# VE215 Intro to Circuits

Mid 1 Review Class

#### **Content for Mid 1**

- 1. Chapter 1: Basic Concepts
- 2. Chapter 2: Basic Laws
- 3. Chapter 3: Methods of Analysis
- 4. Chapter 4: Circuit Theorems
- 5. Chapter 5: Operational Amplifiers

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• The relationship between current i, charge q, and time t:

$$i = \frac{dq}{dt}$$

• The charge transferred between time  $t_0$  and t is obtained by

$$q = \int_{t_0}^{t} i \, dt$$

• The voltage  $v_{ab}$  between two points a and b is defined by

$$v_{ab} = \frac{aw}{dq}$$

# Direction of Voltage & Current

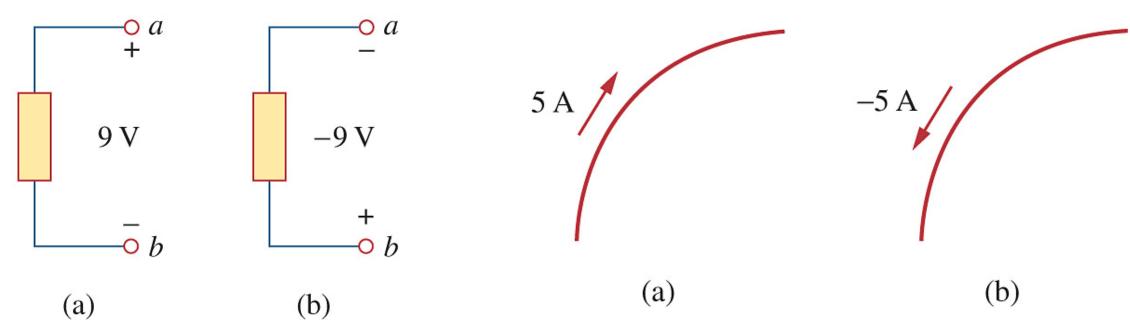


Figure 1.7 Two equivalent representations of the same voltage  $v_{ab}$ : (a) point a is 9 V above point b, (b) point b is -9 V above point a.

Figure 1.5 Conventional current flow: (a) positive current flow, (b) negative current flow.

# Example

• When using *Thevenin's*Theorem, we usually consider  $V_{Th}$  as the voltage between point a and b.

• Be careful in the exam!

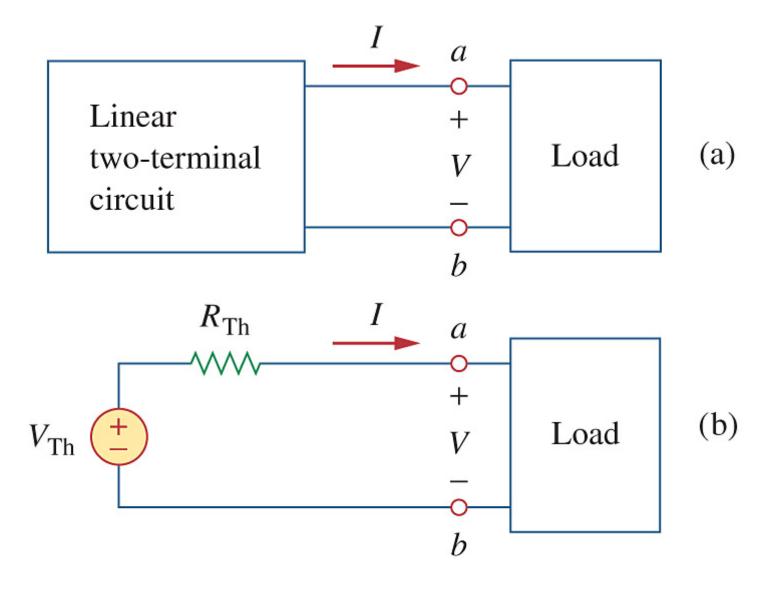
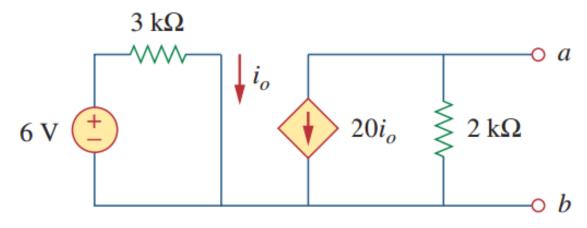


Figure 4.23 Replacing a linear two-terminal circuit by its Thevenin equivalent.

#### Homework 4 – Prob 4.52

**4.52** For the transistor model in Fig. 4.118, obtain the Thevenin equivalent at terminals a-b.



#### **Figure 4.118**

For Prob. 4.52.

$$R_{Th} = 2k \Omega$$
$$V_{Th} = -80 V$$

Detailed solution will be coverd in the fourth part.

• *Power* is the time rate of expending or absorbing energy:

$$p = \frac{dw}{dt}$$

• In circuit, we have the calculation form

$$p = vi$$

• Energy is the capacity to do work

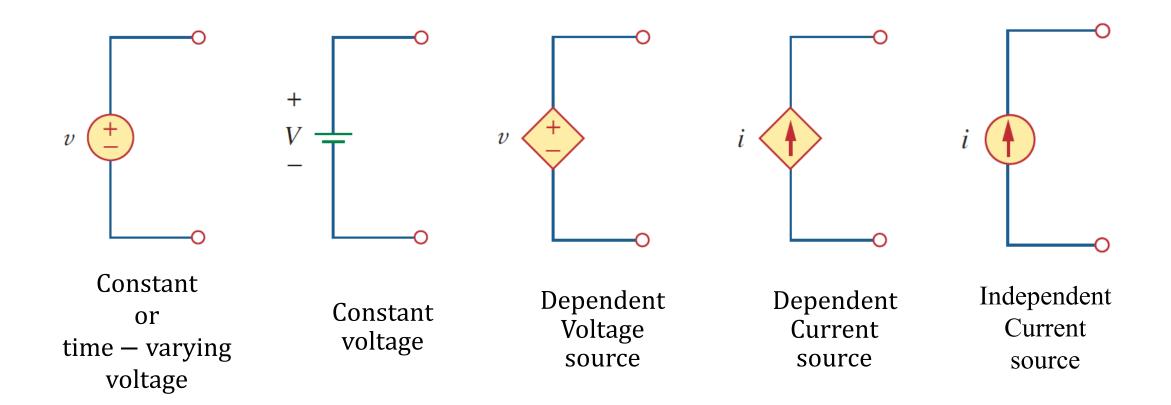
$$w = \int_{t_0}^t p \, dt = \int_{t_0}^t vi \, dt$$

• The law of conservation of energy

$$\sum p = 0$$

the total power supplied to the circuit must balance the total power absorbed, i.e. Power absorbed =  $-Power\ supplied$ .

# **Symbols**



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- Branch:
- A branch b represents a single element.

