

首届CrachFEM失效模拟研讨会

1st ShareFEA CrachFEM Seminar

25 April 2018, Shanghai

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Modelling Non-Reinforced-, Fiber-Reinforced-Polymers and Composites with MF-GenYld+CrachFEM

1st ShareFEA CrachFEM Seminar, 25 April 2018, Shanghai

G. Oberhofer, H. Dell, M. Oehm

Authors

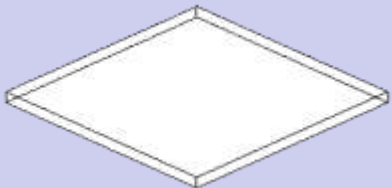
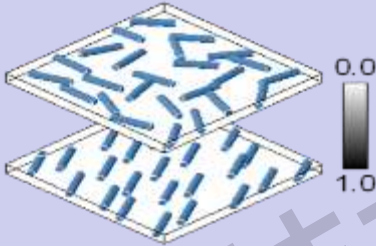
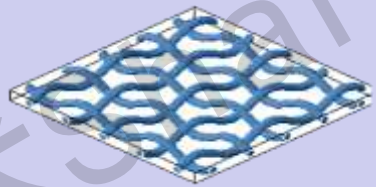
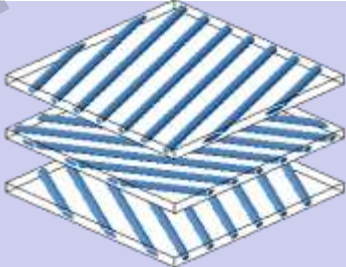
April 25, 2018

Date

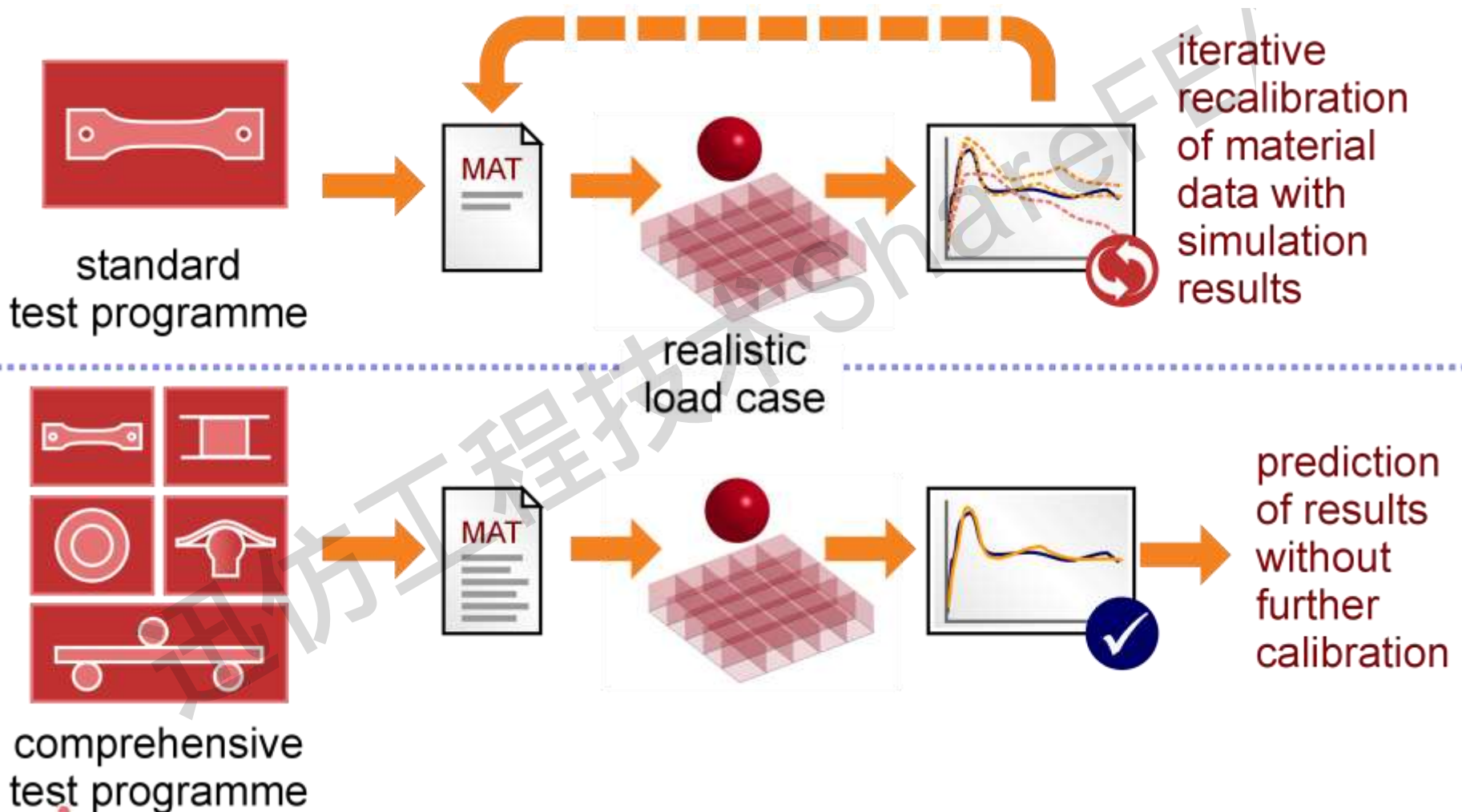
- ▶ Motivation
- ▶ MF-GenYld+CrachFEM for non-reinforced polymers
- ▶ MF-GenYld+CrachFEM for short fiber reinforced polymers
- ▶ MF-GenYld+CrachFEM for endless fiber reinforced polymers – Organic sheets
- ▶ MF-GenYld+CrachFEM for endless fiber reinforced composites (CFRP)
- ▶ Current developments
- ▶ Status of CrachFEM application

- ▶ **Motivation**
- ▶ MF-GenYld+CrachFEM for non-reinforced polymers
- ▶ MF-GenYld+CrachFEM for short fiber reinforced polymers
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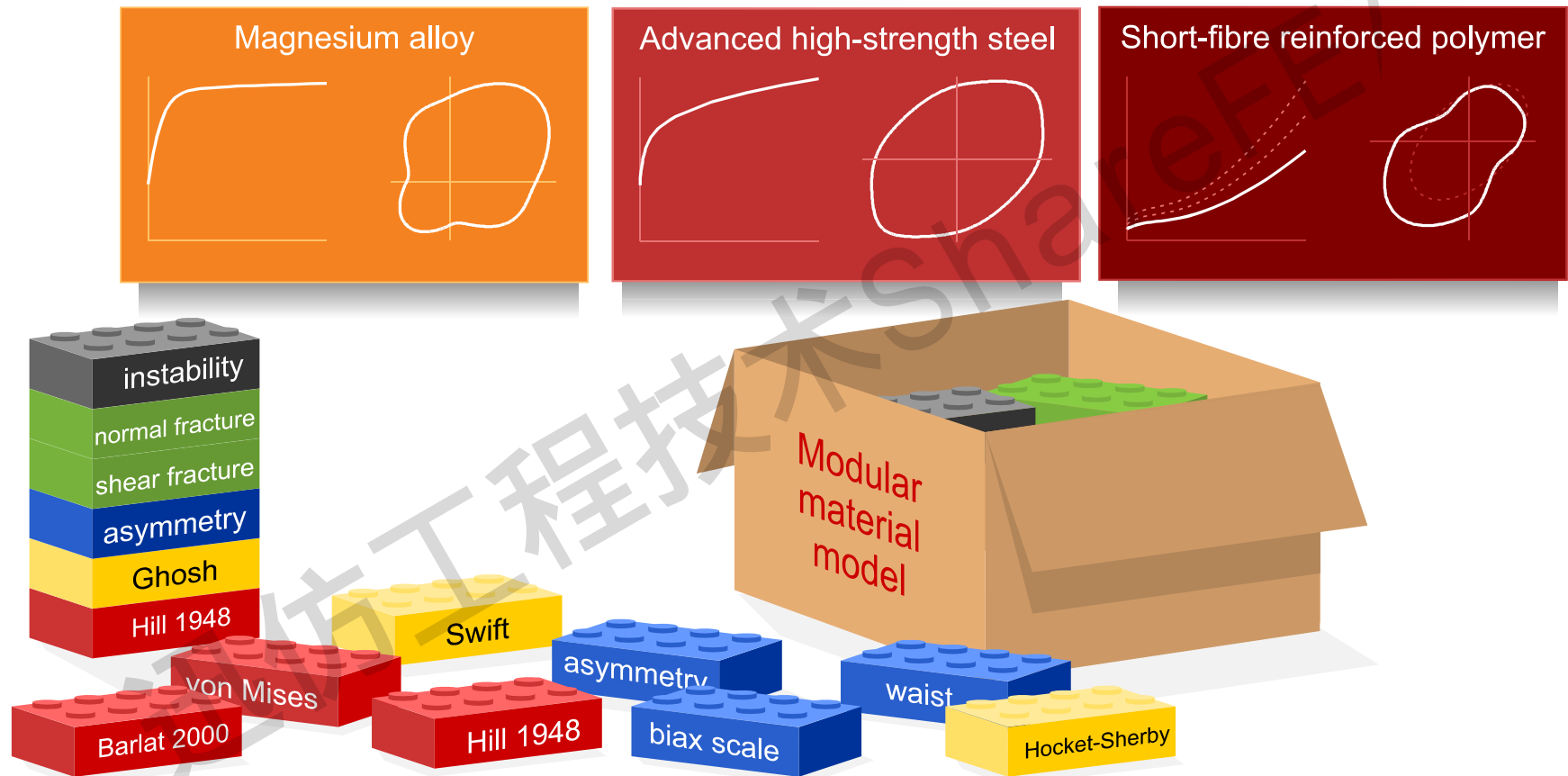
Different Classes of Polymers and Composites

Unreinforced polymers	Short-fiber-reinforced polymers	Endless-fiber-reinforced polymers	
		Organic fabric	Unidirectional layer
			
<ul style="list-style-type: none"> • High ductility (typically) • Stress state dep. hard • Compressibility • Ductile failure crit. suitable 	<ul style="list-style-type: none"> • Reduced ductility • Stress state dependent hardening • Anisotropy of elasticity • Anisotropy of hardening • Ductile failure criterion suitable • Anisotropy of fracture 	<ul style="list-style-type: none"> • Strongly reduced duct. in fiber directions • Significant ductility in other directions • Anisotropy of elasticity • Stress state dep. Hard • Anisotropy of hardening • Ductile failure criterion for ductile direction • Additional stress based failure crit. reasonable • Anisotropy of fracture 	<ul style="list-style-type: none"> • Generally very low ductility • Anisotropy of elasticity • Stress state dependent hardening • Anisotropy of hardening • Stress based failure criterion reasonable • Anisotropy of fracture

