光学课程作业 Homework of Optics

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序言

本文为笔者本科时的"光学"课程作业(Homework of Optics, 2024.9-2025.1)。由于个人学识浅陋,认识有限,文中难免有不妥甚至错误之处,望读者不吝指正,在此感谢。

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最景

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Homework 1: 第一章

1.1 求入射到光纤的角度满足的条件

$$n_0 \sin i = n_g \sin i', \quad n_g \sin(\frac{\pi}{2} - i') = n_c \sin\frac{\pi}{2} \Longrightarrow i \leqslant \arcsin\left(\frac{n_g}{n_0} \sqrt{1 - \frac{n_c^2}{n_g^2}}\right)$$
 (1.1)

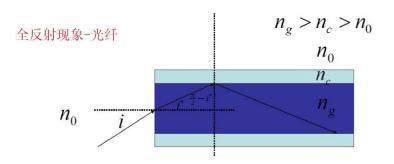


图 1.1: 求入射到光纤的角度满足的条件

1.2 推导光线轨迹方程

在 x-y 平面中,设 y=y(x) 表示光线的轨迹方程,n=n(y) 表示介质的折射率。由几何关系,我们有:

$$\frac{\mathrm{d}y}{\mathrm{d}x} = \tan\theta = \frac{1}{\tan i} = \frac{\sqrt{1 - \sin^2 i}}{\sin i} \tag{1.2}$$

由折射定律,记 $[n(y)\sin i(y)]_{y=0}=C$,则我们有:

$$n(y)\sin i(y) = C \Longrightarrow \frac{\mathrm{d}y}{\mathrm{d}x} = \frac{\sqrt{n^2 - C^2}}{C^2}, \quad \left(\frac{\mathrm{d}y}{\mathrm{d}x}\right)^2 = \frac{n^2}{C^2} - 1$$
 (1.3)

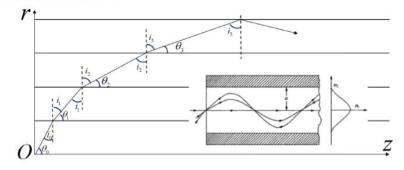
两边同时对x求导,得到:

$$2\left(\frac{\mathrm{d}y}{\mathrm{d}x}\right)\left(\frac{\mathrm{d}^2y}{\mathrm{d}x^2}\right) = \frac{1}{C^2}\left(\frac{\mathrm{d}n^2}{\mathrm{d}y}\right)\left(\frac{\mathrm{d}y}{\mathrm{d}x}\right) \Longrightarrow \frac{\mathrm{d}^2y}{\mathrm{d}x^2} = \frac{1}{2C^2} \cdot \frac{\mathrm{d}n^2}{\mathrm{d}y} \tag{1.4}$$

也即

$$\frac{d^2y}{dx^2} = \frac{1}{2n_0^2 \sin^2 i} \cdot \frac{dn^2}{dy} = \frac{1}{2n_0^2 \cos^2 \theta} \cdot \frac{dn^2}{dy} \quad \Box$$
 (1.5)

折射率连续变化的介质中的折射



折射定律: $n_0 \sin i_0 = n_1 \sin i_1 = n_2 \sin i_2 = n_3 \sin i_3 = \cdots$

图 1.2: 推导光线轨迹方程

事实上,在三维坐标系中考虑上述过程,或者利用费马原理和变分法,又或考虑哈密顿光学,可以得到 更一般的形式,称为光路方程,如下:

$$\nabla n = \frac{\mathrm{d}}{\mathrm{d}s} \left(n \frac{\mathrm{d}\vec{r}}{\mathrm{d}s} \right) \tag{1.6}$$

1.3 (已被删去)

1.4 利用费马原理给出物像关系

折射球面如图,由余弦定理可知:

$$OPL = np + n'p' = n\sqrt{r^2 + (s+r)^2 - 2r(s+r)\cos\phi} + n'\sqrt{r^2 + (s'-r)^2 + 2r(s'-r)\cos\phi}$$
 (1.7)

