 | 15.000 | 37.328 | 13.000 | 40.025 | 14.000 | 42.899 |
| 14.000 | | | | | | | | | | | | | | | | | |
| 18.000 | 16.471 | 16.000 | 30.225 | 17.000 | 26.599 | 17.000 | 26.599 | 18.000 | 16.471 | 16.000 | 30.225 | 18.000 | 16.471 | 16.000 | 30.225 | 17.000 | 26.599 |

根據上表所繪出的Defect主因素分析圖如下:



根據上表所繪出的thickness主因素分析圖如下:



- (c) Suggest the optimal factor setting with results of (a) and (b). 综合考量Defect與thickness這兩項指標的S/N ratio,可選擇每個變數中可使 S/N ratio最大者做為選項,六個變數分別挑選出來的組合及為最佳解。 根據上面兩個指標的主因素分析圖,選擇的最佳參數組合為: [A1, B1, C1, D1, E2, F2]= [temp=T_0-25, Pressure=P_0-200, Nitrogen=S_0-50, Silane=S_0-100, set Time=t_0+8, Cleaning Method=CM2]。
- (d) Use the additive model to predict the results of the suggested optimal factor settings using Test Wafer 1 and Test Wafer 3.

 為驗正挑選的組合為最佳解,我們透過 addictive model 來與原先的 S/N ratio 比較。分別計算原始組合的參數水準與平均 S/N ratio 的差值,再進行相加做比較。結果如下表所示:

| ſ | 00000000 |
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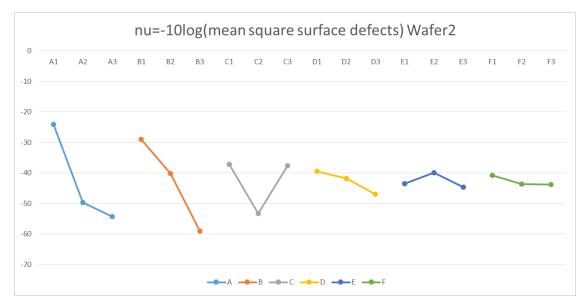
從結果我們可以看到,透過選擇最佳組合的參數表現,在Surface defect表現中提升了近76,而在thickness表現中則提升了約8,優化效果十分顯著。

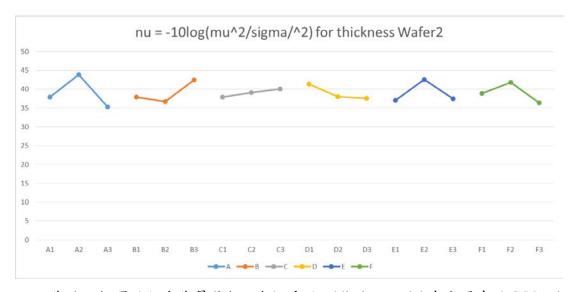
(e) Re-do (a)-(d) for Test Wafer 2 and compare and discuss the results. 僅針對wafer2的三個測量點進行分析,可得defect的S/N ratio如下表:

| thickness約S/N rati | 0如下表: | |
|--------------------|-----------------|-------------|
| II reconsess | | |
| | | |
| | | |
| | | |
| | | |
| Defect的六個參數在三 | 個水準之下的運作狀態平均S/N | N ratio如下表: |
| <u>a</u> | | |
| | | |
| | | |
| | | |

Thickness的六個參數在三個水準之下的運作狀態平均S/N ratio如下表:







為驗正挑選的組合為最佳解,我們透過 addictive model 來與原先的 S/N ratio 比較。分別計算原始組合的參數水準與平均 S/N ratio 的差值,再進行相加

做比較。最佳解選擇[A1, B1, C3, D1, E2, F2] = [temp=T_0-25, Pressure=P_0-200, Nitrogen=S_0-150, Silane=S_0-100, set Time=t_0+8, Cleaning Method=CM2]結果如下表所示:

