

Ve215 Electric Circuits

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Chapter 12

Three-Phase Circuits

12.1 Introduction

So far, we have dealt with *single-phase* circuits. A single-phase ac power system consists of a generator connected through a pair of wires (a transmission line) to a load. Figure 12.1(a) depicts a single-phase two-wire system.



Figure 12.1(a) Single-phase two-wire system.

Circuits or systems in which the sources operate at the same frequency but different phases are known as *polyphase*. Figure 12.3 shows a three-phase four-wire system.

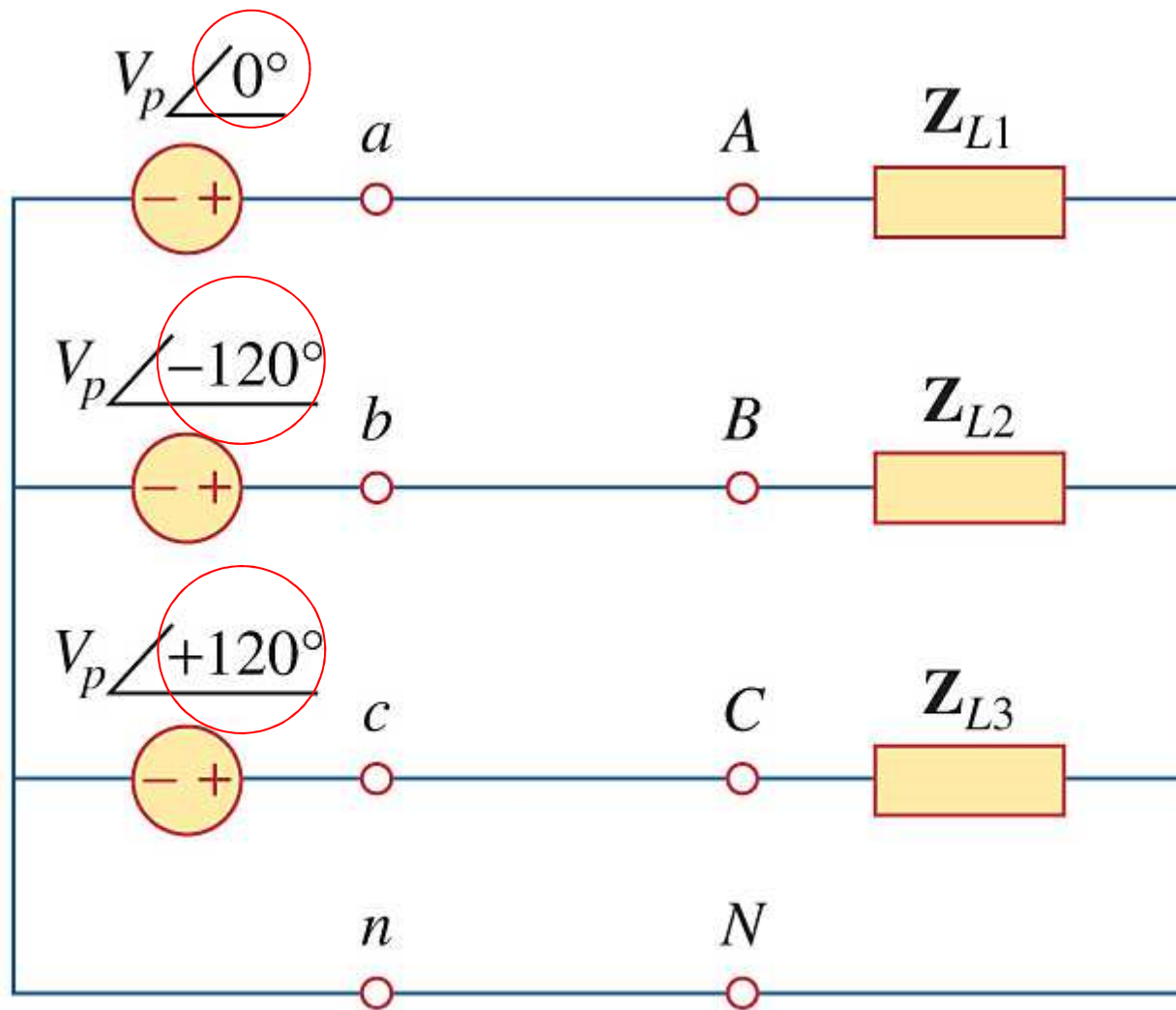


Figure 12.3 Three-phase four-wire system.

As distinct from a single-phase system, a three-phase system is produced by a generator consisting of three sources having the same amplitude and frequency but out of phase with each other by 120° . In this chapter, we study three-phase systems.

12.2 Balanced Three-Phase Voltages

Three-phase voltages are often produced with a three-phase generator (or alternator) whose cross-sectional view is shown in Fig. 12.4. The generator basically consists of a rotating magnet (called the rotor) surrounded by a stationary winding (called the stator).

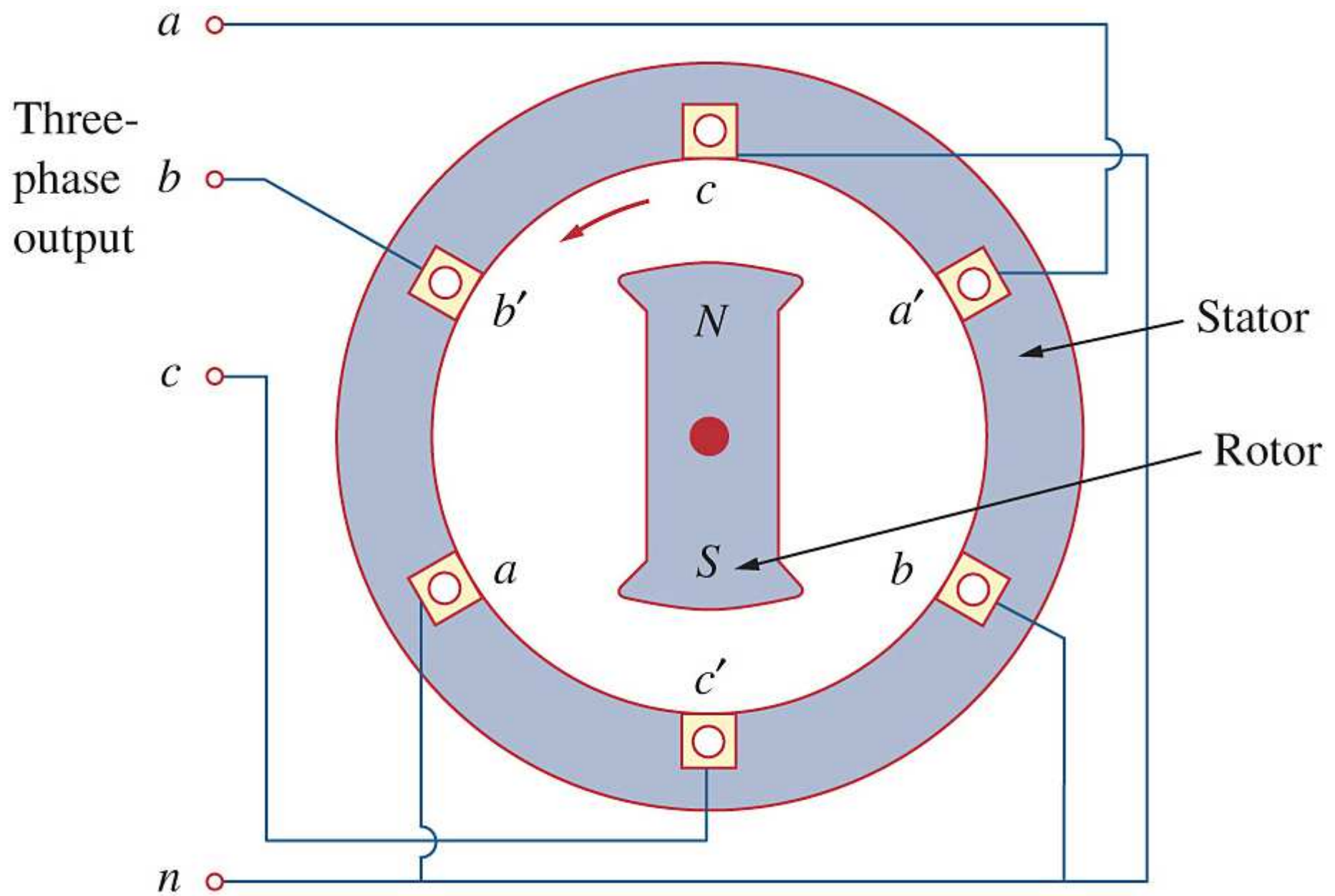


Figure 12.4 A three-phase generator.

As the rotator rotates, the flux through each coil varies sinusoidally with time, inducing a sinusoidal voltage. Because the coils are placed 120° apart, the induced voltages are out of phase by 120° (Fig. 12.5).

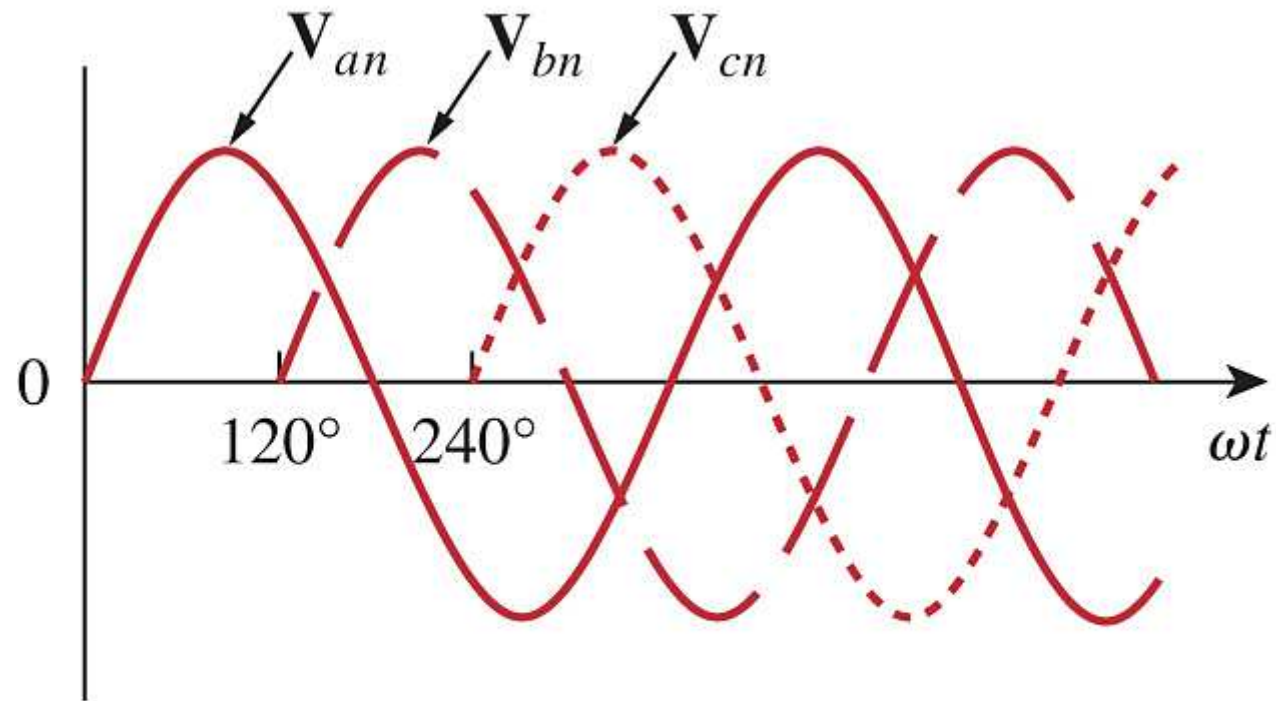


Figure 12.5 The generated voltages are 120° apart from each other.

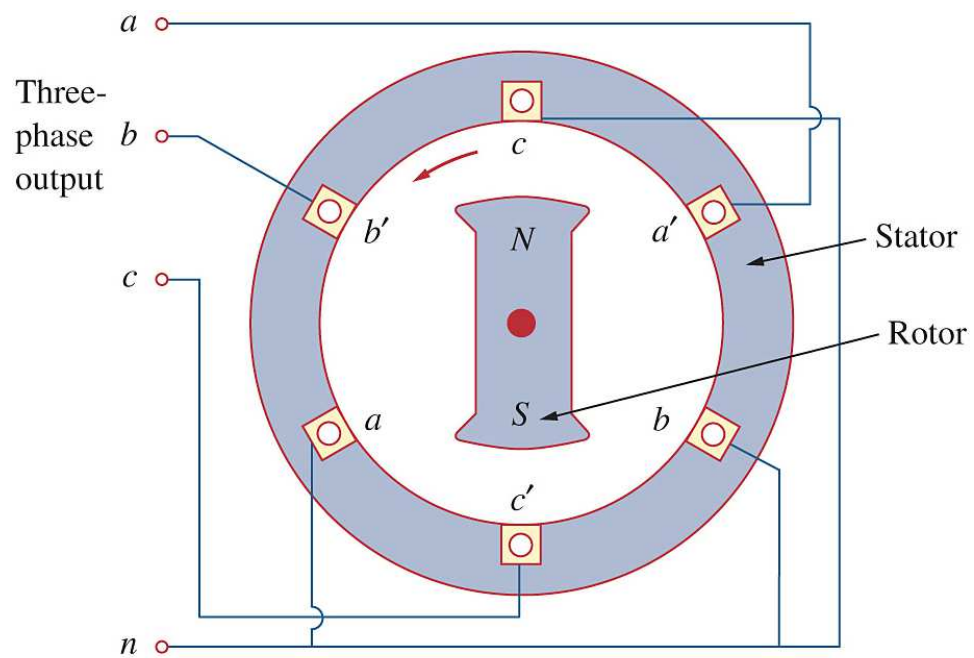


Figure 12.4 A three-phase generator.

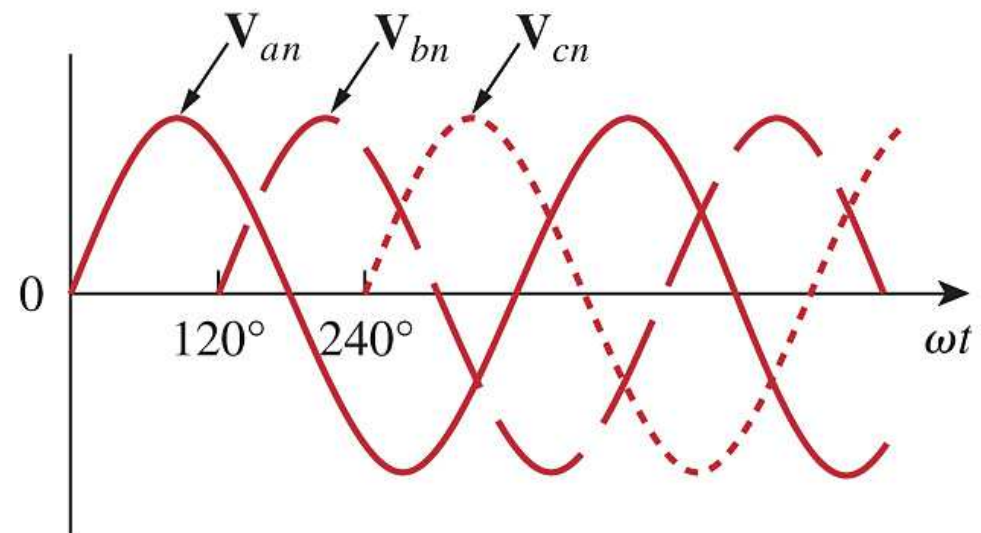
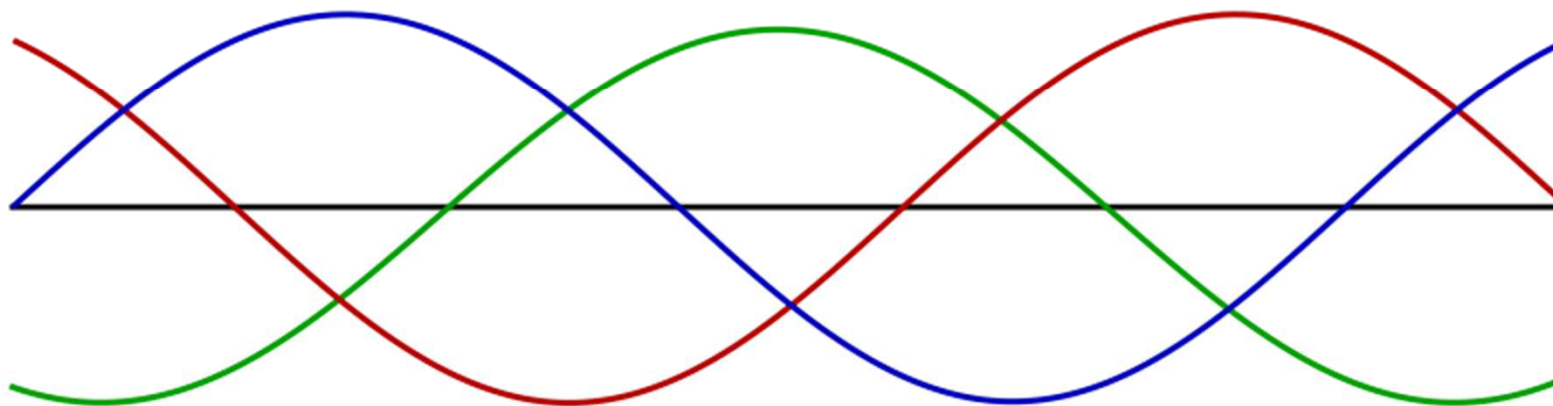
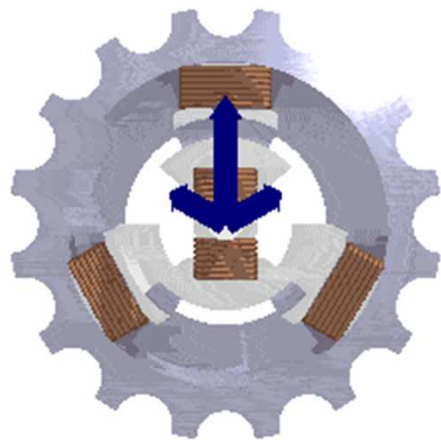


Figure 12.5 The generated voltages are 120° apart from each other.





A typical three-phase system consists of three voltage sources connected to loads by three or four wires. A three-phase system is equivalent to three single-phase systems. The voltage sources can be either wye- or delta-connected, as shown in Fig. 12.6.

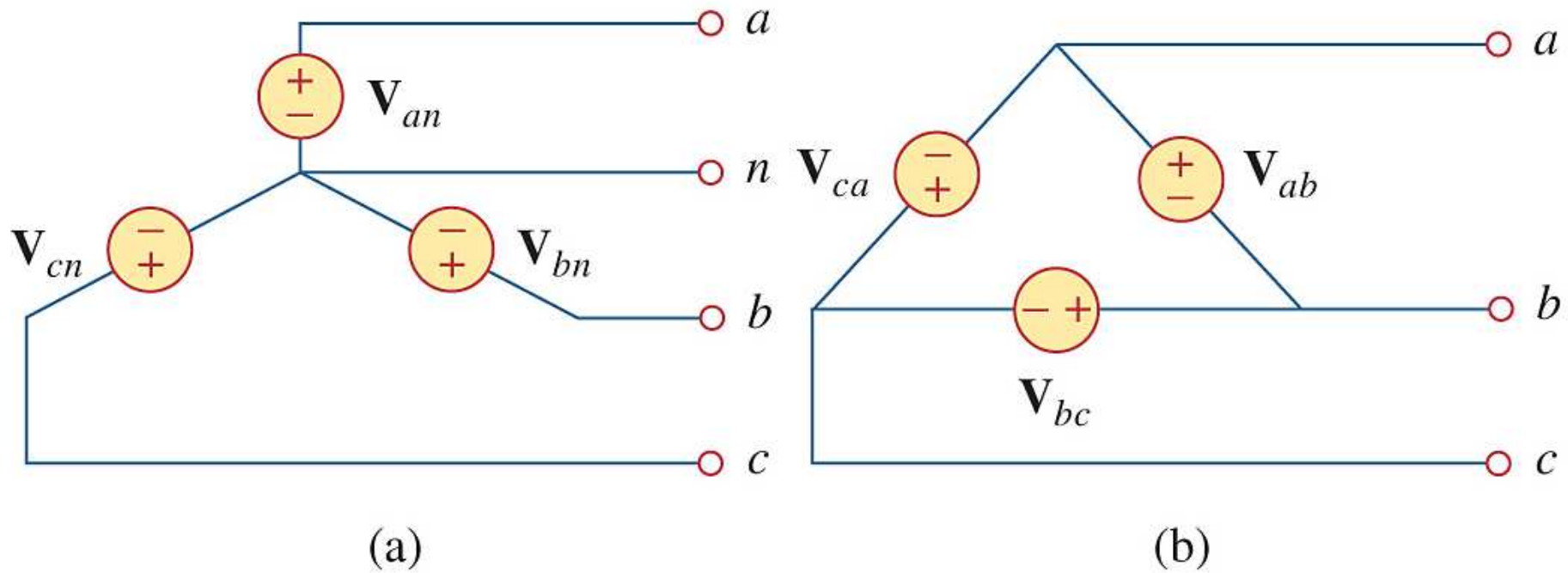
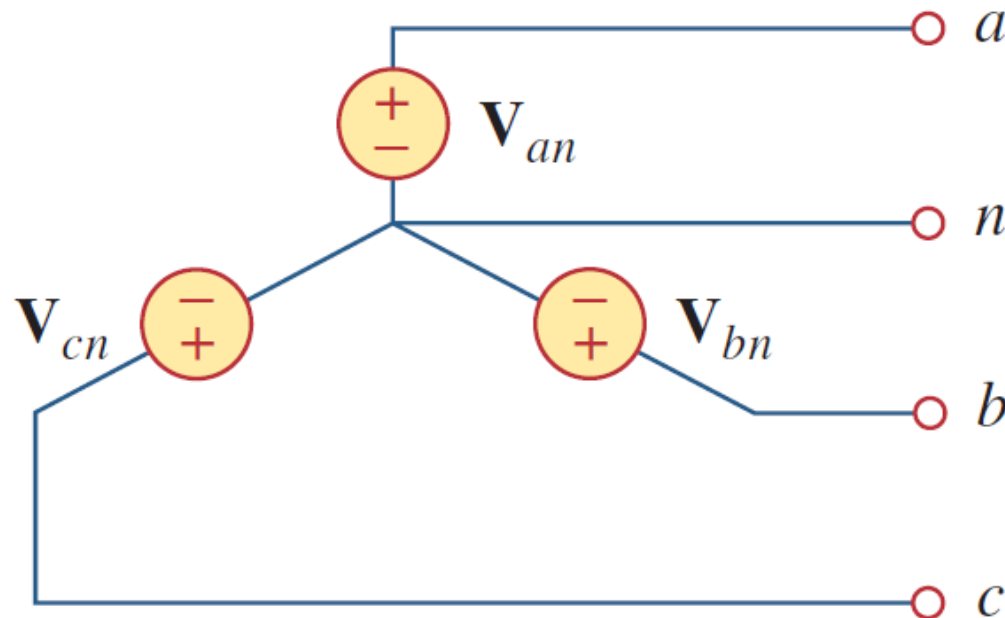


Figure 12.6 Three-phase voltage sources: (a) wye-connected, (b) delta-connected.

Let us consider the wye-connected voltages in Fig. 12.6(a). The voltages \tilde{V}_{an} , \tilde{V}_{bn} , and \tilde{V}_{cn} are respectively between lines a , b , and c , and the neutral line n . These voltages are called *phase voltages*.



If the voltages have the same amplitude and frequency and are out of phase with each other by 120° , the voltages are said to be *balanced*. This implies that (Fig. 12.7)

$$\tilde{V}_{an} + \tilde{V}_{bn} + \tilde{V}_{cn} = 0$$

Balanced source:
Same amplitude and frequency
Out of phase with each other by 120°

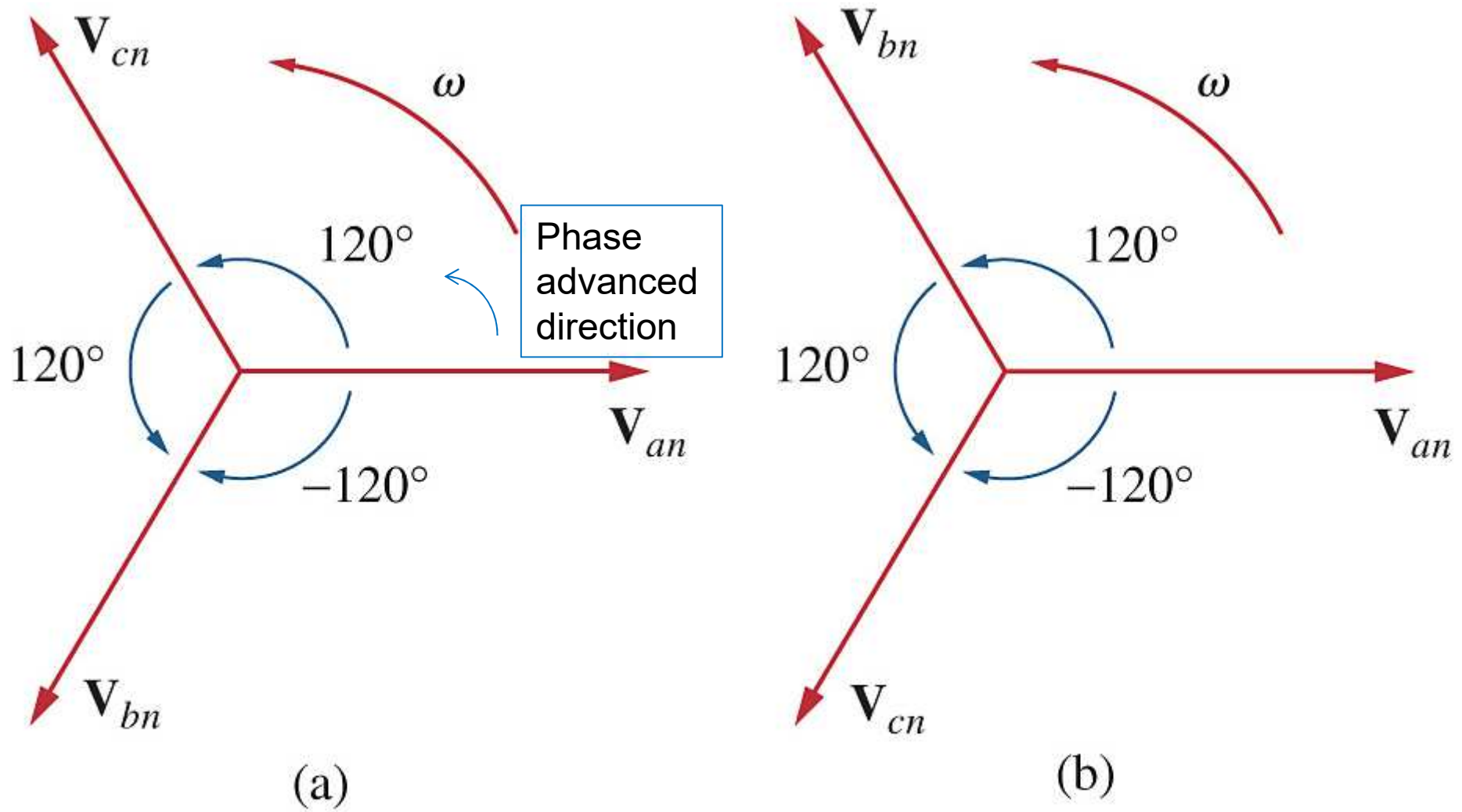


Figure 12.7 Phase sequences: (a) *abc* or positive sequence, (b) *acb* or negative sequence.

abc: a lead b, b leads c (i.e., $\angle a > \angle b > \angle c$)

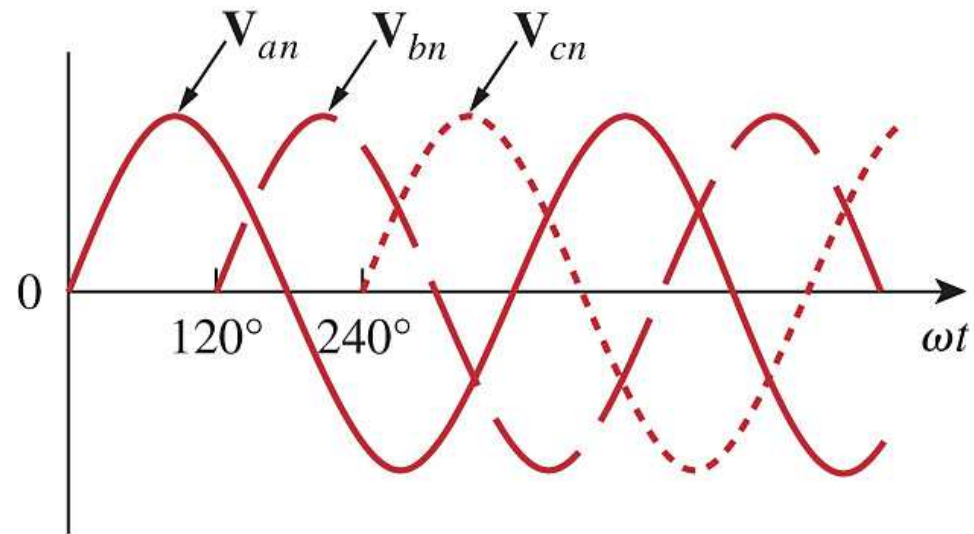


Figure 12.5 The generated voltages are 120° apart from each other.