由费马原理, $\frac{dOPL}{d\phi}=0$,于是:

$$\frac{-nr(s+r)\sin\phi}{p} + \frac{n'r(s'-r)\sin\phi}{p'} = 0 \Longrightarrow \frac{n}{p} + \frac{n'}{p'} = \frac{1}{R}\left(\frac{n's'}{p'} - \frac{ns}{p}\right)$$
(1.8)

在傍轴条件下,有 $s \approx p$, $s' \approx p'$,于是:

$$\frac{n}{s} + \frac{n'}{s'} = \frac{n' - n}{R} \quad \Box \tag{1.9}$$

证毕。

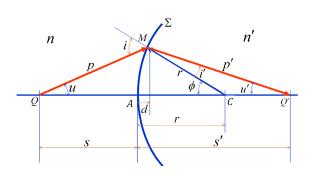


图 1.3: 折射球面物像关系

1.5 推导反射球面的物像公式

这里要注意,由于像是虚像, l_2 贡献虚光程(为负),且 $s_2 < 0$,因此圆心到像点的距离为 $r + s_2$ 而非 $r - s_2$ 。同由余弦定理,写出光程 OPL,有:

$$OPL = n_1 l_1 - n_2 l_2 = n_1 \sqrt{r^2 + (r + s_1)^2 - 2r(r + s_1)\cos\phi} - n_2 \sqrt{r^2 + (r + s_2)^2 - 2r(r + s_2)\cos\phi}$$
 (1.10)

由费马原理, $\frac{dOPL}{d\phi} = 0$, 于是有:

$$\frac{-n_1 r(r+s_1) \sin \phi}{l_1} + \frac{n_2 r(r+s_2) \sin \phi}{l_2} = 0 \Longrightarrow \frac{n_2}{l_2} - \frac{n_1}{l_1} = \frac{1}{r} \left(\frac{n_1 s_1}{l_1} - \frac{n_2 s_2}{l_2} \right)$$
(1.11)

傍轴时,有 $s_1 \approx l_1$, $s_2 \approx -l_2$,于是:

$$-\frac{n_2}{l_2} - \frac{n_1}{l_1} = \frac{1}{r}(n_1 + n_2) \tag{1.12}$$

当反射球面两侧为相同介质时, $n_1 = n_2$, 则:

$$\frac{1}{s_1} + \frac{1}{s_2} = -\frac{2}{r} \quad \Box \tag{1.13}$$

证毕。

1.6 画出图中的像点

如下图所示,左侧为手绘图,右侧为光路仿真软件 Optico 效果图。

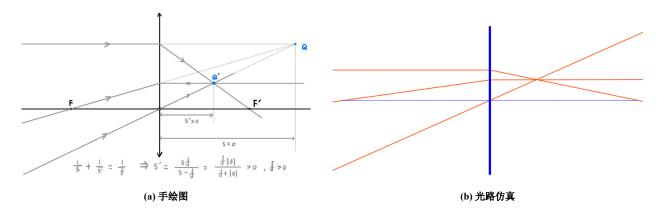


图 1.4: 画出虚物 Q 的像点 Q'

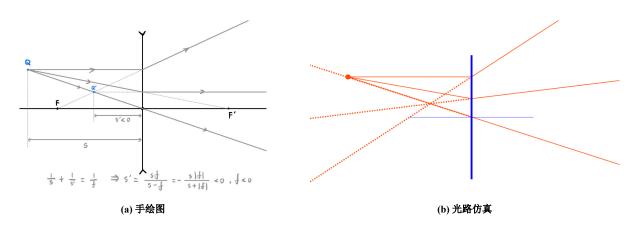


图 1.5: 画出实物 Q 经凹透镜的像点 Q'

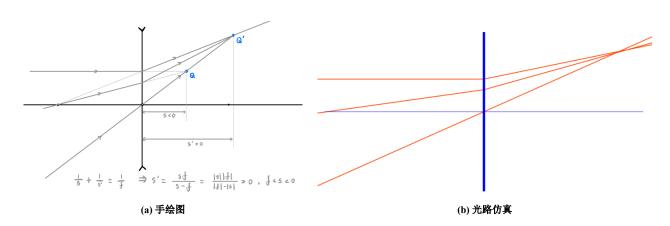


图 1.6: 画出虚物 Q 经凹透镜的像点 Q'