- Node:
- A node *n* is the point connection between two or more branches.
- Loop:
- A loop *l* is any closed path in a circuit.

$$b = l + n - 1$$

- Ohm's Law:
- The voltage v across a resistor is proportional to the current i flowing through the resistor.

$$i = i \times R$$

• The power dissipated by a resistor can be expressed in terms of R.

$$p = vi = i^2 R = \frac{v^2}{R}$$

- Be careful: the equation is only for direct current (DC).
- Conductance

$$G = \frac{1}{R}$$

- Series
- Two or more elements are in series if they exclusively share a single node and consequently carry the same current.

$$R_{total} = \sum R_s$$

- Parallel
- Two or more elements are in **parallel** if they are connected to the same two nodes and consequently have the same voltage across them.

$$\frac{1}{R_{total}} = \sum \frac{1}{R_p}$$

- The principle of voltage division
- For register in series, voltage across each resistor

$$v_n = \frac{R_n}{\sum_{n=1}^{N} R_n} v, \qquad n = 1, 2, ..., N$$

- The principle of current division
- For register in parallel, current across each resistor

$$i_n = \frac{G_n}{\sum_{n=1}^{N} G_n} i, \qquad n = 1, 2, ..., N$$

# Kirchhoff's current law (KCL)

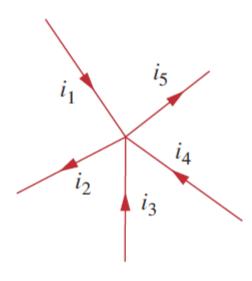
- Definition:
- The algebraic sum of currents entering a node (or a closed boundary) is zero.

$$\sum_{n=1}^{N} i_n = 0$$

• where n is the number of branches connected to the node and  $i_n$  is the n-th current entering (or leaving) the node.

$$\sum i_n = 0$$

$$i_1 - i_2 + i_3 + i_4 - i_5 = 0$$
  
 $i_1 + i_3 + i_4 = i_2 + i_5$ 



**Figure 2.16**Currents at a node illustrating KCL.

# Kirchhoff's voltage law (KVL)

- Definition
- The algebraic sum of all voltages around a closed path (or loop) is zero.

$$\sum_{m=1}^{M} v_m = 0$$

• where M is the number of branches in the loop and  $v_m$  is the m-th voltage drop (or rise) in the loop.

$$\sum v_m = 0$$

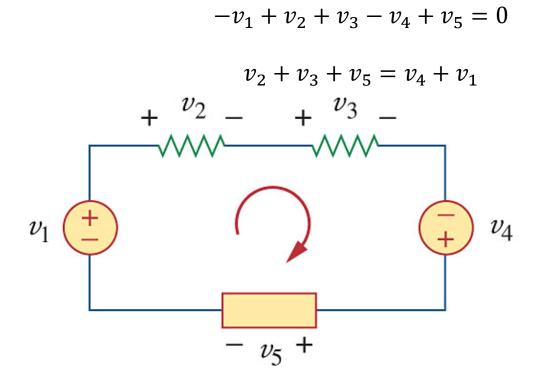


Figure 2.19 A single-loop circuit illustrating KVL.

## **Wye-Delta Transformations**

$$R_1 = \frac{R_b R_c}{R_a + R_b + R_c}$$

$$R_1 = \frac{R_b R_c}{R_a + R_b + R_c} \qquad R_a = \frac{R_1 R_2 + R_2 R_3 + R_3 R_1}{R_1} \qquad 1$$

$$R_2 = \frac{R_c R_a}{R_a + R_b + R_c}$$

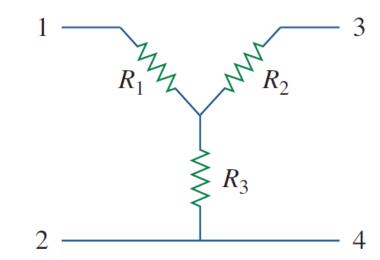
$$R_2 = \frac{R_c R_a}{R_a + R_b + R_c} \qquad R_b = \frac{R_1 R_2 + R_2 R_3 + R_3 R_1}{R_2}$$

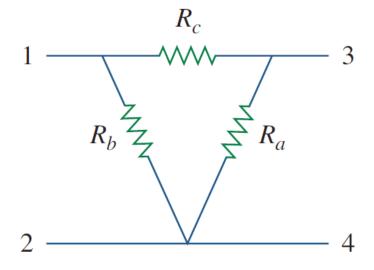
$$R_3 = \frac{R_a R_b}{R_a + R_b + R_c}$$

$$R_3 = \frac{R_a R_b}{R_a + R_b + R_c} \qquad R_c = \frac{R_1 R_2 + R_2 R_3 + R_3 R_1}{R_3}$$

The Y and  $\Delta$  networks are said to be *balanced* when

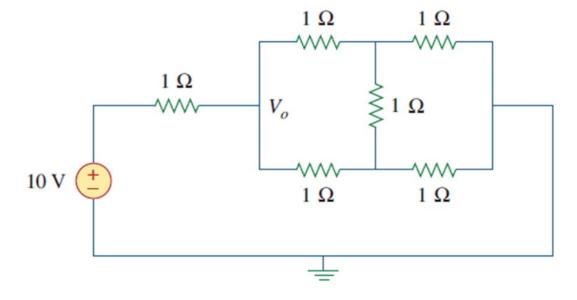
$$R_1 = R_2 = R_3 = R_Y,$$
  $R_a = R_b = R_c = R_\Delta$   $R_Y = \frac{R_\Delta}{3}$  or  $R_\Delta = 3R_Y$ 



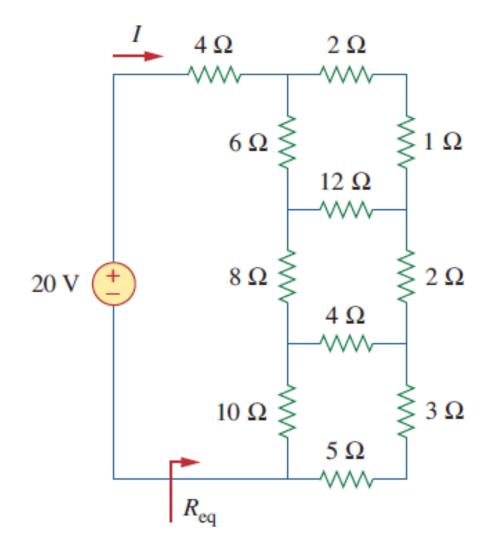


# **Sample Questions**

Find  $V_o$  in the two-way power divider circuit

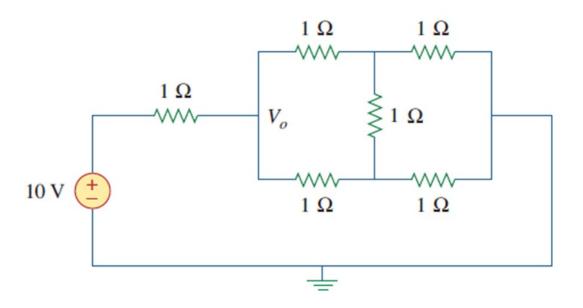


#### Find $R_{eq}$ and I in the circuit

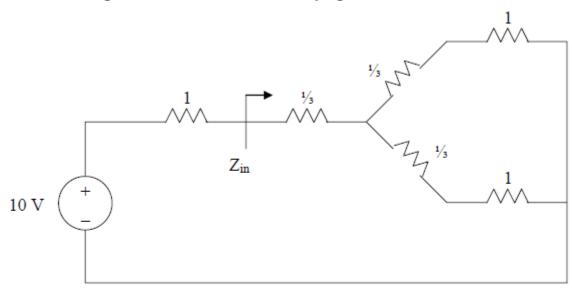


## **Solutions**

Find  $V_o$  in the two-way power divider circuit



Converting the delta subnetwork into wye gives the circuit below.