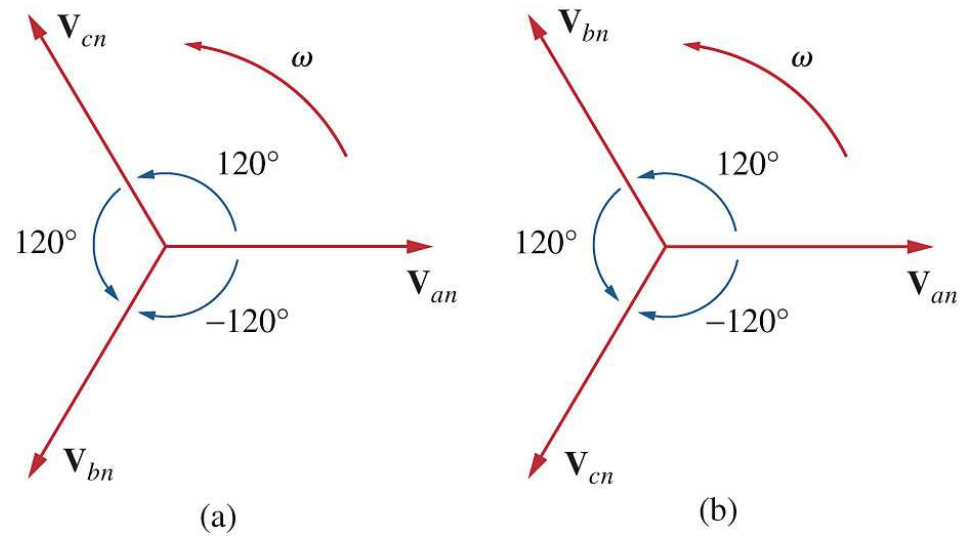


Figure 12.7 Phase sequences: (a) abc or positive sequence, (b) acb or negative sequence.

In Fig. 12.7(a),

$$\tilde{V}_{an} = V_p \angle 0^\circ$$

$$\tilde{V}_{bn} = V_p \angle -120^\circ$$

$$\tilde{V}_{cn} = V_p \angle -240^\circ = V_p \angle +120^\circ$$

where V_p is the effective or rms value of the phase voltages. This is known as the *abc sequence* or *positive sequence*.

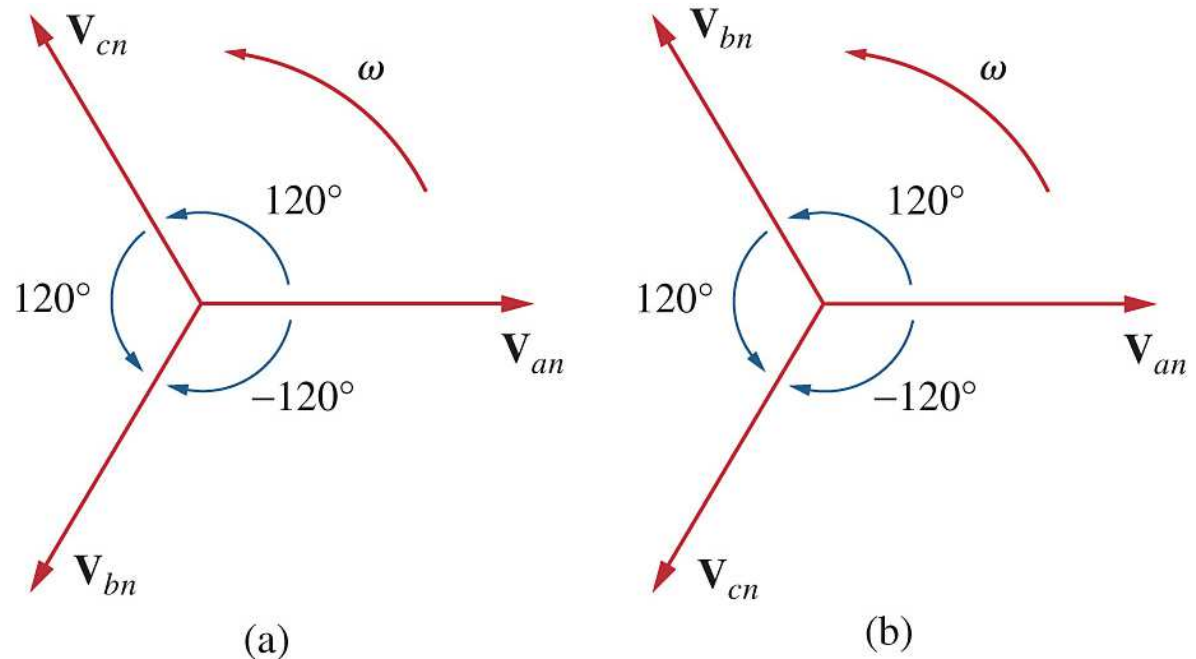


Figure 12.7 Phase sequences: (a) *abc* or positive sequence, (b) *acb* or negative sequence.

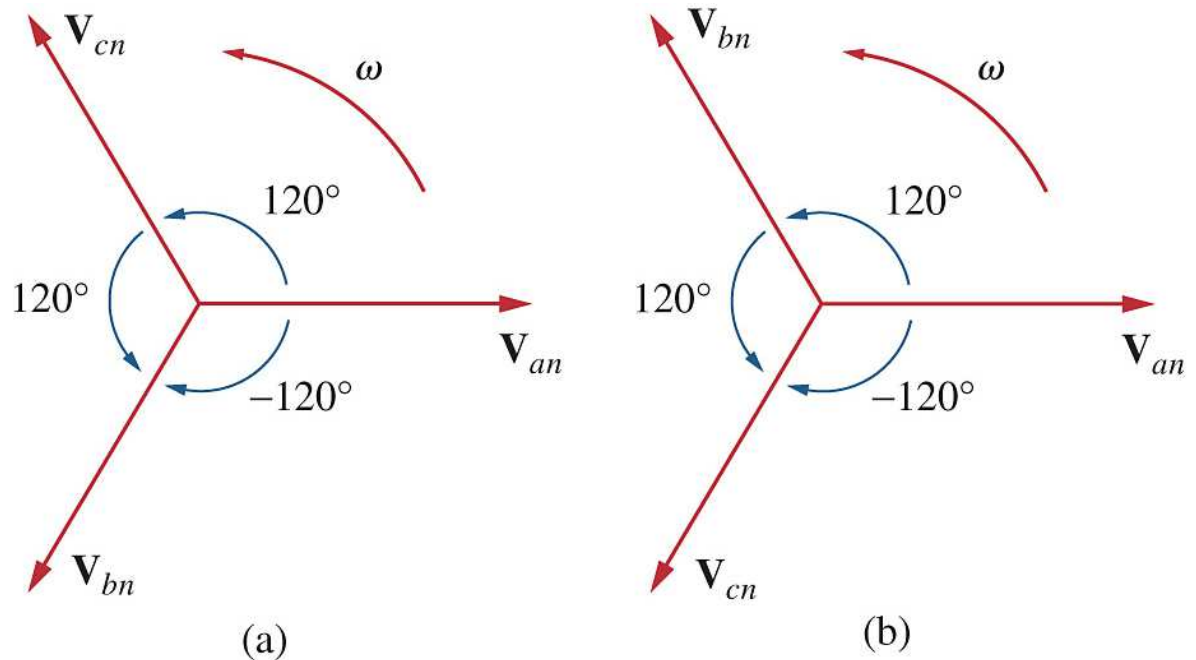


Figure 12.7 Phase sequences: (a) *abc* or positive sequence, (b) *acb* or negative sequence.

In Fig. 12.7(b),

$$\tilde{V}_{an} = V_p \angle 0^\circ$$

$$\tilde{V}_{cn} = V_p \angle -120^\circ$$

$$\tilde{V}_{bn} = V_p \angle -240^\circ = V_p \angle +120^\circ$$

This is called the *acb sequence* or *negative sequence*.

Like the source connections, a three-phase load can be either wye-connected or delta-connected, as shown in Fig. 12.8. The neutral line in Fig. 12.8(a) may or may not be there, depending on whether the system is four- or three-wire.

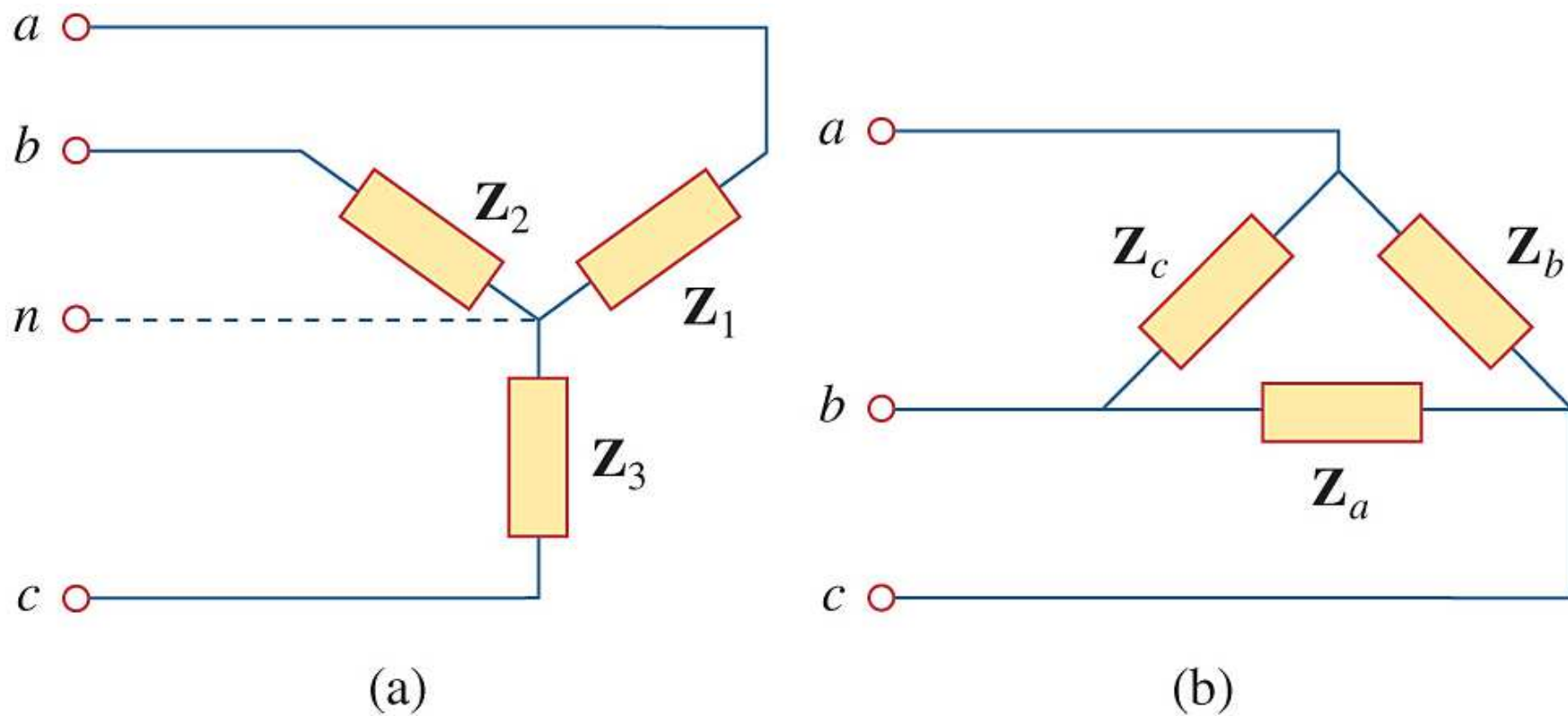


Figure 12.8 Two possible three-phase load configurations: (a) a wye-connected load, (b) a delta-connected load.

A wye- or delta-connected load is said to be balanced if the phase impedances are equal in magnitude and in phase.

For a balanced wye-connected load,

$$Z_1 = Z_2 = Z_3 = Z_Y$$

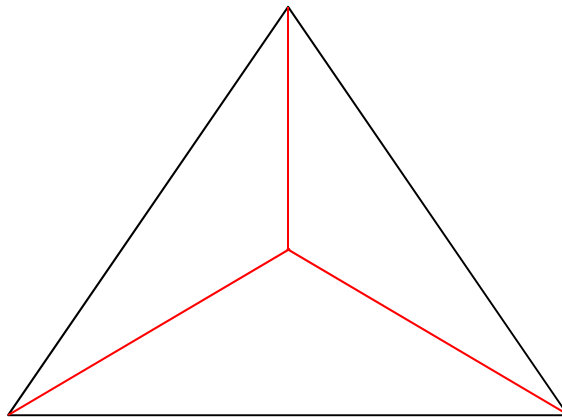
For a balanced delta-connected load,

$$Z_A = Z_B = Z_C = Z_{\Delta}$$

Balanced load:
Same amplitude and phase of impedances

A wye-connected load can be transformed into a delta-connected load, or vice versa.

$$Z_{\Delta} = 3Z_Y \text{ or } Z_Y = \frac{1}{3}Z_{\Delta}$$



Since both the three-phase source and the three-phase load can be either wye- or delta-connected, we have four possible connections:

1. Y-Y connection (i.e., Y-connected source with a Y-connected load).
2. Y- Δ connection.
3. Δ - Δ connection.
4. Δ -Y connection.

Source-Load

12.3 Balanced Wye-Wye Connection

A balanced Y-Y system is a three-phase system with a balanced Y-connected source and a balanced Y-connected load.

Figure 12.9 shows a balanced four-wire Y-Y system, which can be simplified to that shown in Fig. 12.10.

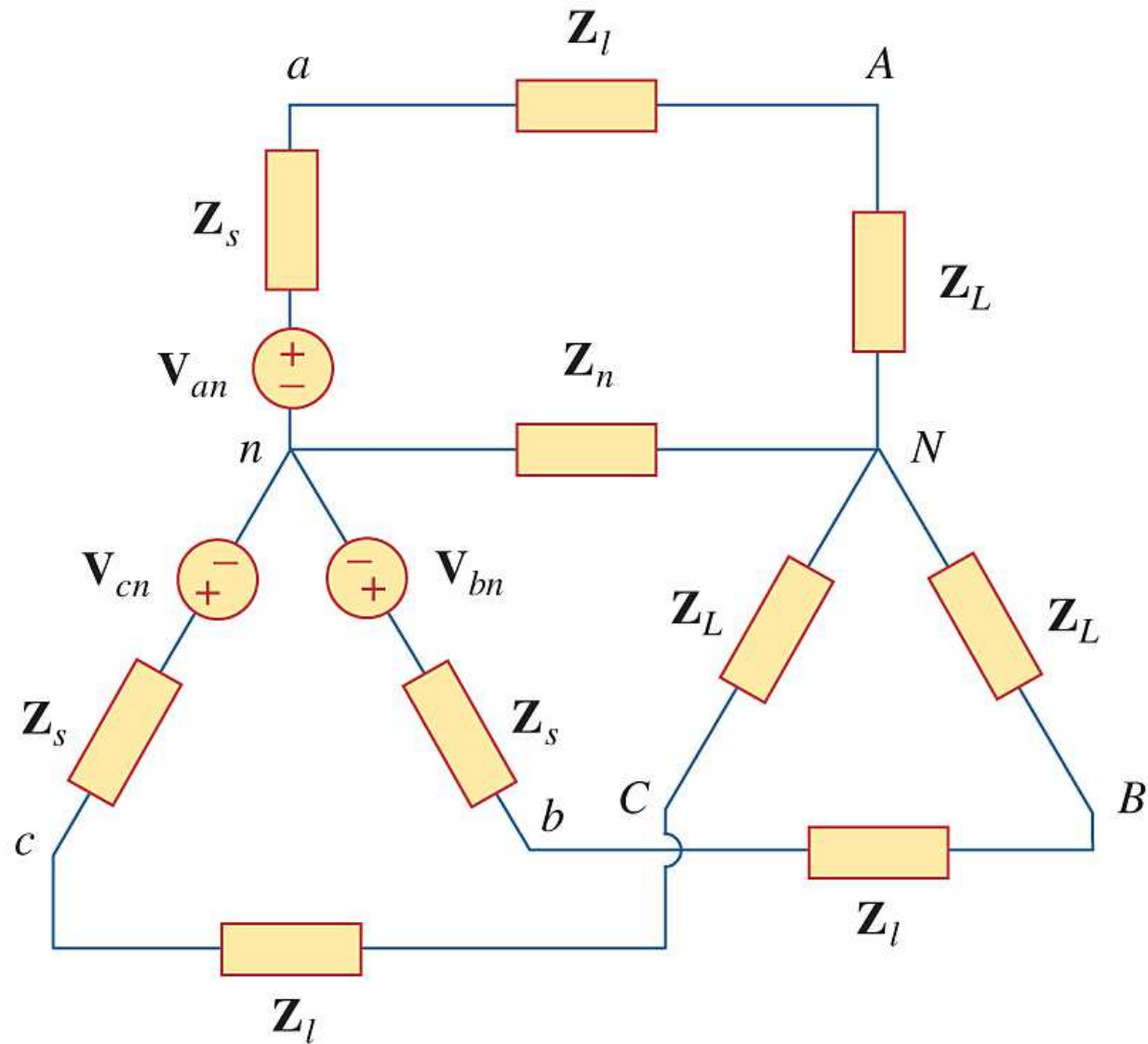


Figure 12.9 A balanced Y-Y system, showing the source, line, and load impedances.

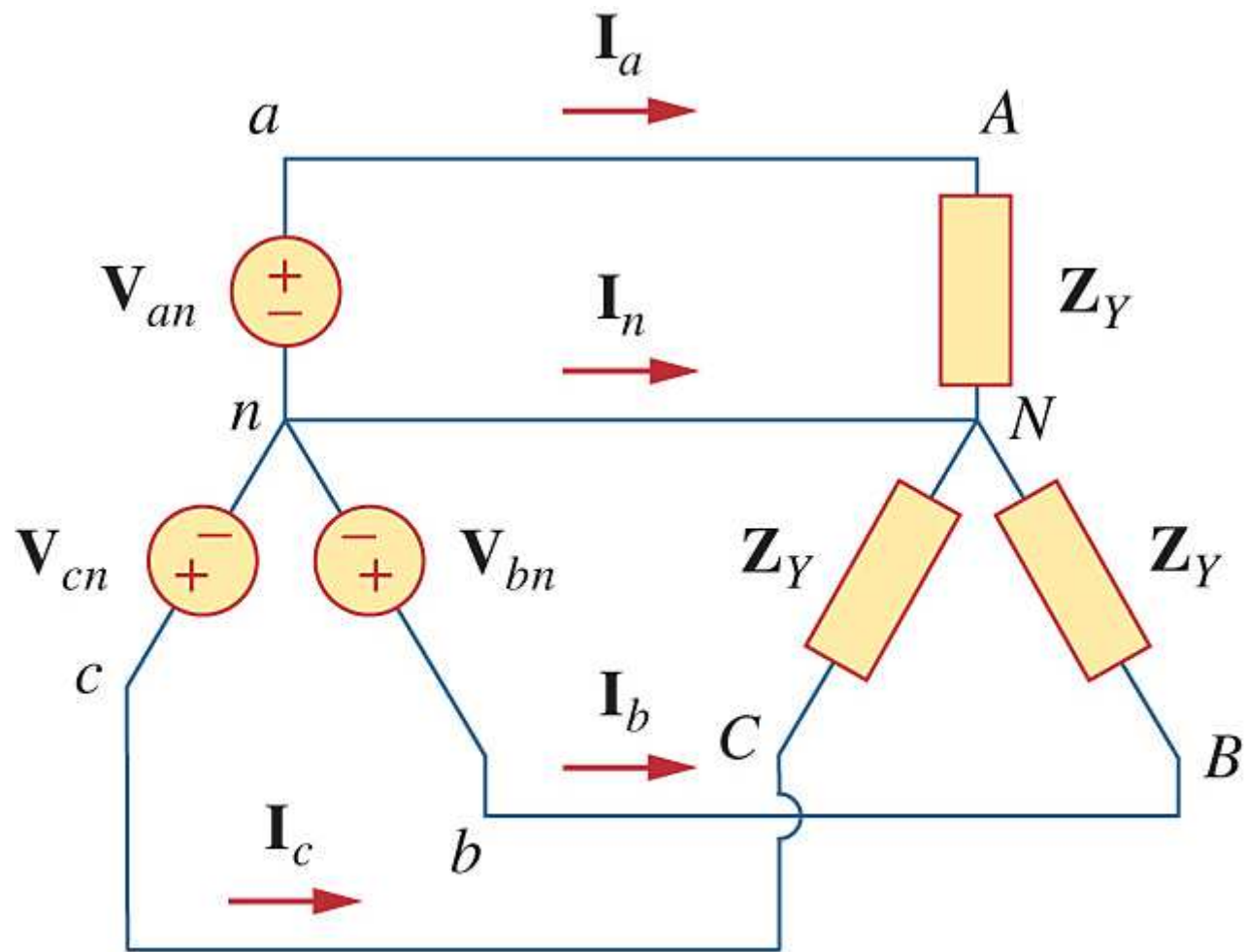


Figure 12.10 Balanced Y-Y connection.

Fig.12.9  Fig. 12.10

If balanced, the system can be simplified.

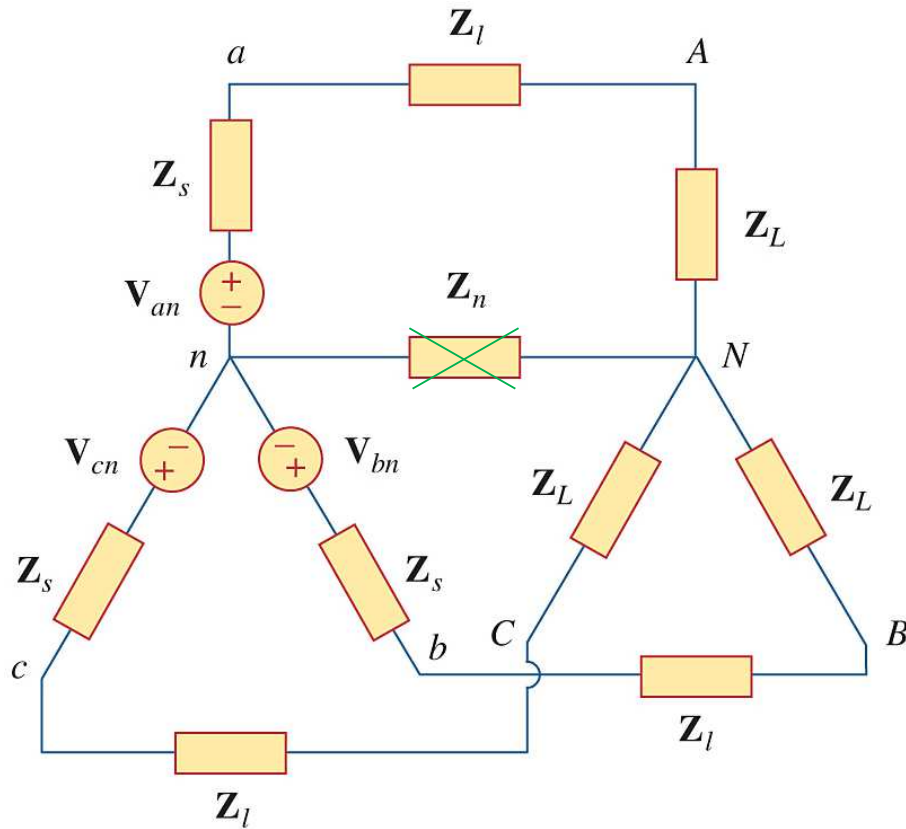


Figure 12.9 A balanced Y-Y system, showing the source, line, and load impedances.

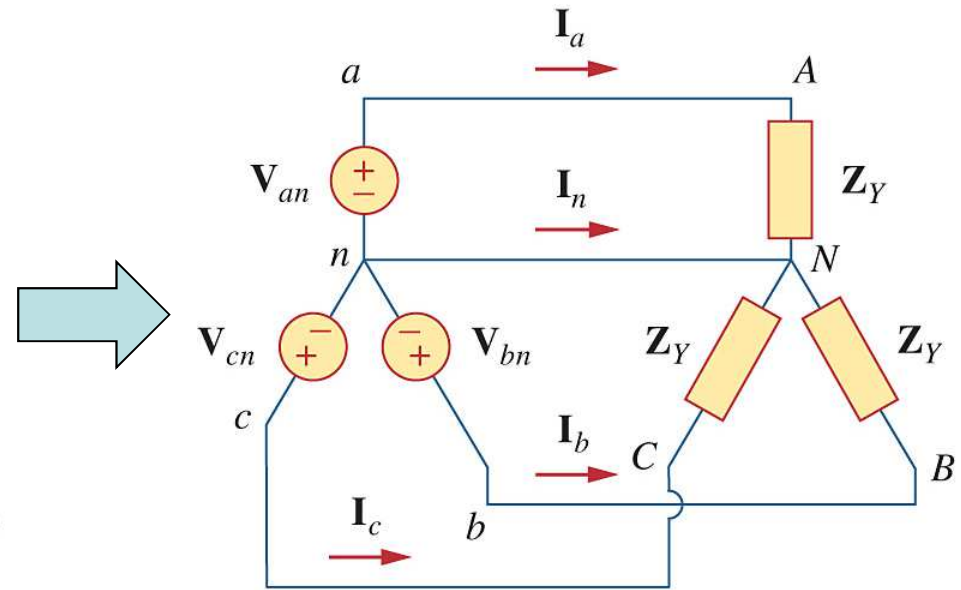


Figure 12.10 Balanced Y-Y connection.

$$Z_Y = Z_S + Z_l + Z_L$$

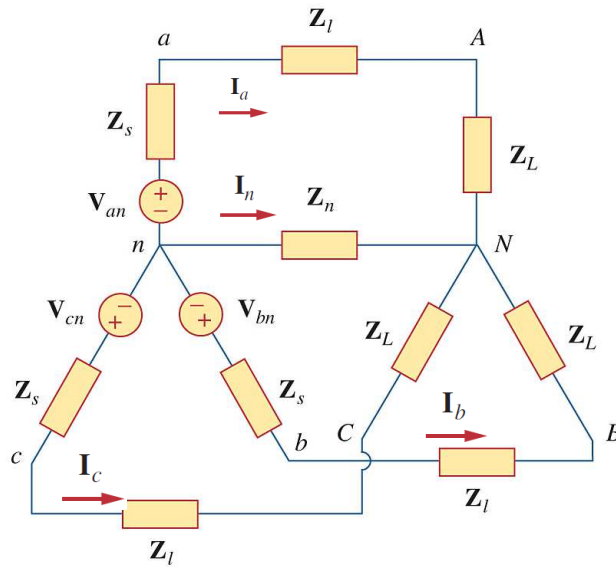


Figure 12.9 A balanced Y-Y system, showing the source, line, and load impedances.

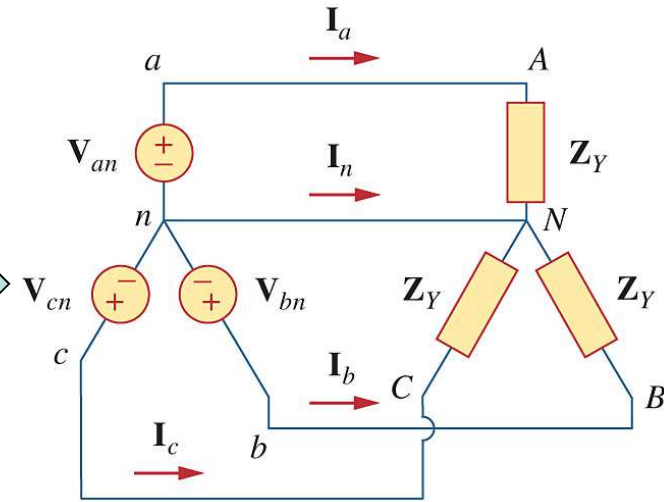
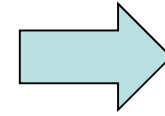


Figure 12.10 Balanced Y-Y connection.

$$\tilde{V}_{an} = \tilde{I}_a (Z_s + Z_l + Z_L) - \tilde{I}_n Z_n$$

$$\tilde{V}_{bn} = \tilde{I}_b (Z_s + Z_l + Z_L) - \tilde{I}_n Z_n$$

$$\tilde{V}_{cn} = \tilde{I}_c (Z_s + Z_l + Z_L) - \tilde{I}_n Z_n$$

$$\tilde{V}_{an} + \tilde{V}_{bn} + \tilde{V}_{cn}$$

$$= (\tilde{I}_a + \tilde{I}_b + \tilde{I}_c)(Z_s + Z_l + Z_L) - 3\tilde{I}_n Z_n$$

but $\tilde{I}_a + \tilde{I}_b + \tilde{I}_c + \tilde{I}_n = 0$, i.e., $\tilde{I}_a + \tilde{I}_b + \tilde{I}_c = -\tilde{I}_n$

$$\underline{\tilde{V}_{an} + \tilde{V}_{bn} + \tilde{V}_{cn}} = -\tilde{I}_n (Z_s + Z_l + Z_L) - 3\tilde{I}_n Z_n$$

$$= -\tilde{I}_n (Z_s + Z_l + Z_L + 3Z_n) = 0$$

$$\tilde{I}_n = 0$$

$$\tilde{V}_{nN} = \tilde{I}_n Z_n = 0$$

Balanced source

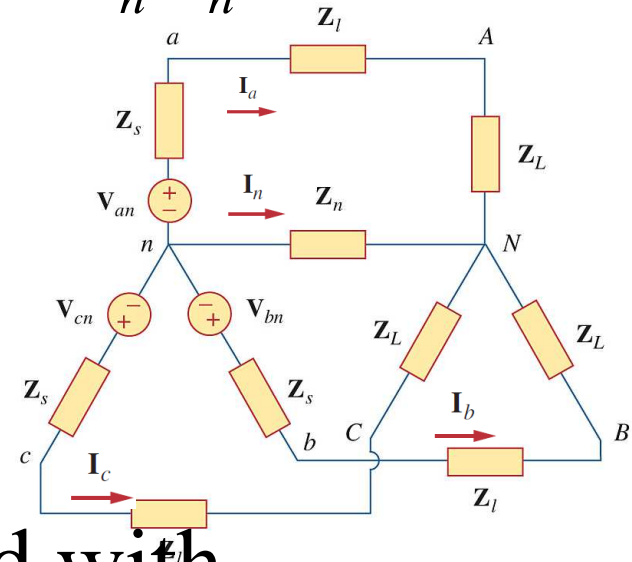


Figure 12.9 A balanced Y-Y system, showing the source, line, and load impedances.

so the neutral line can be replaced with
an open circuit or a short circuit.