Predictive Material Description for Polymers and Composites



Modular Material Model MF-GenYld+CrachFEM



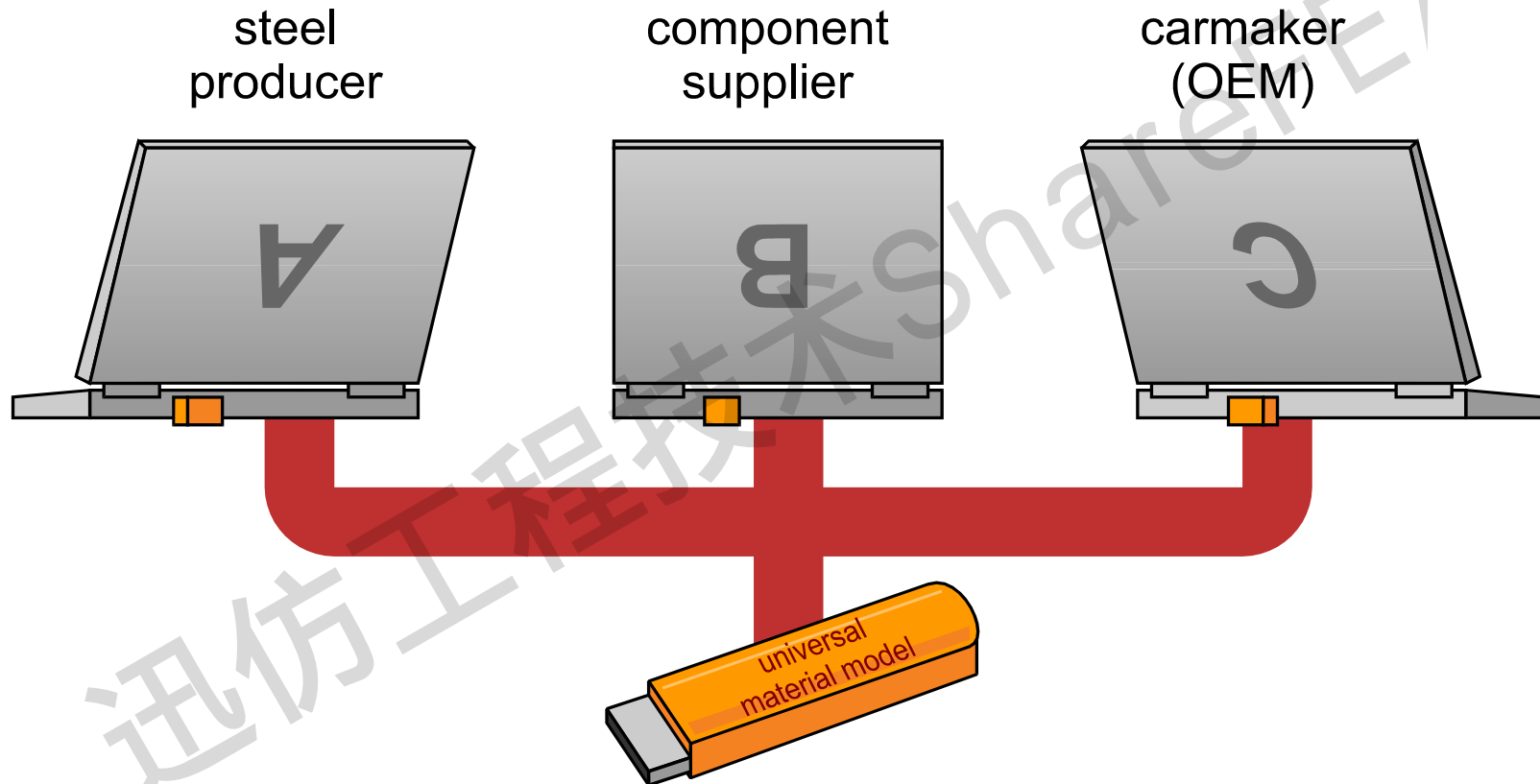
Modular Material Model MF-GenYld+CrachFEM for Polymers and Composites

MF-GenYld+CrachFEM		elastic behaviour	plastic behaviour	stress-space anisotropy	compressibility	normal fracture	shear fracture	stress-based criterion	
									supported
									under development
									not available
isotropic									
orthotropic									
generally anisotropic									
strain-rate dependent									
strain dependent									

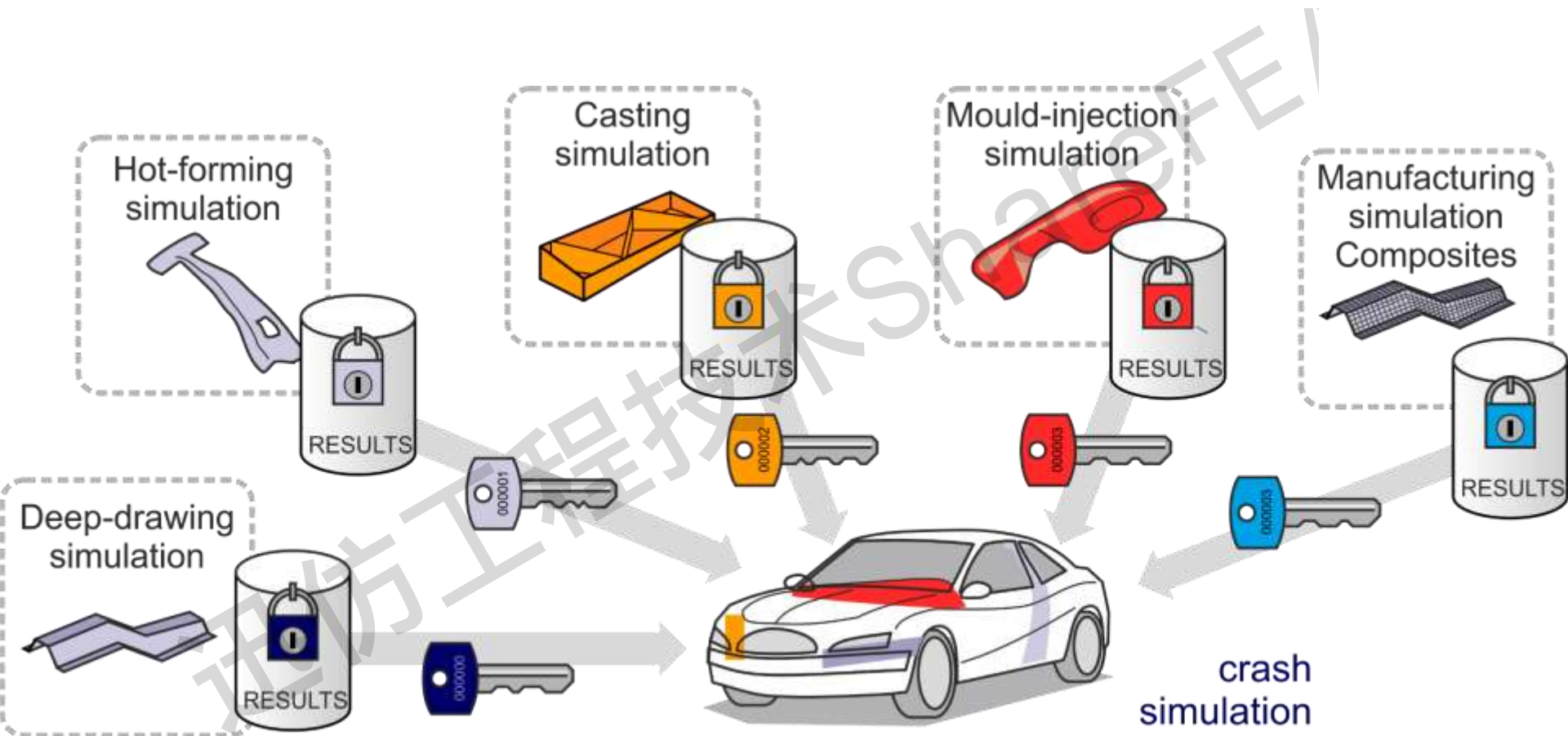
supported
 under development
 not available

LS-Dyna
 Abaqus
 PAM-Crash
 PAM-Stamp
 Radioss

Modular Material Model MF-GenYld+CrachFEM for polymers and CFRPs

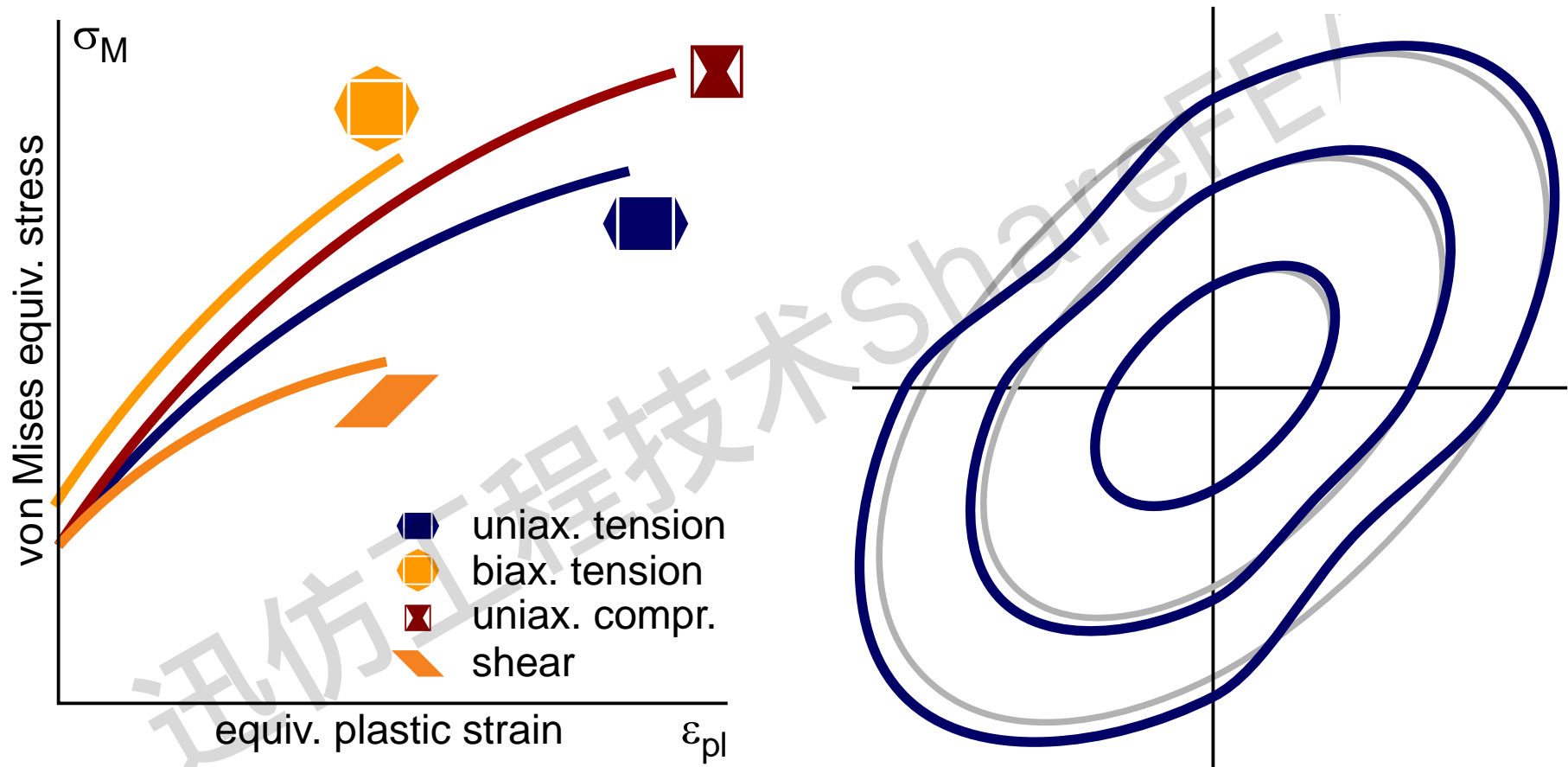


Modular Material Model MF-GenYld+CrachFEM for polymers and CFRPs



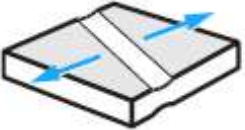










- ▶ Motivation
- ▶ **MF-GenYld+CrachFEM for non-reinforced polymers**
- ▶ MF-GenYld+CrachFEM for short fiber reinforced polymers
- ▶ MF-GenYld+CrachFEM for endless fiber reinforced polymers – Organic sheets
- ▶ MF-GenYld+CrachFEM for endless fiber reinforced composites (CFRP)
- ▶ Current developments
- ▶ Status of CrachFEM application in European OEMs

Anisotropic hardening



Austenitic steel sheets, magnesium sheets and polymers show marked anisotropic hardening

Ductile fracture behaviour

			shell	solid
	Local instability (necking)	Initial FLC (approximate)		(1)
		Prediction with Crach		(1)
		Post-critical elongation		(1)
	Ductile normal fracture	$\varepsilon_{eq}^{**} = \varepsilon_{eq}^{**}(\eta)$		(2)
		$\varepsilon_{eq}^{**} = \varepsilon_{eq}^{**}(\beta)$		
	Ductile shear fracture	$\varepsilon_{eq}^{**} = \varepsilon_{eq}^{**}(\theta)$		