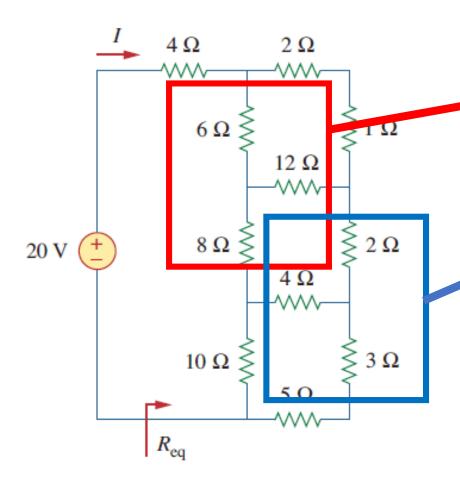


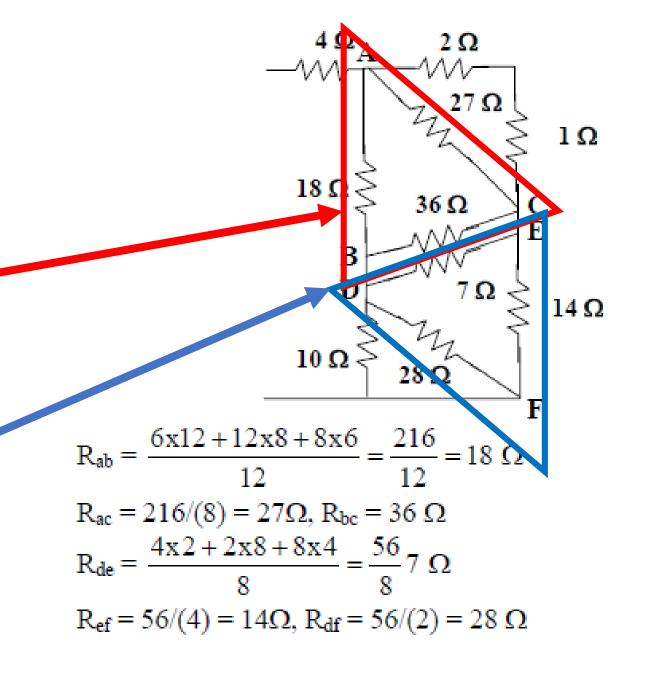
$$Z_{in} = \frac{1}{3} + (1 + \frac{1}{3}) / (1 + \frac{1}{3}) = \frac{1}{3} + \frac{1}{2} (\frac{4}{3}) = 1 \Omega$$

$$V_{o} = \frac{Z_{in}}{1 + Z_{in}} (10) = \frac{1}{1 + 1} (10) = \underline{5 \text{ V}}$$

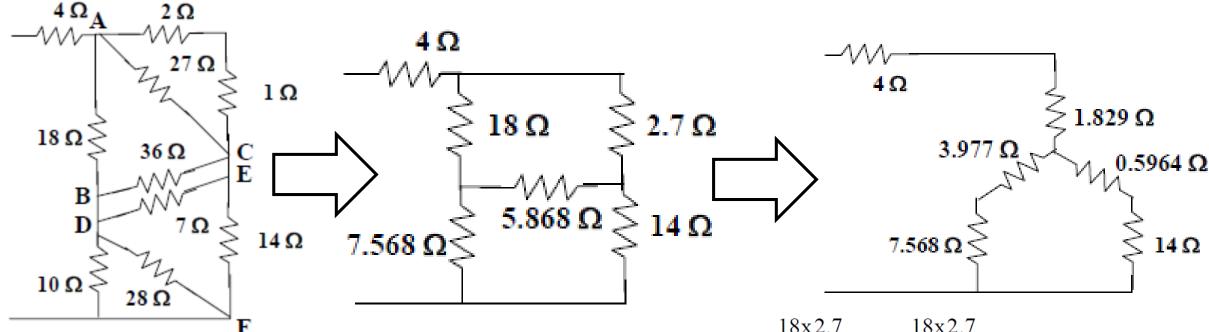
## **Solutions**

Find  $R_{eq}$  and I in the circuit





## **Solutions**



Combining resistors in parallel,

$$10 \|28 = \frac{280}{38} = 7.368\Omega, \ 36 \|7 = \frac{36x7}{43} = 5.868\Omega$$
$$27 \|3 = \frac{27x3}{30} = 2.7\Omega$$

$$R_{an} = \frac{18x2.7}{18 + 2.7 + 5.867} = \frac{18x2.7}{26.567} = 1.829 \Omega$$

$$R_{bn} = \frac{18x5.868}{26.567} = 3.977 \Omega$$

$$R_{cn} = \frac{5.868x2.7}{26.567} = 0.5904 \Omega$$

$$R_{eq} = 4 + 1.829 + (3.977 + 7.368) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14) \| (0.5964 + 14$$

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## **Nodal Analysis**

- Given a circuit with nodes without voltage sources, the nodal analysis involves taking the following four steps:
- 1. Select a node as the reference node (commonly called the ground). We flag the chosen reference node with one of the symbols as in Fig. 3.1.
- 2. Assign node voltages  $v_1$ ,  $v_2$ , K,  $v_{n-1}$  to the remaining n-1 nodes. A node voltage is defined as the voltage rise from the reference node to a nonreference node.

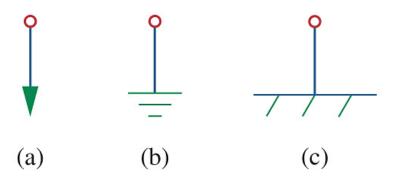


Figure 3.1 Common symbols for indicating a reference node: (a) common ground, (b) ground, (c) chassis ground.

- 3. Apply KCL to each of the nonreference nodes. Use Ohm's law to express the branch currents in terms of node voltages.
- 4. Solve the resulting simultaneous equations to obtain the unknown node voltages.

# **Nodal Analysis**

# Plz Write Down the Matrix in the Exam!

If a circuit with only independent current sources has *N* nonreference nodes, the nodevoltage equations can be written as

$$\begin{bmatrix} G_{11} & G_{12} & \vdots & G_{1N} \\ G_{21} & G_{22} & \vdots & G_{2N} \\ \vdots & \vdots & \vdots & \vdots \\ G_{N1} & G_{N2} & \vdots & G_{NN} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \\ \vdots \\ v_N \end{bmatrix} = \begin{bmatrix} i_1 \\ i_2 \\ \vdots \\ i_N \end{bmatrix}$$

 $G_{kk}$  = Sum of the conductances connected to node k

 $G_{kj} = G_{jk}$  = Negative of the sum of the conductances directly connecting nodes k and  $j, k \neq j$ 

 $v_k$  = Unknown voltage at node k

 $i_k$  = Sum of all independent current sources directly connected to node k, with currents entering the node treated as positive

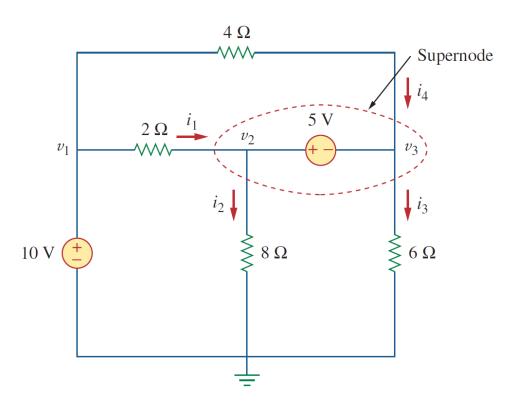
#### Nodal Analysis with the voltage sources

In some cases, there are voltage sources in the circuits. We may adopt the following two principles when we faced with such cases.

- 1. If a voltage source is connected between the reference node and a non-reference node, the node voltage is known.
- 2. If a voltage source is connected between two non-reference nodes, the two non-reference nodes form a **Supernode**. The supernode provides a constraint on the two node voltages.
- 3. A supernode is formed by enclosing a voltage source between two non-reference nodes and any elements connected in parallel with it. Mention that we usually adopt the KCL for the whole super nodes.

It sounds might be slightly abstract. You may consider the examples to understand the method.

# Example



- 1. According to the principle I: we can know that the voltage of node 1  $v_1$  is 10 volts.
- 2. According to the principle II: we can know that the voltage difference between node 2 and node 3:  $v_2 v_3$  is 5 volts.
- 3. Adopt KCL to the supernode formed by node2 and node3(marked by the red circle), we can have the following equation:

$$\frac{v_2 - v_1}{2} + \frac{v_2 - 0}{8} + \frac{v_3 - v_1}{4} + \frac{v_3 - 0}{6} = 0 \tag{1}$$

# Mesh Analysis

- Steps to Determine Mesh Currents for circuit with *n* Meshes without Current Sources :
- 1. Assign mesh currents  $i_1, i_2, ..., i_n$  to the n meshes. (ATTENTION: the mesh current for all meshes are always clockwise!)

• 2. Apply KVL to each of the n meshes. Use Ohm's law to express the voltages in terms of the mesh currents.

• 3. Solve the resulting n simultaneous equations to get the mesh currents.

