Table 6: Model performance with mean \pm standard deviation for MSE and MAE metrics

$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Dataset	$\mid T$	MSE	MAE
$ \begin{array}{ c c c c c } ECL & 144 & 0.143 \pm 0.000 & 0.236 \pm 0.000 \\ 192 & 0.149 \pm 0.000 & 0.244 \pm 0.000 \\ \hline & 192 & 0.349 \pm 0.000 & 0.244 \pm 0.000 \\ \hline \\ & 48 & 0.400 \pm 0.000 & 0.258 \pm 0.004 \\ 96 & 0.368 \pm 0.001 & 0.248 \pm 0.001 \\ 144 & 0.375 \pm 0.000 & 0.255 \pm 0.000 \\ 192 & 0.377 \pm 0.000 & 0.256 \pm 0.000 \\ \hline \\ & 48 & 0.131 \pm 0.001 & 0.170 \pm 0.001 \\ 96 & 0.154 \pm 0.001 & 0.202 \pm 0.002 \\ 144 & 0.172 \pm 0.001 & 0.220 \pm 0.001 \\ 192 & 0.193 \pm 0.000 & 0.241 \pm 0.000 \\ \hline \\ & 192 & 0.193 \pm 0.000 & 0.340 \pm 0.000 \\ 144 & 0.313 \pm 0.002 & 0.361 \pm 0.002 \\ 192 & 0.328 \pm 0.002 & 0.373 \pm 0.002 \\ \hline \\ & 192 & 0.328 \pm 0.002 & 0.373 \pm 0.001 \\ \hline \\ & 192 & 0.241 \pm 0.001 & 0.228 \pm 0.001 \\ 192 & 0.241 \pm 0.001 & 0.304 \pm 0.002 \\ \hline \\ & 144 & 0.405 \pm 0.002 & 0.417 \pm 0.002 \\ 192 & 0.422 \pm 0.003 & 0.432 \pm 0.003 \\ \hline \\ & 144 & 0.335 \pm 0.004 & 0.377 \pm 0.005 \\ 192 & 0.365 \pm 0.003 & 0.397 \pm 0.004 \\ \hline \\ & 111 & 36 & 1.462 \pm 0.071 & 0.728 \pm 0.068 \\ 48 & 1.537 \pm 0.004 & 0.798 \pm 0.003 \\ \hline \\ & 111 & 36 & 1.462 \pm 0.071 & 0.728 \pm 0.068 \\ 48 & 1.537 \pm 0.004 & 0.798 \pm 0.003 \\ \hline \\ & 111 & 36 & 1.462 \pm 0.071 & 0.728 \pm 0.068 \\ 48 & 1.537 \pm 0.004 & 0.798 \pm 0.003 \\ \hline \\ & 124 & 1.556 \pm 0.021 & 0.760 \pm 0.016 \\ \hline \\ & 148 & 1.537 \pm 0.004 & 0.798 \pm 0.003 \\ \hline \\ & 148 & 1.537 \pm 0.004 & 0.798 \pm 0.003 \\ \hline \\ & 148 & 1.537 \pm 0.004 & 0.798 \pm 0.003 \\ \hline \\ & 149 & 0.798 \pm 0.003 \\ \hline \\ & 140 & 0.798 \pm 0.003 \\ \hline \\ & 140 & 0.798 \pm 0.003 \\ \hline \\ & 140 & 0.798 \pm 0.003 \\ \hline \\ & 140 & 0.798 \pm 0.003 \\ \hline \\ & 140 & 0.798 \pm 0.003 \\ \hline \\ & 140 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm 0.003 \\ \hline \\ & 141 & 0.798 \pm $	ECL	48	0.137 ± 0.000	0.229 ± 0.000
		96	0.132 ± 0.001	0.225 ± 0.000
		144	0.143 ± 0.000	0.236 ± 0.000
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		192	0.149 ± 0.000	0.244 ± 0.000