Consider Fig. 12.10. Assuming the positive sequence, the phase voltages (or line-to-neutral voltages) are

$$\tilde{V}_{an} = V_p \angle 0^\circ$$

$$\tilde{V}_{bn} = V_p \angle -120^\circ$$

$$\tilde{V}_{cn} = V_p \angle -240^\circ$$

Balanced source:
Same amplitude and frequency
Out of phase with each other by 120°

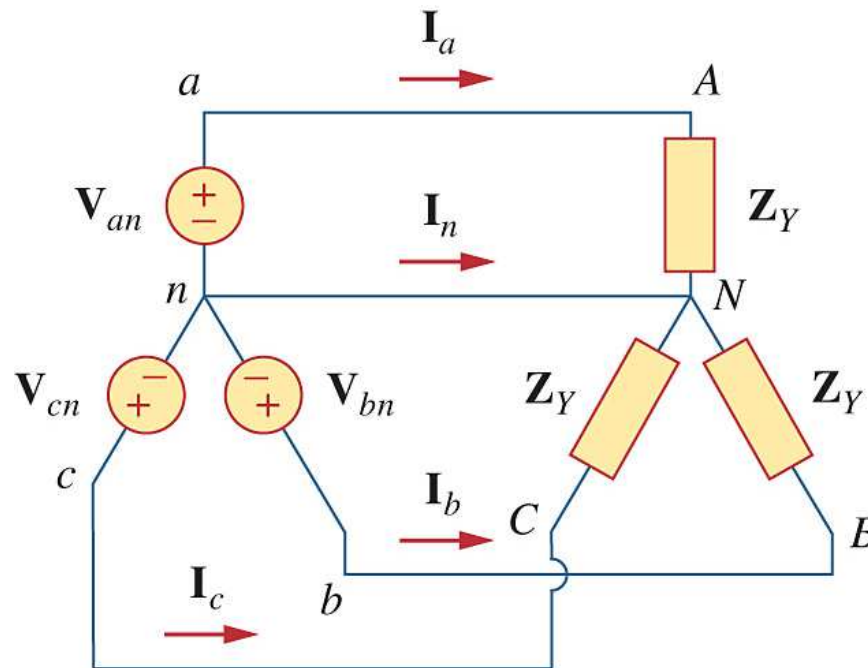


Figure 12.10 Balanced Y-Y connection.

The line voltages (or line-to-line voltages) are

$$\tilde{V}_{ab} = \tilde{V}_{an} - \tilde{V}_{bn} = \sqrt{3}V_p \angle 30^\circ$$

$$\tilde{V}_{bc} = \tilde{V}_{bn} - \tilde{V}_{cn} = \sqrt{3}V_p \angle -90^\circ = \tilde{V}_{ab} \angle -120^\circ$$

$$\tilde{V}_{ca} = \tilde{V}_{cn} - \tilde{V}_{an} = \sqrt{3}V_p \angle -210^\circ = \tilde{V}_{ab} \angle -240^\circ$$

$$\tilde{V}_{ab} + \tilde{V}_{bc} + \tilde{V}_{ca} = 0$$

Line voltages are also balanced.

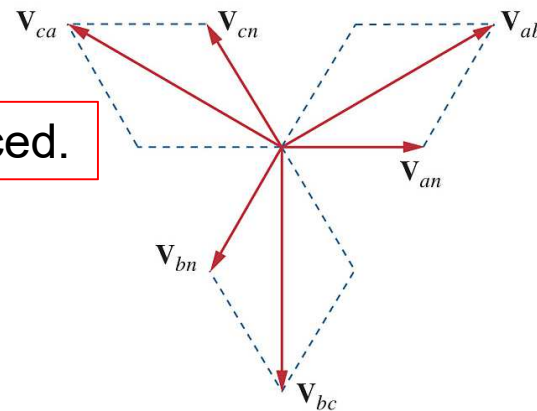


Figure 12.11(b) Phasor diagram illustrating the relationship between line voltages and phase voltages.

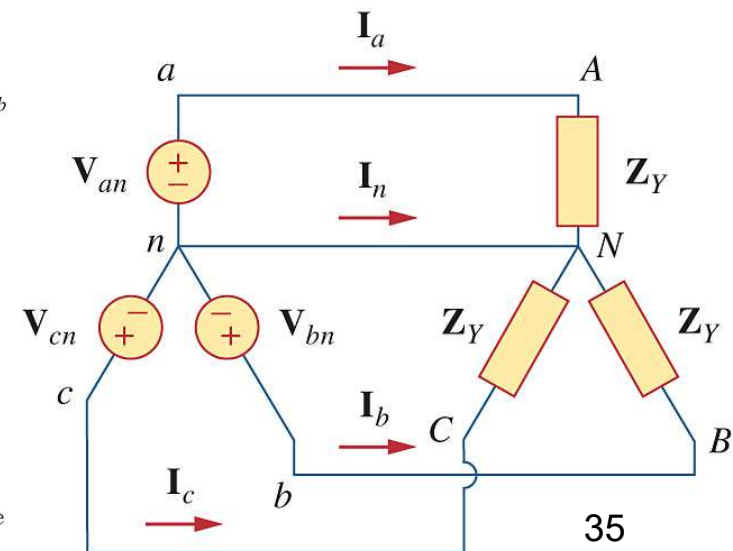


Figure 12.10 Balanced Y-Y connection.

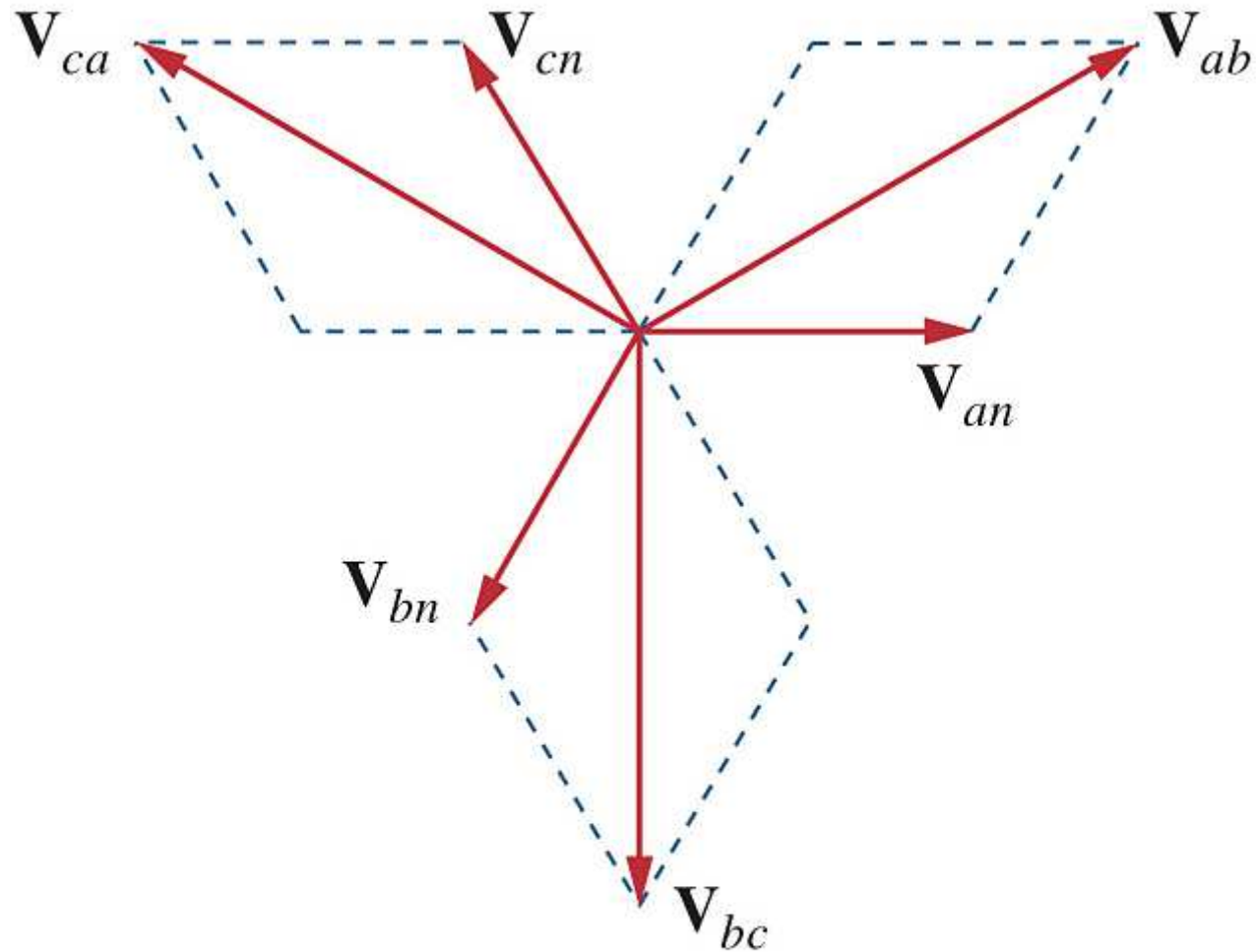


Figure 12.11(b) Phasor diagram illustrating the relationship between line voltages and phase voltages.

The magnitude of the line voltages is $\sqrt{3}$ times the magnitude of the phase voltages.

$$V_L = \sqrt{3}V_p$$

where

$$V_p = |\tilde{V}_{an}| = |\tilde{V}_{bn}| = |\tilde{V}_{cn}|$$

$$V_L = |\tilde{V}_{ab}| = |\tilde{V}_{bc}| = |\tilde{V}_{ca}|$$

V_P

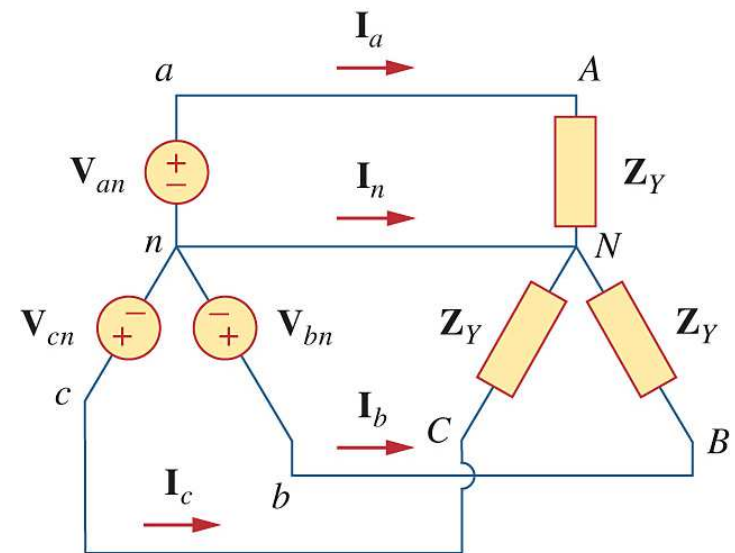


Figure 12.10 Balanced Y-Y connection.

The line voltages lead their corresponding phase voltages by 30° .

$$\angle \tilde{V}_{ab} = \angle \tilde{V}_{an} + 30^\circ$$

$$\angle \tilde{V}_{bc} = \angle \tilde{V}_{bn} + 30^\circ$$

$$\angle \tilde{V}_{ca} = \angle \tilde{V}_{cn} + 30^\circ$$

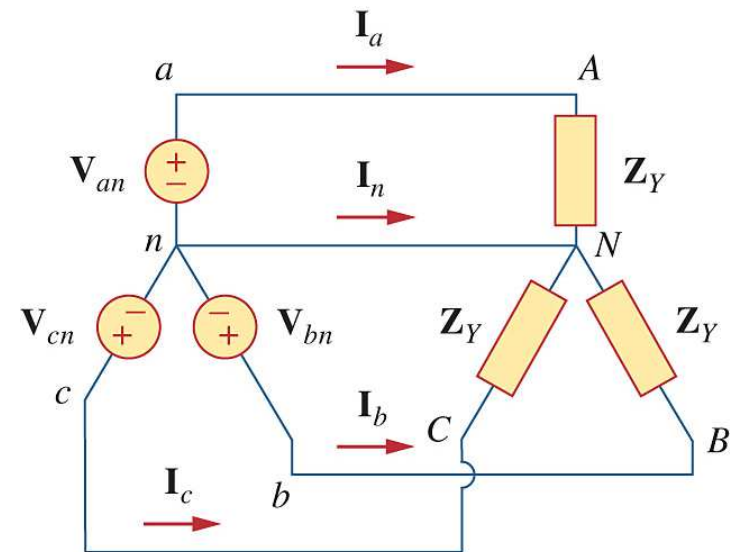


Figure 12.10 Balanced Y-Y connection.

The line currents are

$$\tilde{I}_a = \frac{\tilde{V}_{an}}{Z_Y}$$

$$\tilde{I}_b = \frac{\tilde{V}_{bn}}{Z_Y} = \tilde{I}_a \angle -120^\circ$$

$$\tilde{I}_c = \frac{\tilde{V}_{cn}}{Z_Y} = \tilde{I}_a \angle -240^\circ$$

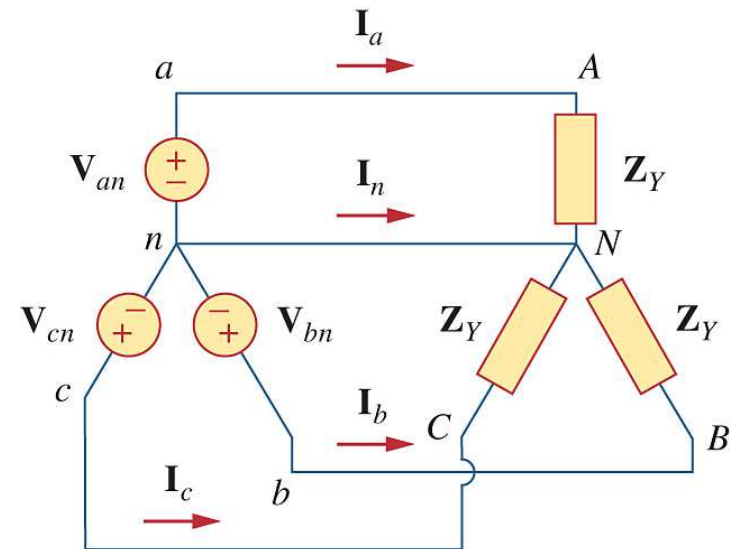


Figure 12.10 Balanced Y-Y connection.

Since $\tilde{I}_n = 0$, the neutral line can be removed without affecting the system. In fact, in long distance power transmission, conductors in multiples of three are used with the earth itself as the neutral ground. Power systems designed in this way are well ground at all critical points to ensure safety.

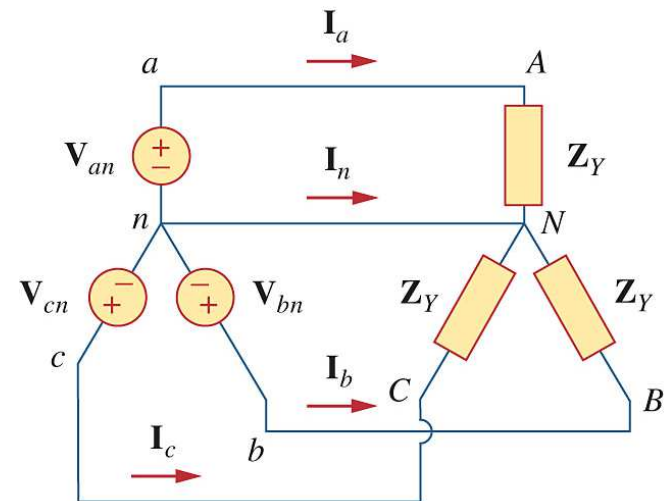


Figure 12.10 Balanced Y-Y connection.

While the line current is the current in each line, the phase current is the current in each phase of the source or load. In the Y-Y system, the line current is the same as the phase current.

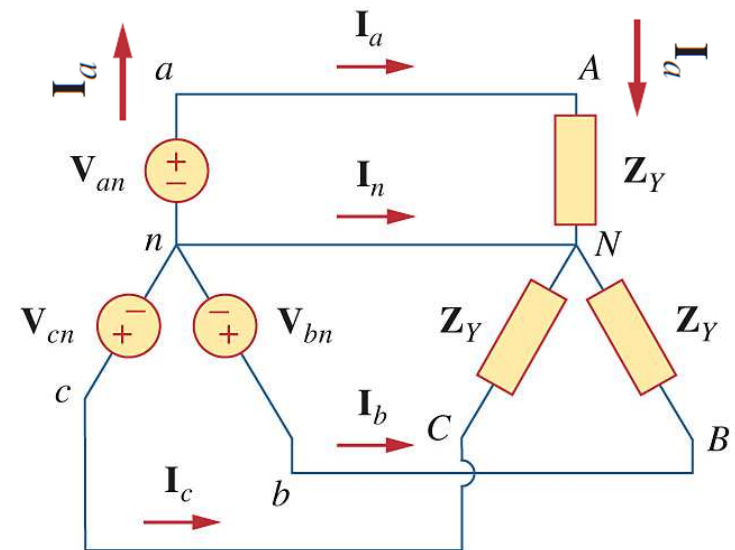


Figure 12.10 Balanced Y-Y connection.

An alternative way of analyzing a balanced Y-Y system is to do so on a per phase basis.

We look at one phase, say phase a , and analyze the single-phase equivalent circuit in Fig. 12.12.

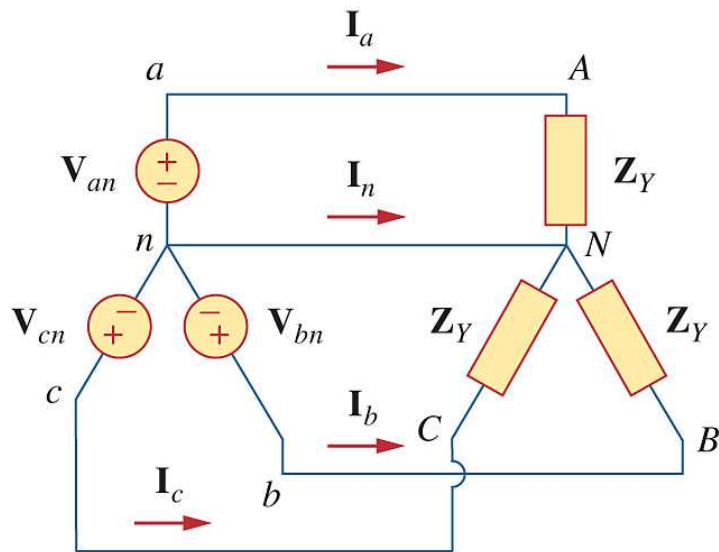


Figure 12.10 Balanced Y-Y connection.

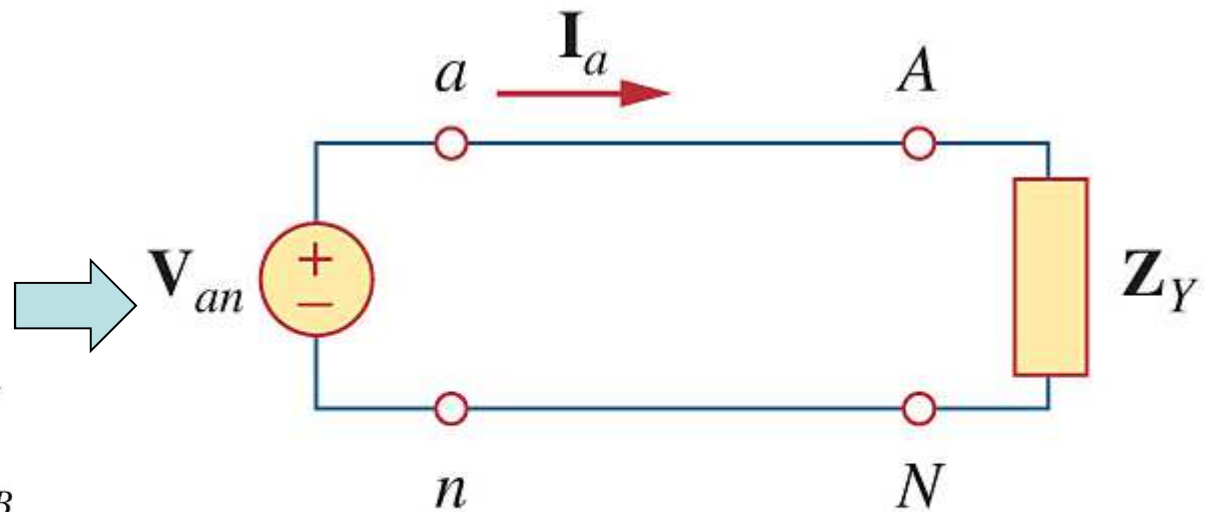


Figure 12.12 A single-phase equivalent circuit.

Summary of balanced Y-Y

If the source (phase voltages) are in abc sequence,

• Voltages: Magnitude

$$V_L = \sqrt{3}V_p$$

Phase

$$\angle \tilde{V}_{ab} = \angle \tilde{V}_{an} + \angle 30^\circ$$

$$\angle \tilde{V}_{bc} = \angle \tilde{V}_{bn} + \angle 30^\circ$$

$$\angle \tilde{V}_{ca} = \angle \tilde{V}_{cn} + \angle 30^\circ$$

Line voltages and phase voltages are in abc sequence

• Currents:

Line currents and phase currents are same, and are in abc sequence

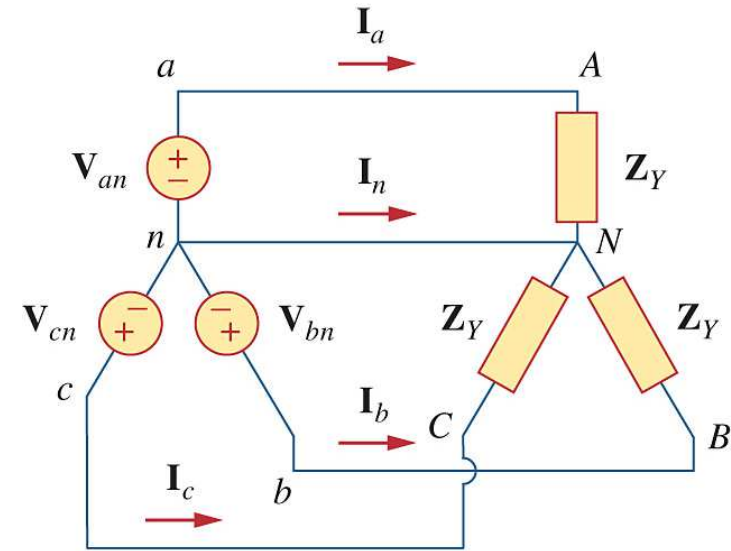


Figure 12.10 Balanced Y-Y connection.

Practice Problem 12.2 A Y-connected balanced three-phase generator with an impedance of $0.4 + j0.3 \, \Omega$ per phase is connected to a Y-connected balanced load with an impedance of $24 + j19 \, \Omega$ per phase. The line joining the generator and the load has an impedance of $0.6 + j0.7 \, \Omega$ per phase. Assuming a positive sequence for the source voltages and that $\tilde{V}_{an} = 120 \angle 30^\circ \text{ V}$, find the line voltages and the line currents.

Solution :

$$Z_Y = Z_s + Z_l + Z_L = (0.4 + j0.3) + (24 + j19) + (0.6 + j0.7) = 25 + j20 \text{ } (\Omega)$$

$$\tilde{I}_a = \frac{\tilde{V}_{an}}{Z_Y} = \frac{120 \angle 30^\circ}{25 + j20} \approx \frac{120 \angle 30^\circ}{32.0156 \angle 38.66^\circ} \approx 3.7482 \angle -8.66^\circ \text{ (A)}$$

$$\tilde{I}_b = \tilde{I}_a \angle -120^\circ = 3.7482 \angle -128.66^\circ \text{ (A)}$$

$$\tilde{I}_c = \tilde{I}_a \angle -240^\circ = 3.7482 \angle -248.66^\circ \text{ (A)}$$

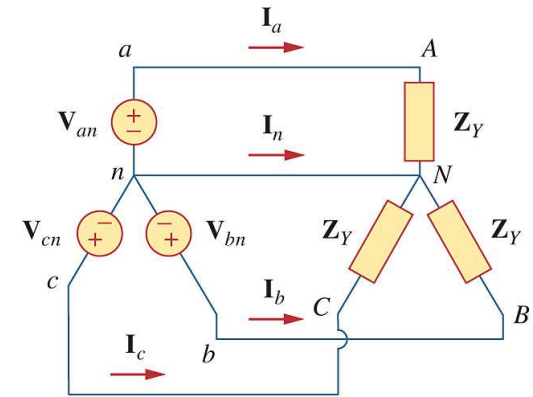


Figure 12.10 Balanced Y-Y connection.

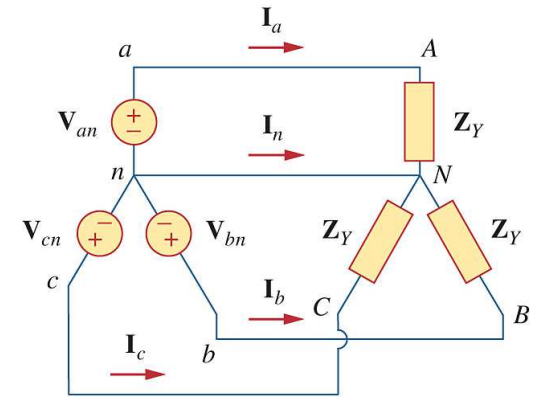


Figure 12.10 Balanced Y-Y connection.

The "ideal" line voltages are

$$\tilde{V}_{ab} = \tilde{V}_{an} \sqrt{3} \angle 30^\circ = 120 \angle 30^\circ \times \sqrt{3} \angle 30^\circ$$

$$\approx 207.8461 \angle 60^\circ \text{ (V)}$$

$$\tilde{V}_{bc} = \tilde{V}_{ab} \angle -120^\circ = 207.8461 \angle -60^\circ \text{ (V)}$$

$$\tilde{V}_{ca} = \tilde{V}_{ab} \angle -240^\circ = 207.8461 \angle -180^\circ \text{ (V)}$$

Note that for a balanced system, the other two voltages/currents can be quickly obtained by their **phase relation**.

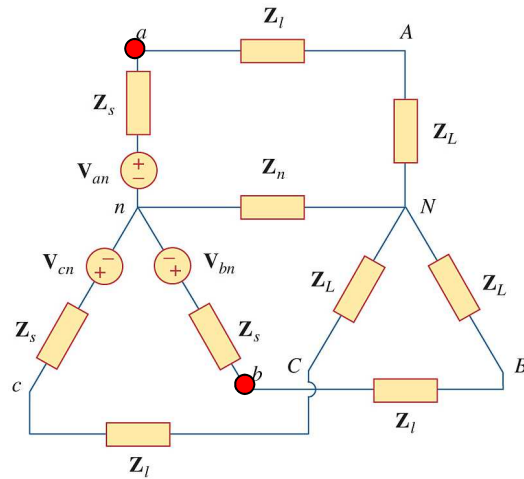


Figure 12.9 A balanced Y-Y system, showing the source, line, and load impedances.

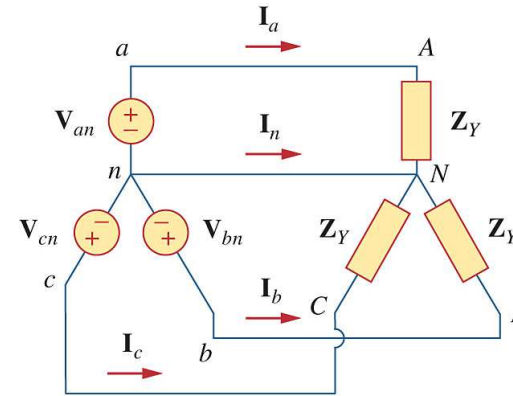


Figure 12.10 Balanced Y-Y connection.