# **Nodal Analysis**

# Plz Write Down the Matrix in the Exam!

If a circuit with only independent voltage sources has N meshes, the node-current equations can be written as

 $R_{kk}$  = Sum of the resistances in mesh k

 $R_{kj} = R_{jk}$  = Negative of the sum of the resistances in common with meshes k and  $j, k \neq j$ 

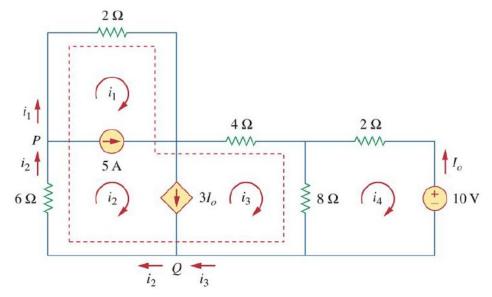
 $i_k$  = Unknown mesh current for mesh k in the clockwise direction

 $v_k$  = Sum taken clockwise of all independent voltage sources in mesh k, with voltage rise treated as positive

#### Mesh Analysis with Current Sources

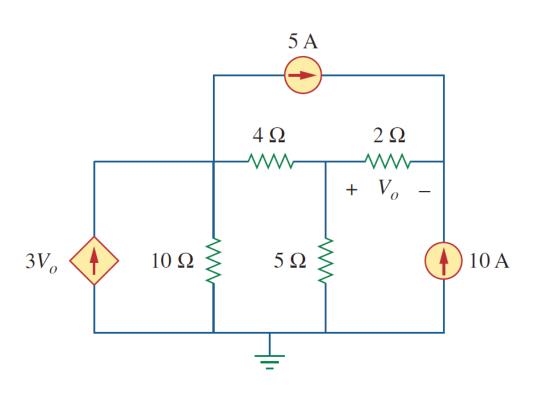
Similar to the Nodal Analysis with Voltage sourses, we can also generate three principles in general:

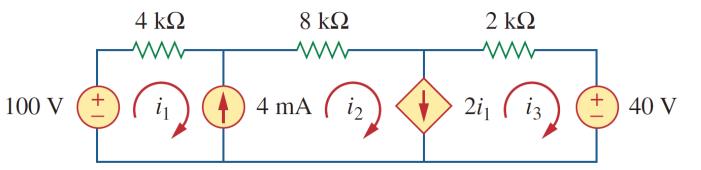
- 1. When a current source is only in one mesh, the mesh current of that mesh is just the value of the current source.
- 2. When a current source locate in between two meshes, then the two meshes forms a **supermesh**. We can get the difference of two meshes currents.
- 3. We usually apply the KVL to the whole supermesh. The total voltage of a supermesh is zero. (Metion that more than two meshes can also form a supermesh. We will discuss that case in the following example.)

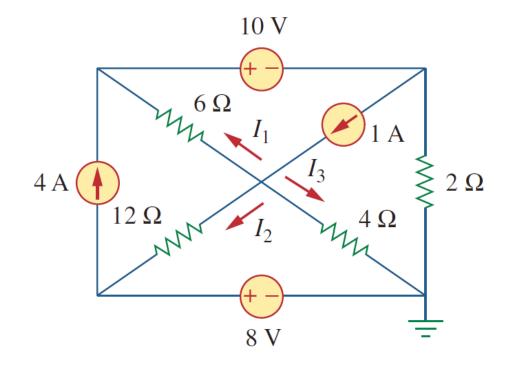


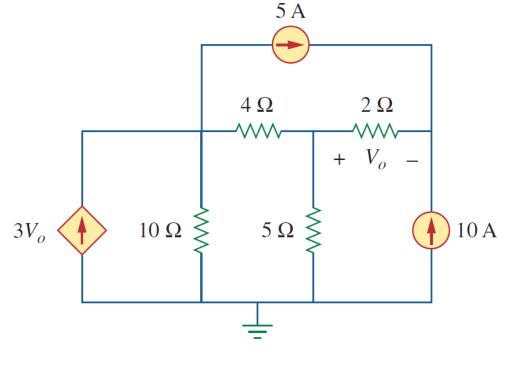
# **Sample Questions**

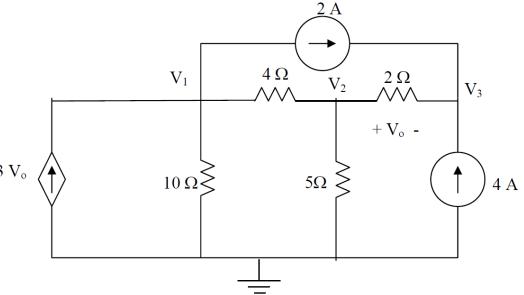
Obtain the node-voltage equations for the circuit











$$\begin{bmatrix} 0.35 & -0.25 & 0 \\ -0.25 & 0.95 & -0.5 \\ 0 & -0.5 & 0.5 \end{bmatrix} V = \begin{bmatrix} V_o \\ 0 \\ 6 \end{bmatrix}$$

Since we actually have four unknowns and only three equations, we need a constraint equation.

$$V_0 = V_2 - V_3$$

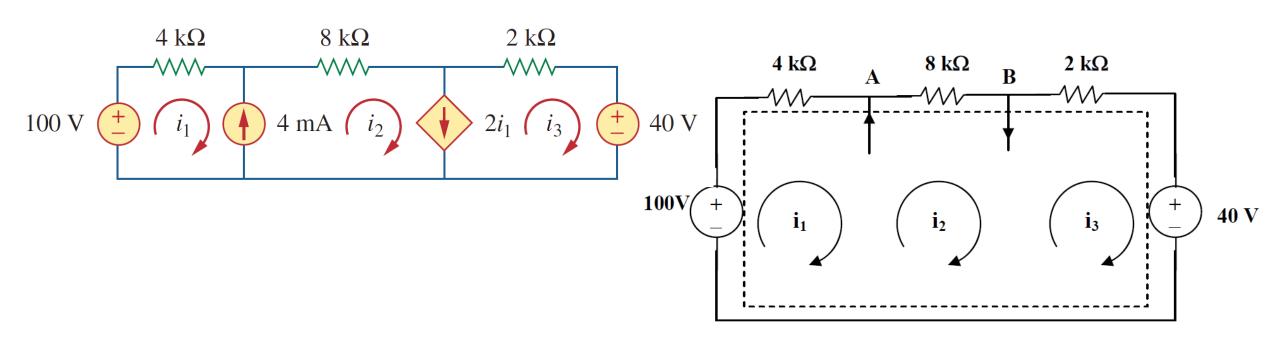
Substituting this back into the matrix equation, the first equation becomes,

$$0.35V_1 - 3.25V_2 + 3V_3 = -2$$

This now results in the following matrix equation,

$$\begin{bmatrix} 0.35 & -3.25 & 3 \\ -0.25 & 0.95 & -0.5 \\ 0 & -0.5 & 0.5 \end{bmatrix} V = \begin{bmatrix} -2 \\ 0 \\ 6 \end{bmatrix}$$

$$V_0 = V_2 - V_3 = -77.89 + 65.89 = -12 V$$
.



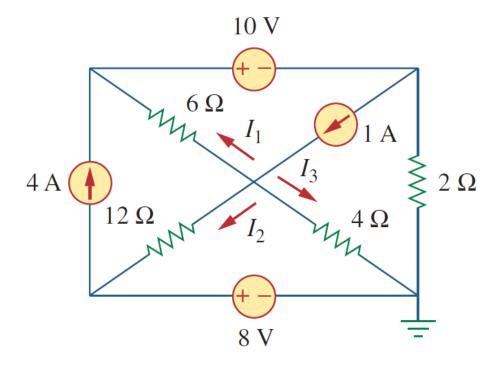
We have a supermesh. Let all R be in  $k\Omega$ , i in mA, and v in volts.