Currently not used for polymers




















































2D: shells

3D: solid elements

(1) not reasonable

(2) not recommended

Relevant Modules

MF-GenYld+CrachFEM		elastic behaviour	plastic behaviour	stress-space anisotropy	compressibility	normal fracture	shear fracture	stress-based criterion	
									
isotropic									 LS-Dyna
orthotropic									
generally anisotropic									 Abaqus
strain-rate dependent									
strain dependent									 PAM-Crash PAM-Stamp
									 Radioss

Influence of compressibility onto failure in case of non-reinforced polymers

Tensile-Test_DIN-EN-ISO_8256_Type3 v=0.5 mm/ms
Time = 0.15
Contours of Effective Plastic Strain
max IP. value
min=0, at elem# 25
max=2.52093, at elem# 245

Plastic compressibility



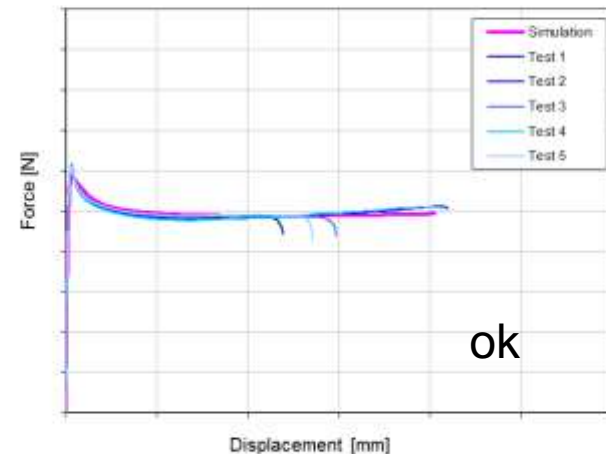
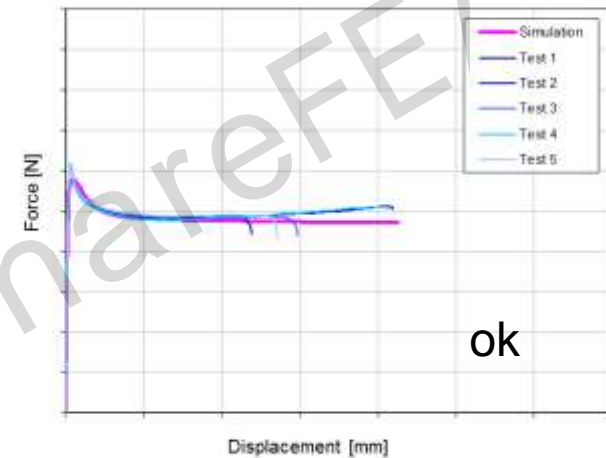
Tensile-Test_DIN-EN-ISO_8256_Type3 v=0.5 mm/ms
Time = 0.15
Contours of Effective Plastic Strain
max IP. value
min=0, at elem# 25
max=1.80544, at elem# 241

Plastic incompressibility



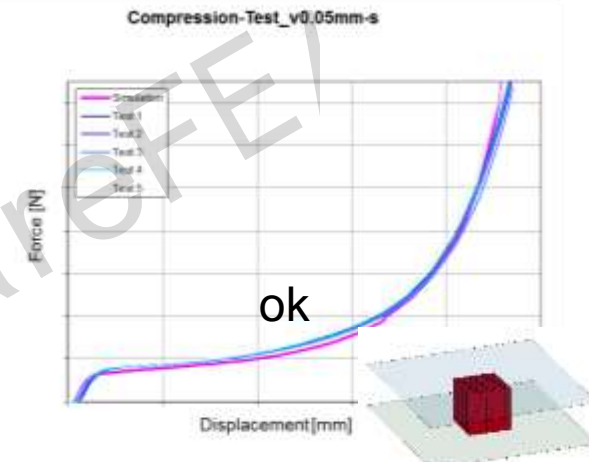
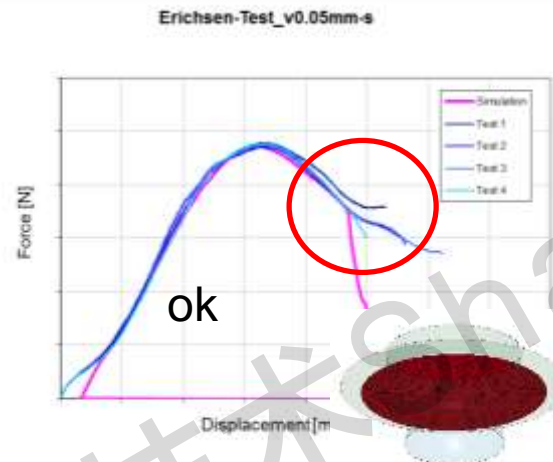
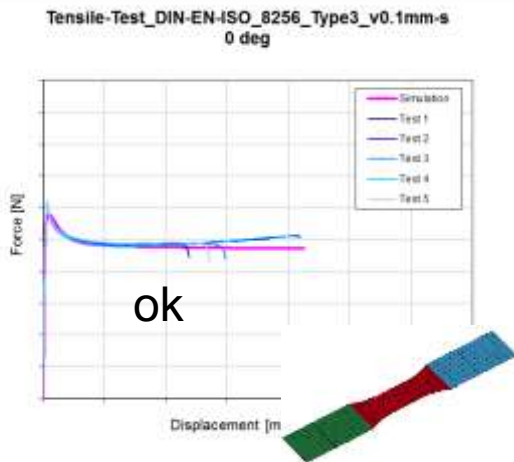
➔ Failure behaviour in case of uniaxial tension ok for both representations

Tensile-Test_DIN-EN-ISO_8256_Type3_v0.1mm-s
0 deg

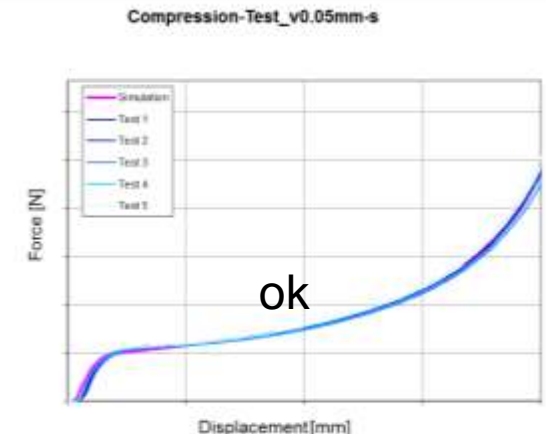
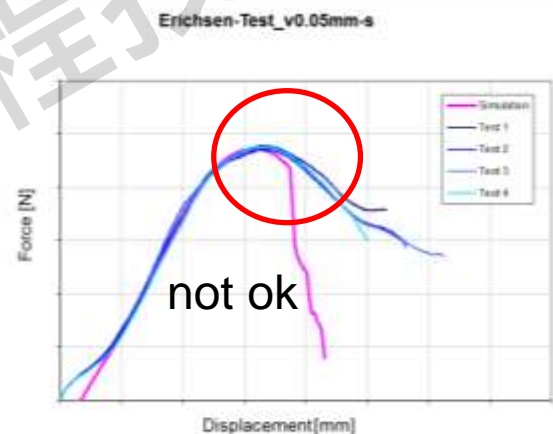
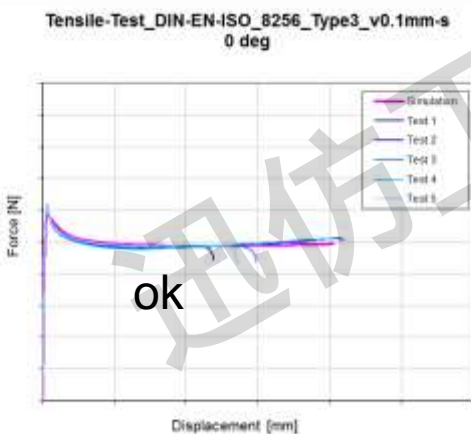