The line voltages seen from the generator terminals are

V_{ab} in the figure

$$\tilde{V}_{ab} = \tilde{I}_a(Z_l + Z_L) - \tilde{I}_b(Z_l + Z_L)$$

$$= \tilde{I}_a \sqrt{3} \angle 30^\circ (Z_l + Z_L)$$

$$= \frac{\tilde{V}_{an}}{Z_Y} \sqrt{3} \angle 30^\circ (Z_l + Z_L) = \tilde{V}_{ab} \left(\frac{Z_l + Z_L}{Z_Y} \right)$$

Line voltage V_{ab}

$$\begin{aligned}
&= 207.8461 \angle 60^\circ \times \left(\frac{24.6 + j19.7}{25 + j20} \right) \\
&\approx 207.8461 \angle 60^\circ \times \frac{31.5159 \angle 38.69^\circ}{32.0156 \angle 38.66^\circ} \\
&\approx 204.6020 \angle 60.03^\circ \text{ (V)}
\end{aligned}$$

V_{bc} in the figure

$$\tilde{V}_{b'c'} = 204.6020 \angle -59.97^\circ \text{ (V)}$$

V_{ca} in the figure

$$\tilde{V}_{c'a'} = 204.6020 \angle -179.97^\circ \text{ (V)}$$

The line voltages seen from the load terminals are

$$V_{AN} - V_{BN}$$

$$I_a - I_b = I_a \sqrt{3} \angle 30^\circ = V_{an} / Z_Y \sqrt{3} \angle 30^\circ = V_{ab} / Z_Y$$

$$\tilde{V}_{AB} = \tilde{I}_a Z_L - \tilde{I}_b Z_L = \tilde{V}_{ab} \frac{Z_L}{Z_Y}$$

$$= 207.8461 \angle 60^\circ \times \left(\frac{24 + j19}{25 + j20} \right)$$

$$\approx 207.8461 \angle 60^\circ \times \frac{30.6105 \angle 38.37^\circ}{32.0156 \angle 38.66^\circ}$$

$$\approx 198.7242 \angle 59.71^\circ \text{ (V)}$$

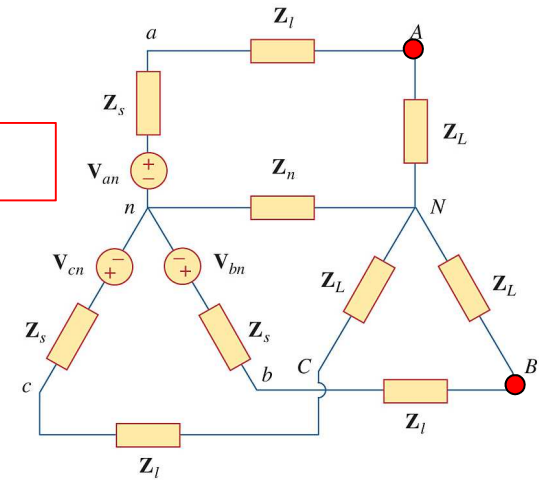


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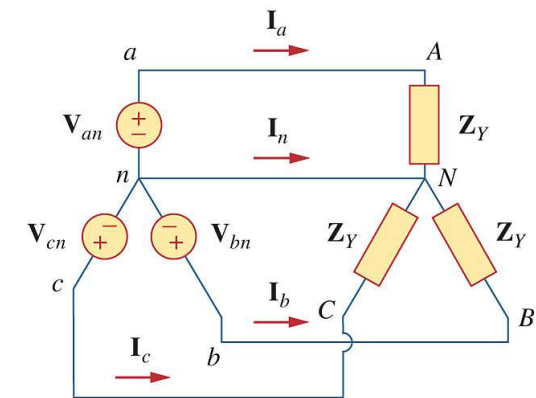


Figure 12.10 Balanced Y-Y connection.

$$\tilde{V}_{BC} \approx 198.7242 \angle -60.29^\circ \text{ (V)}$$

$$\tilde{V}_{CA} \approx 198.7242 \angle -180.29^\circ \text{ (V)}$$

The line voltage drops are

$$\tilde{I}_a Z_l = 3.7482 \angle -8.66^\circ \times (0.6 + j0.7)$$

$$\approx 3.4558 \angle 40.74^\circ \text{ (V)}$$

$$\tilde{I}_b Z_l = 3.4558 \angle -79.26^\circ \text{ (V)}$$

$$\tilde{I}_c Z_l = 3.4558 \angle -199.26^\circ \text{ (V)}$$

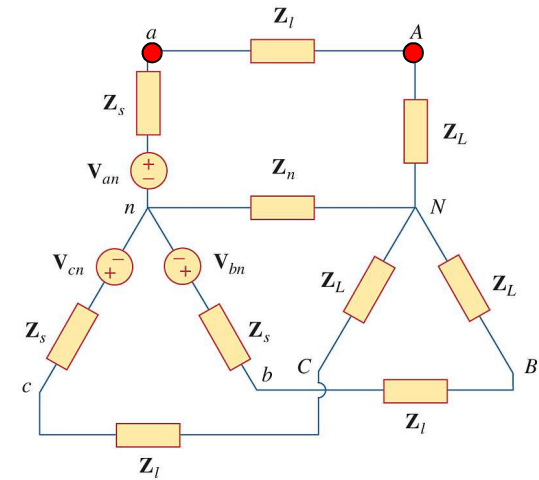


Figure 12.9 A balanced Y-Y system, showing the source, line, and load impedances.

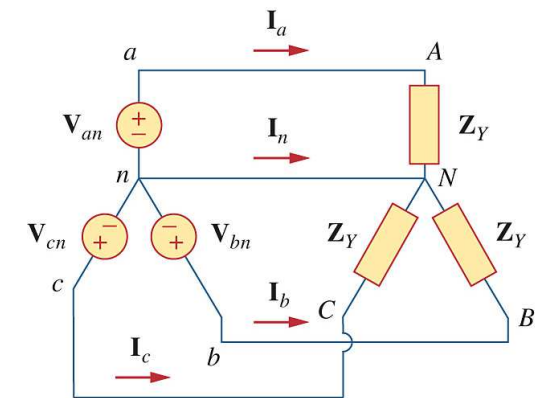


Figure 12.10 Balanced Y-Y connection.

12.4 Balanced Wye-Delta Connection

A Balanced Y- Δ system consists of a balanced Y-connected source feeding a balanced Δ -connected load, as shown in Fig. 12.14.

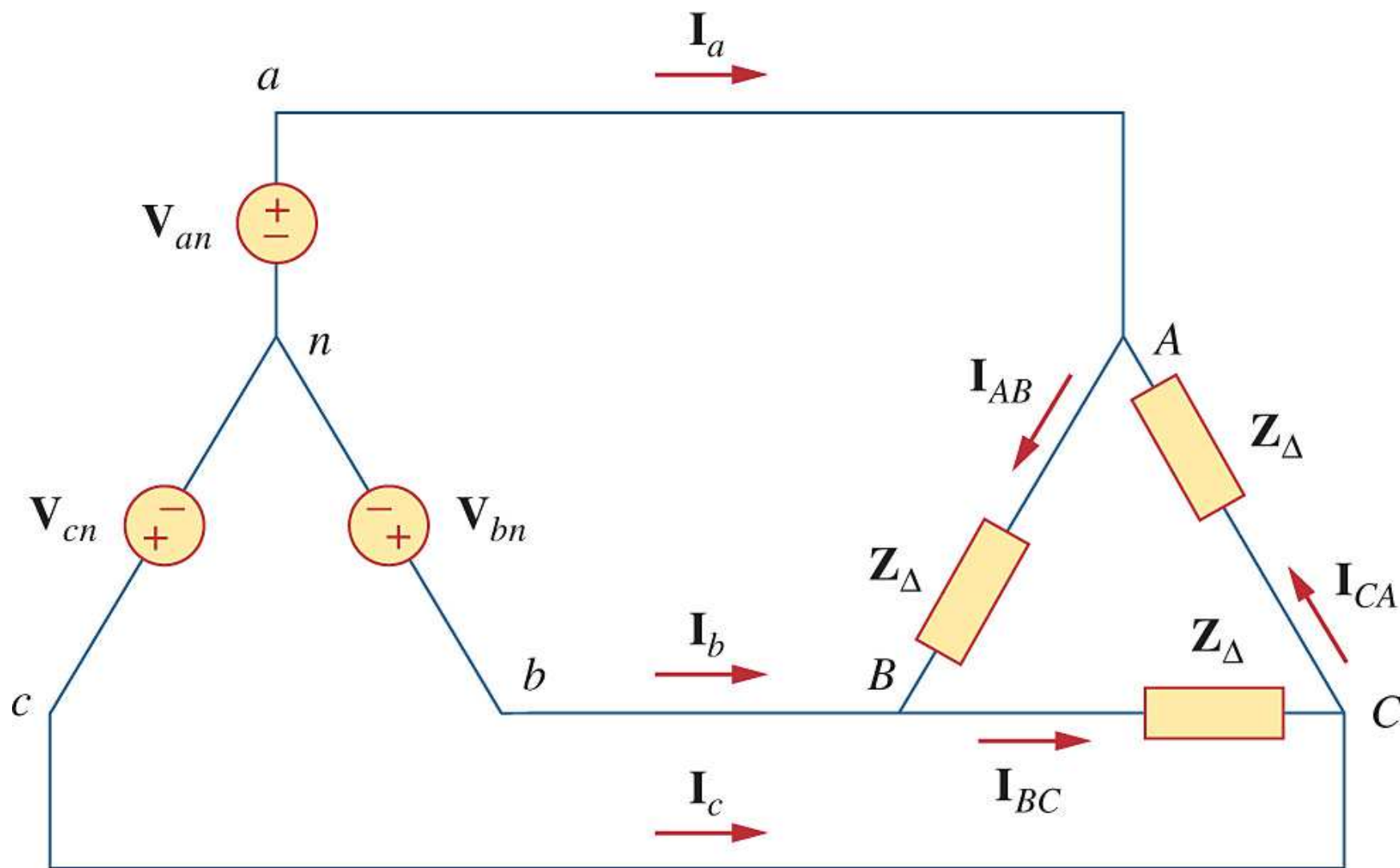


Figure 12.14 Balanced wye-delta connection.

Assume that

$$\tilde{V}_{an} = V_p \angle 0^\circ$$

$$\tilde{V}_{bn} = V_p \angle -120^\circ$$

$$\tilde{V}_{cn} = V_p \angle -240^\circ$$

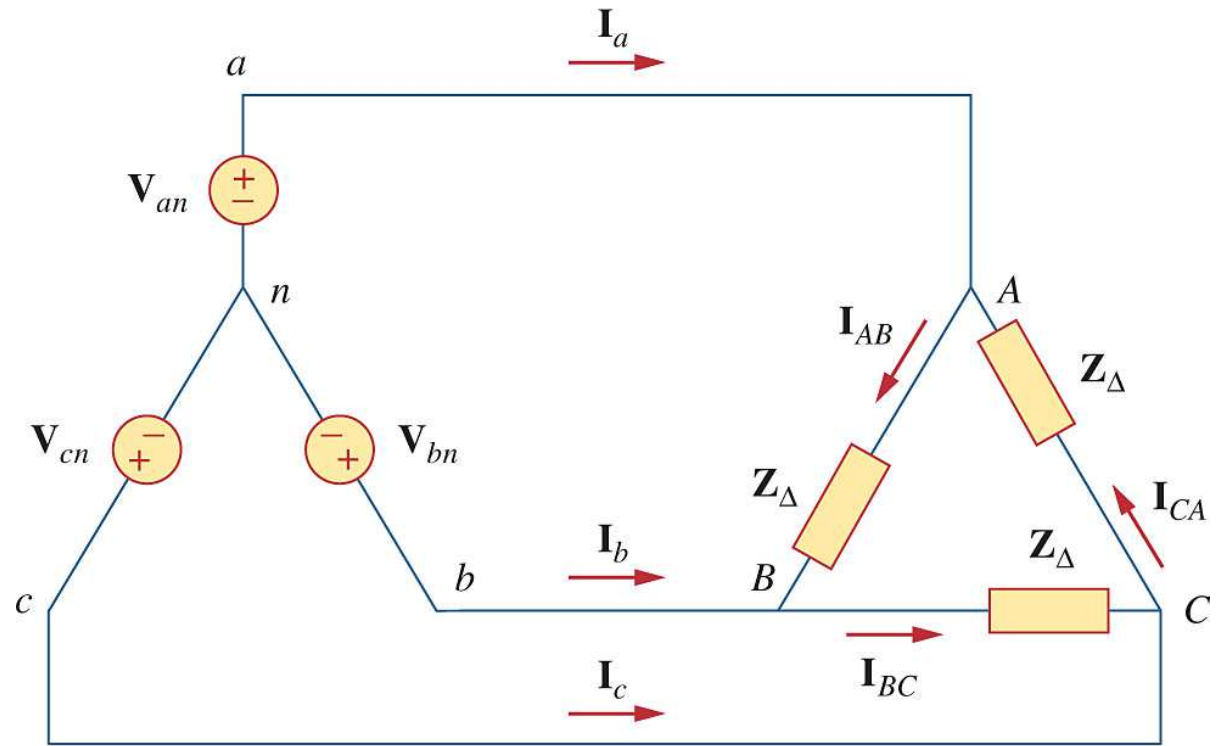


Figure 12.14 Balanced wye-delta connection.

The line voltages are

$$\tilde{V}_{ab} = \sqrt{3}V_p \angle 30^\circ = \tilde{V}_{an} \sqrt{3} \angle 30^\circ = \tilde{V}_{AB}$$

$$\tilde{V}_{bc} = \tilde{V}_{ab} \angle -120^\circ = \tilde{V}_{BC}$$

$$\tilde{V}_{ca} = \tilde{V}_{ab} \angle -240^\circ = \tilde{V}_{CA}$$

Same as Y-Y case

The phase currents are

$$\tilde{I}_{AB} = \frac{\tilde{V}_{AB}}{Z_{\Delta}}$$

$$\tilde{I}_{BC} = \frac{\tilde{V}_{BC}}{Z_{\Delta}} = \tilde{I}_{AB} \angle -120^{\circ}$$

$$\tilde{I}_{CA} = \frac{\tilde{V}_{CA}}{Z_{\Delta}} = \tilde{I}_{AB} \angle -240^{\circ}$$

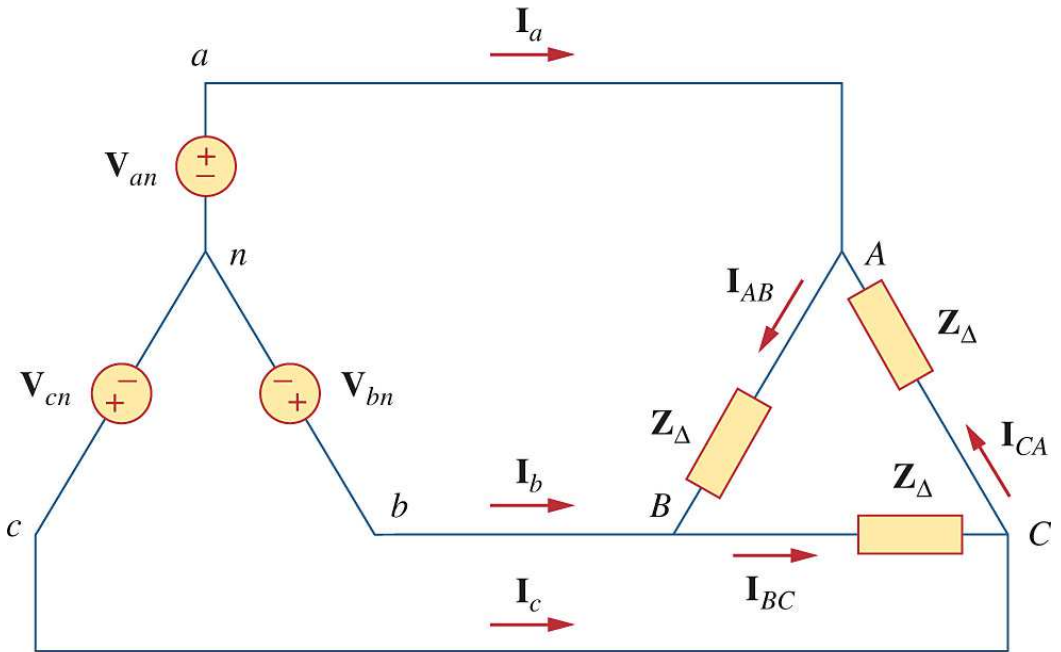


Figure 12.14 Balanced wye-delta connection.

The line currents are

$$\tilde{I}_a = \tilde{I}_{AB} - \tilde{I}_{CA} = \tilde{I}_{AB} \sqrt{3} \angle -30^\circ$$

$$\tilde{I}_b = \tilde{I}_{BC} - \tilde{I}_{AB} = \tilde{I}_{BC} \sqrt{3} \angle -30^\circ = \tilde{I}_a \angle -120^\circ$$

$$\tilde{I}_c = \tilde{I}_{CA} - \tilde{I}_{BC} = \tilde{I}_{CA} \sqrt{3} \angle -30^\circ = \tilde{I}_a \angle -240^\circ$$

showing that

$$I_L = \sqrt{3} I_p$$

where

$$I_L = |\tilde{I}_a| = |\tilde{I}_b| = |\tilde{I}_c|, I_p = |\tilde{I}_{AB}| = |\tilde{I}_{BC}| = |\tilde{I}_{CA}|$$

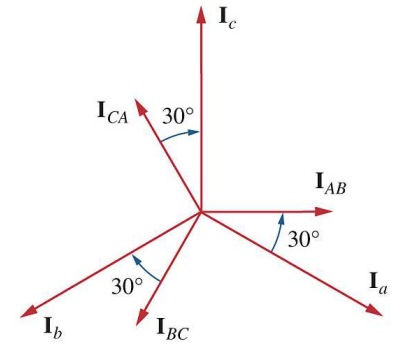


Figure 12.15 Phasor diagram illustrating the relationship between phase and line currents.

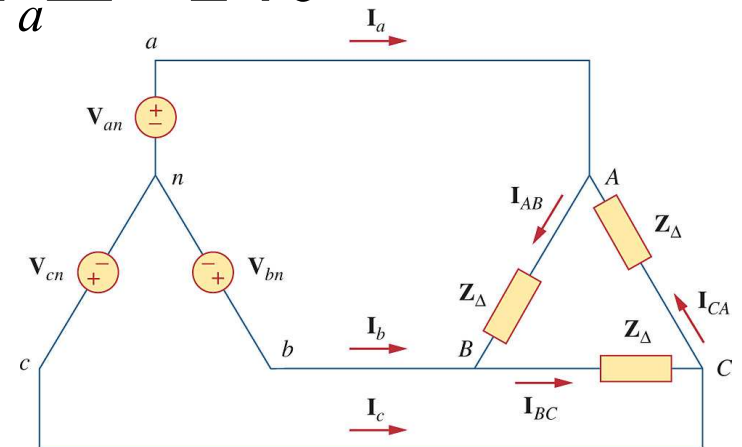


Figure 12.14 Balanced wye-delta connection.

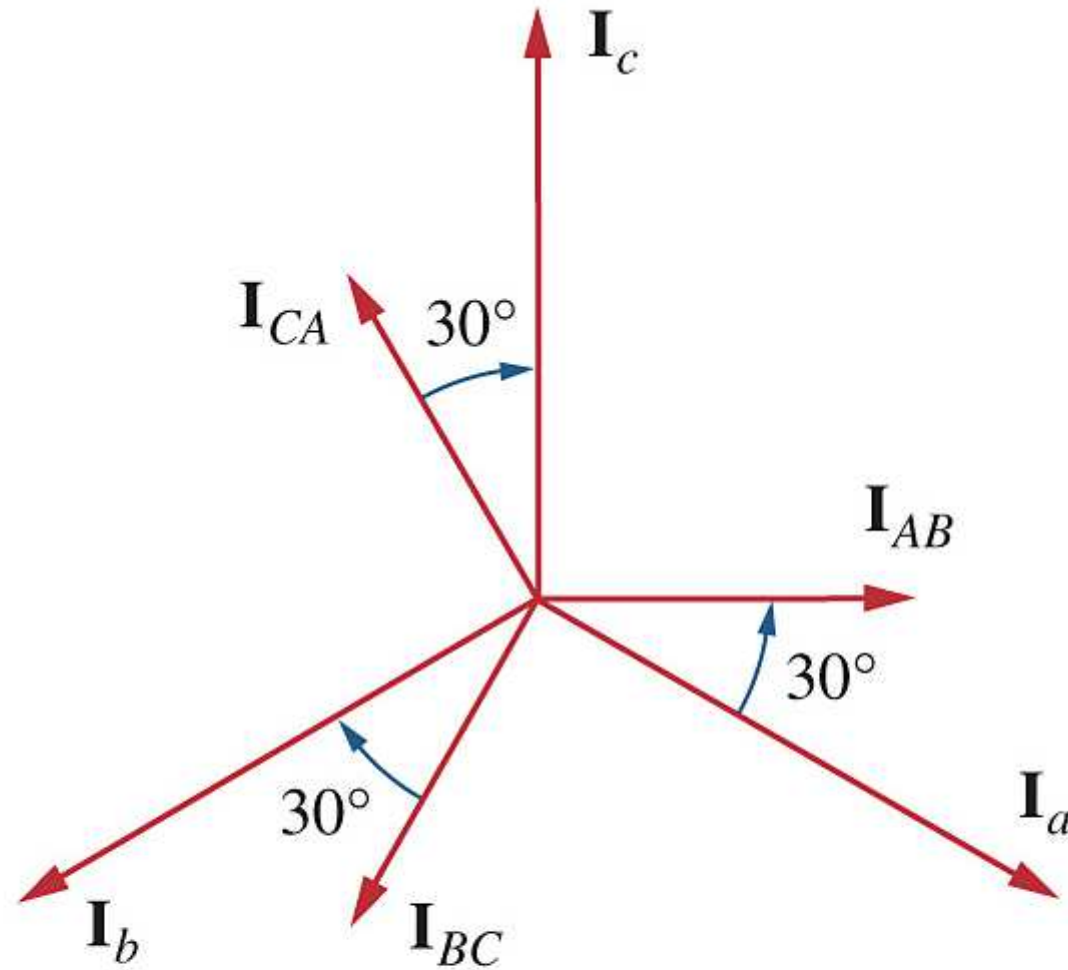


Figure 12.15 Phasor diagram illustrating the relationship between phase and line currents.

Summary of balanced Y-Δ

If the source (phase voltages) are in abc sequence,

• Voltages:

	<u>Magnitude</u>	<u>Phase</u>
$V_L = \sqrt{3}V_p$	$\angle \tilde{V}_{ab} = \angle \tilde{V}_{an} + \angle 30^\circ$	
	$\angle \tilde{V}_{bc} = \angle \tilde{V}_{bn} + \angle 30^\circ$	
	$\angle \tilde{V}_{ca} = \angle \tilde{V}_{cn} + \angle 30^\circ$	

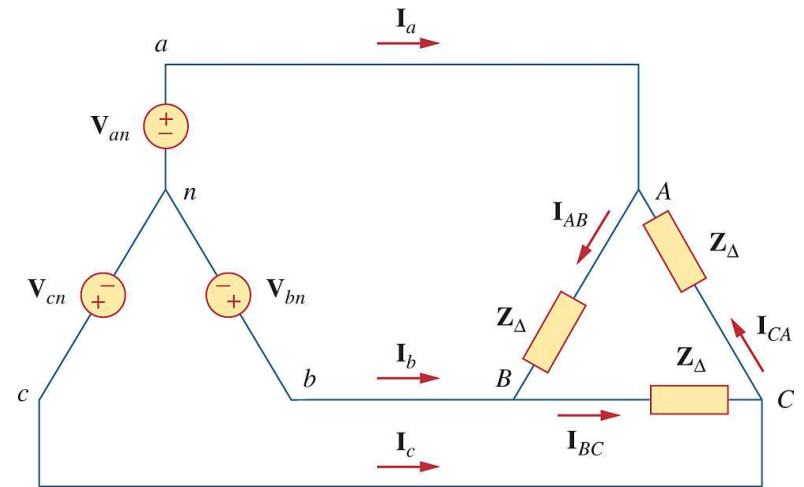


Figure 12.14 Balanced wye-delta connection.

Line voltages and phase voltages are in abc sequence

• Currents:

	<u>Magnitude</u>	<u>Phase</u>
$I_L = \sqrt{3}I_p$	$\tilde{I}_a = \tilde{I}_{AB} \sqrt{3} \angle -30^\circ$	
	

Line currents and phase currents are in abc sequence

Practice Problem 12.3 One line voltage of a balanced Y-connected source is $\tilde{V}_{AB} = 240\angle -20^\circ$ V. If the source is connected to a Δ -connected load of $20\angle 40^\circ \Omega$, find the phase and line currents. Assume the *abc* sequence.

Solution :

$$\tilde{I}_{AB} = \frac{\tilde{V}_{AB}}{Z_{\Delta}} = \frac{240\angle -20^\circ}{20\angle 40^\circ} = 12\angle -60^\circ \text{ (A)}$$

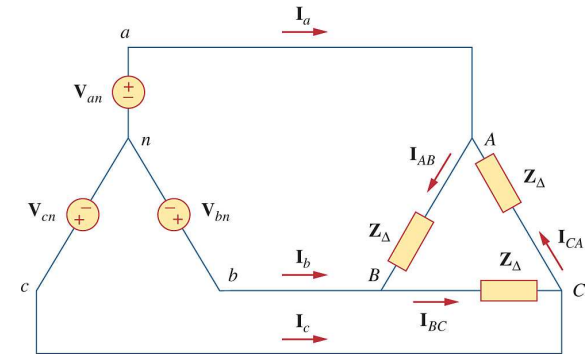


Figure 12.14 Balanced wye-delta connection.

$$\tilde{I}_{BC} = \tilde{I}_{AB} \angle -120^\circ = 12 \angle -180^\circ \text{ (A)}$$

$$\tilde{I}_{CA} = \tilde{I}_{AB} \angle +120^\circ = 12 \angle 60^\circ \text{ (A)}$$

$$\tilde{I}_a = \tilde{I}_{AB} \sqrt{3} \angle -30^\circ \approx 20.7846 \angle -90^\circ \text{ (A)}$$

$$\tilde{I}_b = \tilde{I}_a \angle +240^\circ = 20.7846 \angle 150^\circ \text{ (A)}$$

$$\tilde{I}_c = \tilde{I}_a \angle +120^\circ = 20.7846 \angle 30^\circ \text{ (A)}$$

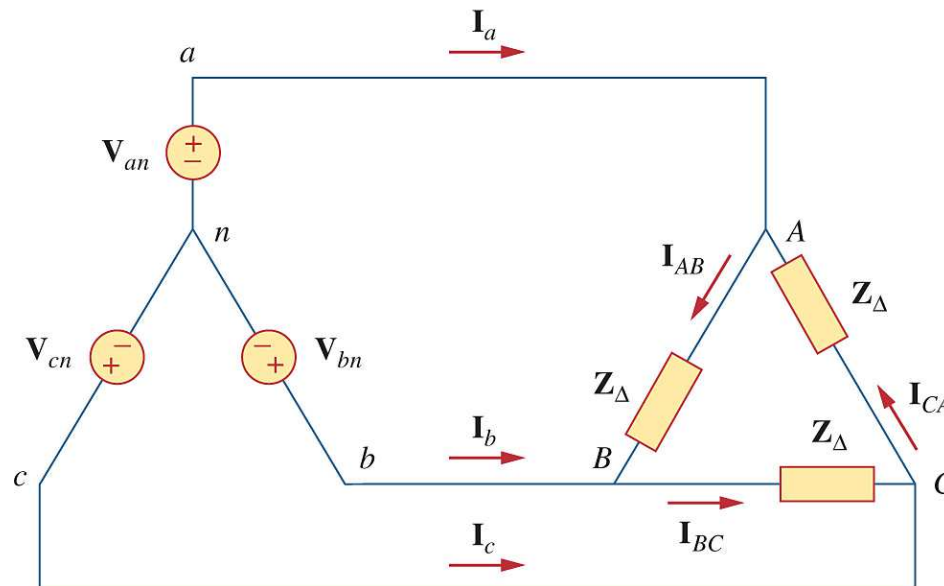


Figure 12.14 Balanced wye-delta connection.

12.5 Balanced Delta-Delta Connection

A balanced Δ - Δ system is one in which both the balanced source and balanced load are Δ -connected, as shown in Fig. 12.17.

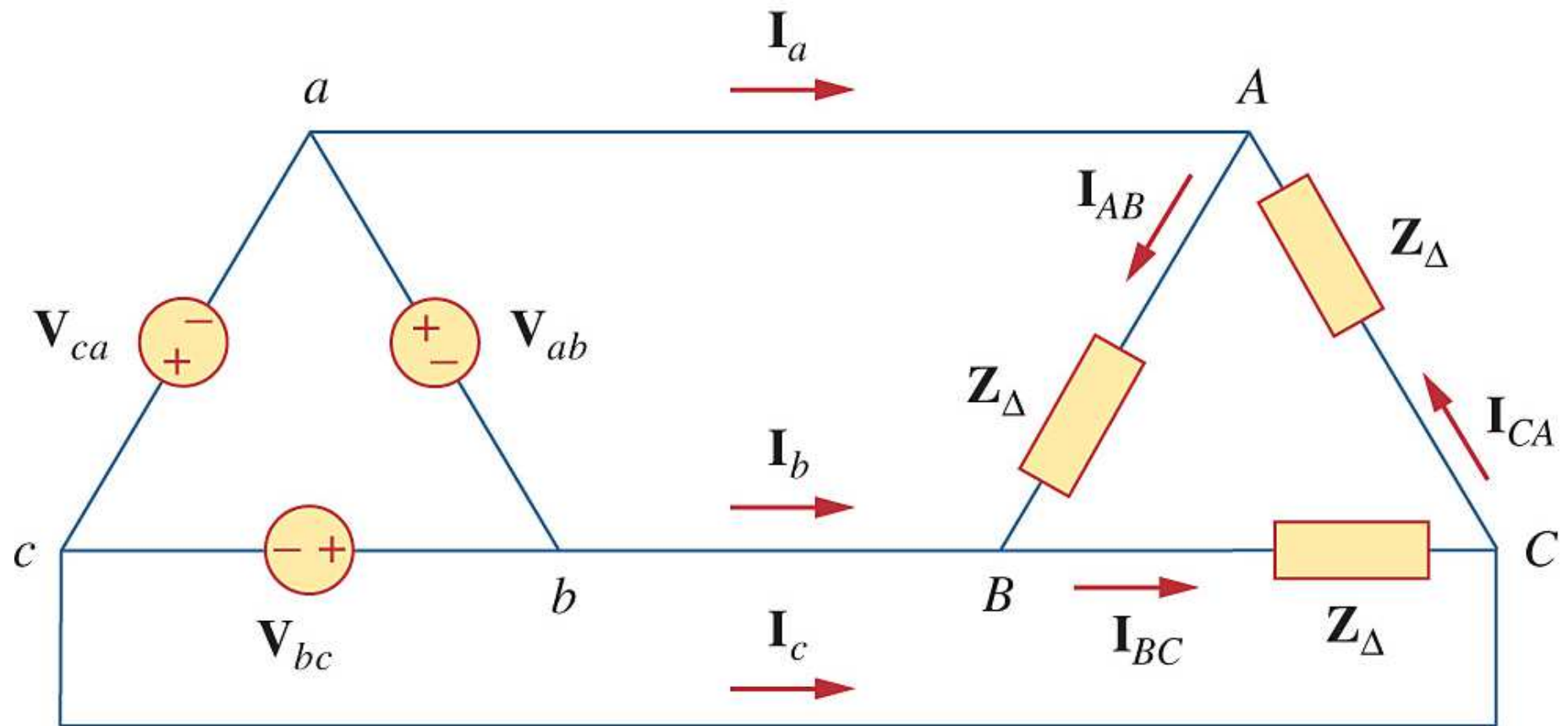


Figure 12.17 A balanced delta-delta connection.