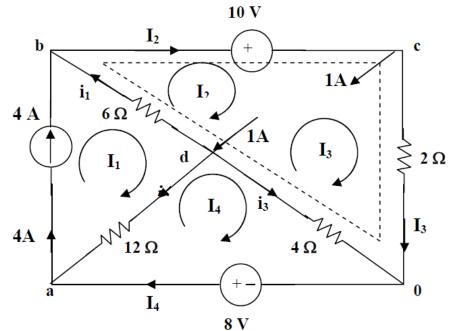
For the supermesh, 
$$-100 + 4i_1 + 8i_2 + 2i_3 + 40 = 0$$
 or  $30 = 2i_1 + 4i_2 + i_3$  (1)

At node A, 
$$i_1 + 4 = i_2$$
 (2)

At node B, 
$$i_2 = 2i_1 + i_3$$
 (3)

Solving (1), (2), and (3), we get  $i_1 = 2 \text{ mA}$ ,  $i_2 = 6 \text{ mA}$ , and  $i_3 = 2 \text{ mA}$ .





It is evident that 
$$I_1 = 4$$
 (1)

For mesh 4, 
$$12(I_4 - I_1) + 4(I_4 - I_3) - 8 = 0$$
 (2)

For the supermesh 
$$6(I_2 - I_1) + 10 + 2I_3 + 4(I_3 - I_4) = 0$$
 or 
$$-3I_1 + 3I_2 + 3I_3 - 2I_4 = -5$$
 (3)

At node c, 
$$I_2 = I_3 + 1$$
 (4)

Solving (1), (2), (3), and (4) yields,  $I_1 = 4A$ ,  $I_2 = 3A$ ,  $I_3 = 2A$ , and  $I_4 = 4A$ 

At node b,  $i_1 = I_2 - I_1 = -1A$ 

At node a,  $i_2 = 4 - I_4 = 0A$ 

At node 0,  $i_3 = I_4 - I_3 = 2A$ 

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- Linearity:
- A linear circuit is one whose **output** (also called response) is linearly related to its **input** (also called excitation).
- The linearity property is a combination of both the **homogeneity** (scaling) property and the **additivity** property.
- Superposition:
- Superposition principle is based on additivity. It states that whenever a linear system is excited, or driven, by more than one independent source, the total response is the sum of the individual responses.

#### **4.12** Determine $v_0$ in the circuit of Fig. 4.80 using the Superposition Principle Steps

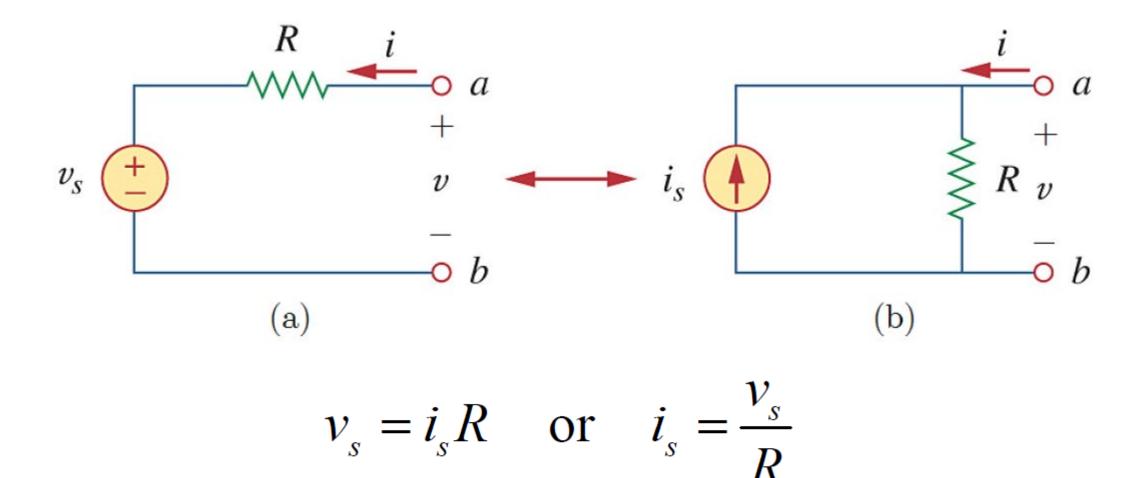
- To apply the superposition principle, we must keep two things in mind:
- – We consider only one independent source at a time while all other independent sources are turned off. This implies that we replace every voltage source by 0 V (or a short circuit), and every current source by 0 A (or an open circuit).
- – Dependent sources are left intact because they are controlled by circuit variables.

 $6\Omega$  $5 \Omega$  $12 \Omega$ Figure 4.80 For Prob. 4.12.

superposition principle.

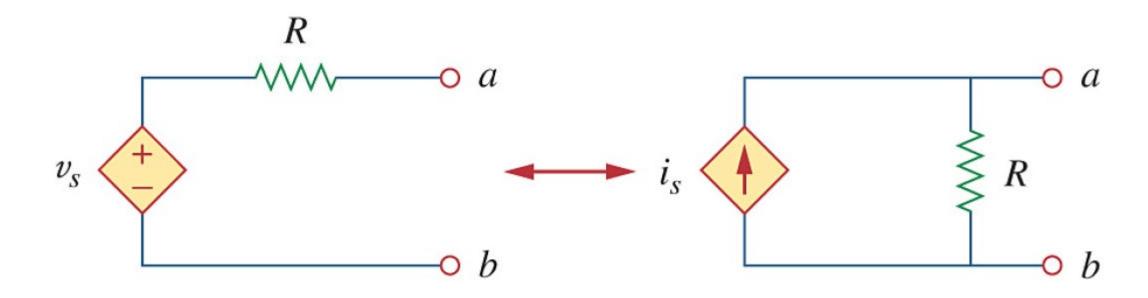
• Add all the outputs up. Plz Analyze the Sources separately!

## **Source Transformation**



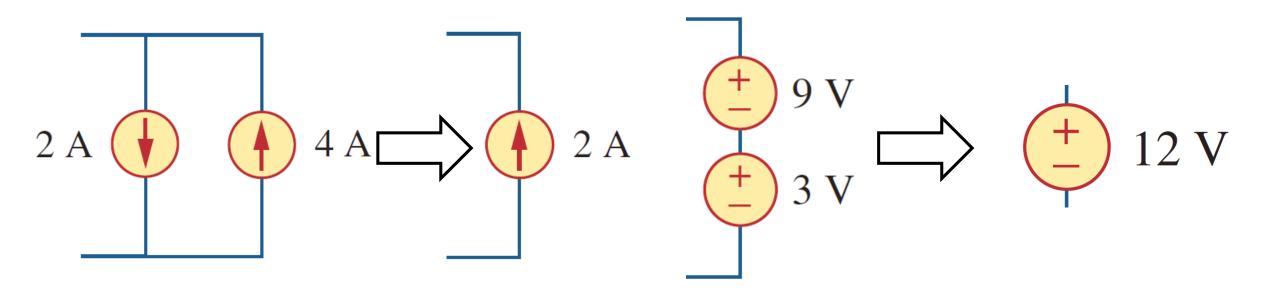
Replacing a voltage source in series with a resistor by a current source in parallel with a resistor, or vice versa.

# Source Transformation (dependent sources)



Source transformation also applies to dependent sources, provided we carefully handle the dependent variable.

# Source Transformation (special)



Source transformation also applies to dependent sources, provided we carefully handle the dependent variable.