Homework 2: 第二章

2.1 对于正入射的情况,写出菲涅尔公式

菲涅尔公式如下:

类型	振幅反射系数 r		振幅透射系数 t	
s 波	$r_s = \frac{n_i \cos \theta_i - n_t \cos \theta_t}{n_i \cos \theta_i + n_t \cos \theta_t}$	$-\frac{\sin(\theta_i - \theta_t)}{\sin(\theta_i + \theta_t)}$	$t_s = \frac{2n_i \cos \theta_i}{n_i \cos \theta_i + n_t \cos \theta_t}$	$+rac{2\sin heta_t\cos heta_i}{\sin(heta_i+ heta_t)}$
p 波	$r_p = \frac{n_t \cos \theta_i - n_i \cos \theta_t}{n_t \cos \theta_i + n_i \cos \theta_t}$	$+rac{ an(heta_i- heta_t)}{ an(heta_i+ heta_t)}$	$t_p = \frac{2n_i \cos \theta_i}{n_i \cos \theta_t + n_t \cos \theta_i}$	$+\frac{2\sin\theta_t\cos\theta_i}{\sin(\theta_i+\theta_t)\cos(\theta_i-\theta_t)}$

正入射时, $\theta_i = \theta_t = 0$, 于是有:

$$r_p = (-r_s) = \frac{n_t - n_i}{n_t + n_i}, \quad t_p = t_s = \frac{2n_i}{n_i + n_t}$$

$$F = R_s = R_p = \left(\frac{n_t - n_i}{n_t + n_i}\right)^2$$
(2.1)

$$F = R_s = R_p = \left(\frac{n_t - n_i}{n_t + n_i}\right)^2 \tag{2.2}$$

不妨作出相关的图像,图 2.1 是 s 波、p 波振幅系数关于入射角 θ_i 的变化情况^①。

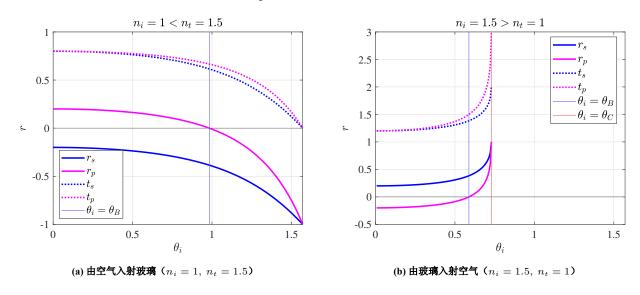


图 2.1: 振幅系数 r 随入射角 θ_i 的变化

2.2 一自然光以 Brewster Angle 入射到空气中的一块玻璃,已知功率透射率为 0.86。

(1) 求功率的反射率

T = 0.86, 由能量守恒,功率反射率 R = 0.14。

(2) 若输入为 1000 W, 求透射光 s 分量上的功率

光束为自然光,因此 s 分量和 p 分量的功率相同,都为 500 W,也即 $\Phi_{e,i,s} = \Phi_{e,i,p} = 500$ W。又由 Brewster Angle 入射,因此反射光的 p 分量为 0,也即 $R_p = 0$,于是:

$$T_p = 1 - R_p = 1, \quad T_s = 2T - T_p = 0.72$$
 (2.3)

由此可求得透射光 s 分量上的辐射通量(即辐射功率):

$$\Phi_{e,t,s} = T_s \Phi_{e,i,s} = 0.72 \times 500 \text{ W} = 360 \text{ W}$$
 (2.4)

^①源码见附录 A.1

(2.7)

(3) 求玻璃的折射率

虽然题目并未要求^②,但我们不妨求解一下玻璃的折射率 n_t 。在题设条件下,R = 0.14,默认空气折射率为 1,则唯一的未知量是玻璃折射率 n_t ,这是可以求解的,方程如下:

$$R = \frac{1}{2}(R_s + R_p) = 0.14, \quad \theta_i = \theta_B = \arctan\left(\frac{n_t}{n_i}\right), \quad n_i = 1 \Longrightarrow$$
 (2.5)

$$\left[\frac{\cos(\arctan n_t) - \sqrt{n_t^2 - \sin^2(\arctan n_t)}}{\cos(\arctan n_t) + \sqrt{n_t^2 - \sin^2(\arctan n_t)}} \right]^2 + \left[\frac{n_t^2 \cos(\arctan n_t) - \sqrt{n_t^2 - \sin^2(\arctan n_t)}}{n_t^2 \cos(\arctan n_t) + \sqrt{n_t^2 - \sin^2(\arctan n_t)}} \right]^2 = 2 \times 0.14 \quad (2.6)$$