$ \begin{array}{ c c c c c } \hline \text{Traffic} & 144 & 0.375 \pm 0.000 & 0.255 \pm 0.000 \\ \hline 192 & 0.377 \pm 0.000 & 0.256 \pm 0.000 \\ \hline \\ \hline 48 & 0.131 \pm 0.001 & 0.170 \pm 0.001 \\ \hline 96 & 0.154 \pm 0.001 & 0.202 \pm 0.002 \\ \hline 144 & 0.172 \pm 0.001 & 0.220 \pm 0.001 \\ \hline 192 & 0.193 \pm 0.000 & 0.241 \pm 0.000 \\ \hline \\ \hline ETTm1 & 48 & 0.280 \pm 0.001 & 0.330 \pm 0.002 \\ \hline 96 & 0.287 \pm 0.000 & 0.340 \pm 0.002 \\ \hline 144 & 0.313 \pm 0.002 & 0.361 \pm 0.002 \\ \hline 192 & 0.328 \pm 0.002 & 0.373 \pm 0.002 \\ \hline 192 & 0.328 \pm 0.002 & 0.373 \pm 0.001 \\ \hline 192 & 0.241 \pm 0.001 & 0.228 \pm 0.001 \\ \hline 192 & 0.241 \pm 0.001 & 0.304 \pm 0.002 \\ \hline 192 & 0.241 \pm 0.001 & 0.373 \pm 0.001 \\ \hline 192 & 0.422 \pm 0.003 & 0.432 \pm 0.003 \\ \hline 144 & 0.405 \pm 0.002 & 0.417 \pm 0.002 \\ \hline 192 & 0.422 \pm 0.003 & 0.432 \pm 0.003 \\ \hline 192 & 0.365 \pm 0.004 & 0.377 \pm 0.005 \\ \hline 192 & 0.365 \pm 0.004 & 0.377 \pm 0.004 \\ \hline 144 & 1.556 \pm 0.021 & 0.760 \pm 0.016 \\ \hline 36 & 1.462 \pm 0.071 & 0.728 \pm 0.068 \\ \hline 48 & 1.537 \pm 0.004 & 0.798 \pm 0.003 \\ \hline 144 & 1.537 \pm 0.004 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.798 \pm 0.003 \\ \hline 144 & 0.798 \pm 0.003 & 0.7$	Traffic	48	0.400 ± 0.000	0.258 ± 0.004
		96	0.368 ± 0.001	0.248 ± 0.001
$ \begin{tabular}{ l l l l l l l l l l l l l l l l l l l$		144		0.255 ± 0.000
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		192	0.377 ± 0.000	0.256 ± 0.000
$ \begin{array}{ c c c c c } \hline \text{Weather} & 144 & 0.172 \pm 0.001 & 0.220 \pm 0.001 \\ 192 & 0.193 \pm 0.000 & 0.241 \pm 0.000 \\ \hline \\ \hline & 48 & 0.280 \pm 0.001 & 0.330 \pm 0.002 \\ 96 & 0.287 \pm 0.000 & 0.340 \pm 0.002 \\ 144 & 0.313 \pm 0.002 & 0.361 \pm 0.002 \\ 192 & 0.328 \pm 0.002 & 0.373 \pm 0.002 \\ \hline \\ $	Weather	48		0.170 ± 0.001
		96	0.154 ± 0.001	0.202 ± 0.002
		144	0.172 ± 0.001	0.220 ± 0.001
		192	0.193 ± 0.000	0.241 ± 0.000
$ \begin{array}{ c c c c c } \hline \text{ETTm1} & 144 & 0.313 \pm 0.002 & 0.361 \pm 0.002 \\ \hline 192 & 0.328 \pm 0.002 & 0.373 \pm 0.002 \\ \hline \\ $	ETTm1	48	0.280 ± 0.001	0.330 ± 0.002
		96	0.287 ± 0.000	0.340 ± 0.000
		144	0.313 ± 0.002	0.361 ± 0.002
		192	0.328 ± 0.002	0.373 ± 0.002