Influence of compressibility onto failure in case of non-reinforced polymers

Plastic compressible



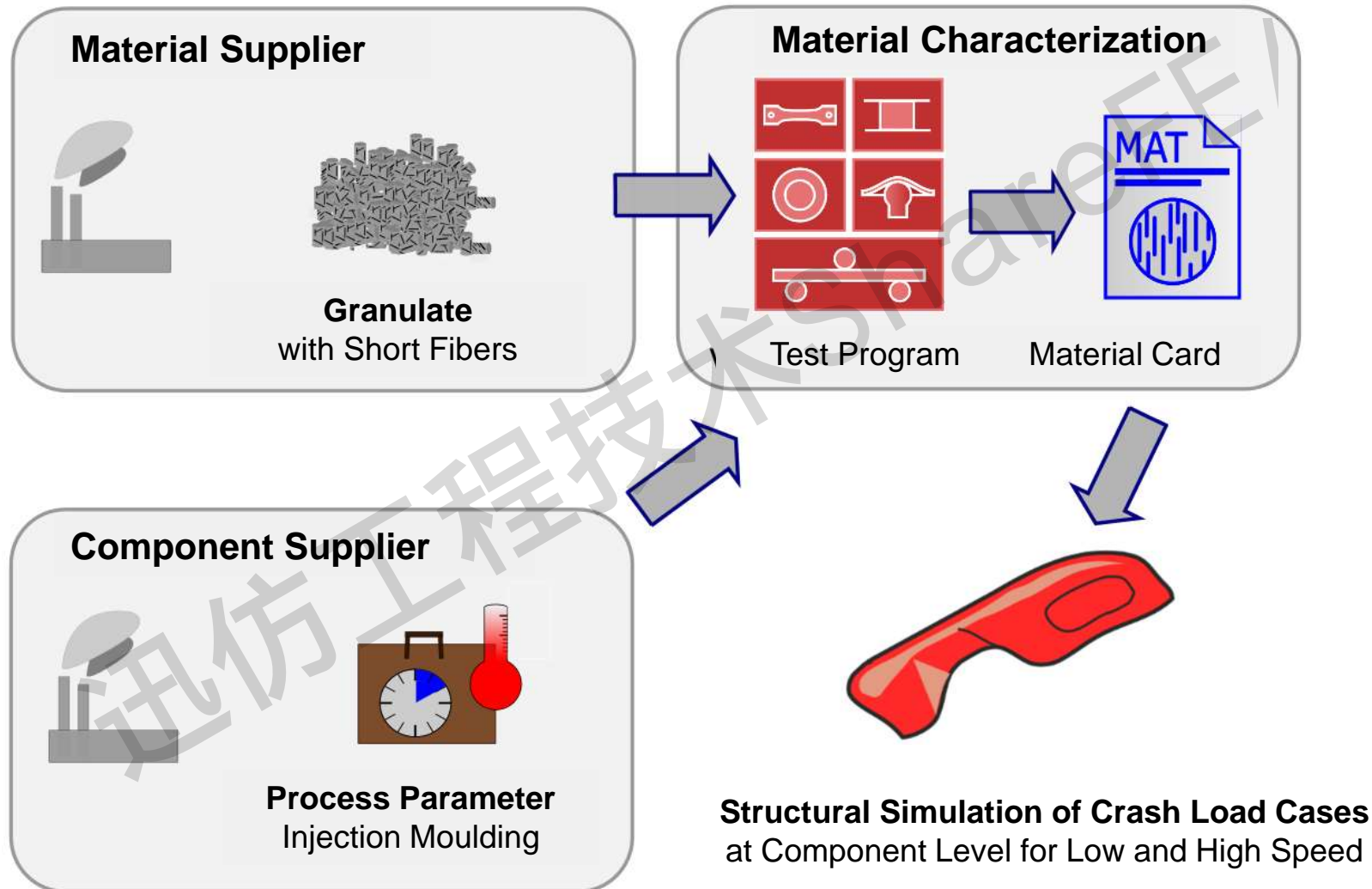
Plastic incompressible



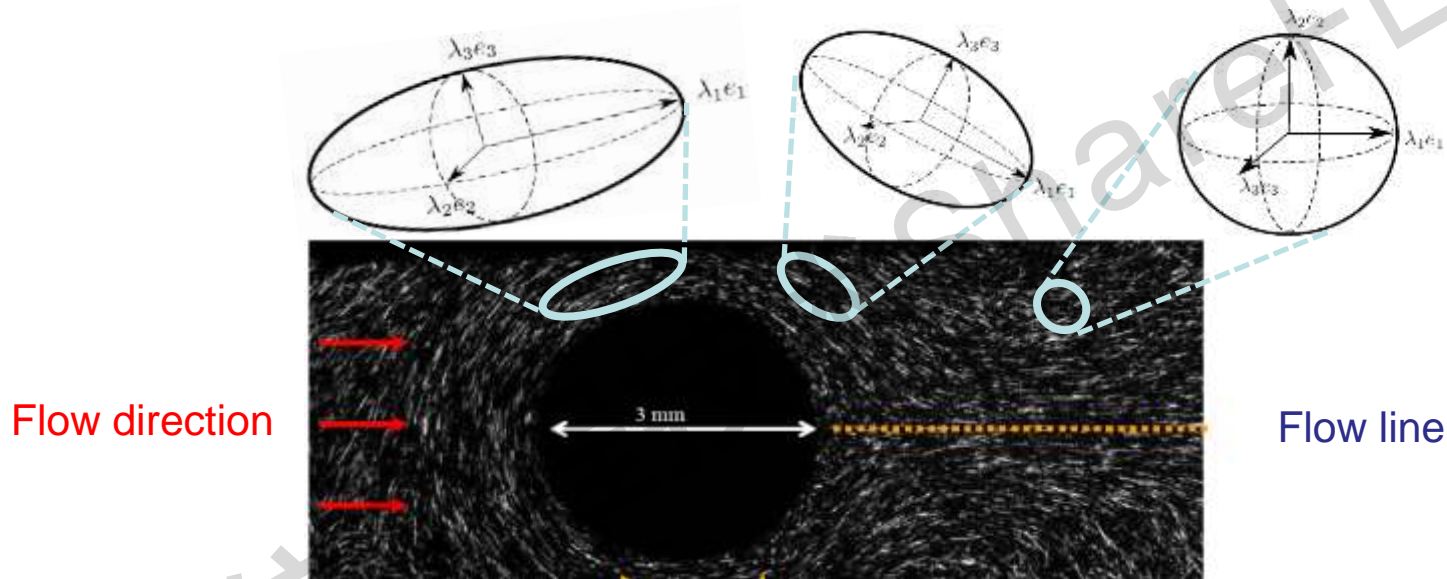
➡ Not all stress states can be described well with the incompressible approach

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Influence of production process



Mapping from mould injection simulation



CT-Scan of an injection moulded plate with barrier and flow line

Quelle: M. Vogler „New Material modeling approaches for thermoplastics, composites and organic sheet“, 9th European LS-Dyna Conference 2013

Relevant Modules

MF-GenYld+CrachFEM		elastic behaviour	plastic behaviour	stress-space anisotropy	compressibility	normal fracture	shear fracture	stress-based criterion	
isotropic									
orthotropic									
generally anisotropic									
strain-rate dependent									
strain dependent									
									supported under development not available activated
									LS-Dyna Abaqus PAM-Crash PAM-Stamp Radioss

Anisotropic behaviour in case of short fiber reinforced Polymers

Random
Fiber Orientation

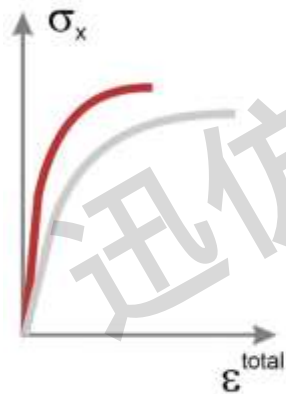


Unidirectional
Fiber Orientation

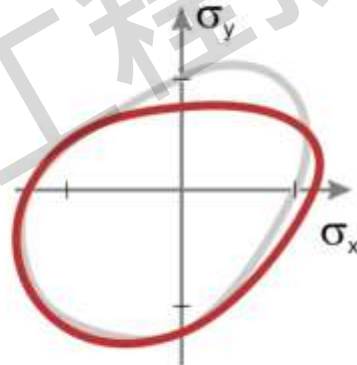


MF GenYld+CrachFEM supports automatic interpolation between different states

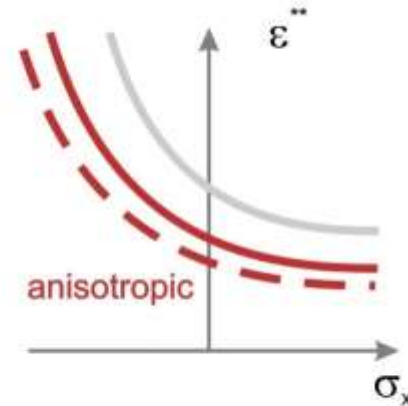
Elasticity / Hardening



Yield Locus



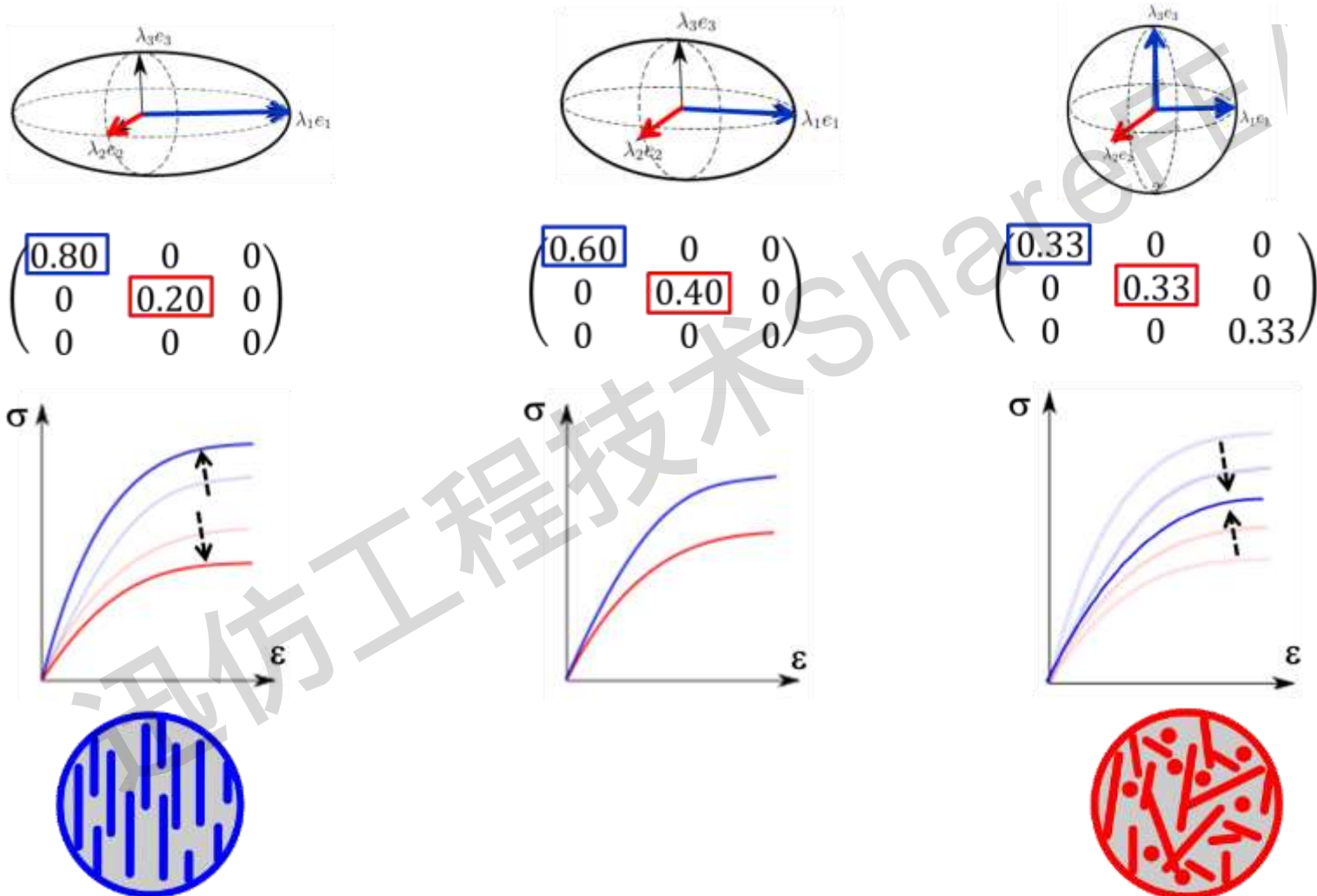
Fracture



— High degree of orient. — High degree of orient.

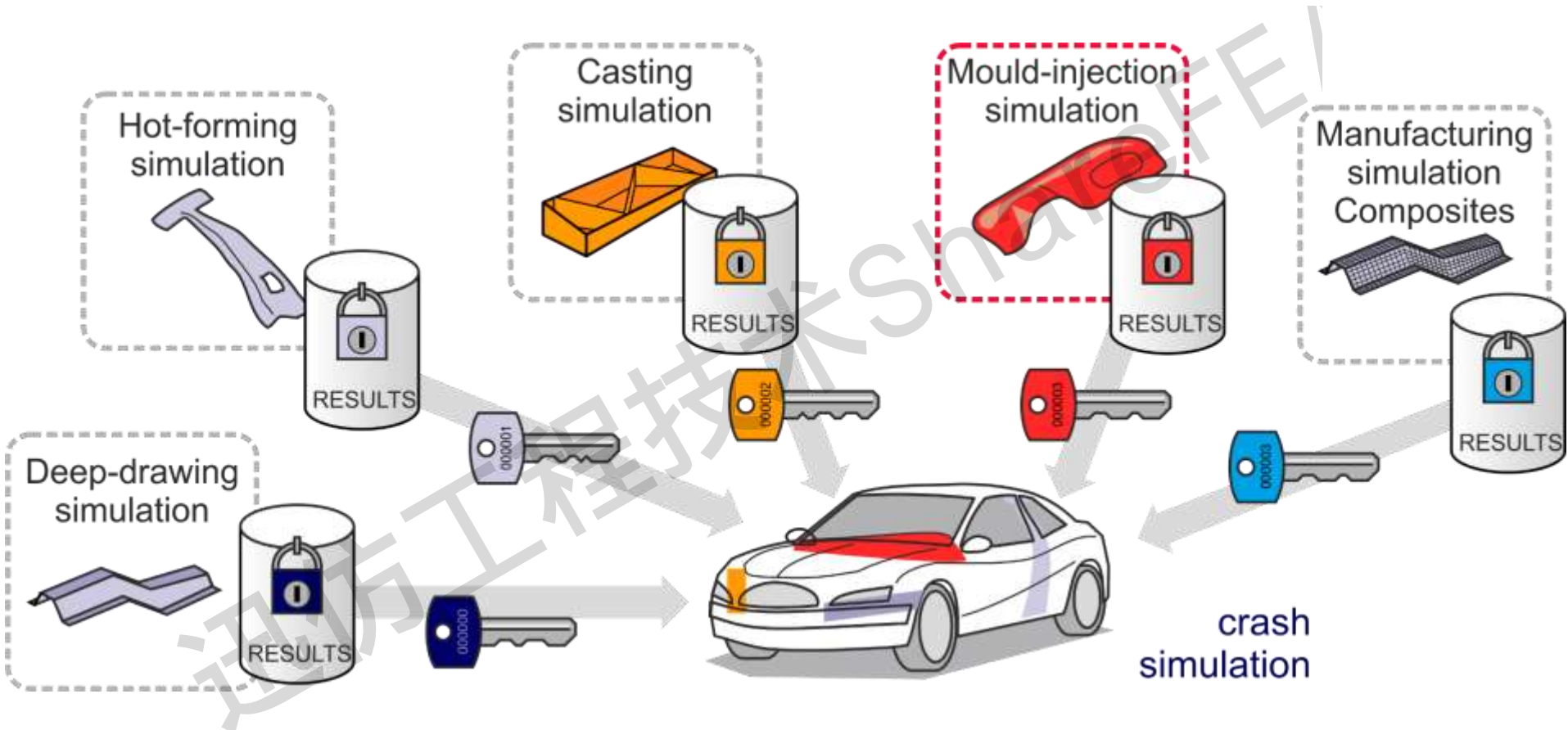
x = fiber direction

Mapping from mould injection simulation – Orientation tensor



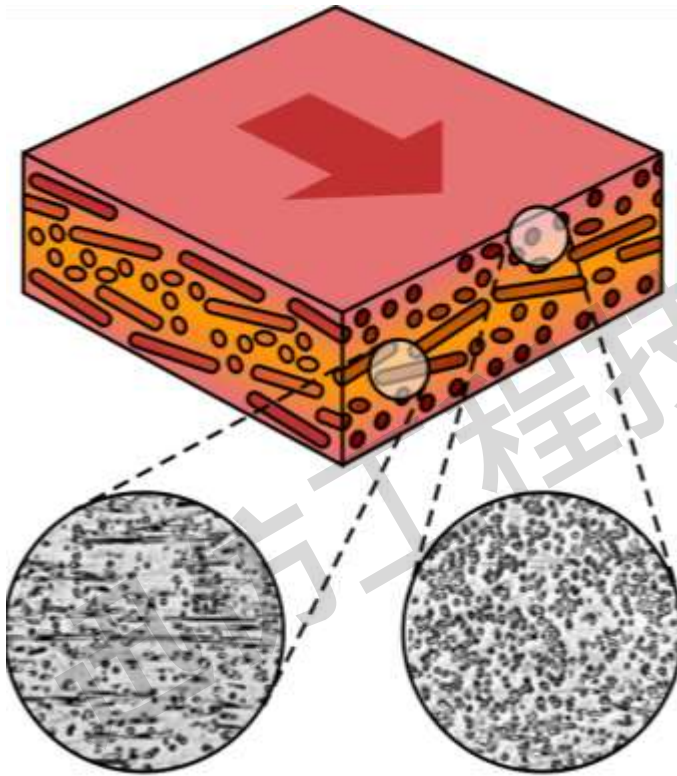
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Mapping from mould injection simulation