## Thevenin's Theorem & Norton's Theorem

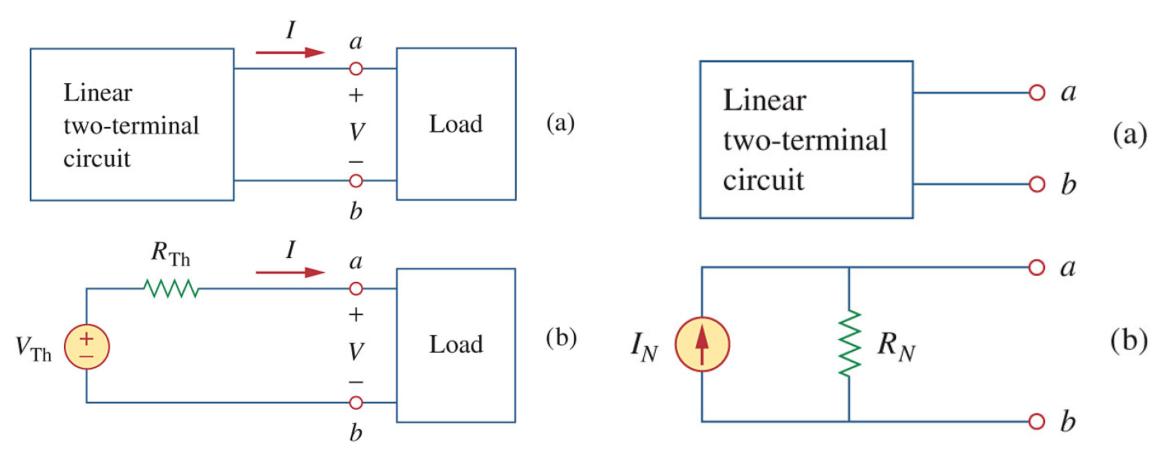
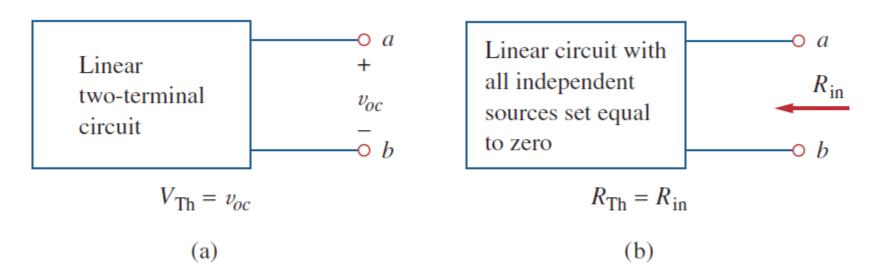


Figure 4.23 Replacing a linear two-terminal circuit by its Thevenin equivalent.

Figure 4.37 (a) Original circuit, (b) Norton equivalent circuit.

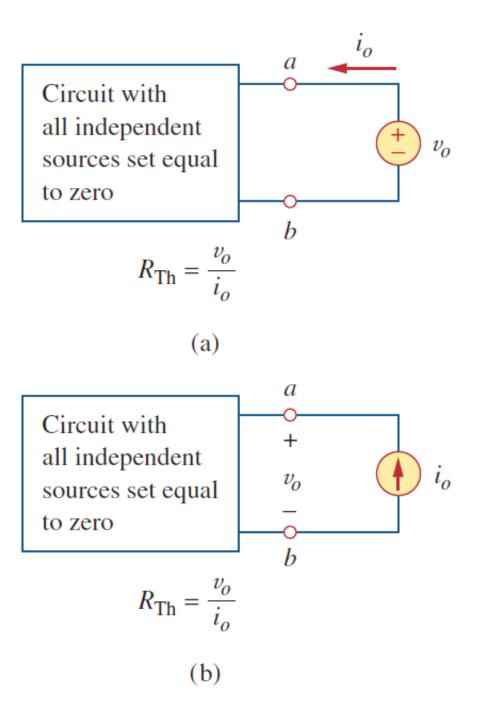
#### Thevenin's Theorem

- To apply this idea in finding the Thevenin resistance  $R_{Th}$ , we need to consider two cases.
- CASE 1 If the network has no dependent sources, we turn off all independent sources.  $R_{Th}$  is the input resistance of the network looking between terminals a and b.



 $V_{Th}$  is the open-circuit voltage across the terminals

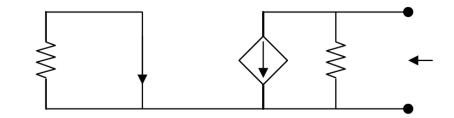
• CASE 2 If the network has dependent sources, we turn off all independent sources. As with superposition, dependent sources are not to be turned off because they are controlled by circuit variables. We apply a voltage source at terminals a and b and determine the resulting current. Then  $R_{Th} = v_0/i_0$ . Alternatively, we may insert a current source  $i_0$  at terminals a - b and find the terminal voltage. Again  $R_{Th} = v_0/i_0$ . Either of the two approaches will give the same result. In either approach we may assume any value of  $v_0$  and  $i_0$ .

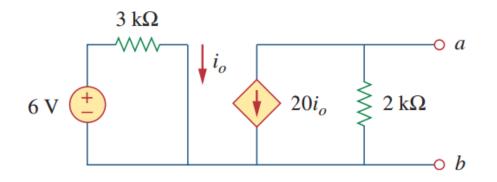


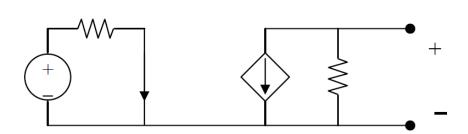
For  $R_{Th}$ , consider the circuit in Fig. (a).

# Homework 4 – Prob 4.52

**4.52** For the transistor model in Fig. 4.118, obtain the Thevenin equivalent at terminals *a-b*.







For Fig. (a),  $I_0 = 0$ , hence the current source is inactive and

$$R_{Th} = 2 k ohms$$

For  $V_{Th}$ , consider the circuit in Fig. (b).

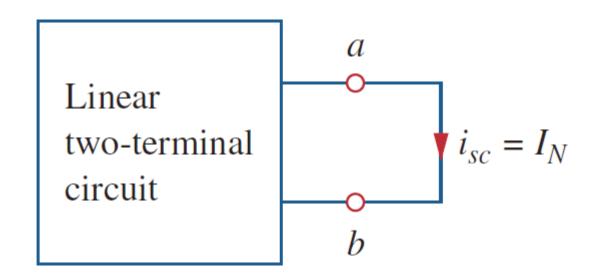
$$I_0 = 6/3k = 2 \text{ mA}$$

$$V_{Th} = (-20I_o)(2k) = -20x2x10^{-3}x2x10^3 = -80 \text{ V}$$

## Norton's Theorem

$$R_N = R_{\rm Th}$$

 $I_N$  is the short-circuit current.



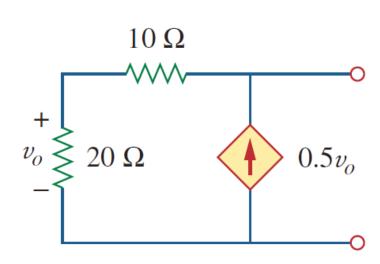
## Figure 4.38

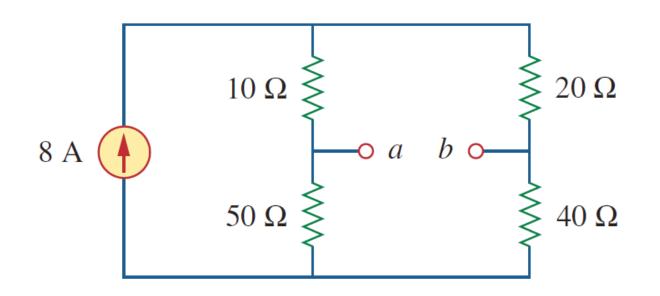
Finding Norton current  $I_N$ .

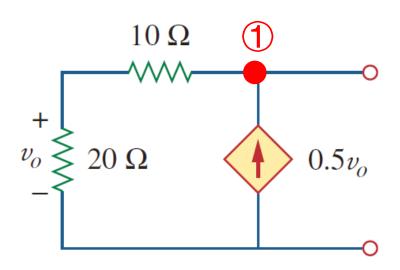
# Sample Questions terminals a-b of the circuit

Determine the Thevenin and Norton equivalents at terminals *a-b* of the circuit

Find the Norton equivalent for the circuit

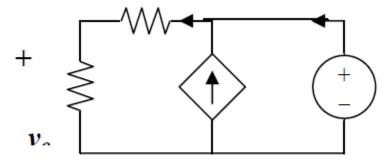






Because there are no independent sources,  $I_N = I_{sc} = \underline{0} \underline{A}$ 

 $R_N$  can be found using the circuit below.