此方程有唯一未知量 n_t ,用 Matlab 解此非线性方程组³,得到玻璃折射率 n_t ,以及其它参量⁴:

$$\begin{cases} n_t = 0.554902, & \theta_i = \theta_B = 29.025970^\circ \\ \theta_t = 60.974030^\circ, & \theta_C = 33.703947^\circ \\ R = 0.1400, & R_s = 0.280000, R_p = 0.000000 \\ T = 0.8600, & T_s = 0.720000, T_p = 1.000000 \end{cases} \begin{cases} n_t = 1.802121, & \theta_i = \theta_B = 60.974030^\circ \\ \theta_t = 29.025970^\circ, & \theta_C = 90.000000^\circ \\ R = 0.1400, & R_s = 0.280000, R_p = 0.000000 \\ T = 0.8600, & T_s = 0.720000, T_p = 1.000000 \end{cases}$$

也即上述方程有两解,考虑 $n_{ti} \in [0, 2]$,令方程 左边为 $f(n_{ti})$,作出图像如右。图 2.2 说明了我们并没 有漏掉其它解。

一般玻璃的折射率在 1.5 左右,即使是特殊玻璃(例如高折射率镜片),也基本在 1.3 至 1.9 之间,0.5 的玻璃折射率显然是不合理的,即使是考虑介质折射率关于波长的变化(如 X 射线或 Gamma 射线),也不会达到如此低的折射率。因此舍去 $n_t=0.554902$,最终得 $n_t=1.802121$ 。

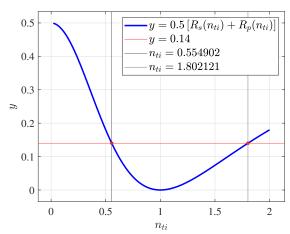


图 2.2: 方程 2.5 左边函数值随 n_{ti} 的变化情况

上题改编:一自然光由空气入射玻璃,玻璃折射率为1.5,已知功率透射率为0.86。

(1) 求功率的反射率:

T = 0.86, 由能量守恒,功率反射率 R = 0.14。

(2) 若输入为 1000 W, 求透射光 s 分量上的功率

光束为自然光,因此 s 分量和 p 分量的功率相同,都为 500 W。先求解入射角 θ_i ,由菲涅尔定理和能量关系:

$$R = \frac{1}{2}(R_s + R_p), \ R_s = \left[\frac{\cos\theta_i - \sqrt{n_{ti}^2 - \sin^2\theta_i}}{\cos\theta_i + \sqrt{n_{ti}^2 - \sin^2\theta_i}}\right]^2, \ R_p = \left[\frac{n_{ti}^2 \cos\theta_i - \sqrt{n_{ti}^2 - \sin^2\theta_i}}{n_{ti}^2 \cos\theta_i + \sqrt{n_{ti}^2 - \sin^2\theta_i}}\right]^2$$
(2.8)

其中 $n_i = 1$, $n_t = 1.5$, 因此 $n_{ti} = 1.5$, 代入即得:

$$\left[\frac{\cos \theta_i - \sqrt{1.5^2 - \sin^2 \theta_i}}{\cos \theta_i + \sqrt{1.5^2 - \sin^2 \theta_i}} \right]^2 + \left[\frac{1.5^2 \cos \theta_i - \sqrt{1.5^2 - \sin^2 \theta_i}}{1.5^2 \cos \theta_i + \sqrt{1.5^2 - \sin^2 \theta_i}} \right]^2 = 2 \times 0.14$$
(2.9)