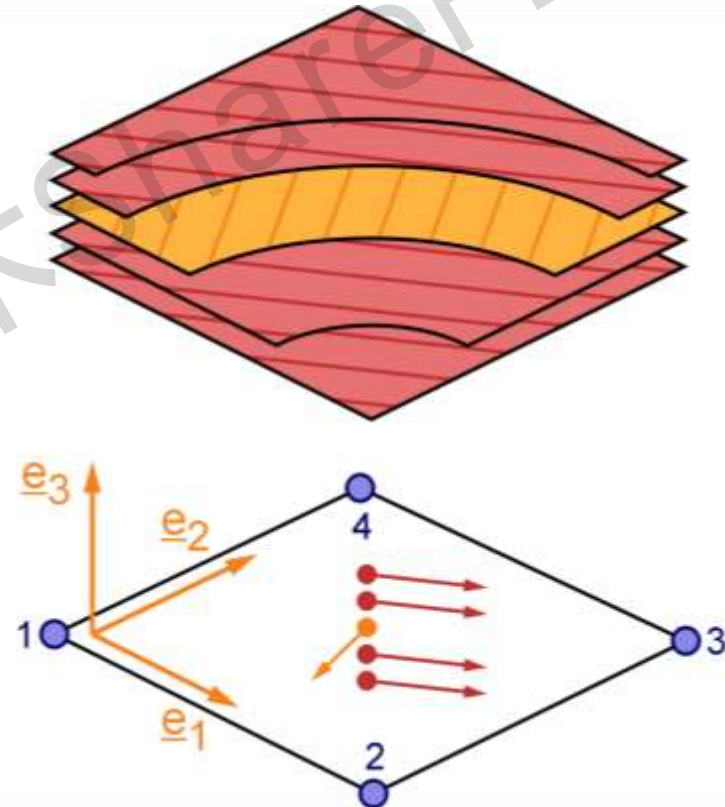


Mapping from mould injection simulation

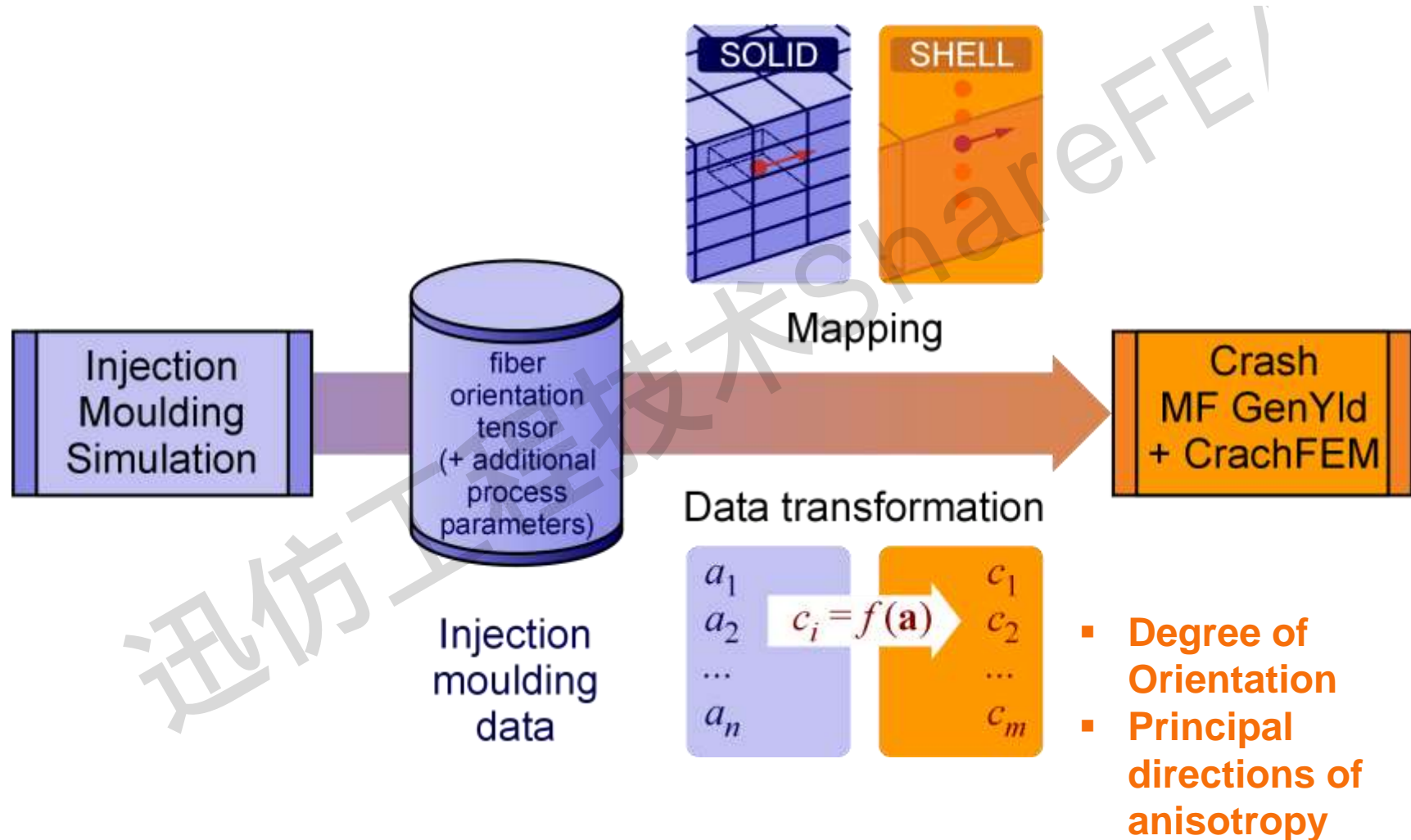
Different orientation of fibers over wall thickness resulting from material flow



Initialization of material orthotropy for different integration points of shell elements over thickness




















































Mapping from mould injection simulation

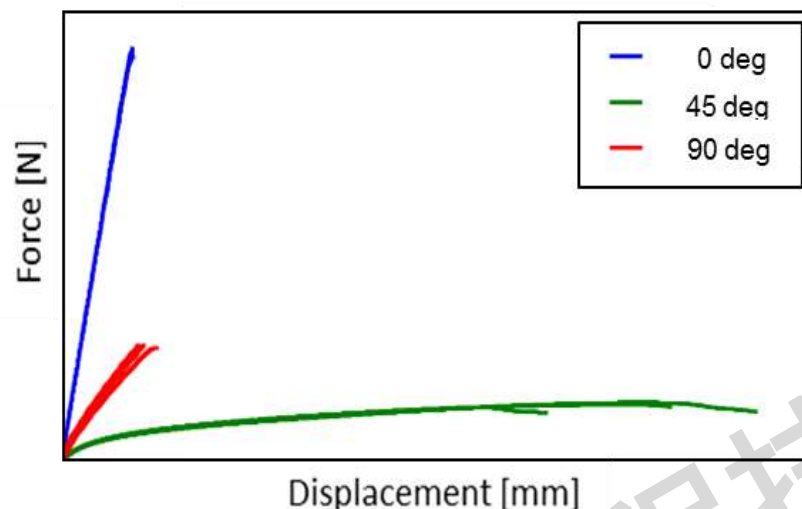


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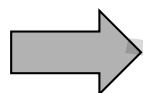
Relevant Modules

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strain-rate dependent									
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Characteristic Tensile Behavior



- Strongly reduced ductility in fiber directions
- Significant ductility in other directions
- Anisotropy of elasticity
- Stress state dependent hardening
- Anisotropy of hardening
- Ductile failure criterion suitable for ductile direction
- Additional stress based failure criterion reasonable
- Anisotropy of fracture

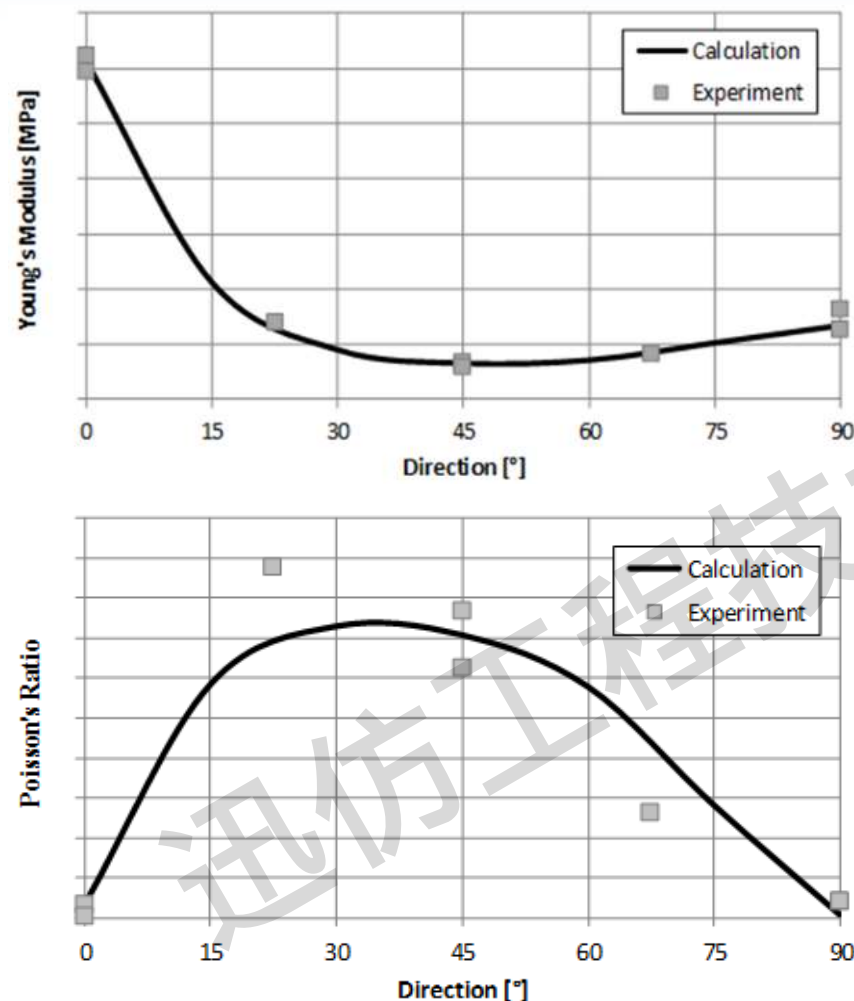


Challenging behavior for material model with respect to elasto-plastic and failure behavior