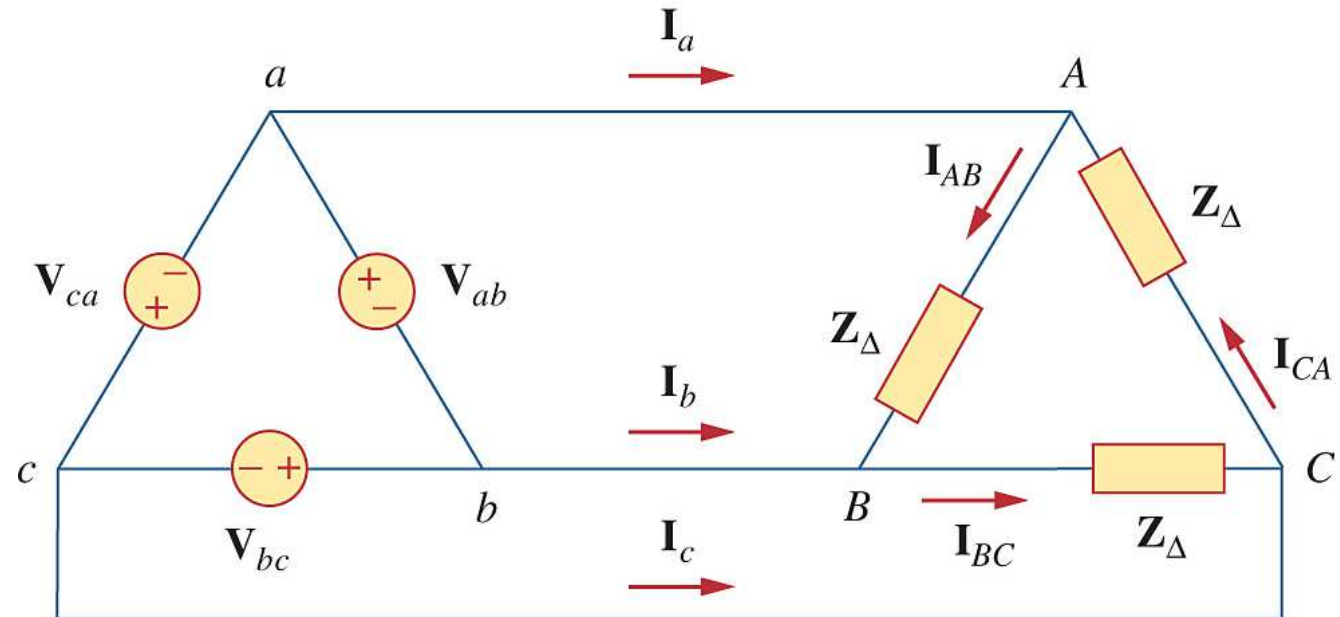


Figure 12.17 A balanced delta-delta connection.

Assume that

$$\tilde{V}_{ab} = V_p \angle 0^\circ$$

$$\tilde{V}_{bc} = V_p \angle -120^\circ$$

$$\tilde{V}_{ca} = V_p \angle +120^\circ$$

The line voltages are

$$\tilde{V}_{ab} = \tilde{V}_{AB}, \tilde{V}_{bc} = \tilde{V}_{BC}, \tilde{V}_{ca} = \tilde{V}_{CA}$$

The phase currents are

$$\tilde{I}_{AB} = \frac{\tilde{V}_{AB}}{Z_{\Delta}}$$

$$\tilde{I}_{BC} = \frac{\tilde{V}_{BC}}{Z_{\Delta}} = \tilde{I}_{AB} \angle -120^{\circ}$$

$$\tilde{I}_{CA} = \frac{\tilde{V}_{CA}}{Z_{\Delta}} = \tilde{I}_{AB} \angle +120^{\circ}$$

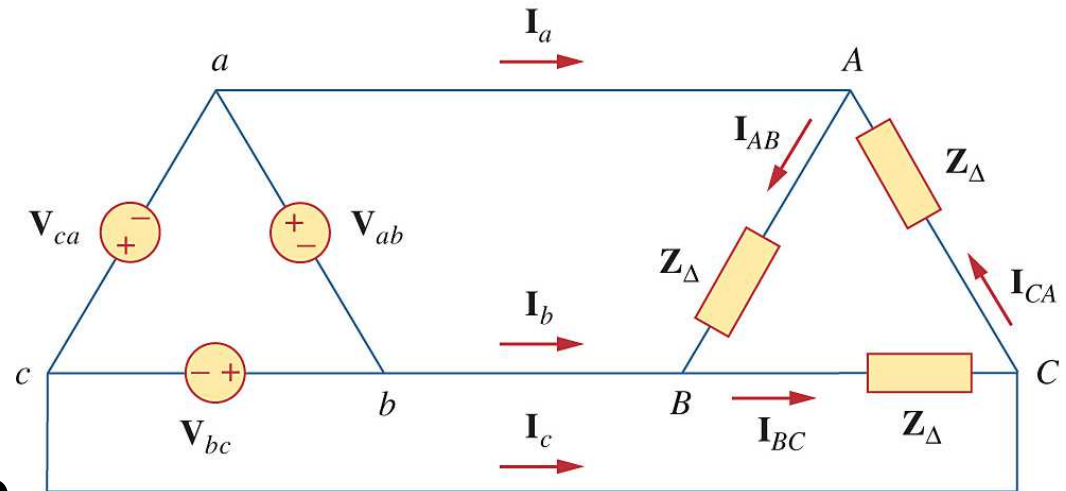


Figure 12.17 A balanced delta-delta connection.

The line currents are

$$\tilde{I}_a = \tilde{I}_{AB} - \tilde{I}_{CA} = \tilde{I}_{AB} \sqrt{3} \angle -30^\circ$$

$$\tilde{I}_b = \tilde{I}_{BC} - \tilde{I}_{AB} = \tilde{I}_{BC} \sqrt{3} \angle -30^\circ = \tilde{I}_a \angle -120^\circ$$

$$\tilde{I}_c = \tilde{I}_{CA} - \tilde{I}_{BC} = \tilde{I}_{CA} \sqrt{3} \angle -30^\circ = \tilde{I}_a \angle -240^\circ$$

showing that

$$I_L = \sqrt{3} I_p$$

where

$$I_L = |\tilde{I}_a| = |\tilde{I}_b| = |\tilde{I}_c|, I_p = |\tilde{I}_{AB}| = |\tilde{I}_{BC}| = |\tilde{I}_{CA}|$$

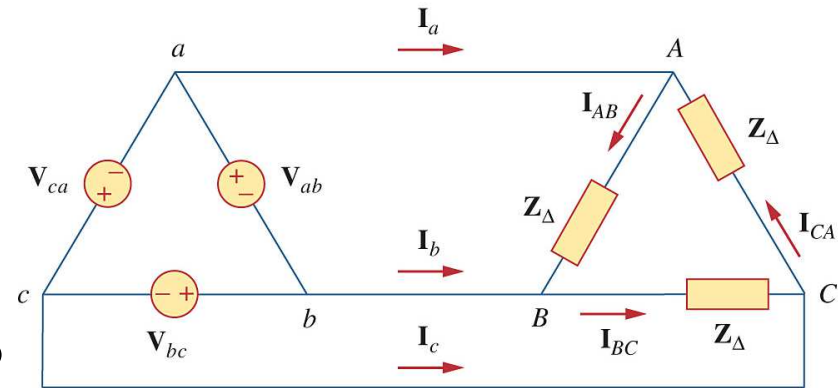


Figure 12.17 A balanced delta-delta connection.

Summary of balanced Δ - Δ

If the source (phase voltages) are in abc sequence,

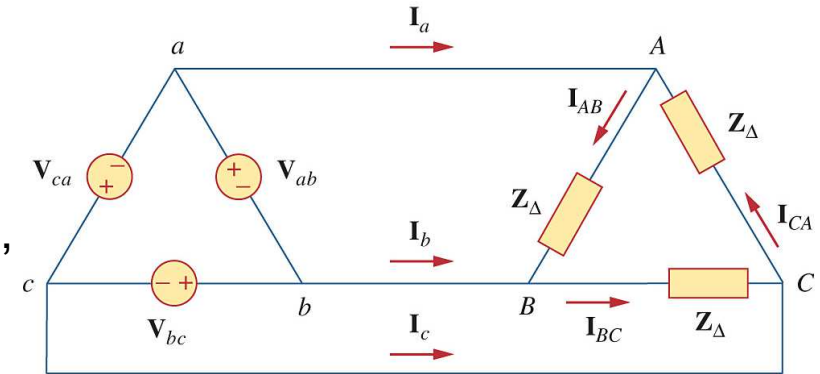


Figure 12.17 A balanced delta-delta connection.

- Voltages:

Line voltages and phase voltages are same, and are in abc sequence

- Currents: Magnitude Phase

$$I_L = \sqrt{3}I_p \quad \tilde{I}_a = \tilde{I}_{AB} \sqrt{3} \angle -30^\circ$$

.....

Line currents and phase currents are in abc sequence

12.6 Balanced Delta-Wye Connection

A balanced Δ -Y system consists of a balanced Δ -connected source feeding a balanced Y-connected load, as shown in Fig. 12.18.

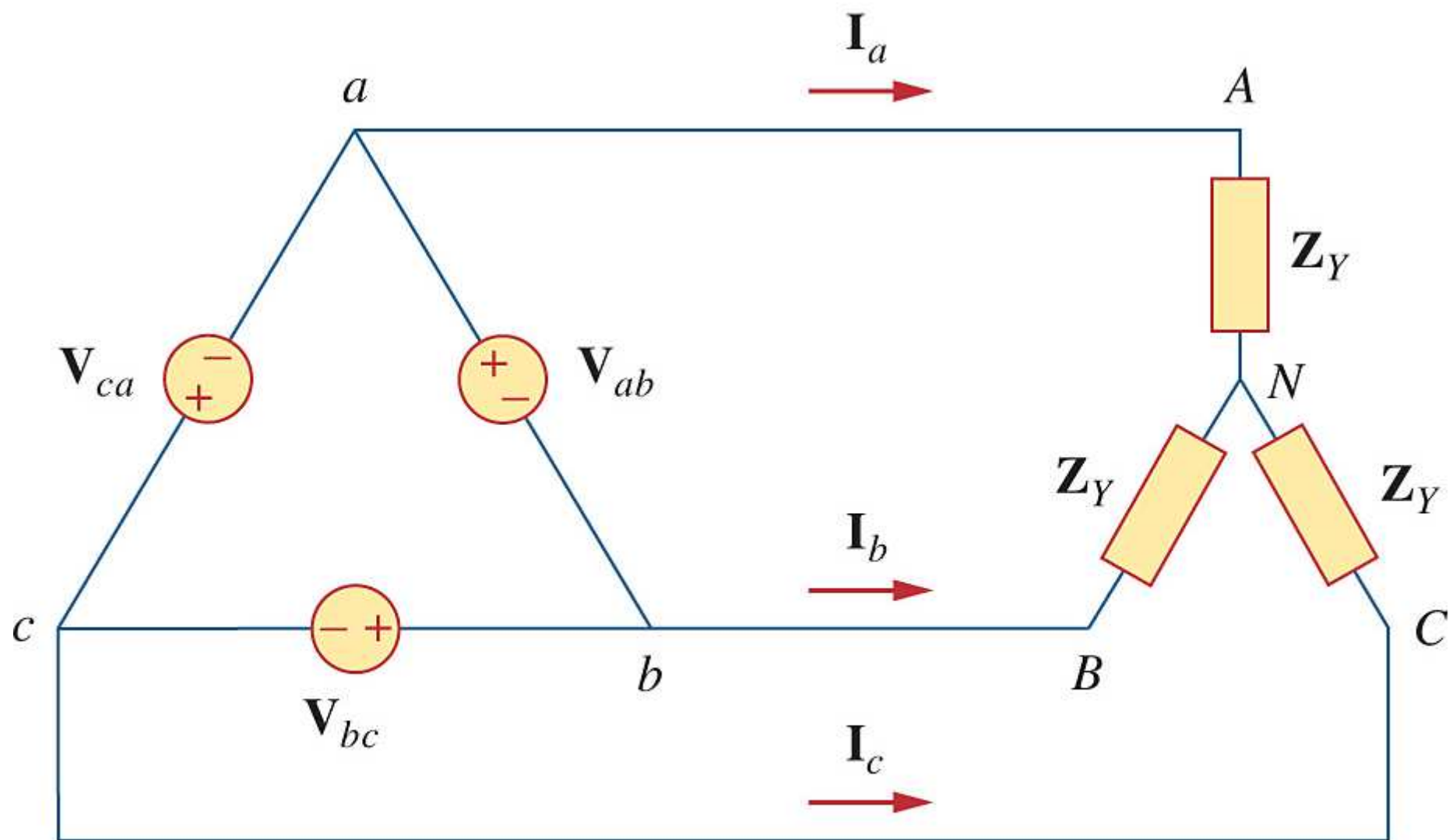


Figure 12.18 A balanced delta-wye connection.

Assume that

$$\tilde{V}_{ab} = V_p \angle 0^\circ$$

$$\tilde{V}_{bc} = V_p \angle -120^\circ$$

$$\tilde{V}_{ca} = V_p \angle +120^\circ$$

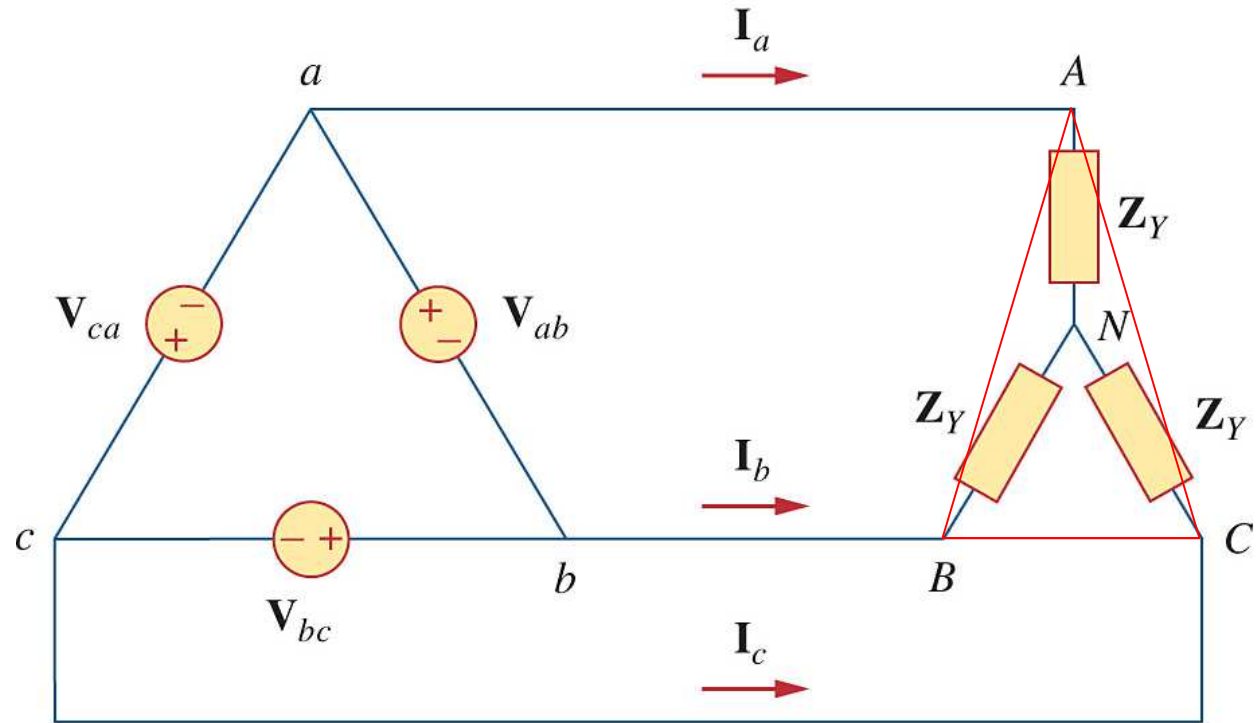


Figure 12.18 A balanced delta-wye connection.

Replace the Y-connected load with its equivalent Δ -connected load and recall that for a Δ -connected load,

$$\tilde{I}_a = \tilde{I}_{AB} \sqrt{3} \angle -30^\circ$$

$$\tilde{I}_a = \tilde{I}_{AB} \sqrt{3} \angle -30^\circ = \frac{\tilde{V}_{AB}}{Z_\Delta} \sqrt{3} \angle -30^\circ$$

$$\begin{aligned} Z_\Delta &= 3Z_Y \\ Z_Y &= Z_\Delta/3 \end{aligned}$$

$$= \frac{\tilde{V}_{ab}}{3Z_Y} \sqrt{3} \angle -30^\circ = \frac{\tilde{V}_{ab}}{\sqrt{3}Z_Y} \angle -30^\circ$$

$$\tilde{I}_b = \frac{\tilde{V}_{bc}}{\sqrt{3}Z_Y} \angle -30^\circ = \tilde{I}_a \angle -120^\circ$$

$$\tilde{I}_c = \frac{\tilde{V}_{ca}}{\sqrt{3}Z_Y} \angle -30^\circ = \tilde{I}_a \angle +120^\circ$$

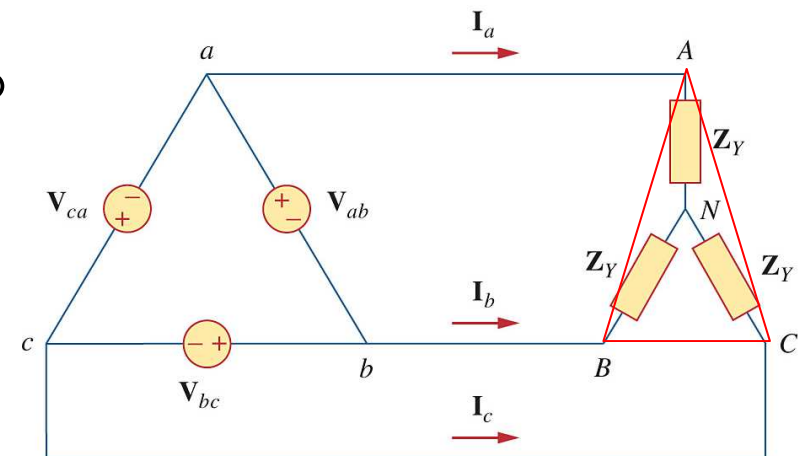


Figure 12.18 A balanced delta-wye connection.

Summary of balanced Δ -Y

If the source (phase voltages) are in abc sequence,

- Voltages:

Line voltages and phase voltages are same, and are in abc sequence

- Currents:

Line currents and phase currents are same, and are in abc sequence

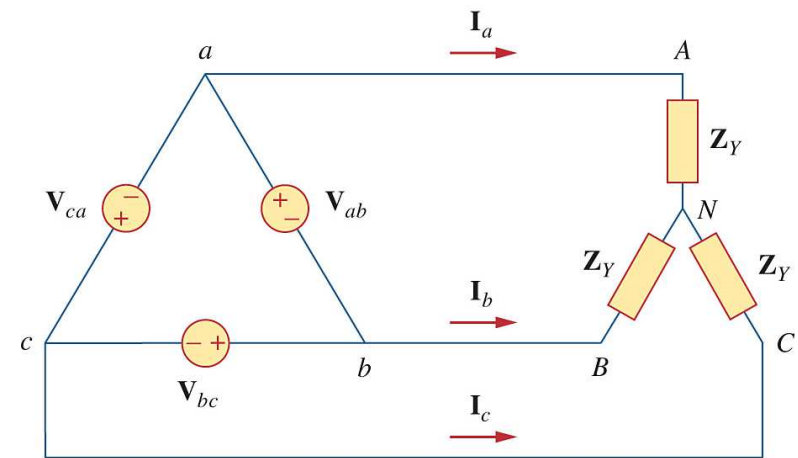


Figure 12.18 A balanced delta-wye connection.

12.7 Power in a Balanced System

We begin by examining the instantaneous power absorbed by the load. For a Y-connected load, the phase voltages are

$$v_{AN} = \sqrt{2}V_p \cos \omega t$$

$$v_{BN} = \sqrt{2}V_p \cos(\omega t - 120^\circ)$$

$$v_{CN} = \sqrt{2}V_p \cos(\omega t + 120^\circ)$$

V_p is the rms value

→ Peak value: $\sqrt{2}V_p$

If $Z_Y = Z \angle \theta$, the phase currents are

$$i_a = \sqrt{2}I_p \cos(\omega t - \theta)$$

$$i_b = \sqrt{2}I_p \cos(\omega t - \theta - 120^\circ)$$

$$i_c = \sqrt{2}I_p \cos(\omega t - \theta + 120^\circ)$$

$$I = V/Z$$

$$\rightarrow \angle I = \angle V - \angle Z$$

The total instantaneous power is

$$p = p_a + p_b + p_c = v_{AN}i_a + v_{BN}i_b + v_{CN}i_c$$

$$\begin{aligned}
&= 2V_p I_p [\cos \omega t \cos(\omega t - \theta) \\
&\quad + \cos(\omega t - 120^\circ) \cos(\omega t - \theta - 120^\circ) \\
&\quad + \cos(\omega t + 120^\circ) \cos(\omega t - \theta + 120^\circ)] \\
&= 2V_p I_p \left\{ \frac{\cos \theta + \cos(2\omega t - \theta)}{2} \right. \\
&\quad + \frac{\cos \theta + \cos(2\omega t - \theta - 240^\circ)}{2} \\
&\quad \left. + \frac{\cos \theta + \cos(2\omega t - \theta + 240^\circ)}{2} \right] \\
&= 3V_p I_p \cos \theta
\end{aligned}$$

$$p(t) = 3V_p I_p \cos(\theta)$$

Thus the total instantaneous power in a balanced three-phase system is constant – it does not change with time as the instantaneous power of each phase does. This result is true whether the load is Y- or Δ -connected. This is one important reason for using a three-phase system to generate and distribute power.

The advantage over a single-phase AC system:
constant $p(t)$

Since the total instantaneous power is independent of time, the average power per phase P_p for the Y- or Δ -connected load is $p / 3$, or

$$P_p = V_p I_p \cos \theta$$

Recall:

$$Z_Y = Z \angle \theta$$

θ is the power factor angle

and the reactive power per phase is

$$Q_p = V_p I_p \sin \theta$$

The apparent power per phase is

$$|S_p| = V_p I_p$$

The complex power per phase is

$$S_p = P_p + jQ_p = \tilde{V}_p \tilde{I}_p^*$$

The total average power is

$$P = P_a + P_b + P_c = 3P_p$$

By AC power conservation

$$= 3V_p I_p \cos \theta$$

and Y-connected source

For a Y-connected load, $I_L = I_p$ but $V_L = \sqrt{3}V_p$, whereas for a Δ -connected load, $I_L = \sqrt{3}I_p$ but $V_L = V_p$. Thus,

and Δ -connected source

$$P = 3V_p I_p \cos \theta = \sqrt{3}V_L I_L \cos \theta$$

V_p : phase voltage
 I_p : phase current

V_L : line voltage
 I_L : line current

The total reactive power is

$$Q = 3Q_p = 3V_p I_p \sin \theta = \sqrt{3} V_L I_L \sin \theta$$

The total complex power is

$$S = 3S_p = 3\tilde{V}_p \tilde{I}_p^* = 3I_p^2 Z_p = \frac{3V_p^2}{Z_p^*}$$

where Z_p is the load impedance per phase.

$$S = P + jQ = 3V_p I_p \cos \theta + j3V_p I_p \sin \theta$$

$$= \sqrt{3}V_L I_L \cos \theta + j\sqrt{3}V_L I_L \sin \theta$$

Remember that V_p , I_p , V_L , and I_L are all rms values and that θ is the angle of the load impedance or the angle between the phase voltage and the phase current.

Recall:

$$Z_Y = Z \angle \theta, \quad \theta = \angle V_p - \angle I_p$$

θ is the power factor angle

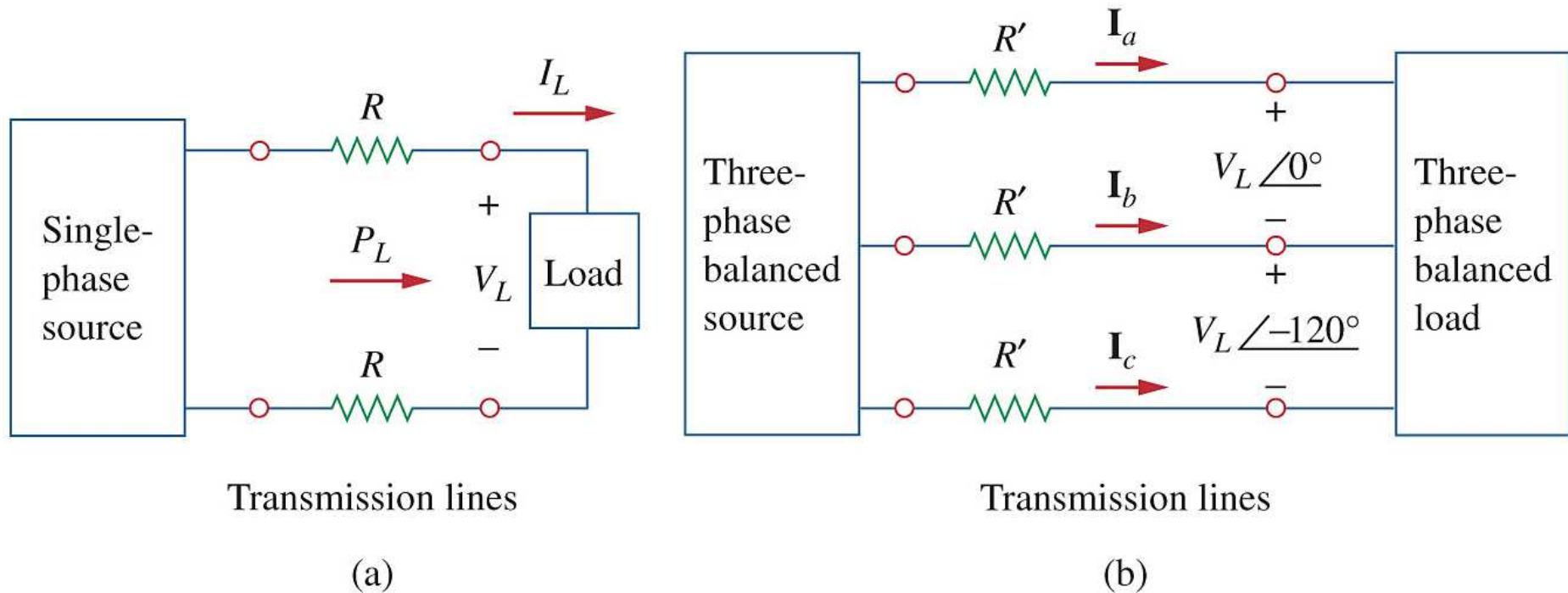


Figure 12.21 Comparing the power loss in (a) single-phase system, and (b) a three-phase system.