²查阅资料发现,此题来自于光学(尤金,第五版)Optics (Eugene Hecht) 的 Page 152

[®]源码见附录 A.2

[®]图 2.2 源码见附录 A.4

用 Matlab 解此非线性方程组⁵,得到入射角 θ_i 和其它参量:

$$\theta_i = 1.173220 \text{ rad} = 67.220559^\circ$$

$$R = 0.140000, \quad R_s = 0.256933, \ R_p = 0.023067$$

$$T = 0.860000, \quad T_s = 0.743067, \ T_p = 0.976933$$
 (2.10)

于是透射光 s 分量上的辐射通量为:

$$\Phi_{e,t,s} = T_s \Phi_{e,i,s} = 0.743067 \times 500 \text{ W} = 371.5335 \text{ W}$$
 (2.11)

2.3 光束垂直入射到玻璃-空气界面,玻璃折射率 1.5,求出能量反射率和透射率

 $\theta_i = 0$ 时,由菲涅尔定律和能量关系,有:

$$R = \frac{1}{2}(R_s + R_p), \quad T = 1 - R \tag{2.12}$$

$$R_{s} = \left[\frac{\cos\theta_{i} - \sqrt{n_{ti}^{2} - \sin^{2}\theta_{i}}}{\cos\theta_{i} + \sqrt{n_{ti}^{2} - \sin^{2}\theta_{i}}}\right]^{2} = \left[\frac{1 - n_{ti}}{1 + n_{ti}}\right]^{2}, R_{p} = \left[\frac{n_{ti}^{2} \cos\theta_{i} - \sqrt{n_{ti}^{2} - \sin^{2}\theta_{i}}}{n_{ti}^{2} \cos\theta_{i} + \sqrt{n_{ti}^{2} - \sin^{2}\theta_{i}}}\right]^{2} = \left[\frac{n_{ti}^{2} - n_{ti}}{n_{ti}^{2} + n_{ti}}\right]^{2} (2.13)$$

由空气入射玻璃时, $n_{ti}=1.5$,由玻璃入射空气时, $n_{ti}=\frac{2}{3}$,代入得到:

空气入射玻璃: R = 0.04, T = 0.96

玻璃入射空气: R = 0.04, T = 0.96

也即无论从哪边入射,能量反射率和透射率分别为 0.04 和 0.96。

[®]源码见附录 A.3

Homework 3: 第三章

附录 A. Matlab 代码

A.1 图 2.1 源码

```
%%%%%%%% 空气入射玻璃 %%%%%%%%%%
 2
    global n_i n_t
    n_i = 1;
    n_t = 1.5;
4
 6
    theta_t = @(theta_i) asin(n_i/n_t*sin(theta_i));
    r_s = @(theta_i, theta_t) - sin(theta_i - theta_t)./sin(theta_i + theta_t);
    r_p = @(theta_i, theta_t) + tan(theta_i - theta_t)./tan(theta_i + theta_t);
8
9
    t_s = @(theta_i, theta_t) 2*sin(theta_t).*cos(theta_i)./sin(theta_i + theta_t);
    t_p = @(theta_i, theta_t) 2*sin(theta_t).*cos(theta_i) ./ ( sin(theta_i + theta_t).*
        cos(theta_i - theta_t) );
11
    theta_B = atan(n_t/n_i);
12
    theta_C = asin(n_t/n_i);
13
14
    theta_array = linspace(-0.1, pi/2, 101);
15
    Y = [
        r_s(theta_array, theta_t(theta_array))
16
17
        r_p(theta_array, theta_t(theta_array))
18
        t_s(theta_array, theta_t(theta_array))
19
        t_p(theta_array, theta_t(theta_array))
20
21
    stc = MyPlot(theta_array, Y);
22
    xline(theta_B, 'b')
23
    yline(0)
24
    xlim([0, pi/2])
25
    ylim([-1, 1])
    stc.leg.String = ["$r_s$"; "$r_p$"; "$t_s$"; "$t_p$"; "$\theta_i = \theta_B$"];
26
    stc.leg.Interpreter = "latex";
27
2.8
    stc.leg.FontSize = 14;
29
    stc.leg.Location = "southwest";
30
    stc.axes.Title.String = '$n_i = 1 < n_t = 1.5$';</pre>
    stc.axes.Title.Interpreter = "latex";
31
32
    stc.label.x.String = '$\theta_i$';
33
    stc.label.y.String = '$r$';
34
    stc.plot.plot_3.LineStyle = ":";
35
    stc.plot.plot_3.Color = 'b';
    stc.plot.plot_4.LineStyle = ":";
36
37
    stc.plot.plot_4.Color = [1 0 1];
38
    %MyExport_pdf
39
40
    %%%%%%%% 玻璃入射空气 %%%%%%%%%%
41
    n_i = 1.5;
42.
    n_t = 1;
43
```

```
44
    theta_t = @(theta_i) asin(n_i/n_t*sin(theta_i));
45
    r_s = @(theta_i, theta_t) - sin(theta_i - theta_t)./sin(theta_i + theta_t);
    r_p = @(theta_i, theta_t) + tan(theta_i - theta_t)./tan(theta_i + theta_t);
46
47
    t_s = @(theta_i, theta_t) 2*sin(theta_t).*cos(theta_i)./sin(theta_i + theta_t);
    t_p = @(theta_i, theta_t) 2*sin(theta_t).*cos(theta_i) ./ ( sin(theta_i + theta_t).*
48
        cos(theta_i - theta_t) );
49
    theta_B = atan(n_t/n_i);
50
    theta_C = asin(n_t/n_i);
51
52
53
    theta array = linspace(0, theta C, 101);
54
    Y = [
55
        r_s(theta_array, theta_t(theta_array))
56
        r_p(theta_array, theta_t(theta_array))
57
        t_s(theta_array, theta_t(theta_array))
58
        t_p(theta_array, theta_t(theta_array))
59
    stc = MyPlot(theta array, Y);
    xline(theta_B, 'b')
61
    xline(theta_C, 'r')
62
63
    yline(0)
    xlim([0, pi/2])
64
    ylim([-0.5, 3])
65
    stc.leg.String = ["$r_s$"; "$r_p$"; "$t_s$"; "$t_p$"; "$\theta_i = \theta_B$"; "$\
66
        theta_i = \theta_C$"];
    stc.leg.Interpreter = "latex";
67
    stc.axes.Title.String = '$n_i = 1.5 > n_t = 1$';
68
    stc.axes.Title.Interpreter = "latex";
70
    stc.label.x.String = '$\theta_i$';
71
    stc.label.y.String = '$r$';
72
    stc.plot.plot_3.LineStyle = ":";
73
    stc.plot.plot_3.Color = 'b';
74
    stc.plot.plot 4.LineStyle = ":";
75
    stc.plot.plot_4.Color = [1 0 1];
    %MyExport pdf
```

A.2 公式 2.5 源码

```
R_s = @(n_ti, t) ( (cos(t) - sqrt(n_ti^2 - sin(t)^2)) / (cos(t) + sqrt(n_ti^2 - sin(t) ^2)) )^2;
R_p = @(n_ti, t) ( (n_ti^2*cos(t) - sqrt(n_ti^2 - sin(t)^2)) / (n_ti^2*cos(t) + sqrt( n_ti^2 - sin(t)^2)) )^2;
theta_B = @(n_ti) atan(n_ti);
n_ti = fzero(@(n_ti) atan(n_ti);
n_ti = fzero(@(n_ti) atan(n_ti);
theta_C = @(n_ti) asin(n_ti);
theta_C = @(n_ti) asin(n_ti);
```

```
8
    theta_B = @(n_{ti}) atan(n_ti);
9
    theta_t = @(n_ti, theta_i) asin(sin(theta_i)/n_ti);
11
    disp(['n ti = ', num2str(n ti, '%.6f')])
    disp(['theta_i = theta_B = ', num2str(theta_B(n_ti), '%.6f') ' rad = ', num2str(
12
        rad2deg(theta_B(n_ti)), '%.6f'), ' deg'])
13
    disp(['theta_t = ', num2str(theta_t(n_ti, theta_B(n_ti)), '%.6f') ' rad = ', num2str(
        rad2deg(theta_t(n_ti, theta_B(n_ti))), '%.6f'), ' deg'])
    disp(['theta_C = ', num2str(theta_C(n_ti), '%.6f') ' rad = ', num2str(rad2deg(theta_C(
14
        n ti)), '%.6f'), ' deg'])
     disp(['R_s = ', num2str(R_s(n_ti, theta_B(n_ti)), '%.6f')])
15
16
     disp(['R_p = ', num2str(R_p(n_ti, theta_B(n_ti)), '%.6f')])
     disp(['T_s = ', num2str(1 - R_s(n_ti, theta_B(n_ti)), '%.6f')])
18
     disp(['T_p = ', num2str(1 - R_p(n_ti, theta_B(n_ti)), '%.6f')])
19
    disp(['R = ', num2str( 0.5*(R_s(n_ti), theta_B(n_ti)) + R_p(n_ti, theta_B(n_ti))) , '
    disp(['T = ', num2str( 0.5*(2 - R_s(n_ti, theta_B(n_ti)) - R_p(n_ti, theta_B(n_ti))),
        '%.6f')])
22
23
    %{
24
    >> Output:
25
    n_{ti} = 0.554902
    theta i = theta B = 0.506599 rad = 29.025970 deg
26
27
    theta t = 1.064198 \text{ rad} = 60.974030 \text{ deg}
    theta C = 0.588245 \text{ rad} = 33.703947 \text{ deg}
28
29
    R_s = 0.280000
    R p = 0.000000
30
    T s = 0.720000
    T p = 1.000000
32
33
    R = 0.140000
34
    T = 0.860000
35
    %}
```