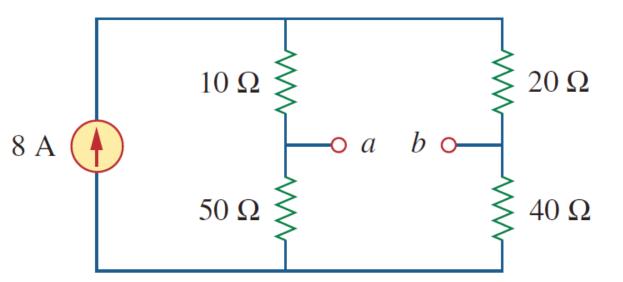


Applying KCL at node 1, 
$$v_1 = 1$$
, and  $v_0 = (20/30)v_1 = 2/3$ 

$$i_0 = (v_1/30) - 0.5v_0 = (1/30) - 0.5x2/3 = 0.03333 - 0.33333 = -0.3 A.$$

Hence,

$$R_N = 1/(-0.3) = -3.333 \text{ ohms}$$



$$R_{Th} = (10 + 20)||(50 + 40) \ 30||90 = 22.5 \text{ ohms}$$

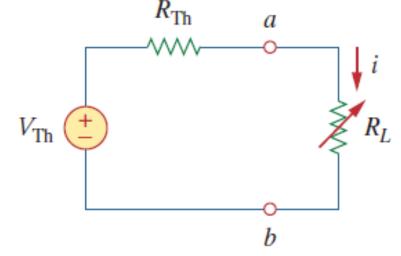
To find  $V_{Th}$ , consider the circuit below.

$$i_1 = i_2 = 8/2 = 4$$
,  $10i_1 + V_{Th} - 20i_2 = 0$ , or  $V_{Th} = 20i_2 - 10i_1 = 10i_1 = 10x4$   $V_{Th} = 40V$ , and  $I_N = V_{Th}/R_{Th} = 40/22.5 = 1.7778 A$ 

## **Maximum Power Transfer**

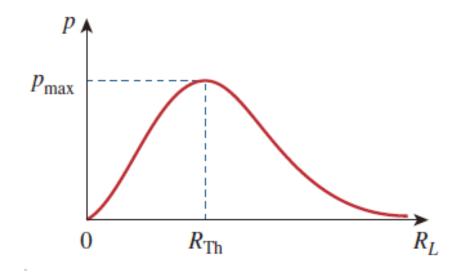
• Maximum power is transferred to the load when the load resistance equals the Thevenin

**resistance** as seen from the load  $(R_L = R_{Th})$ .



$$p = i^2 R_L = \left(\frac{V_{\text{Th}}}{R_{\text{Th}} + R_L}\right)^2 R_L$$

the power delivered to the load



$$p_{\text{max}} = \frac{V_{\text{Th}}^2}{4R_{\text{Th}}}$$

## **Content for Mid 1**

- 1. Chapter 1: Basic Concepts
- 2. Chapter 2: Basic Laws
- 3. Chapter 3: Methods of Analysis
- 4. Chapter 4: Circuit Theorems
- 5. Chapter 5: Operational Amplifiers

# **Basic Concept**

• The op amp is an electronic unit that behaves like a voltage-controlled voltage source.

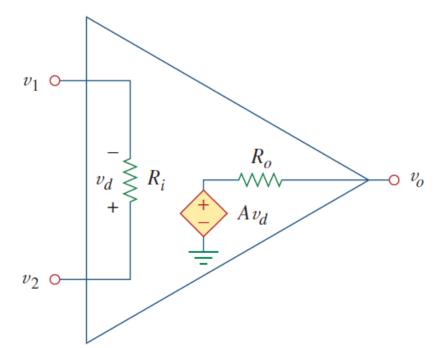


Figure 5.4
The equivalent circuit of the nonideal op amp.

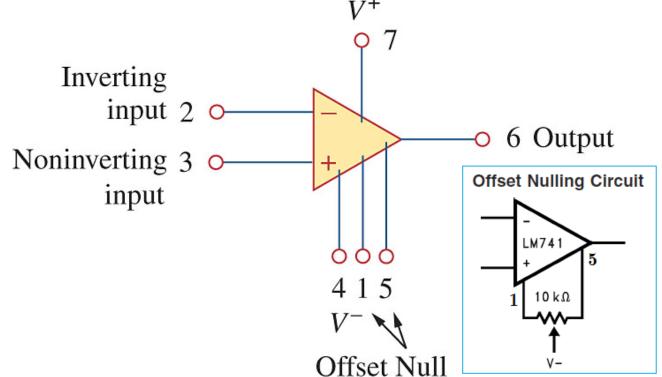


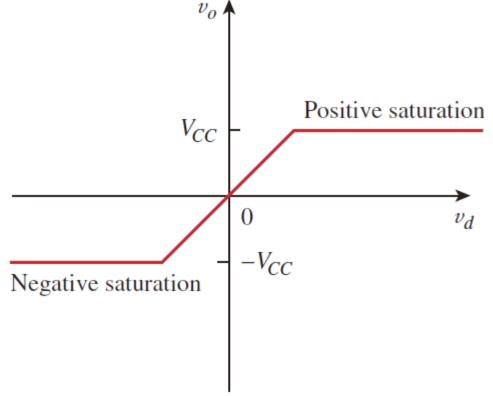
Figure 5.2(b) A typical op amp: circuit symbol.

$$v_o = Av_d = A(v_2 - v_1)$$

A is called the open-loop voltage gain

$$A = rac{output}{input}$$
, i.e.  $A_v = rac{v_{out}}{v_{in}}$ ,  $A_i = rac{i_{out}}{i_{in}}$ 

# **Basic Concept**



#### Figure 5.5

Op amp output voltage  $v_o$  as a function of the differential input voltage  $v_d$ .

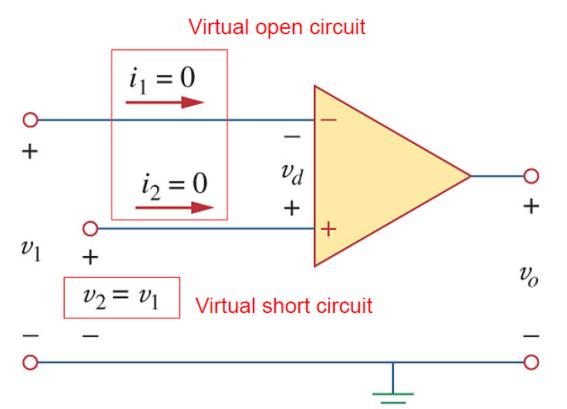
A practical limitation of the op amp is that the magnitude of its output voltage cannot exceed  $|V_{CC}|$ . In other words, the output voltage is dependent on and is limited by the power supply voltage. Figure 5.5 illustrates that the op amp can operate in three modes, depending on the differential input voltage  $v_d$ :

- 1. Positive saturation,  $v_o = V_{CC}$ .
- 2. Linear region,  $-V_{CC} \le v_o = Av_d \le V_{CC}$ .
- 3. Negative saturation,  $v_o = -V_{CC}$ .