Conditions in the comparison:

1. Same line voltages V_L in the two cases.
2. To deliver the same total power P_L
3. The same power loss P_{loss} is tolerated

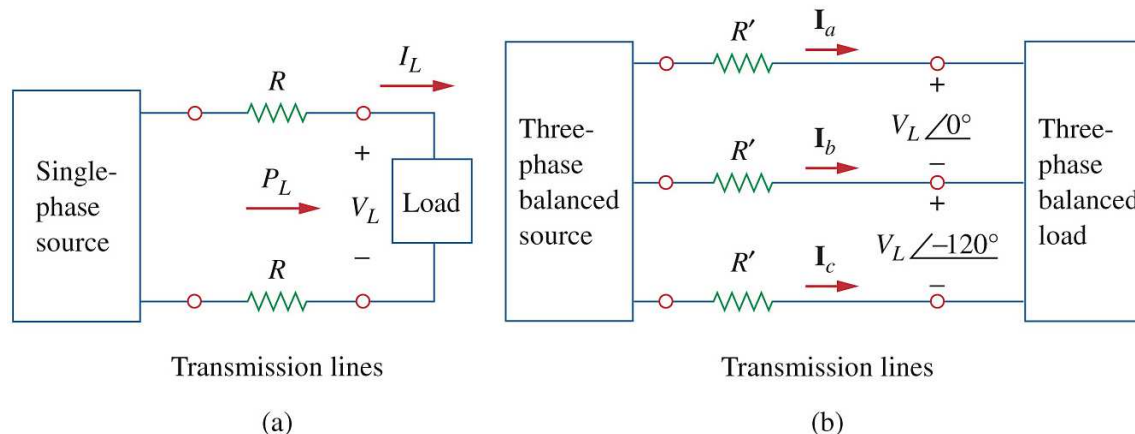
Consider Fig. 12.21. For the single-phase two-wire system, $P_L = V_L I_L$, the power loss in the two wires is

2 wires

$$P_{loss} = 2I_L^2 R = 2 \left(\frac{P_L}{V_L} \right)^2 R$$

R: the total resistance of one transmission line

For the three-phase three-wire system, $P_L = \sqrt{3} V_L I'_L$, the power loss in the three wires is



' means case 2, not derivative

I'_L : line current
 R' : line resistance

Figure 12.21 Comparing the power loss in (a) single-phase system, and (b) a three-phase system.

3 wires

$$P'_{loss} = 3I_L'^2 R' = 3 \left(\frac{P_L}{\sqrt{3}V_L} \right)^2 R' = \left(\frac{P_L}{V_L} \right)^2 R'$$

The equations show that for the same total power delivered P_L and the same line voltage V_L ,

$$\frac{P_{loss}}{P'_{loss}} = \frac{2R}{R'} = \frac{2\rho l / (\pi r^2)}{\rho l / (\pi r'^2)} = \frac{2r'^2}{r^2}$$

ρ : resistivity

l : length of transmission line

r : radius of the transmission line

If the same power loss is tolerated in both systems, then $r^2 = 2r'^2$, so

$$\frac{\text{Material for single-phase}}{\text{Material for three-phase}} = \frac{2(\pi r^2 l)}{3(\pi r'^2 l)} = \frac{2r^2}{3r'^2} = \frac{4}{3}$$

Two wires

Three wires

This is the second major advantage of three-phase systems for power distribution.

The advantage over a single-phase AC system:
Less materials for transmission lines

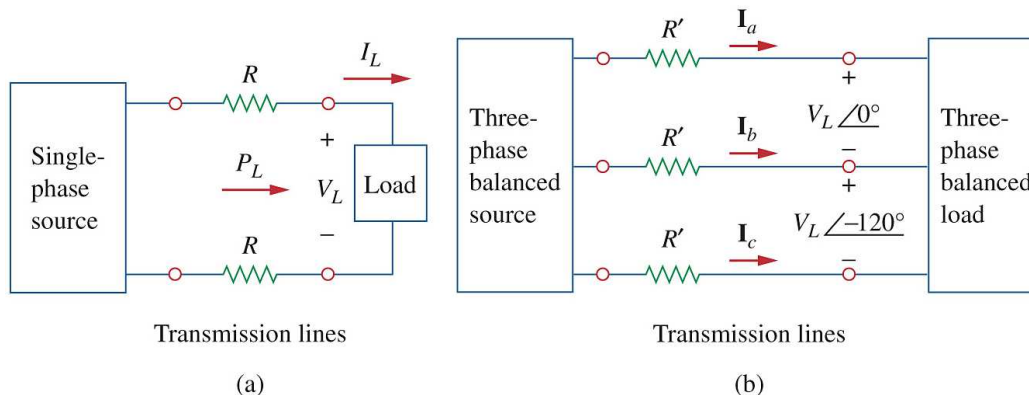


Figure 12.21 Comparing the power loss in (a) single-phase system, and (b) a three-phase system.

Summary of the advantages of 3- ϕ system

1. The total instantaneous power in a balanced three-phase system is constant.
2. The material (transmission line) to deliver the same power and to tolerate the same loss needed is $\frac{3}{4}$ times less.

Example 12.8 Two balanced loads are connected to a 240-kV rms 60-Hz line, as shown in Fig. 12.22(a). Load 1 draws 30 kW at a power factor of 0.6 lagging, while load 2 draws 45 kVAR at a power factor of 0.8 lagging. Assuming the *abc* sequence,

Line voltage

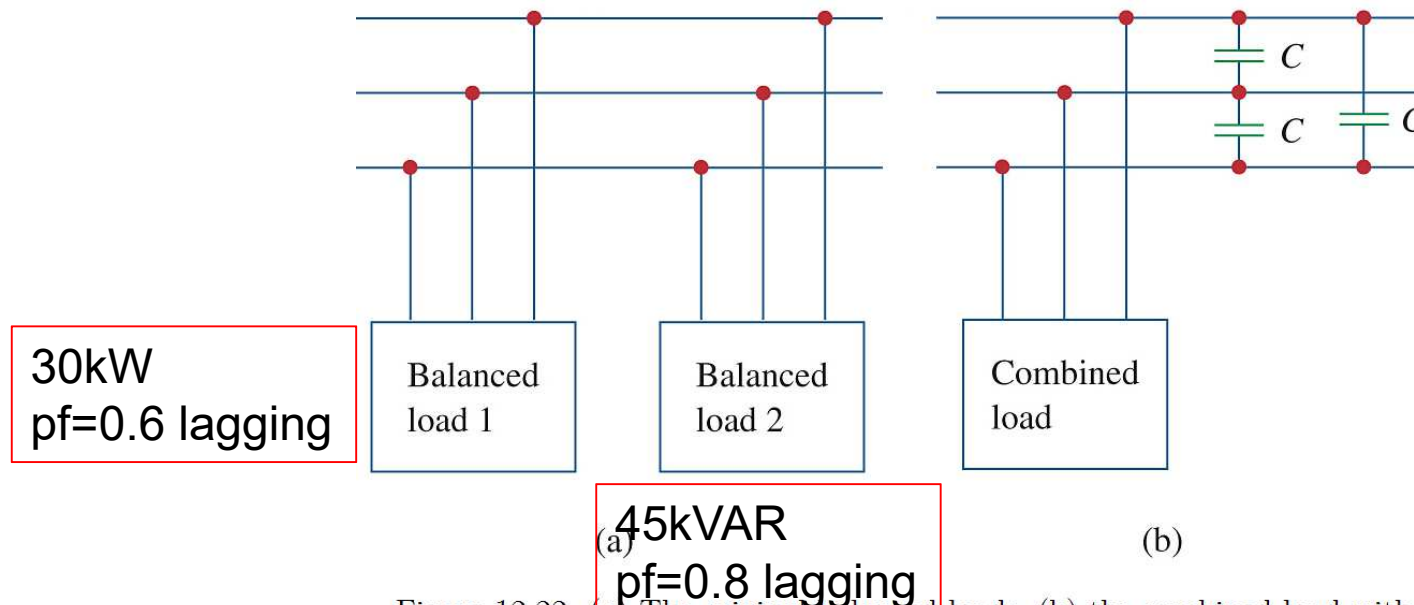


Figure 12.22 (a) The original balanced loads, (b) the combined load with improved power factor.

determine: (a) the complex, real, and reactive powers absorbed by the combined load, (b) the line current, and (c) the kVAR rating of the three capacitors Δ -connected in parallel with the load that will raise the power factor to 0.9 lagging and the capacitance of each capacitor.

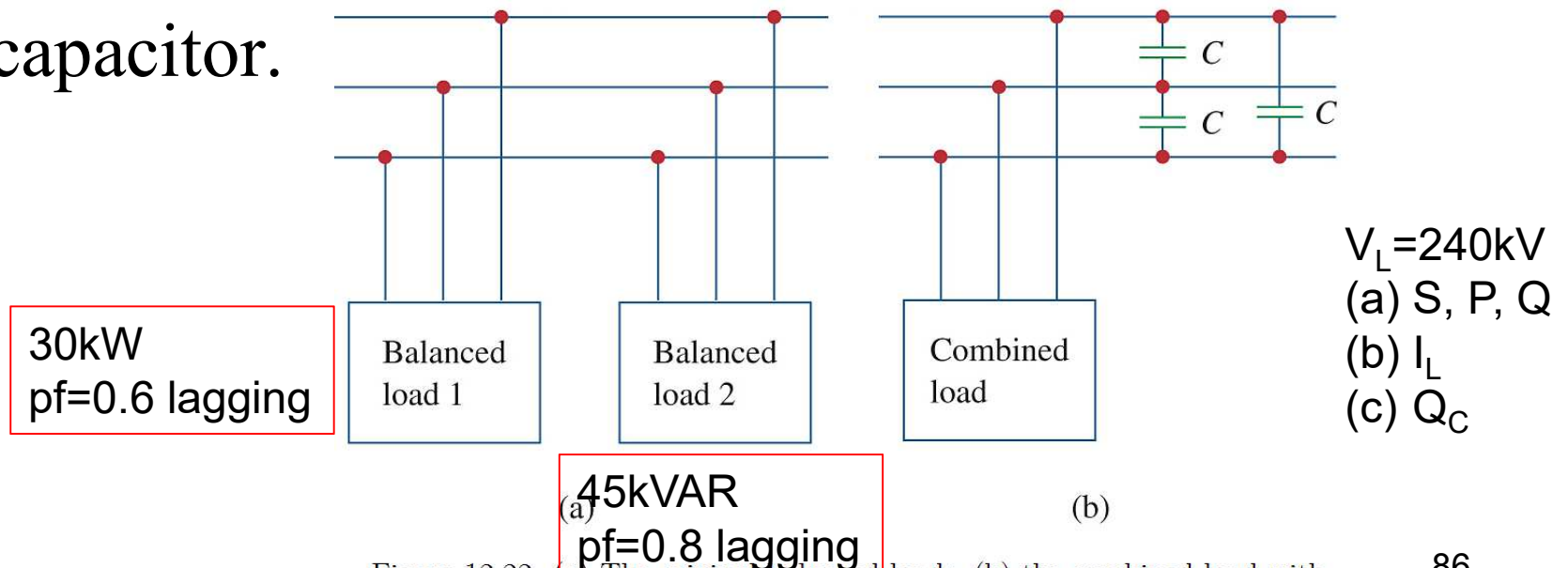


Figure 12.22 (a) The original balanced loads, (b) the combined load with improved power factor.

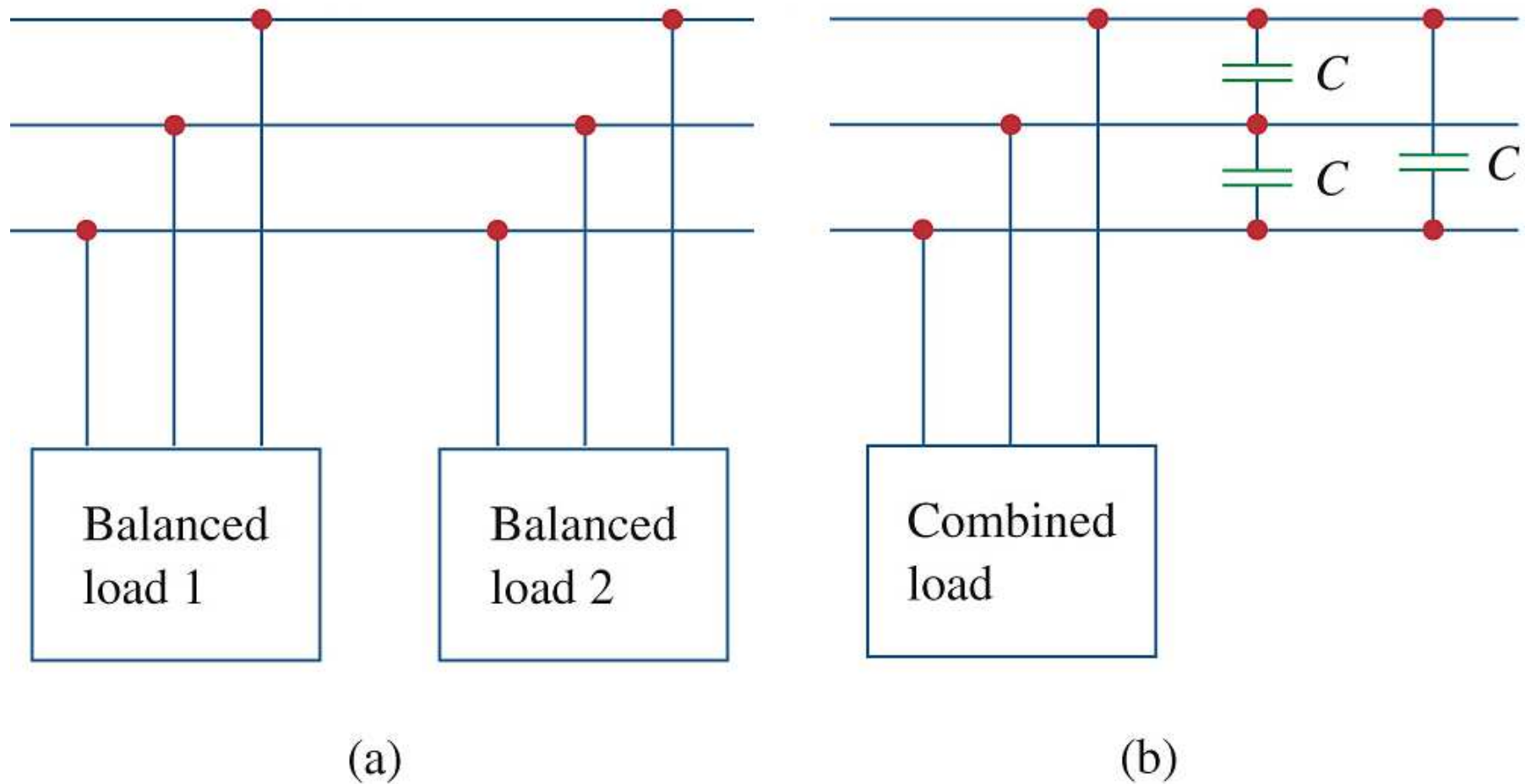


Figure 12.22 (a) The original balanced loads, (b) the combined load with improved power factor.

Solution :

$V_L = 240\text{kV}$
 (a) S, P, Q
 (b) I_L
 (c) Q_C

$$(a) \cos \theta_1 = 0.6 \Rightarrow \sin \theta_1 = 0.8$$

$$Q_1 = P_1 \tan \theta_1 = 30 \times \frac{0.8}{0.6} = 40 \text{ (kVAR)}$$

$$S_1 = P_1 + jQ_1 = 30 + j40 \text{ (kVA)}$$

$$\cos \theta_2 = 0.8 \Rightarrow \sin \theta_2 = 0.6$$

$$P_2 = Q_2 / \tan \theta_2 = 45 / (0.6 / 0.8) = 60 \text{ (kW)}$$

$$S_2 = P_2 + jQ_2 = 60 + j45 \text{ (kVA)}$$

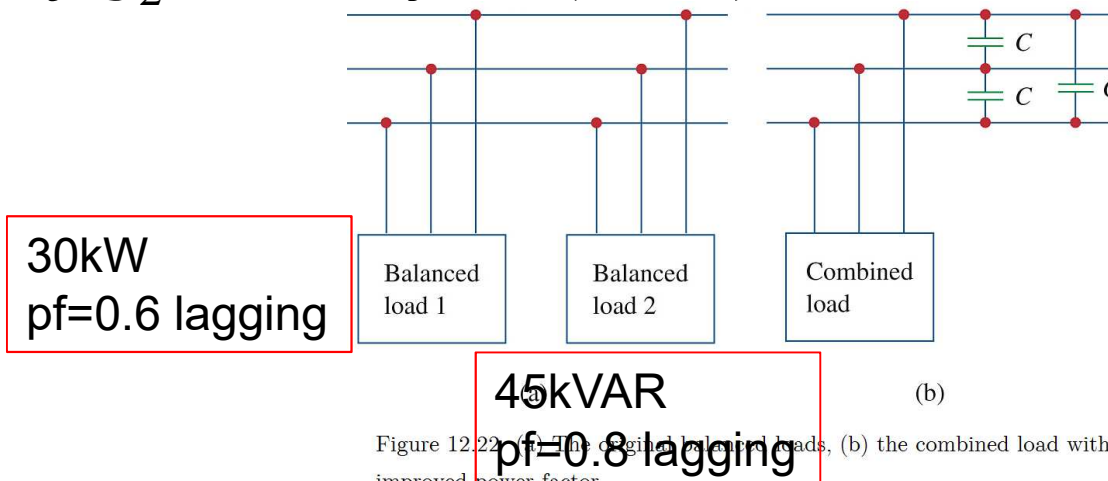


Figure 12.22 (a) the original balanced loads, (b) the combined load with improved power factor

$$S = S_1 + S_2 = (30 + j40) + (60 + j45)$$

$$= 90 + j85 \text{ (kVA)}$$

$$P = 90 \text{ kW}, Q = 85 \text{ kVA}$$

$$(b) \theta = \tan^{-1} \left(\frac{85}{90} \right) \approx 43.36^\circ$$

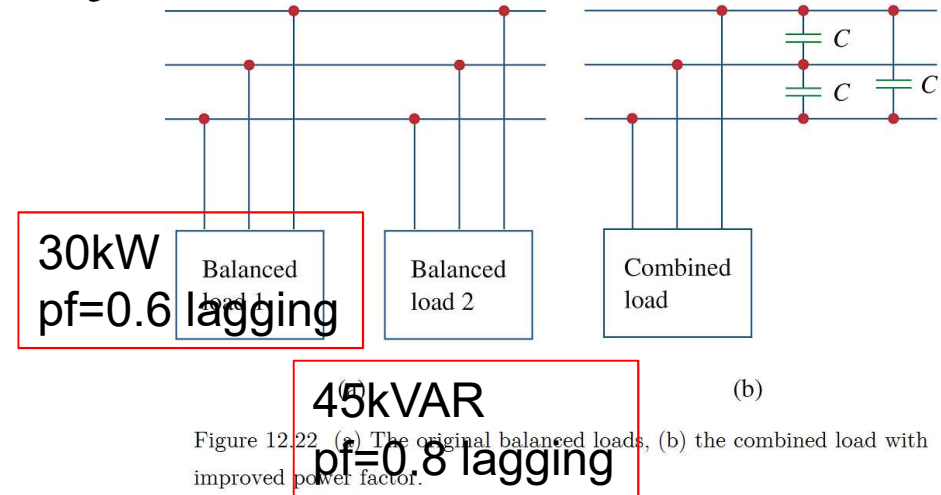


Figure 12.22. (a) The original balanced loads, (b) the combined load with improved power factor.

$V_L = 240 \text{ kV}$
 (a) S, P, Q
 (b) I_L
 (c) Q_C

$$P = \sqrt{3} V_L I_L \cos \theta \Rightarrow I_L = \frac{P}{\sqrt{3} V_L \cos \theta}$$

$$I_L = \frac{90 \times 10^3}{\sqrt{3} \times 240 \times 10^3 \times \cos 43.36^\circ} \approx 0.2978 \text{ (A)}$$

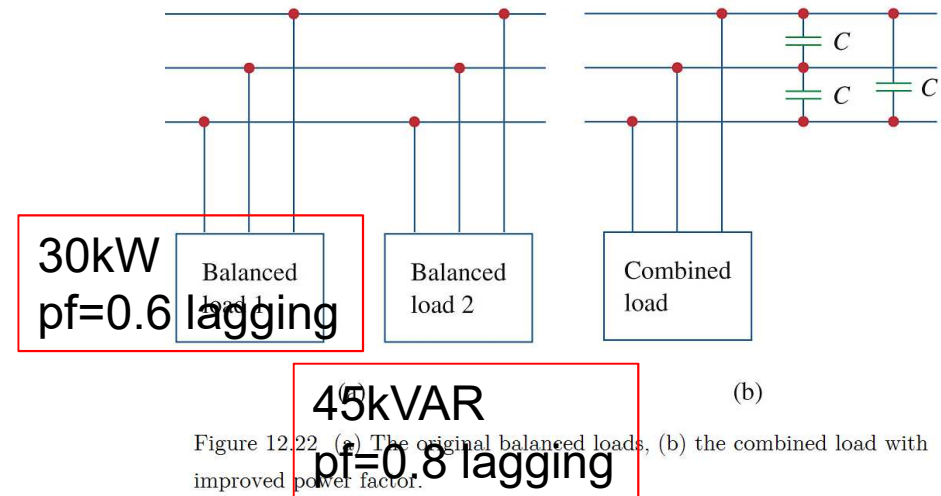


Figure 12.22. (a) The original balanced loads, (b) the combined load with improved power factor.

$V_L = 240\text{kV}$
 (a) S, P, Q
 (b) I_L
 (c) Q_C

$$(c) \theta_{old} = \tan^{-1} \left(\frac{85}{90} \right) \approx 43.36^\circ$$

$$\theta_{new} = \cos^{-1} 0.9 \approx 25.84^\circ$$

$$\begin{aligned} |Q_C| &= P(\tan \theta_{old} - \tan \theta_{new}) \\ &= 90 \times (\tan 43.36^\circ - \tan 25.84^\circ) \\ &\approx 41.40 \text{ (kVAR)} \end{aligned}$$

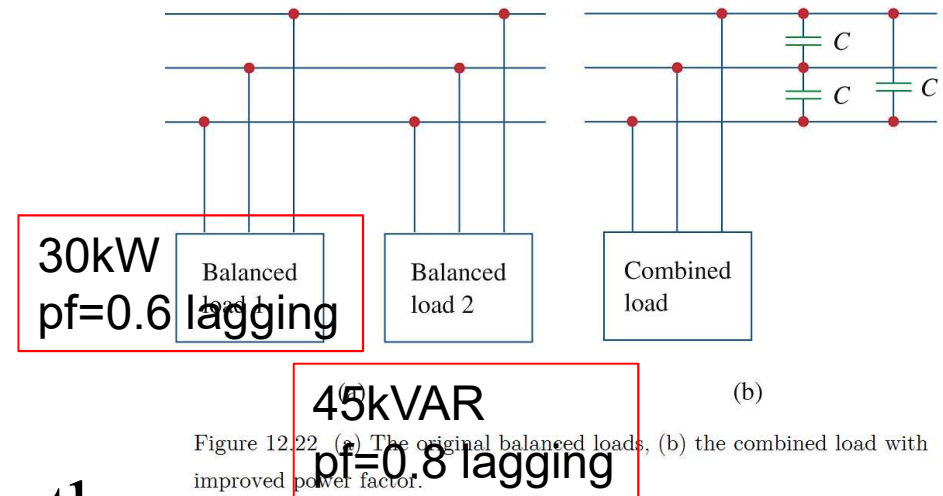


Figure 12.22. (a) The original balanced loads, (b) the combined load with improved power factor.

$V_L = 240\text{kV}$
 (a) S, P, Q
 (b) I_L
 (c) Q_C

This reactive power is for the three capacitors. For each capacitor,

$$|Q'_C| = |Q_C| / 3 \approx 13.80 \text{ (kVAR)}$$

$$C = \frac{|Q'_C|}{\omega V_L^2} = \frac{13.80 \times 10^3}{2\pi \times 60 \times (240 \times 10^3)^2}$$

$$\approx 6.3551 \times 10^{-10} \text{ (F)}$$

$$\approx 635.51 \text{ pF}$$

$$Q_C = I^2 X = V^2 / X$$

for purely capacitive case

12.8 Unbalanced Three-Phase Systems

An unbalanced system is caused by two possible situations: (1) the source voltages are not equal in magnitude and/or differ in phase by angles that are unequal, or (2) load impedances are unequal.

Unbalanced three-phase systems are solved by direct application of mesh and nodal analysis. Figure 12.23 shows an unbalanced system that consists of balanced source voltages and an unbalanced Y-connected load.

The formulas for a balanced source are still applicable.

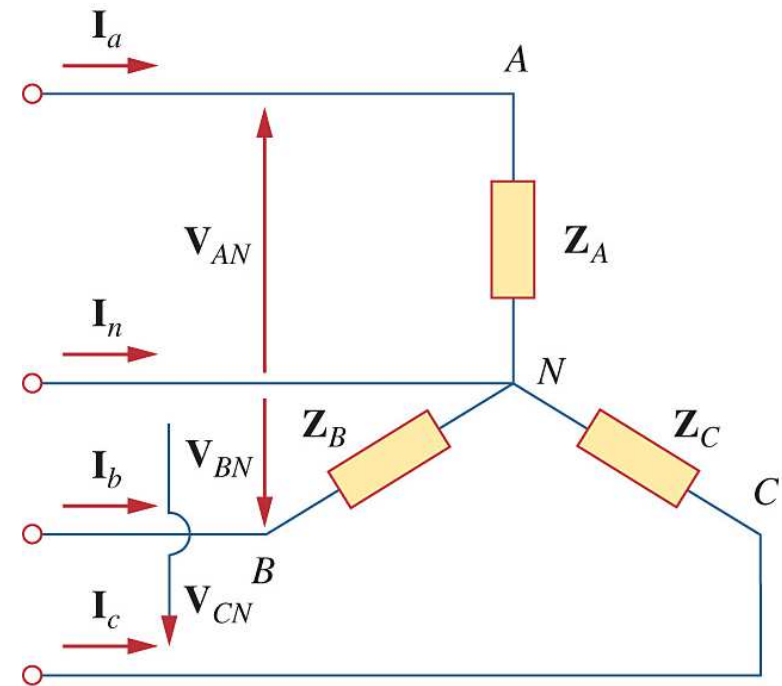


Figure 12.23 Unbalanced three-phase Y-connected load.

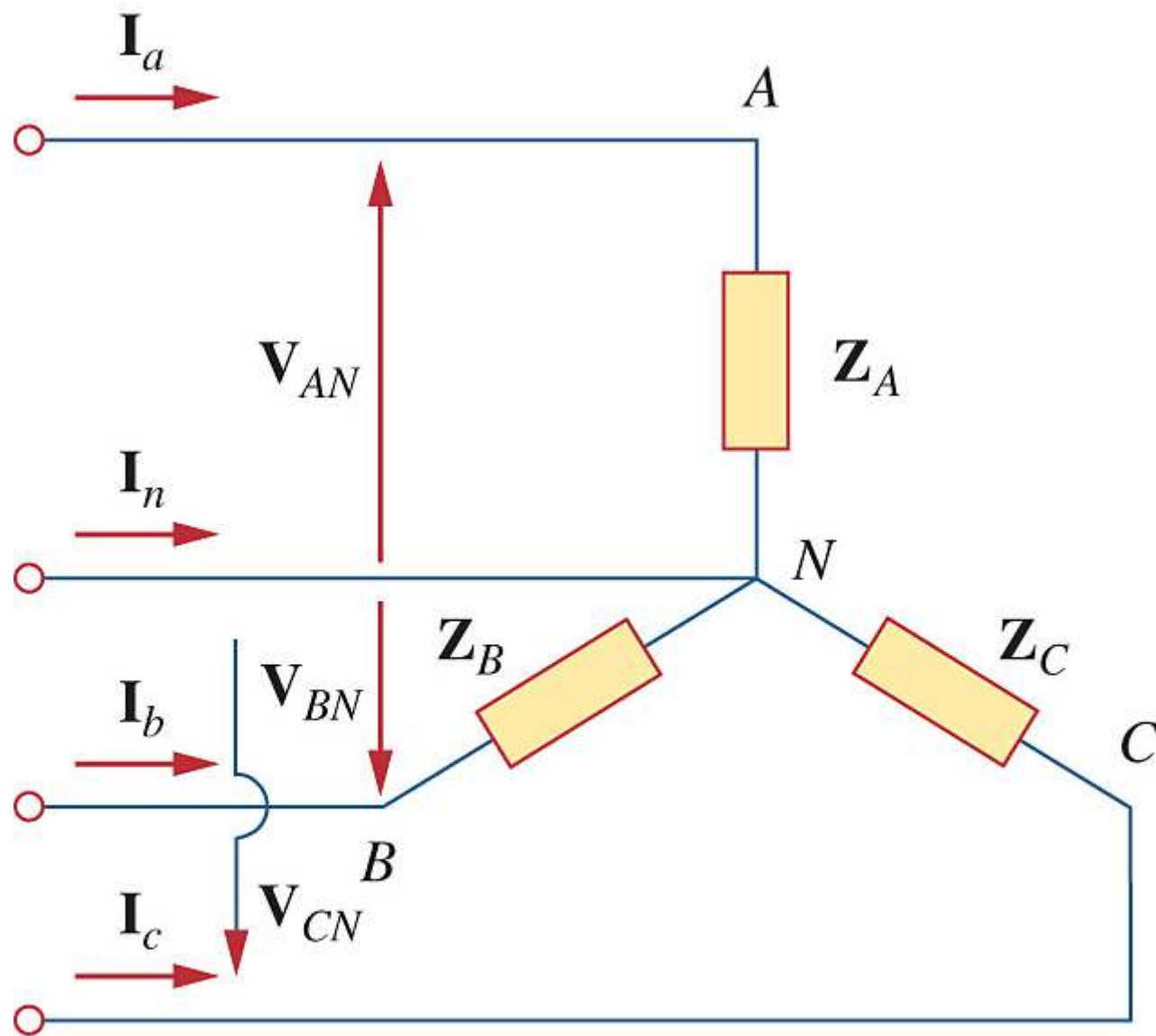


Figure 12.23 Unbalanced three-phase Y-connected load.

Example 12.9 The unbalanced Y-load of Fig. 12.23 has balanced voltages of 100 V and the *acb* sequence. Calculate the line currents and the neutral current. Take $Z_A = 15 \Omega$, $Z_B = 10 + j5 \Omega$, $Z_C = 6 - j8 \Omega$.