A.3 公式 2.10 源码

```
disp(['R = ', num2str( 0.5*(R_s(1.5, theta_i) + R_p(1.5, theta_i)) , '%.6f')])
11
12
    disp(['T = ', num2str( 0.5*(2 - R_s(1.5, theta_i) - R_p(1.5, theta_i)), '%.6f')])
13
14
    %{
15
    >> Output:
16
    theta_i = 1.173220 rad
17
    theta i = 67.220559 \text{ deg}
18
    R s = 0.256933
19
    R_p = 0.023067
    T s = 0.743067
21
    T p = 0.976933
22
    R = 0.140000
    T = 0.860000
23
24
```

A.4 图 2.2 源码

```
R_s = @(n_{ti}, t) ((cos(t) - sqrt(n_{ti^2} - sin(t)^2)) / (cos(t) + sqrt(n_{ti^2} - sin(t)^2))
   1
                         ^2)) )^2;
              R_p = @(n_{ti}, t) ( (n_{ti}^2 * cos(t) - sqrt(n_{ti}^2 - sin(t)^2)) / (n_{ti}^2 * cos(t) + sqrt(n_{ti}^2 - sin(t)^2)) / (n_{ti}^2 * cos(t) + sqrt(n_{ti}^2 - sin(t)^2)) / (n_{ti}^2 + sin(ti)^2 + sqrt(n_{ti}^2 - sin(t)^2)) / (n_{ti}^2 + sin(
  2
                         n_{ti^2} - \sin(t)^2))^2;
  3
              theta_B = @(n_ti) atan(n_ti);
  4
  5
              eq_left = @(n_ti) 0.5*(R_s(n_ti), theta_B(n_ti)) + R_p(n_ti), theta_B(n_ti)))
  6
  7
             X = linspace(0, 2, 100);
  8
              Y = zeros(size(X));
  9
              for i = 1:length(X)
10
                          Y(i) = eq_left(X(i));
11
              end
12
13
              stc = MyPlot(X, Y);
14
              yline(0.14, 'Color', 'r', 'LineWidth', 0.4);
              xline(0.554902, 'Color', [0.1, 0.1, 0.1], 'LineWidth', 0.4)
15
              xline(1.802121, 'Color', [0.3, 0.3, 0.3], 'LineWidth', 0.4)
16
17
              stc.axes.Title.String = '';
18
              stc.label.x.String = '$n_{ti}$';
19
              stc.leg.Location = 'northeast';
              hold on
21
              scatter([0.554902, 1.802121], [0.14, 0.14], 180, '.r')
22
              stc.leg.String = ["$y = 0.5\left[ R_s(n_{ti}) + R_p(n_{ti}) \right]$"; "$y = 0.14$";
                          "$n_{ti} = 0.554902$"; "$n_{ti} = 1.802121$"];
              %MyExport_pdf
```