If we attempt to increase  $v_d$  beyond the linear range, the op amp becomes saturated and yields  $v_o = V_{CC}$  or  $v_o = -V_{CC}$ . Throughout this book, we will assume that our op amps operate in the linear mode. This means that the output voltage is restricted by

$$-V_{CC} \le v_o \le V_{CC} \tag{5.4}$$

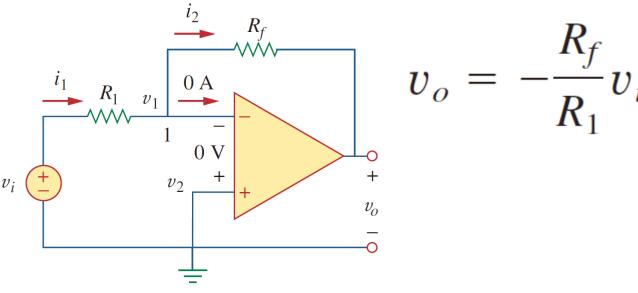
# **Basic Concept**



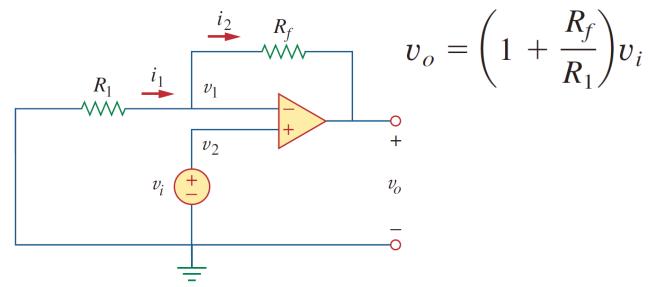
#### Figure 5.8

Ideal op amp model.

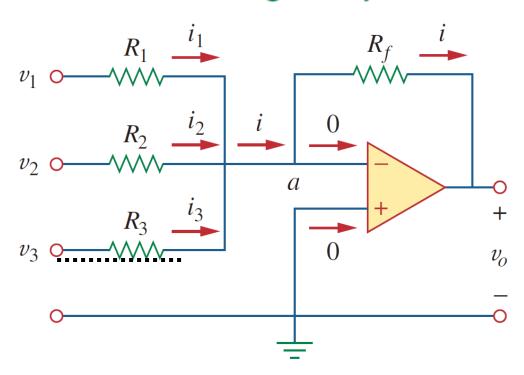
## Inverting Amplifier



#### Noninverting Amplifier

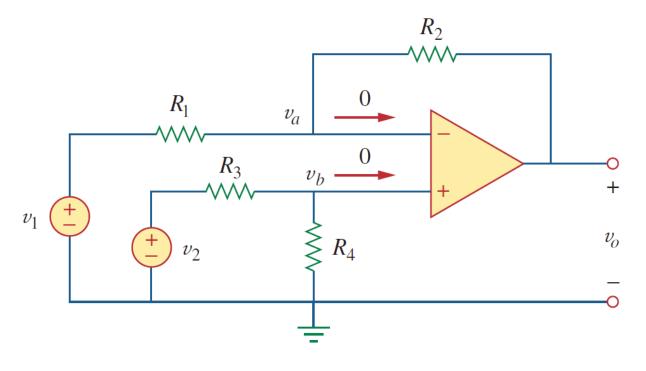


#### Summing Amplifier



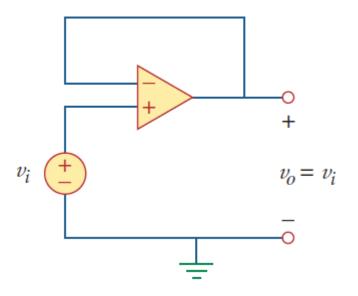
$$v_o = -\left(\frac{R_f}{R_1}v_1 + \frac{R_f}{R_2}v_2 + \frac{R_f}{R_3}v_3\right)$$

## Difference Amplifier

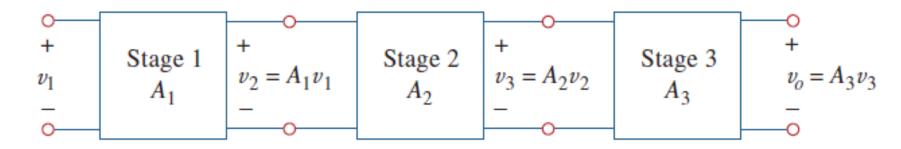


$$v_o = \frac{R_2(1 + R_1/R_2)}{R_1(1 + R_3/R_4)}v_2 - \frac{R_2}{R_1}v_1$$

The voltage follower.



#### Cascaded Op Amp Circuits



$$A = A_1 A_2 A_3$$

# **Sample Questions**

Figure 5.105 displays a two-op-amp instrumentation amplifier. Derive an expression for  $v_o$  in terms of  $v_1$  and  $v_2$ . How can this amplifier be used as a subtractor?

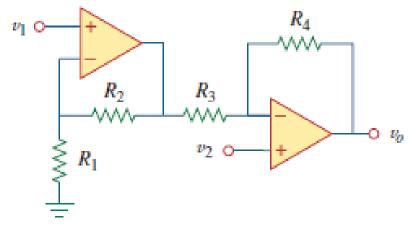


Figure 5.105

Find  $v_o$  in the op amp circuit of Fig. 5.92.

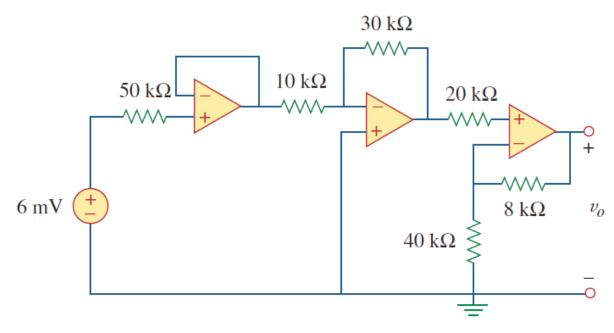
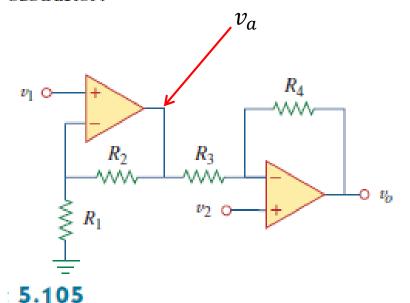


Figure 5.92

Figure 5.105 displays a two-op-amp instrumentation amplifier. Derive an expression for  $v_o$  in terms of  $v_1$  and  $v_2$ . How can this amplifier be used as a subtractor?



The output, v<sub>a</sub>, of the first op amp is,

$$v_a = (1 + (R_2/R_1))v_1 \tag{1}$$

Also, 
$$v_o = (-R_4/R_3)v_a + (1 + (R_4/R_3))v_2$$
 (2)

Substituting (1) into (2),

$$v_o = (-R_4/R_3) (1 + (R_2/R_1))v_1 + (1 + (R_4/R_3))v_2$$

Or, 
$$V_0 = (1 + (R_4/R_3))v_2 - (R_4/R_3 + (R_2R_4/R_1R_3))v_1$$

If 
$$R_4 = R_1$$
 and  $R_3 = R_2$ , then,  
 $v_0 = (1 + (R_4/R_3))(v_2 - v_1)$ 

which is a subtractor with a gain of  $(1 + (R_4/R_3))$ .

Find  $v_o$  in the op amp circuit of Fig. 5.92.

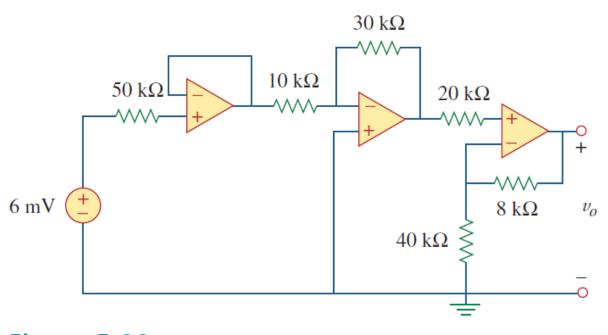


Figure 5.92

The output of the first op amp (to the left) is 6 mV. The second op amp is an inverter so that its output is

$$v_o' = -\frac{30}{10}(6\text{mV}) = -18\text{mV}$$

The third op amp is a noninverter so that

$$v_o' = \frac{40}{40 + 8} v_o \longrightarrow v_o = \frac{48}{40} v_o' = -21.6 \text{ mV}$$

# Thanks for Listening!