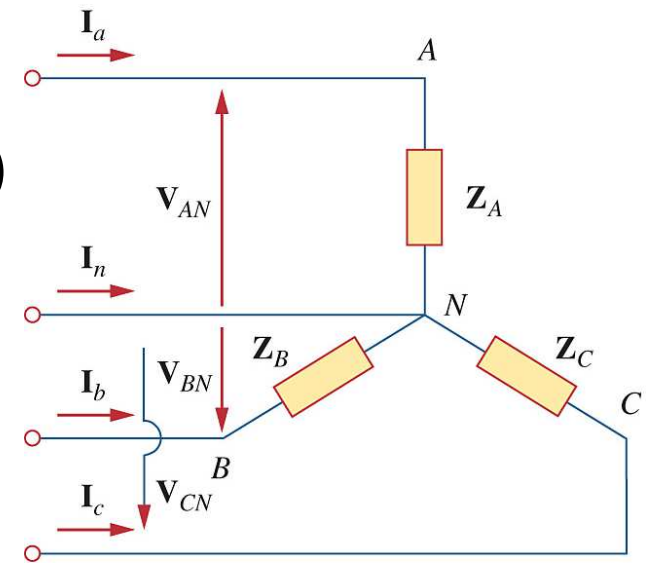
Phase voltage V_p

Balanced source
Unbalanced load

$I_L ?$
 $I_N ?$

Solution :

$$\tilde{I}_a = \frac{\tilde{V}_{AN}}{Z_A} = \frac{100 \angle 0^\circ}{15} \approx 6.6667 \angle 0^\circ \text{ (A)}$$



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Figure 12.23 Unbalanced three-phase Y-connected load.

$$\tilde{I}_b = \frac{\tilde{V}_{BN}}{Z_B} = \frac{100\angle+120^\circ}{10+j5} \approx 8.9443\angle93.43^\circ \text{ (A)}$$

$$\tilde{I}_c = \frac{\tilde{V}_{CN}}{Z_C} = \frac{100\angle-120^\circ}{6-j8} \approx 10\angle-66.87^\circ \text{ (A)}$$

$$\tilde{I}_n = -(\tilde{I}_a + \tilde{I}_b + \tilde{I}_c)$$

$$= -(6.6667\angle0^\circ + 8.9443\angle93.43^\circ + 10\angle-66.87^\circ)$$

$$\approx -(6.6667 - 0.5351 + j8.9283 + 3.9282 - j9.1962)$$

$$= -10.0598 + j0.2679$$

$$\approx 10.0634\angle178.47^\circ \text{ (A)}$$

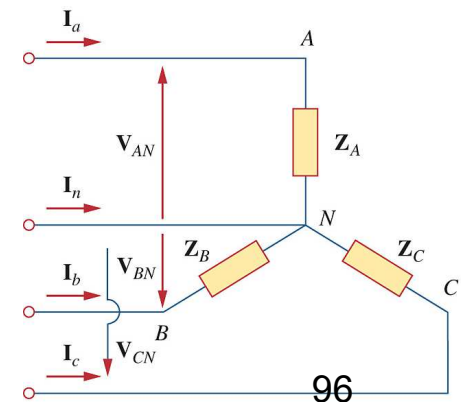


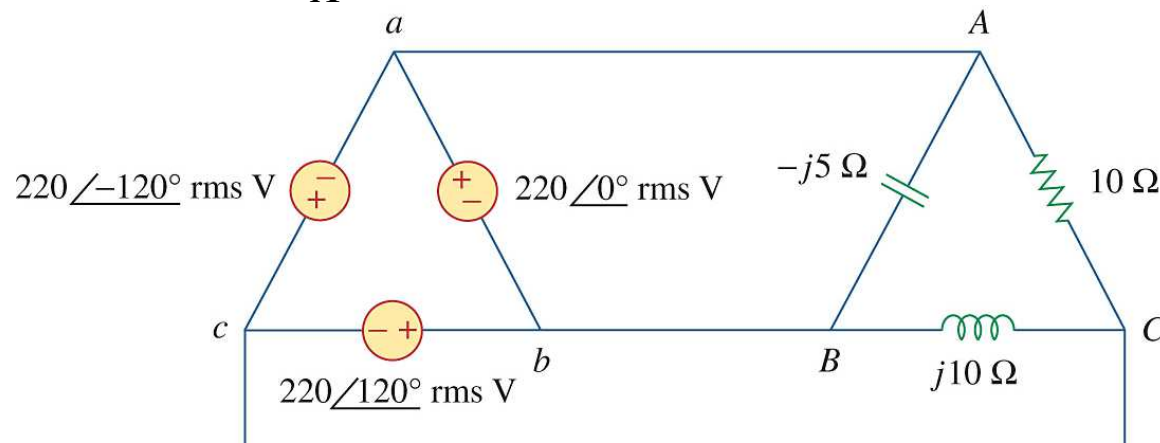
Figure 12.23 Unbalanced three-phase Y-connected load.

Practice Problem 12.10 Find the line currents in the unbalanced three-phase circuit of Fig. 12.26 and the real power absorbed by the load.

$I_L ?$
 $P ?$

Solution :

$$\tilde{I}_{AB} = \frac{\tilde{V}_{AB}}{Z_A} = \frac{220\angle 0^\circ}{-j5} = 44\angle 90^\circ \text{ (A)}$$



Balanced source
Unbalanced load

Figure 12.26

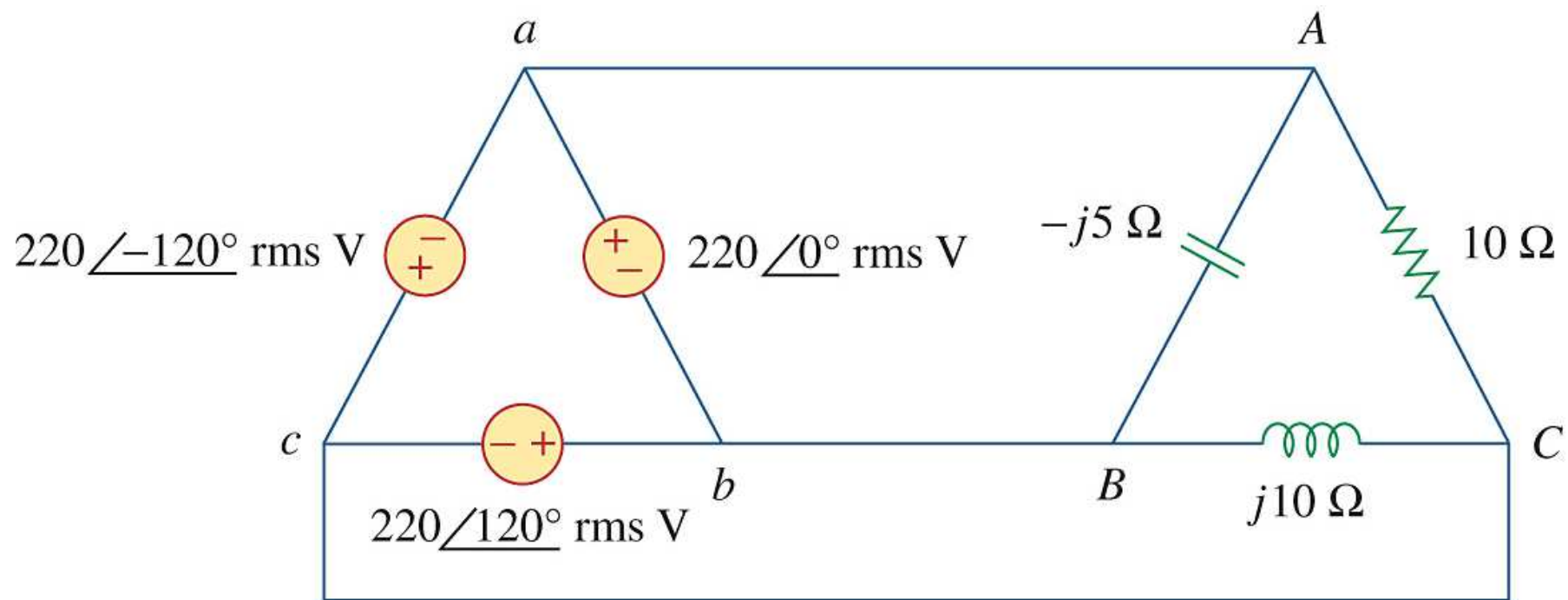


Figure 12.26

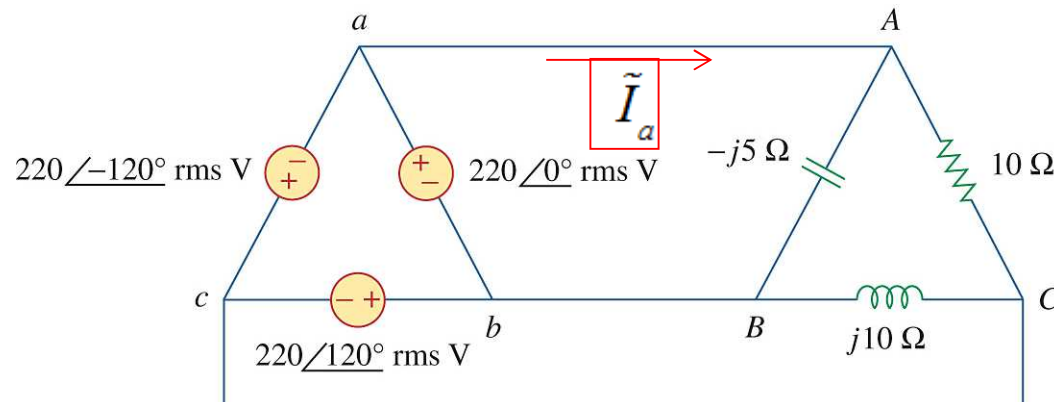
$$\tilde{I}_{BC} = \frac{\tilde{V}_{BC}}{Z_B} = \frac{220\angle 120^\circ}{j10} = 22\angle 30^\circ \text{ (A)}$$

$$\tilde{I}_{CA} = \frac{\tilde{V}_{CA}}{Z_C} = \frac{220\angle -120^\circ}{10} = 22\angle -120^\circ \text{ (A)}$$

$$\tilde{I}_a = \tilde{I}_{AB} - \tilde{I}_{CA} = 44\angle 90^\circ - 22\angle -120^\circ$$

$$= j44 - (-11 - j19.0526)$$

$$= 11 + j63.05266 \approx 64.0049\angle 80.10^\circ \text{ (A)}$$



$I_L ?$
 $P ?$

Balanced source
Unbalanced load

Figure 12.26

$$\tilde{I}_b = \tilde{I}_{BC} - \tilde{I}_{AB} = 22\angle 30^\circ - 44\angle 90^\circ$$

$$= (19.0526 + j11) - j44$$

$$= 19.0526 - j33 \approx 38.1051\angle -60^\circ \text{ (A)}$$

$$\tilde{I}_c = \tilde{I}_{CA} - \tilde{I}_{BC} = 22\angle -120^\circ - 22\angle 30^\circ$$

$$= (-11 - j19.0526) - (19.0526 + j11)$$

$$= -30.0526 - j30.0526 \approx 42.5008\angle -135^\circ \text{ (A)}$$

$$P_L = P_{CA} = I_{CA}^2 R = 22^2 \times 10 = 4,840 \text{ (W)}$$

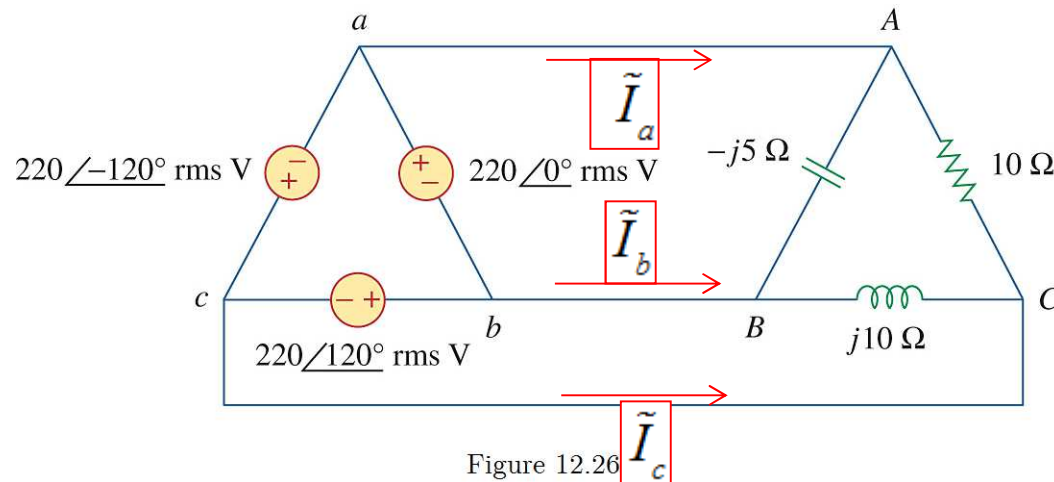


Figure 12.26

$I_L ?$
 $P ?$

Balanced source
Unbalanced load

12.10 Applications

Three - Phase Power Measurement The wattmeter is the instrument for measuring the average power. P

The traditional analog wattmeter is an electrodynamic instrument. The device consists of two coils. One coil, called the *current coil*, is stationary and carries a current proportional to the load current.

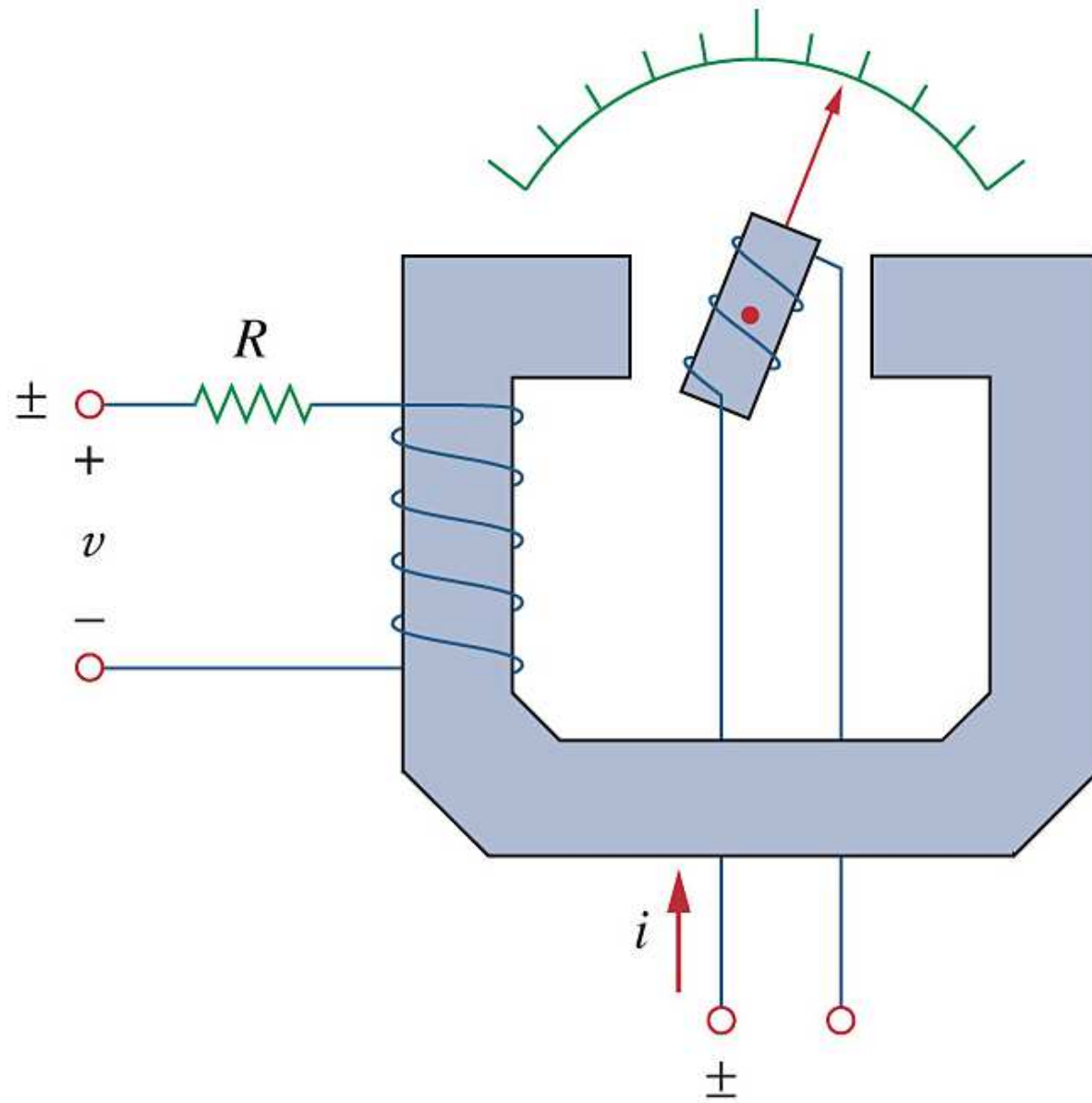


Figure 11.30 A wattmeter.

The second coil, called the *potential coil*, is movable and carries a current proportional to the load voltage. The average deflection of the pointer (or needle) attached to the movable coil is proportional to the average value of the product $v(t)i(t)$. The direction in which the pointer deflects depends on the instantaneous polarity of $v(t)$ and the instantaneous direction of $i(t)$. Therefore

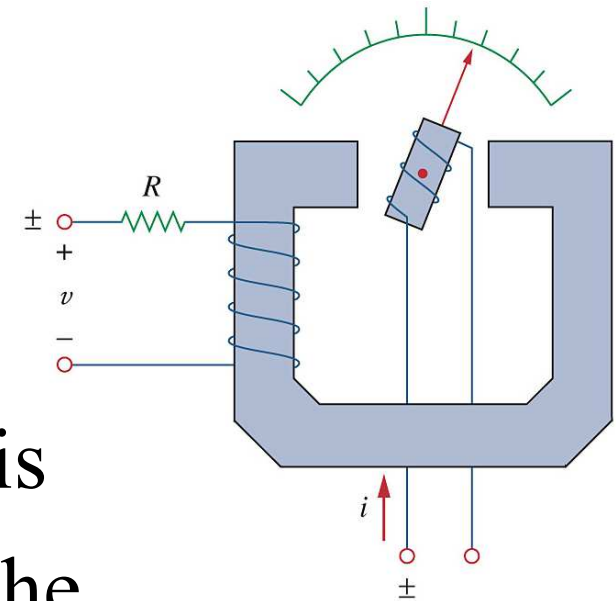


Figure 11.30 A wattmeter.

i.e., P

each coil has one terminal marked \pm . The pointer deflects upscale when⁽¹⁾ the \pm terminal of the current coil is toward the source, while⁽²⁾ the \pm terminal of the potential coil is connected to the same line as the current coil. Reversing both coil connections still results in upscale deflection. However, reversing one coil and not the other results in downscale deflection and no wattmeter reading.

$$vi = (-v)(-i)$$

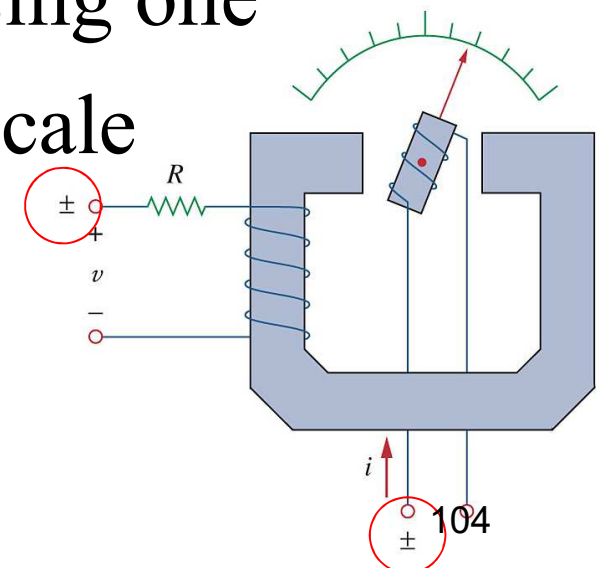


Figure 11.30 A wattmeter.

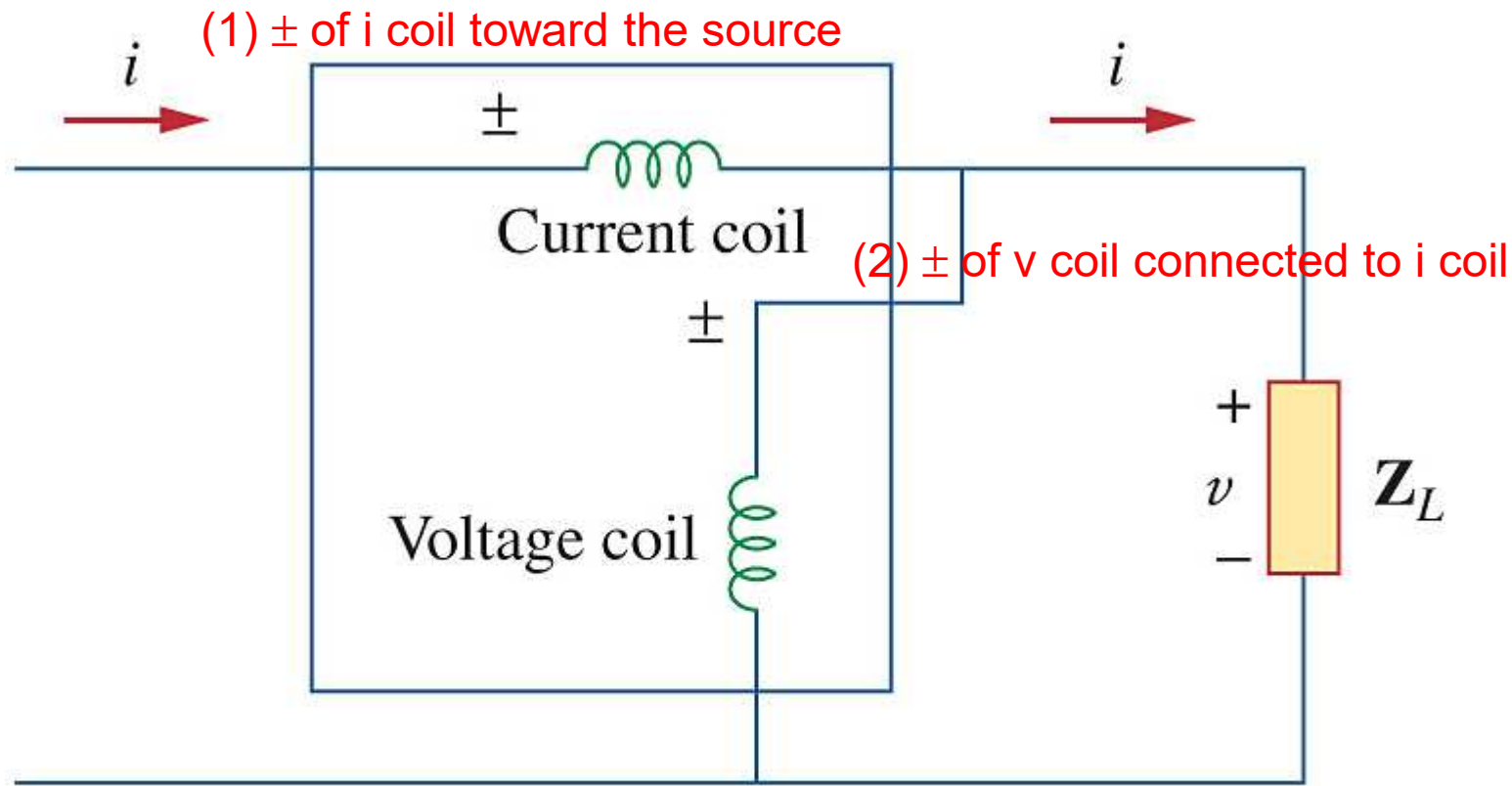


Figure 11.31 The wattmeter connected to the load

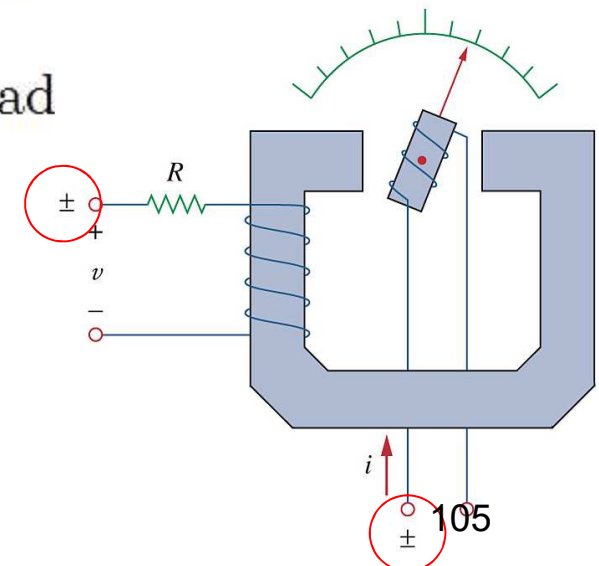


Figure 11.30 A wattmeter.

A single wattmeter can also measure the average power in a three-phase system that is balanced, so that $P_1 = P_2 = P_3$; the total power is three times the reading of that one wattmeter.

$$P_T = 3P_1$$

However, two or three wattmeters are necessary to measure power if the system is unbalanced.

The three-wattmeter method
Actually, 2 is sufficient. (shown later)

The three-wattmeter method, shown in Fig. 12.33, will work regardless of whether the load is balanced or unbalanced, wye- or delta-connected. The total average power is the algebraic sum of the three wattmeter readings,

$$P_T = P_1 + P_2 + P_3$$

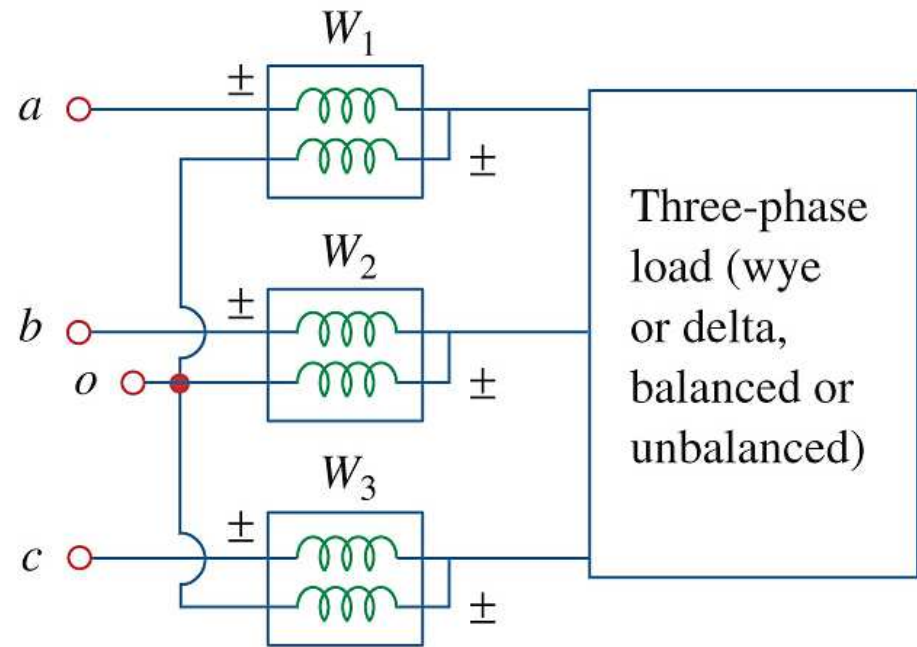


Figure 12.33 Three-wattmeter method for measuring three-phase power.

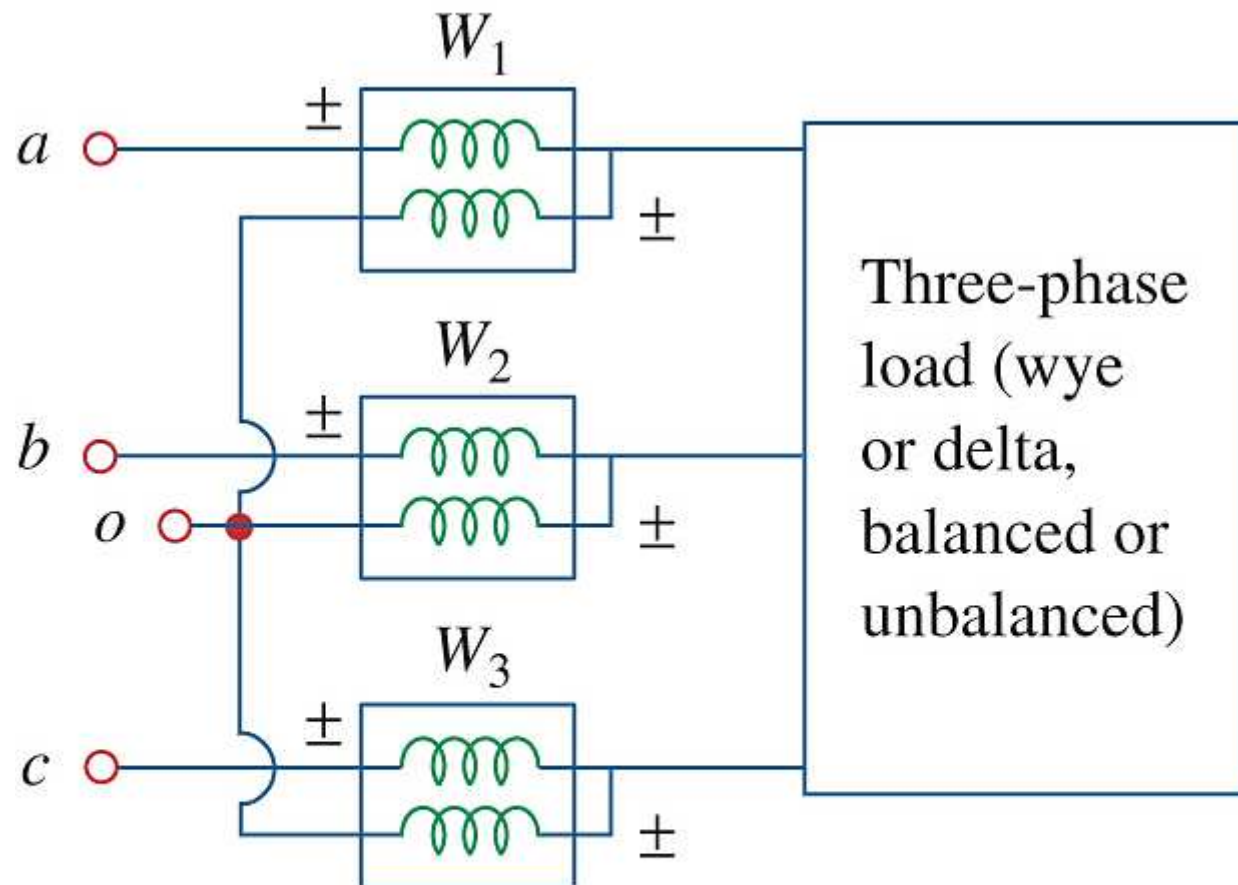


Figure 12.33 Three-wattmeter method for measuring three-phase power.

where P_1 , P_2 , and P_3 correspond to the readings of wattmeters W_1 , W_2 , and W_3 , respectively. Notice that the reference point o is selected arbitrarily. If the load is wye-connected, point o can be connected to the neutral point n . For a delta-connected load, point o can be connected to any point.