Behavior can be different between tension and compression

Source: M. Franzen et al.; Improved Crash Simulation of Continuous-Fiber-Reinforced Thermoplastics: Organic Sheets; International Congress „Kunststoffe im Automobilbau“ March 28/29, 2017, Mannheim

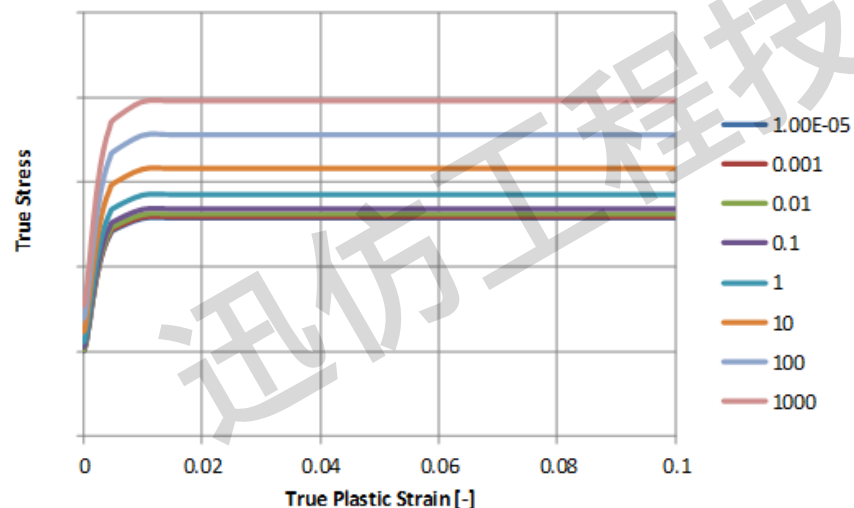
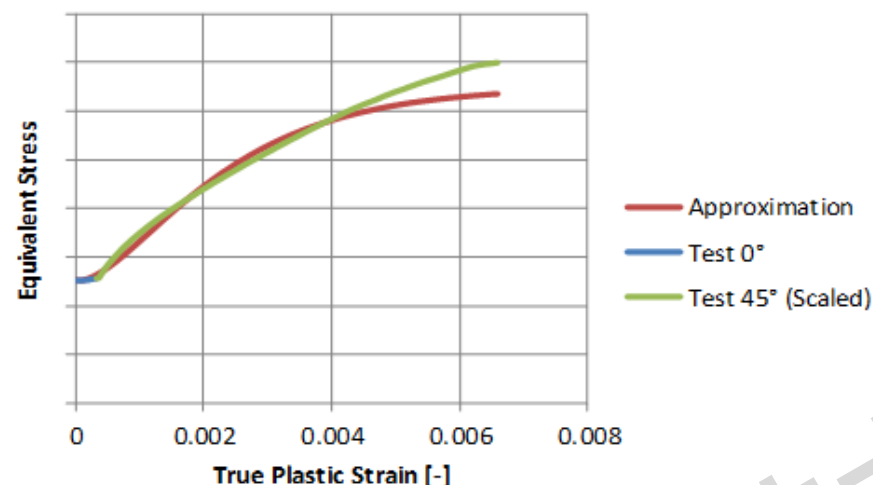
Elastic Material Behavior



- Elastic behavior is assumed to be linear
- A significant rate dependency has not been observed
- Due to the different fiber density in 0° and 90° orientation the Young's modulus differs significantly in these orientations

Source: M. Franzen et al.; Improved Crash Simulation of Continuous-Fiber-Reinforced Thermoplastics: Organic Sheets; International Congress „Kunststoffe im Automobilbau“ March 28/29, 2017, Mannheim

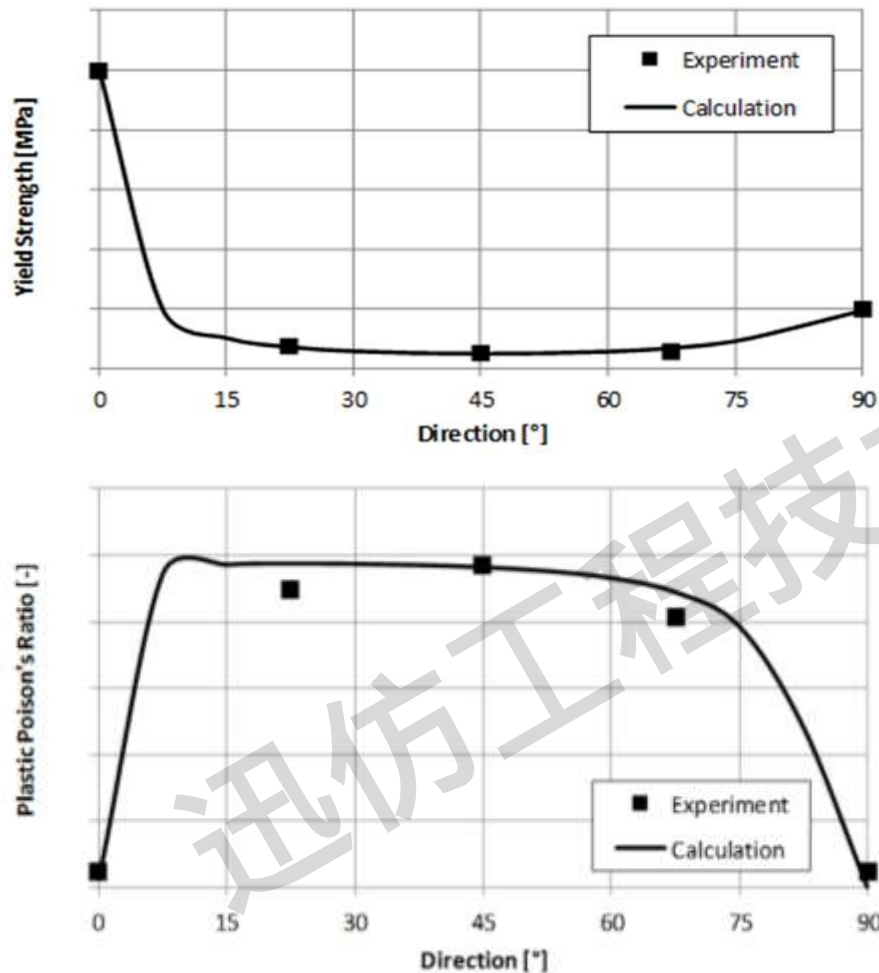
Elasto-Plastic Material Behavior



- Reference hardening curve is hardening curve for uniaxial tension in 0°
- Experimentally determined hardening curve is approximated and extrapolated to higher strains
- Based on tensile tests at different strain rates the yield strength is defined as a function of plastic strain and strain rate
- Even though failure in uniaxial tension happens at very low plastic strains the reference curves must be defined up to high plastic strains due to high fracture strains for other loadings

Source: M. Franzen et al.; Improved Crash Simulation of Continuous-Fiber-Reinforced Thermoplastics: Organic Sheets; International Congress „Kunststoffe im Automobilbau“ March 28/29, 2017, Mannheim

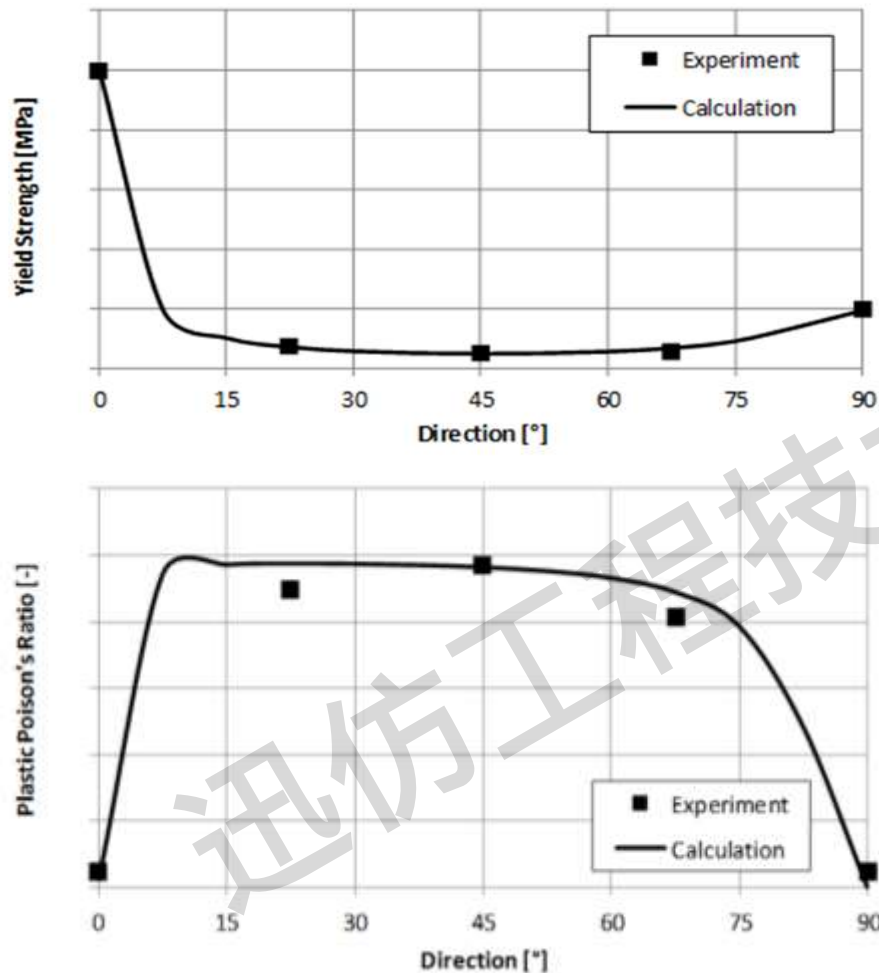
Elasto-Plastic Material Behavior



- Plastic orthotropy is characterized by direction dependency of yield strength and plastic Poisson's ratio
- Due to the different fiber density in 0° and 90° orientation the yield strength differs significantly in these orientations

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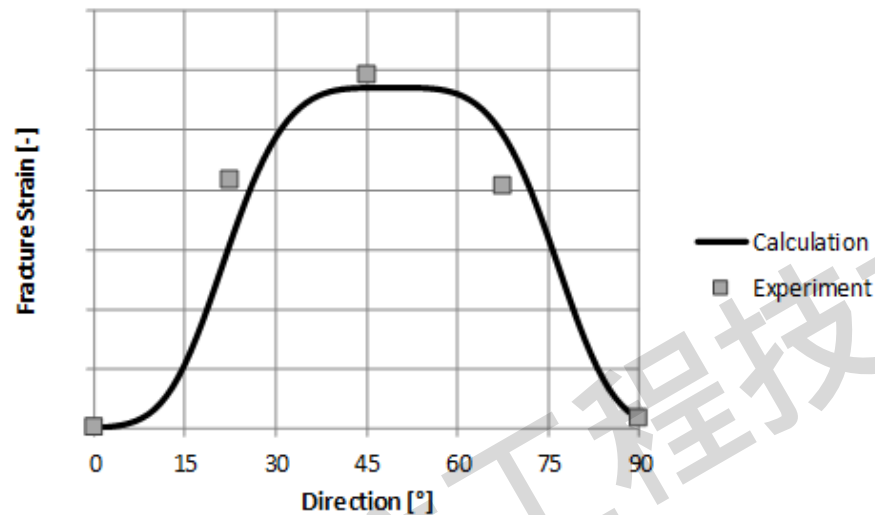
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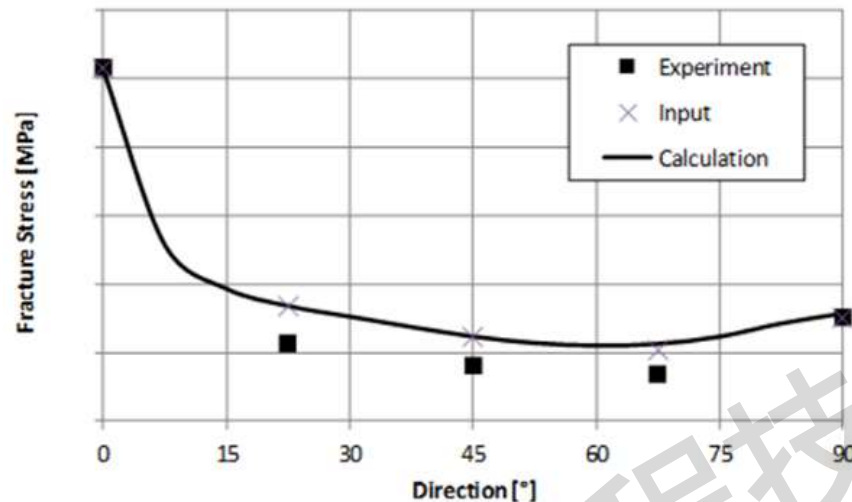
Strain Based Failure Behavior