| | | start condition | | optimum condition | | | |
|--------------|---------|-----------------|-----------|-------------------|-----------------|-----------|--|
| | | contributi | on | | contributi | on | |
| Factor | setting | surface defects | thickness | setting | surface defects | thickness | |
| A | A2 | -6.980958871 | 4.84129 | A1 | 18.63435885 | -1.1175 | |
| В | B2 | 2.557577827 | -2.3095 | B1 | 13.74078022 | -1.1508 | |
| C | C1 | 5.490873856 | -1.1336 | C3 | 5.148548355 | 1.06962 | |
| D | D3 | -4.200486963 | -1.3838 | D1 | 3.25229637 | 2.38332 | |
| Е | E1 | -0.810786184 | -1.9581 | E2 | 2.775368898 | 3.55396 | |
| F | F1 | 1.980876377 | -0.1564 | F2 | -0.878209303 | 2.81439 | |
| overall mean | | -42.71044813 | 39.0264 | | -42.71044813 | 39.0264 | |
| total | | -44.67335209 | 36.9262 | | -0.037304743 | 46.5794 | |

從表中我們可看到,選擇最佳組合會使surface defects提升約44,在 thickness上進步了大約10,優化效果十分顯著。

與謹評估wafer1&wafer3時所選擇的最佳化參數組合,只有在C的參數項目有所不同(Nitrogen),但不論選擇C1或C3做為參數對結果皆不會有太大的影響,因此任意一組參數組合都可以對實驗有優話的效果。

2. Please find an orthogonal array suitable for an experiment for three 2-level factors and nine 3-level factors. Provide the experimental matrix.

For three 2-level factor, an $L_4(2^3)$ is sufficient.

| | 1 | 2 | 3 |
|---|---|---|---|
| 1 | 1 | 1 | 1 |
| 2 | 1 | 2 | 2 |
| 3 | 2 | 1 | 2 |
| 4 | 2 | 2 | 1 |

For nine 3-level factors, an $L_{27}(3^{13})$ is sufficient.

| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|----|---|---|---|---|---|---|---|---|---|
| 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 2 | 1 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 2 |
| 3 | 1 | 1 | 1 | 1 | 3 | 3 | 3 | 3 | 3 |
| 4 | 1 | 2 | 2 | 2 | 1 | 1 | 1 | 2 | 2 |
| 5 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 |
| 6 | 1 | 2 | 2 | 2 | 3 | 3 | 3 | 1 | 1 |
| 7 | 1 | 3 | 3 | 3 | 1 | 1 | 1 | 3 | 3 |
| 8 | 1 | 3 | 3 | 3 | 2 | 2 | 2 | 1 | 1 |
| 9 | 1 | 3 | 3 | 3 | 3 | 3 | 3 | 2 | 2 |
| 10 | 2 | 1 | 2 | 3 | 1 | 2 | 3 | 1 | 2 |
| 11 | 2 | 1 | 2 | 3 | 2 | 3 | 1 | 2 | 3 |
| 12 | 2 | 1 | 2 | 3 | 3 | 1 | 2 | 3 | 1 |
| 13 | 2 | 2 | 3 | 1 | 1 | 2 | 3 | 2 | 3 |
| 14 | 2 | 2 | 3 | 1 | 2 | 3 | 1 | 3 | 1 |
| 15 | 2 | 2 | 3 | 1 | 3 | 1 | 2 | 1 | 2 |
| 16 | 2 | 3 | 1 | 2 | 1 | 2 | 3 | 3 | 1 |
| 17 | 2 | 3 | 1 | 2 | 2 | 3 | 1 | 1 | 2 |
| 18 | 2 | 3 | 1 | 2 | 3 | 1 | 2 | 2 | 3 |
| 19 | 3 | 1 | 3 | 2 | 1 | 3 | 2 | 1 | 3 |
| 20 | 3 | 1 | 3 | 2 | 2 | 1 | 3 | 2 | 1 |
| 21 | 3 | 1 | 3 | 2 | 3 | 2 | 1 | 3 | 2 |
| 22 | 3 | 2 | 1 | 3 | 1 | 3 | 2 | 2 | 1 |
| 23 | 3 | 2 | 1 | 3 | 2 | 1 | 3 | 3 | 2 |
| 24 | 3 | 2 | 1 | 3 | 3 | 2 | 1 | 1 | 3 |
| 25 | 3 | 3 | 2 | 1 | 1 | 3 | 2 | 3 | 2 |
| 26 | 3 | 3 | 2 | 1 | 2 | 1 | 3 | 1 | 3 |
| 27 | 3 | 3 | 2 | 1 | 3 | 2 | 1 | 2 | 1 |