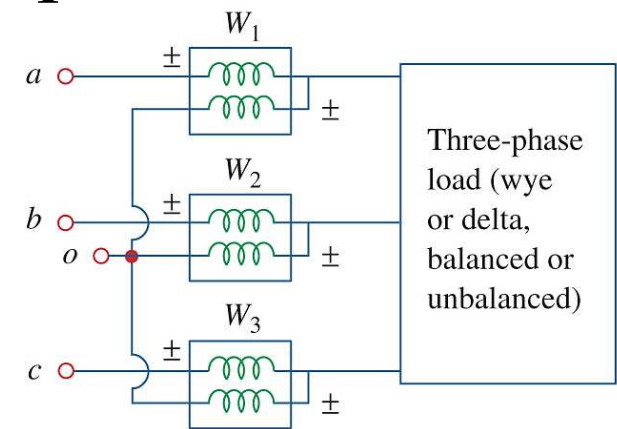
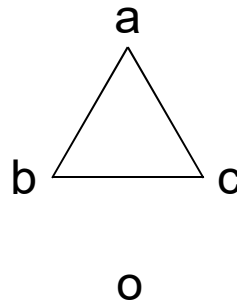
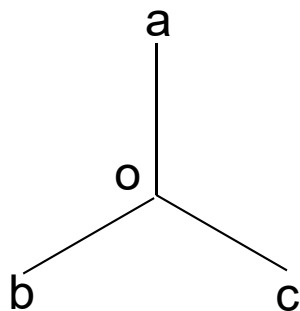


Figure 12.33 Three-wattmeter method for measuring three-phase power.

If point o is connected to point b , for example, the potential coil in wattmeter W_2 reads zero and $P_2 = 0$, indicating that wattmeter W_2 is not necessary. Thus, two wattmeters are sufficient to measure the total power.

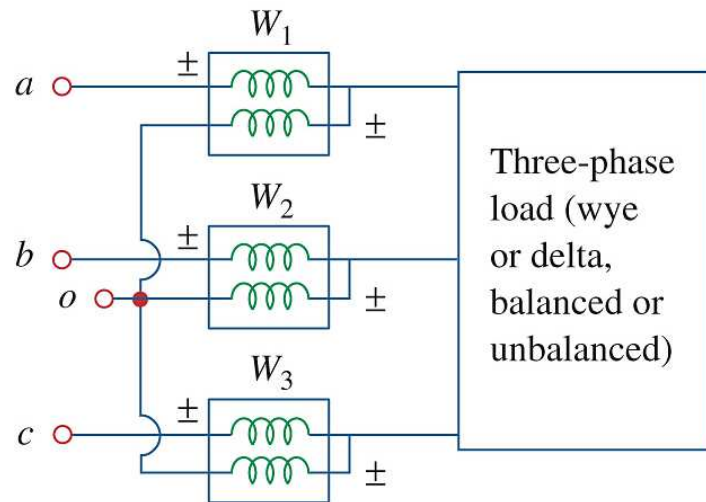


Figure 12.33 Three-wattmeter method for measuring three-phase power.

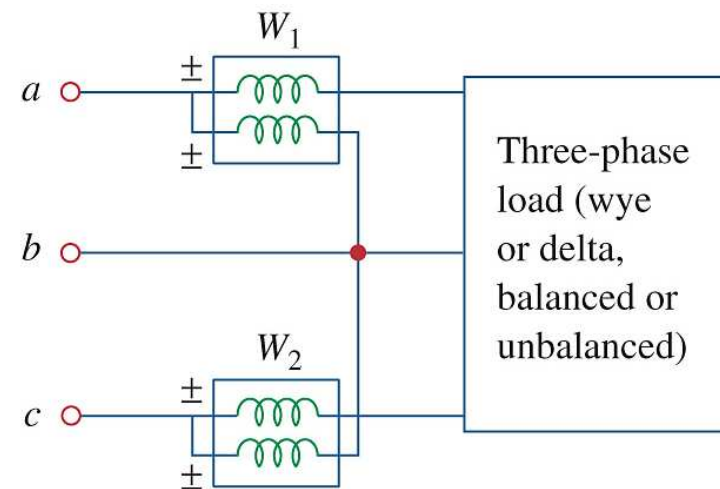
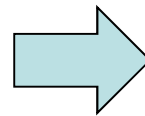


Figure 12.34 Two-wattmeter method for measuring three-phase power.

The two-wattmeter method is the most commonly used method for three-phase power measurement. The two wattmeters must be properly connected to any two phases, as shown in Fig. 12.34. The total real power is equal to the algebraic sum of the two wattmeter readings,

$$P_T = P_1 + P_2$$

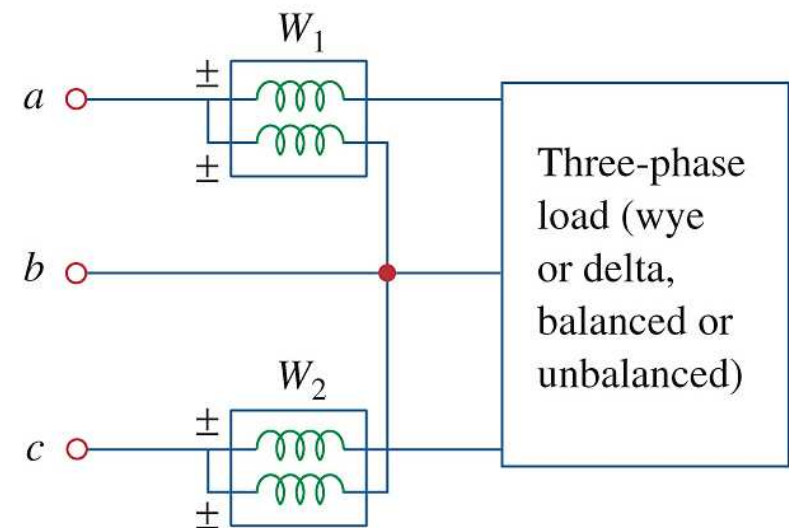


Figure 12.34 Two-wattmeter method for measuring three-phase power.

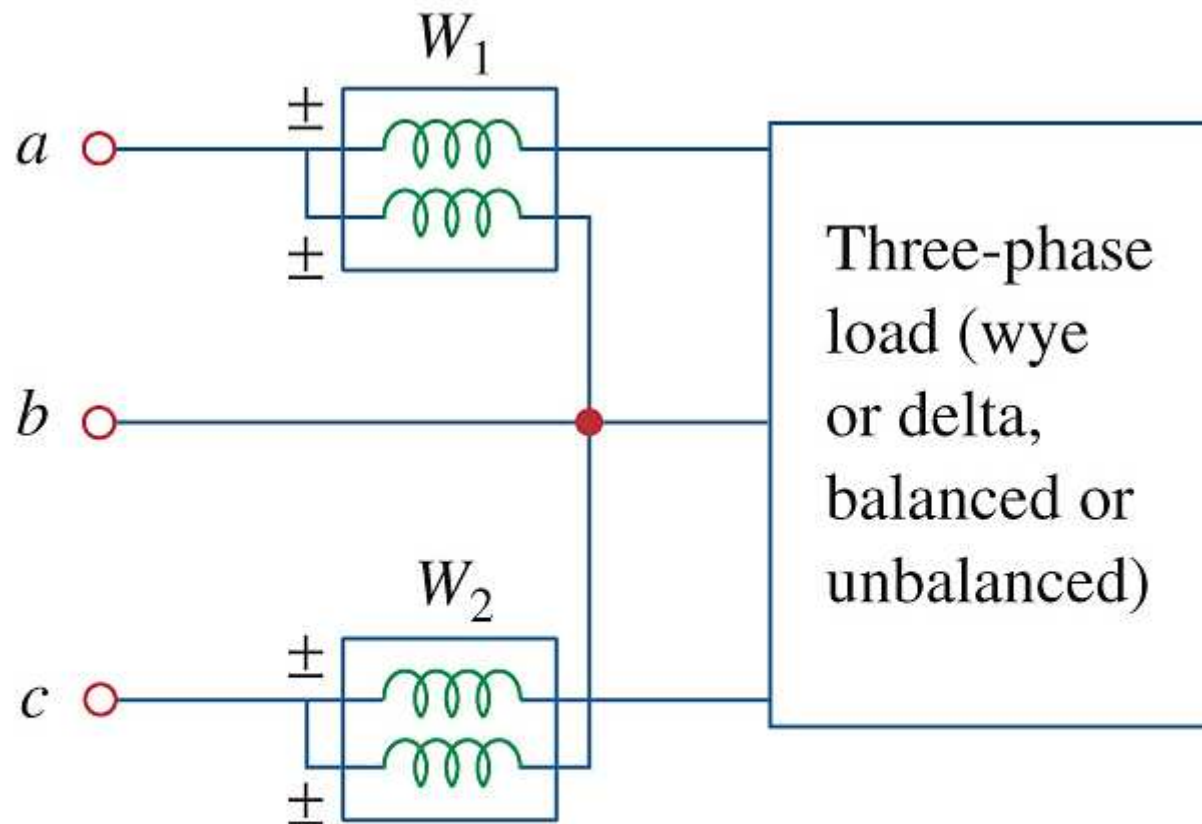


Figure 12.34 Two-wattmeter method for measuring three-phase power.

<Proof> Two-wattmeter method is sufficient

Proof :

$$P_1 = \text{Re}(\dot{V}_{ab} \dot{I}_a^*), P_2 = \text{Re}(\dot{V}_{cb} \dot{I}_c^*)$$

$$P_1 + P_2 = \text{Re}(\dot{V}_{ab} \dot{I}_a^*) + \text{Re}(\dot{V}_{cb} \dot{I}_c^*)$$

$$= \text{Re}(\dot{V}_{ab} \dot{I}_a^* + \dot{V}_{cb} \dot{I}_c^*)$$

CASE1: Y-connected load

If the load is wye-connected,

$$\dot{V}_{ab} \dot{I}_a^* + \dot{V}_{cb} \dot{I}_c^* = (\dot{V}_{an} - \dot{V}_{bn}) \dot{I}_a^* + (\dot{V}_{cn} - \dot{V}_{bn}) \dot{I}_c^*$$

$$= \dot{V}_{an} \dot{I}_a^* - \dot{V}_{bn} (\dot{I}_a^* + \dot{I}_c^*) + \dot{V}_{cn} \dot{I}_c^*$$

$$= \dot{V}_{an} \dot{I}_a^* - \dot{V}_{bn} (\dot{I}_a + \dot{I}_c)^* + \dot{V}_{cn} \dot{I}_c^*$$

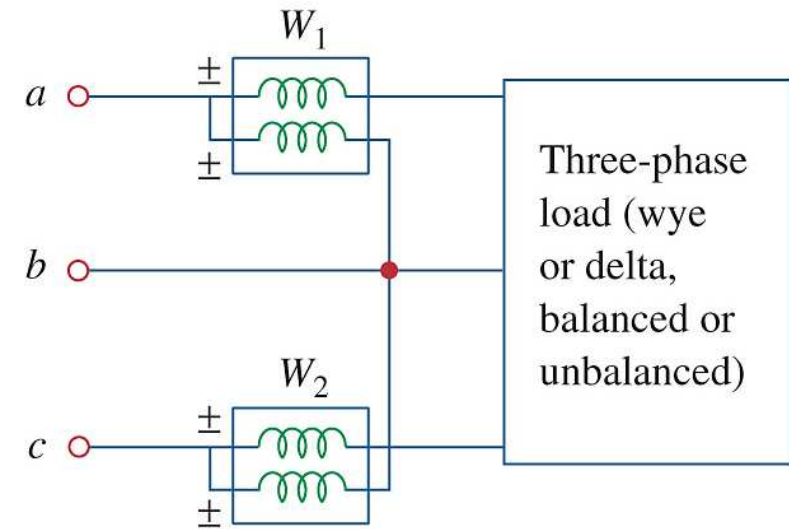
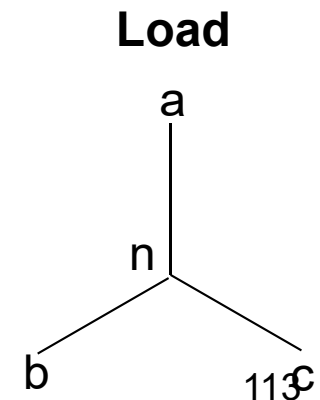


Figure 12.34 Two-wattmeter method for measuring three-phase power.

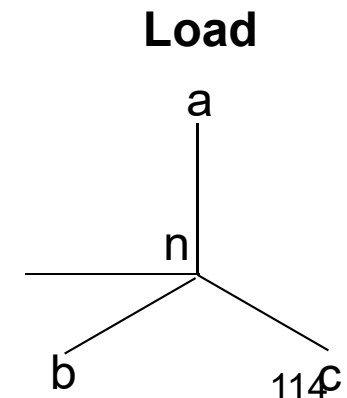


If $\dot{I}_a + \dot{I}_b + \dot{I}_c = 0$, then

$$\dot{V}_{ab}\dot{I}_a^* + \dot{V}_{cb}\dot{I}_c^* = \dot{V}_{an}\dot{I}_a^* + \dot{V}_{bn}\dot{I}_b^* + \dot{V}_{cn}\dot{I}_c^*$$

$$\begin{aligned}\underline{P_1 + P_2} &= \text{Re}\left(\dot{V}_{an}\dot{I}_a^* + \dot{V}_{bn}\dot{I}_b^* + \dot{V}_{cn}\dot{I}_c^*\right) \\ &= \text{Re}(\dot{V}_{an}\dot{I}_a^*) + \text{Re}(\dot{V}_{bn}\dot{I}_b^*) + \text{Re}(\dot{V}_{cn}\dot{I}_c^*) \\ &= \underline{P_a + P_b + P_c = P_T}\end{aligned}$$

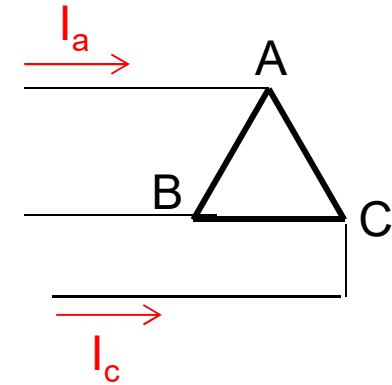
The condition $\dot{I}_a + \dot{I}_b + \dot{I}_c = 0$ implies that the two-wattmeter method cannot be used in a four-wire system unless $\dot{I}_n = 0$.



CASE2: Δ -connected load

If the load is delta-connected,

$$\begin{aligned}
 \dot{V}_{ab} \dot{I}_a^* + \dot{V}_{cb} \dot{I}_c^* &= \dot{V}_{AB} (\dot{I}_{AB} - \dot{I}_{CA})^* + \dot{V}_{CB} (\dot{I}_{CA} - \dot{I}_{BC})^* \\
 &= \dot{V}_{AB} (\dot{I}_{AB} - \dot{I}_{CA})^* - \dot{V}_{BC} (\dot{I}_{CA} - \dot{I}_{BC})^* \\
 &= \dot{V}_{AB} \dot{I}_{AB}^* + \dot{V}_{BC} \dot{I}_{BC}^* - (\dot{V}_{AB} + \dot{V}_{BC}) \dot{I}_{CA}^* \\
 &= \dot{V}_{AB} \dot{I}_{AB}^* + \dot{V}_{BC} \dot{I}_{BC}^* + \dot{V}_{CA} \dot{I}_{CA}^*
 \end{aligned}$$



$$\begin{aligned}
 \underline{P_1 + P_2} &= \text{Re}(\dot{V}_{AB} \dot{I}_{AB}^* + \dot{V}_{BC} \dot{I}_{BC}^* + \dot{V}_{CA} \dot{I}_{CA}^*) \\
 &= \text{Re}(\dot{V}_{AB} \dot{I}_{AB}^*) + \text{Re}(\dot{V}_{BC} \dot{I}_{BC}^*) + \text{Re}(\dot{V}_{CA} \dot{I}_{CA}^*) \\
 &= \underline{P_{AB} + P_{BC} + P_{CA} = P_T}
 \end{aligned}$$

Consider a balanced, Y load

It can be shown that for a balanced three-phase system,

See TEXT, p.536

$$P_1 = V_L I_L \cos(\theta + 30^\circ), P_2 = V_L I_L \cos(\theta - 30^\circ)$$

(If $\theta > 60^\circ$, W_1 reads negative; If $\theta < -60^\circ$, W_2 reads negative.)

$$P_1 + P_2 = \sqrt{3} V_L I_L \cos \theta = P_T$$

$$P_2 - P_1 = V_L I_L \sin \theta = \frac{Q_T}{\sqrt{3}}$$

$$\tan \theta = \frac{Q_T}{P_T} = \sqrt{3} \frac{P_2 - P_1}{P_2 + P_1}$$

Sum to product formulas:

$$\cos u + \cos v = 2 \cos \left(\frac{u+v}{2} \right) \cos \left(\frac{u-v}{2} \right)$$

$$\cos u - \cos v = -2 \sin \left(\frac{u+v}{2} \right) \sin \left(\frac{u-v}{2} \right)$$

Form the readings of P_1 , P_2 , we can calculate the P, Q, and θ .

Proof of $P_1 = V_L I_L \cos(\theta + 30^\circ)$

(1) $\mathbf{Z}_Y = Z_Y \angle \theta$: \mathbf{V}_Y leads \mathbf{I}_a by θ

(2) For a Δ or Y source, \mathbf{V}_{ab} leads \mathbf{V}_Y by 30°

For Δ case, some analysis needed.

→ \mathbf{V}_{ab} leads \mathbf{I}_a by $\theta + 30^\circ$

$$P_1 = \text{Re}[\mathbf{V}_{ab} \mathbf{I}_a^*] = V_{ab} I_a \cos(\theta + 30^\circ) = V_L I_L \cos(\theta + 30^\circ) \quad (12.63)$$

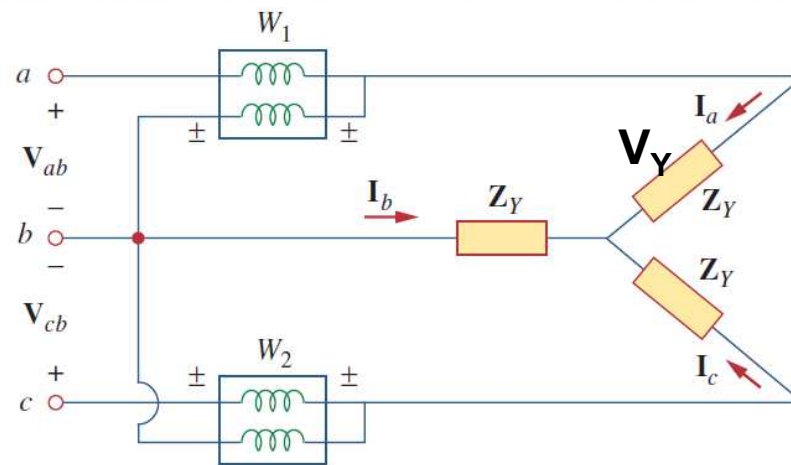


Figure 12.35

Two-wattmeter method applied to a balanced wye load.

Consider a balanced, Δ load

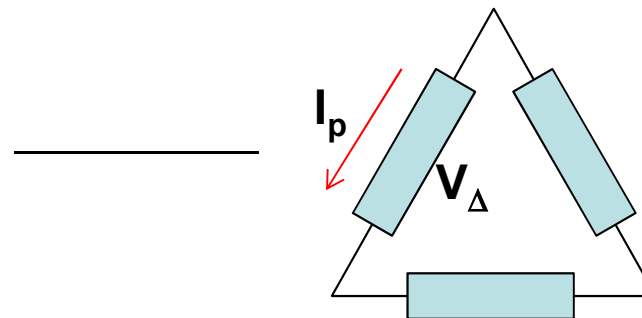
Proof $P_1 = V_L I_L \cos(\theta + 30^\circ)$

(1) $\mathbf{Z}_\Delta = Z_\Delta \angle \theta$: \mathbf{V}_Δ leads \mathbf{I}_p by θ , \mathbf{I}_p leads \mathbf{I}_a by 30°

(2) For a Δ or Y source, $\angle \mathbf{V}_{ab} = \angle \mathbf{V}_\Delta$

→ \mathbf{V}_{ab} leads \mathbf{I}_a by $\theta + 30^\circ$

$$P_1 = \operatorname{Re}[\mathbf{V}_{ab} \mathbf{I}_a^*] = V_{ab} I_a \cos(\theta + 30^\circ) = V_L I_L \cos(\theta + 30^\circ) \quad (12.63)$$



The formulas can be used for all 4 cases.

Practice Problem 12.14 Let the line voltage $V_L = 208 \text{ V}$ and the wattmeter readings of the balanced system in Fig. 12.35 be $P_1 = -560 \text{ W}$ and $P_2 = 800 \text{ W}$. Determine:

- (a) the total average power
- (b) the total reactive power
- (c) the power factor
- (d) the phase impedance

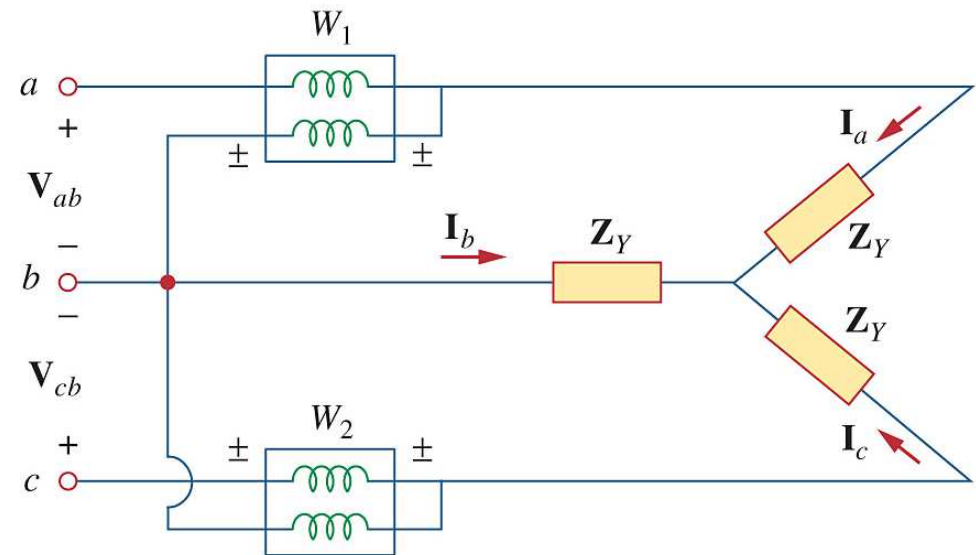


Figure 12.35 Two-wattmeter method applied to a balanced wye load.

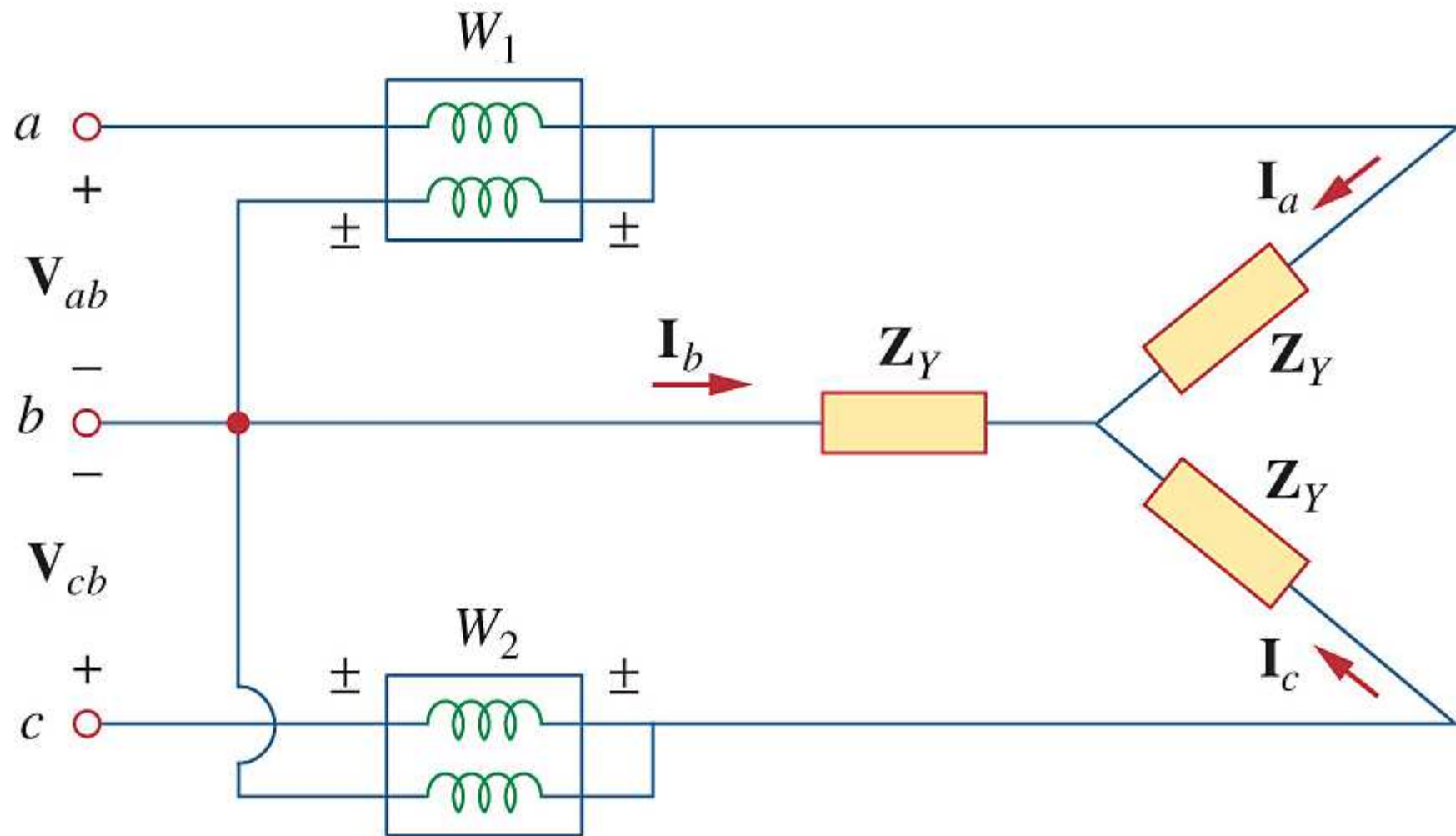


Figure 12.35 Two-wattmeter method applied to a balanced wye load.

Solution :

$$(a) P_T = P_1 + P_2 = -560 + 800 = 240 \text{ (W)}$$

$$(b) Q_T = \sqrt{3}(P_2 - P_1) = \sqrt{3}[800 - (-560)] \\ \approx 2355.5891 \text{ (VAR)}$$

$$(c) \theta = \tan^{-1} \left(\frac{Q_T}{P_T} \right) = \tan^{-1} \left(\frac{2355.5891}{240} \right) \\ \approx 84.18^\circ$$

$$\text{pf} = \cos \theta = \cos 84.18^\circ \approx 0.1014 \text{ lagging}$$

$$\theta > 0 \rightarrow \theta_v > \theta_i$$

$$(d) P_p = P_T / 3 = 240 / 3 = 80 \text{ (W)}$$

Balanced system
Real power per phase

$$P_p = V_p I_p \cos \theta \Rightarrow I_p = \frac{P_p}{V_p \cos \theta}$$

$$|Z_Y| = \frac{V_p}{I_p} = \frac{V_p}{P_p / (V_p \cos \theta)} = \frac{V_p^2 \cos \theta}{P_p}$$

$$= \frac{V_L^2 \cos \theta}{3P_p} = \frac{208^2 \times 0.1014}{3 \times 80} \approx 18.2790 \text{ } (\Omega)$$

$V_p = V_L / \sqrt{3}$
for Y-Y

$$Z_Y = 18.2790 \angle 84.18^\circ \text{ } \Omega, \text{ inductive.}$$