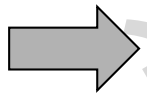
- Comparatively ductile behavior for loading angles beyond fiber orientation
- Comparatively brittle behavior in fiber orientation
- Purely strain based failure criteria can cause problems in the vicinity of the fiber orientation causing an unphysical brittle behavior

Source: M. Franzen et al.; Improved Crash Simulation of Continuous-Fiber-Reinforced Thermoplastics: Organic Sheets; International Congress „Kunststoffe im Automobilbau“ March 28/29, 2017, Mannheim

Stress Based Failure Behavior



- Comparatively ductile behavior for loading angles beyond fiber orientation
- Comparatively brittle behavior in fiber orientation
- Purely stress based failure criteria can cause problems in ductile orientation as the hardening behavior is very low (stress based criteria 'unsharp')



The use of stress based criteria in combination with strain based criteria is used further on and gives promising results

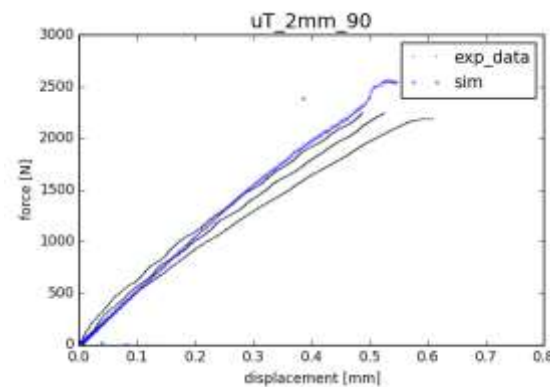
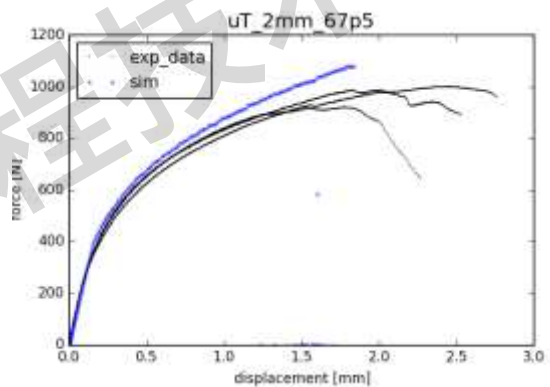
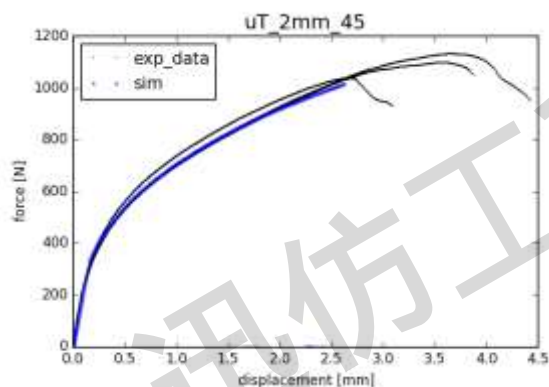
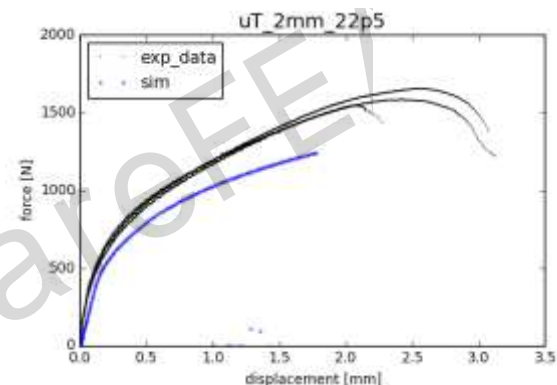
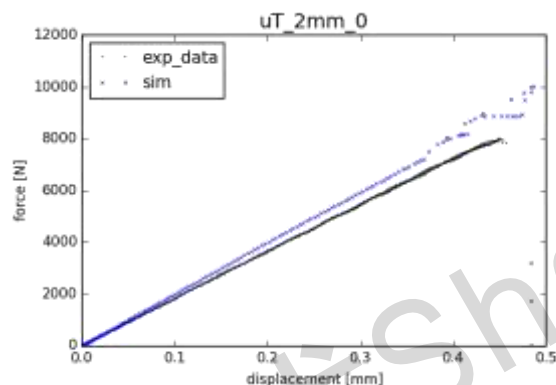
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Tensile Tests (Different Orientations)

Simulation
Experiment

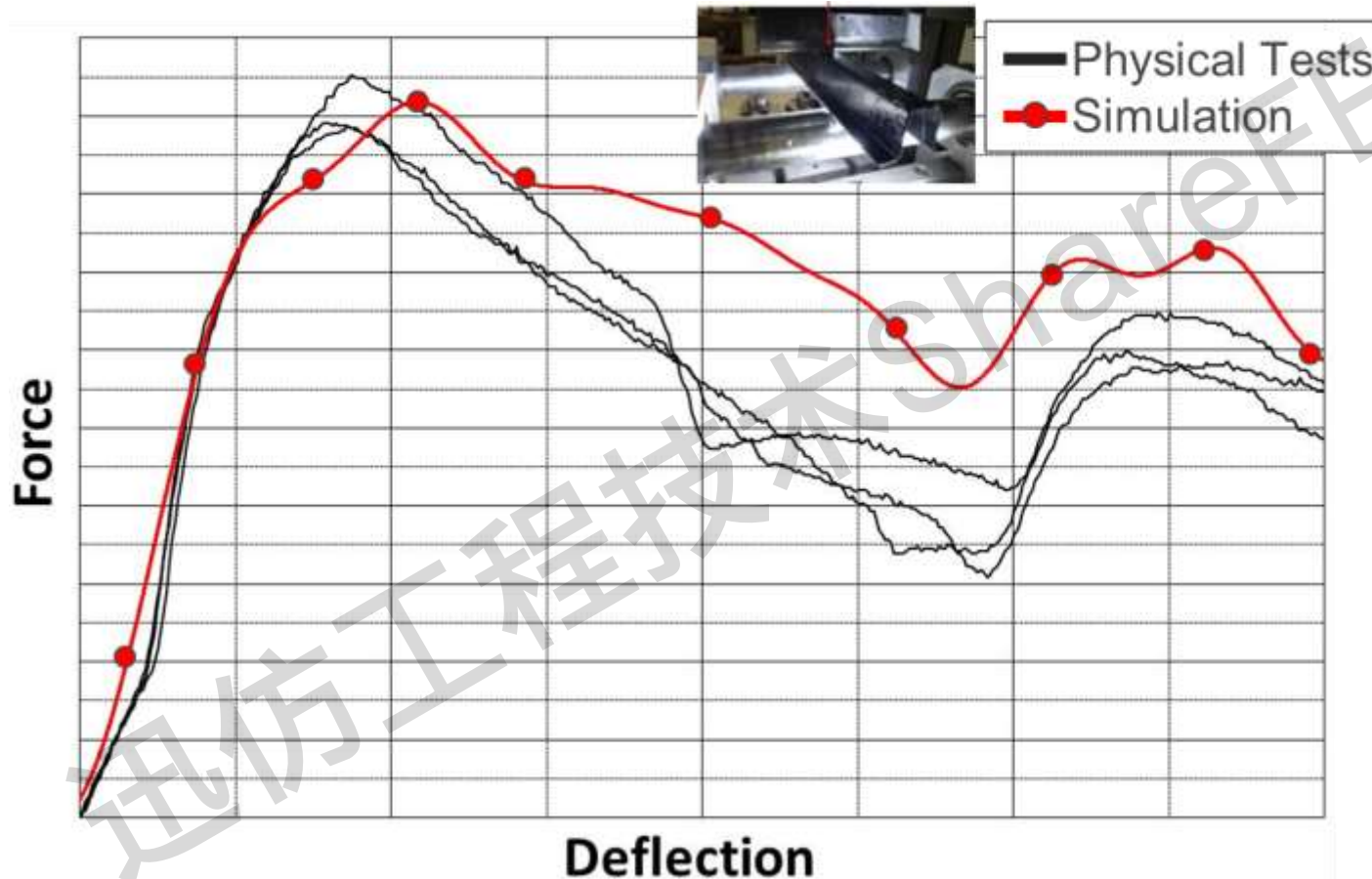


LS-DYNA
Shell Elements
Element length: 2 mm



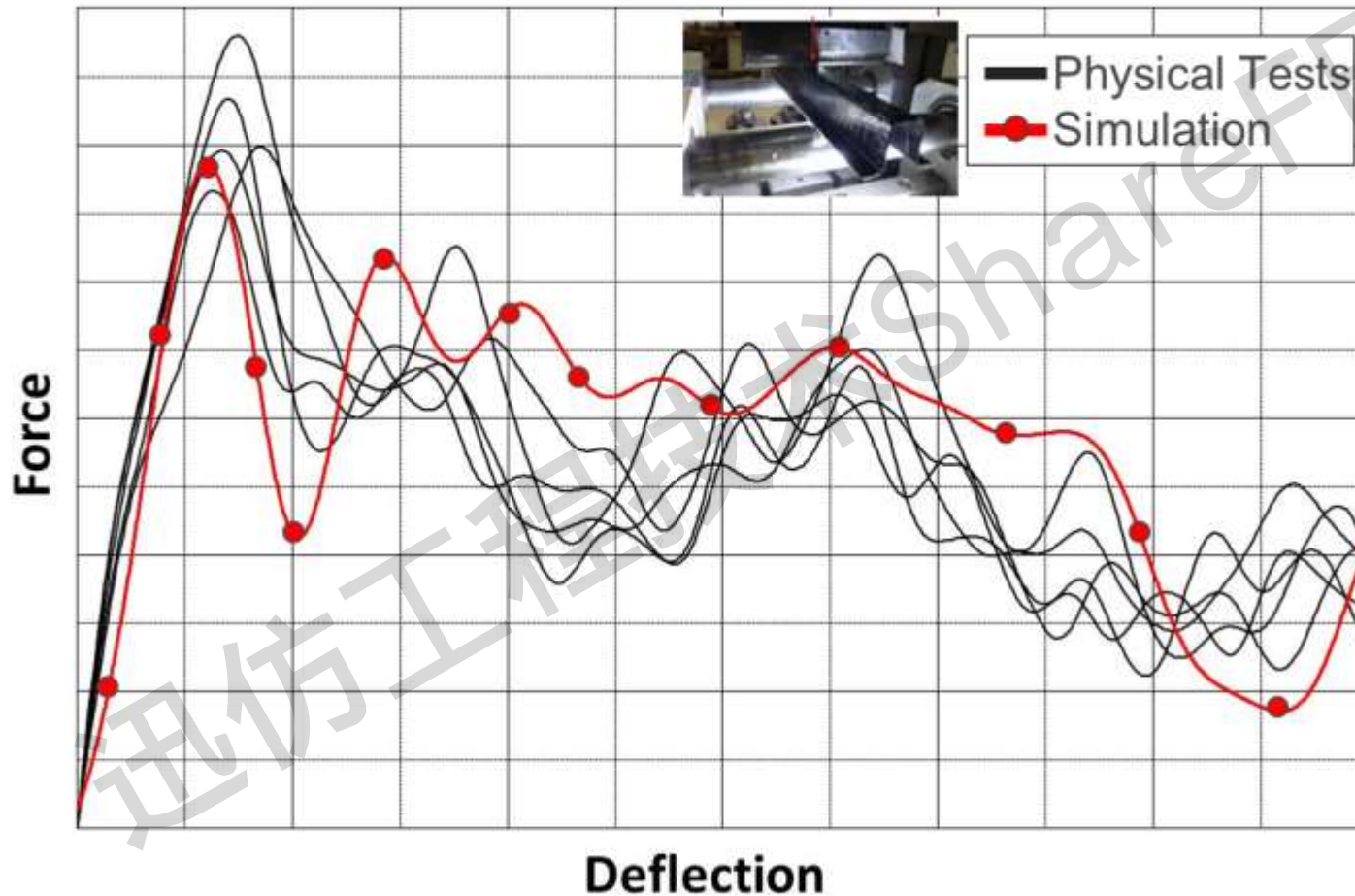
Source: M. Franzen et al.; Improved Crash Simulation of Continuous-Fiber-Reinforced Thermoplastics: Organic Sheets; International Congress „Kunststoffe im Automobilbau“ March 28/29, 2017, Mannheim