$ \begin{array}{ c c c c c } \hline \text{ETTm2} & 144 & 0.209 \pm 0.001 & 0.283 \pm 0.001 \\ 192 & 0.241 \pm 0.001 & 0.304 \pm 0.002 \\ \hline \\ \hline \\ ETTh1 & 48 & 0.333 \pm 0.001 & 0.373 \pm 0.001 \\ 96 & 0.371 \pm 0.001 & 0.398 \pm 0.001 \\ 144 & 0.405 \pm 0.002 & 0.417 \pm 0.002 \\ 192 & 0.422 \pm 0.003 & 0.432 \pm 0.003 \\ \hline \\ ETTh2 & 48 & 0.238 \pm 0.001 & 0.306 \pm 0.000 \\ 96 & 0.299 \pm 0.003 & 0.352 \pm 0.004 \\ 144 & 0.335 \pm 0.004 & 0.377 \pm 0.005 \\ 192 & 0.365 \pm 0.003 & 0.397 \pm 0.004 \\ \hline \\ ILI & 24 & 1.556 \pm 0.021 & 0.760 \pm 0.016 \\ 36 & 1.462 \pm 0.071 & 0.728 \pm 0.068 \\ 48 & 1.537 \pm 0.004 & 0.798 \pm 0.003 \\ \hline \end{array} $	ETTm2	48	0.134 ± 0.001	0.228 ± 0.001
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		96	0.171 ± 0.002	0.255 ± 0.001
$ \begin{tabular}{ c c c c c c c c c c c c c c c c c c c$		144	0.209 ± 0.001	0.283 ± 0.001
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		192	0.241 ± 0.001	0.304 ± 0.002
ETTh1	ETTh1	48	0.333 ± 0.001	0.373 ± 0.001
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		96	0.371 ± 0.001	0.398 ± 0.001
ETTh2 $ \begin{vmatrix} 48 & 0.238 \pm 0.001 & 0.306 \pm 0.000 \\ 96 & 0.299 \pm 0.003 & 0.352 \pm 0.004 \\ 144 & 0.335 \pm 0.004 & 0.377 \pm 0.005 \\ 192 & 0.365 \pm 0.003 & 0.397 \pm 0.004 \end{vmatrix} $ $ \begin{vmatrix} 24 & 1.556 \pm 0.021 & 0.760 \pm 0.016 \\ 36 & 1.462 \pm 0.071 & 0.728 \pm 0.068 \\ 48 & 1.537 \pm 0.004 & 0.798 \pm 0.003 \end{vmatrix} $		144	0.405 ± 0.002	0.417 ± 0.002
ETTh2		192	0.422 ± 0.003	0.432 ± 0.003
$ \begin{array}{ c c c c c c c } \hline E11h2 & 144 & 0.335 \pm 0.004 & 0.377 \pm 0.005 \\ \hline & 192 & 0.365 \pm 0.003 & 0.397 \pm 0.004 \\ \hline & & 24 & 1.556 \pm 0.021 & 0.760 \pm 0.016 \\ \hline & 36 & 1.462 \pm 0.071 & 0.728 \pm 0.068 \\ 48 & 1.537 \pm 0.004 & 0.798 \pm 0.003 \\ \hline \end{array} $	ETTh2	48		0.306 ± 0.000
		96	0.299 ± 0.003	0.352 ± 0.004
ILI		144	0.335 ± 0.004	0.377 ± 0.005
ILI $\begin{vmatrix} 36 & 1.462 \pm 0.071 & 0.728 \pm 0.068 \\ 48 & 1.537 \pm 0.004 & 0.798 \pm 0.003 \end{vmatrix}$		192	0.365 ± 0.003	0.397 ± 0.004
1LI 48 1.537 ± 0.004 0.798 ± 0.003	ILI	24		0.760 ± 0.016
$ 48 1.537 \pm 0.004 0.798 \pm 0.003$				0.728 ± 0.068
$ 60 2.187 \pm 0.043 0.995 \pm 0.050$		48		0.798 ± 0.003
		60	2.187 ± 0.043	0.995 ± 0.050