Component Validations – quasi static – 3-Point-Bending - 80/20



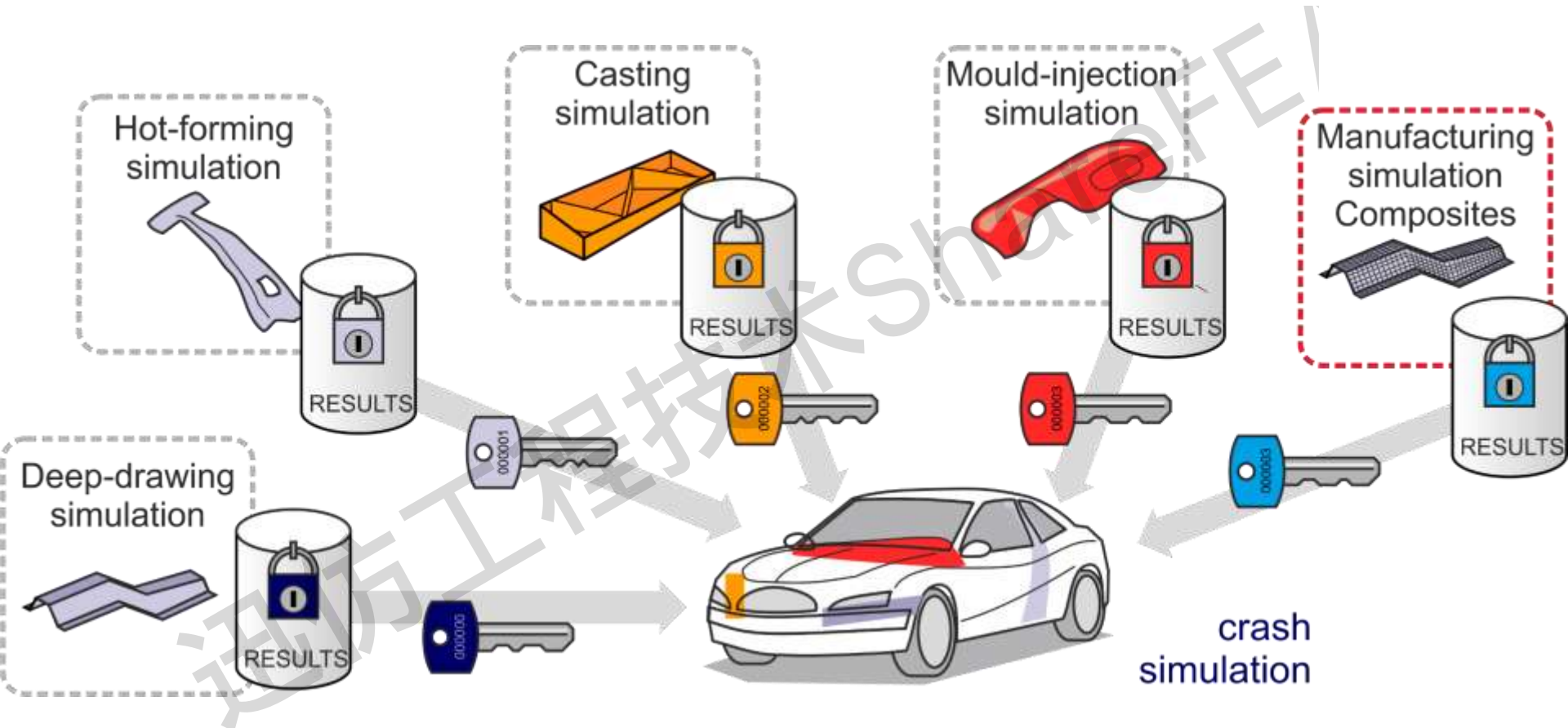
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Component Validations – dynamic – 3-Point-Bending - 80/20



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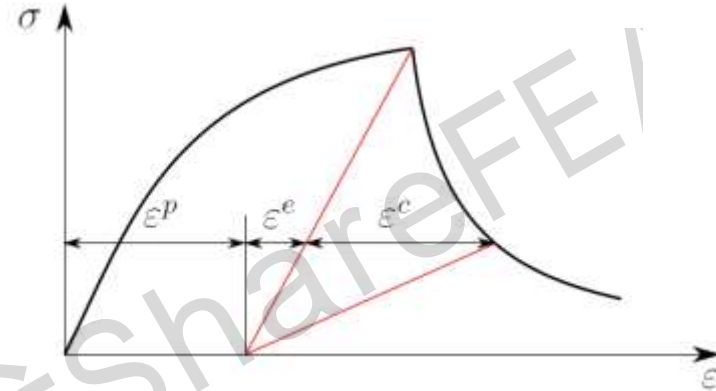
Mapping from manufacturing simulation



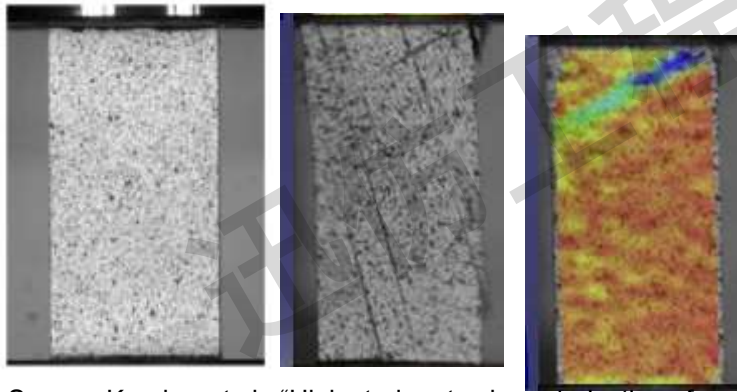
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Schematic Material Behaviour

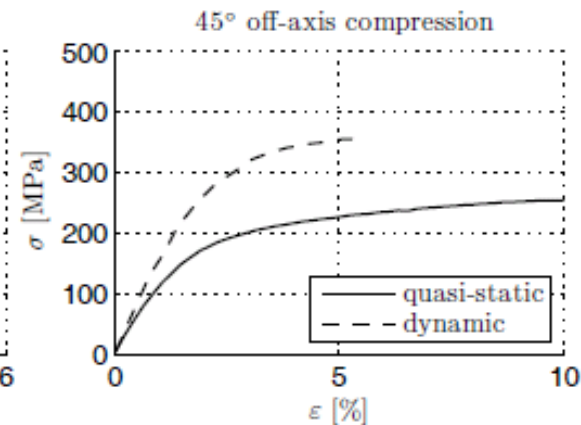
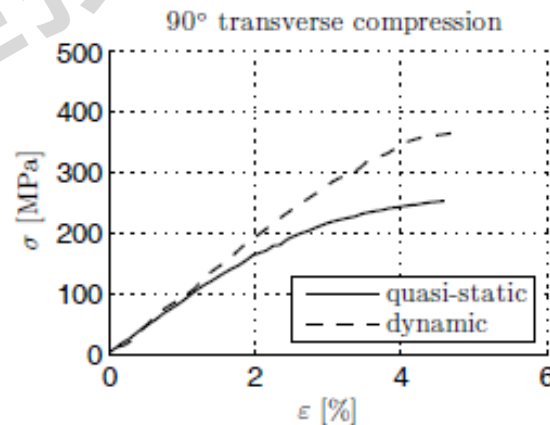
- Prefailure nonlinearities
- Fracture behavior
























































Quasi-static and dynamic off-axis compression tests



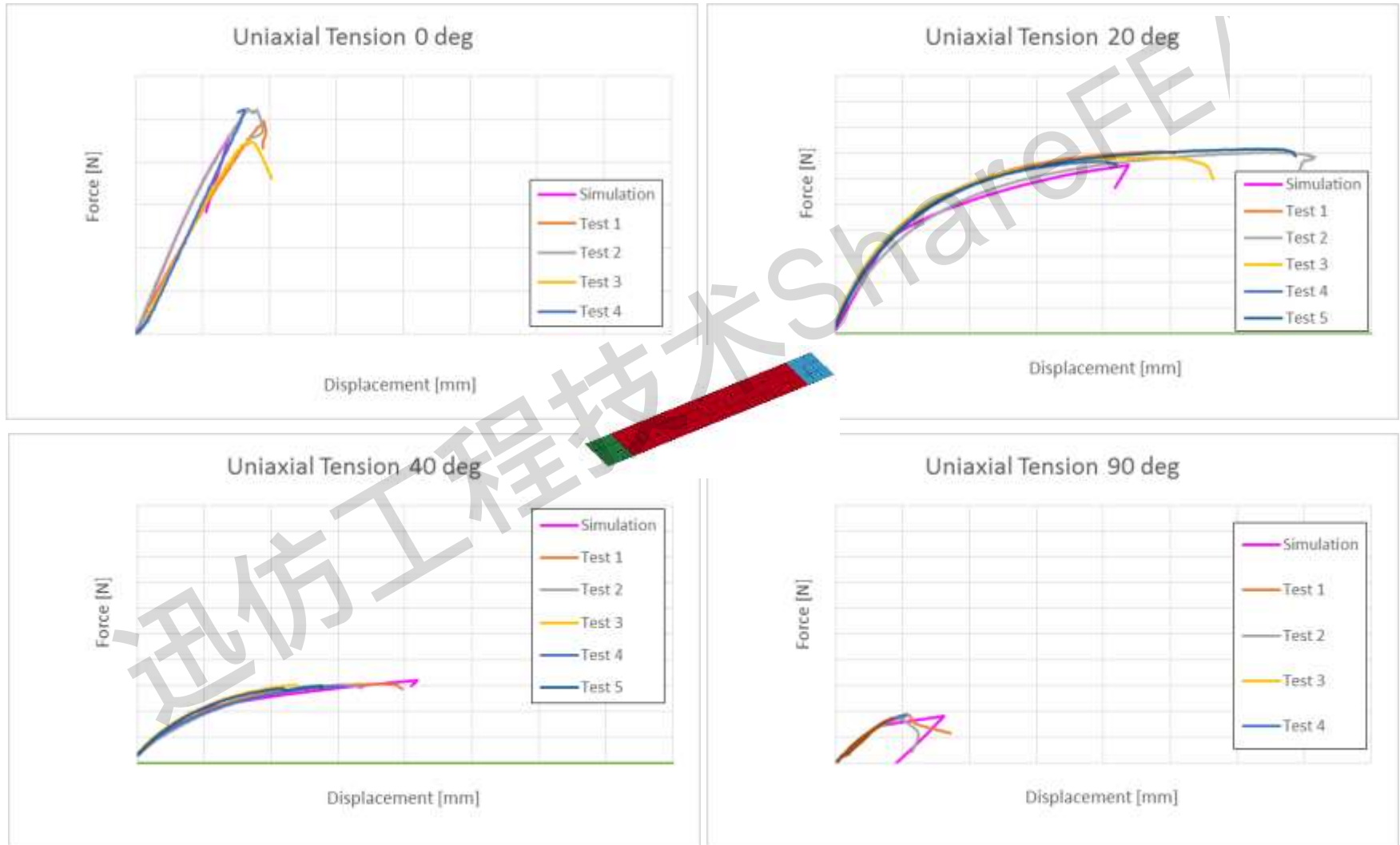
Source: Koerber et al.: "High strain rate characterisation of unidirectional carbon-epoxy IM7-8552 in transverse compression and in-plane shear using digital image correlation"



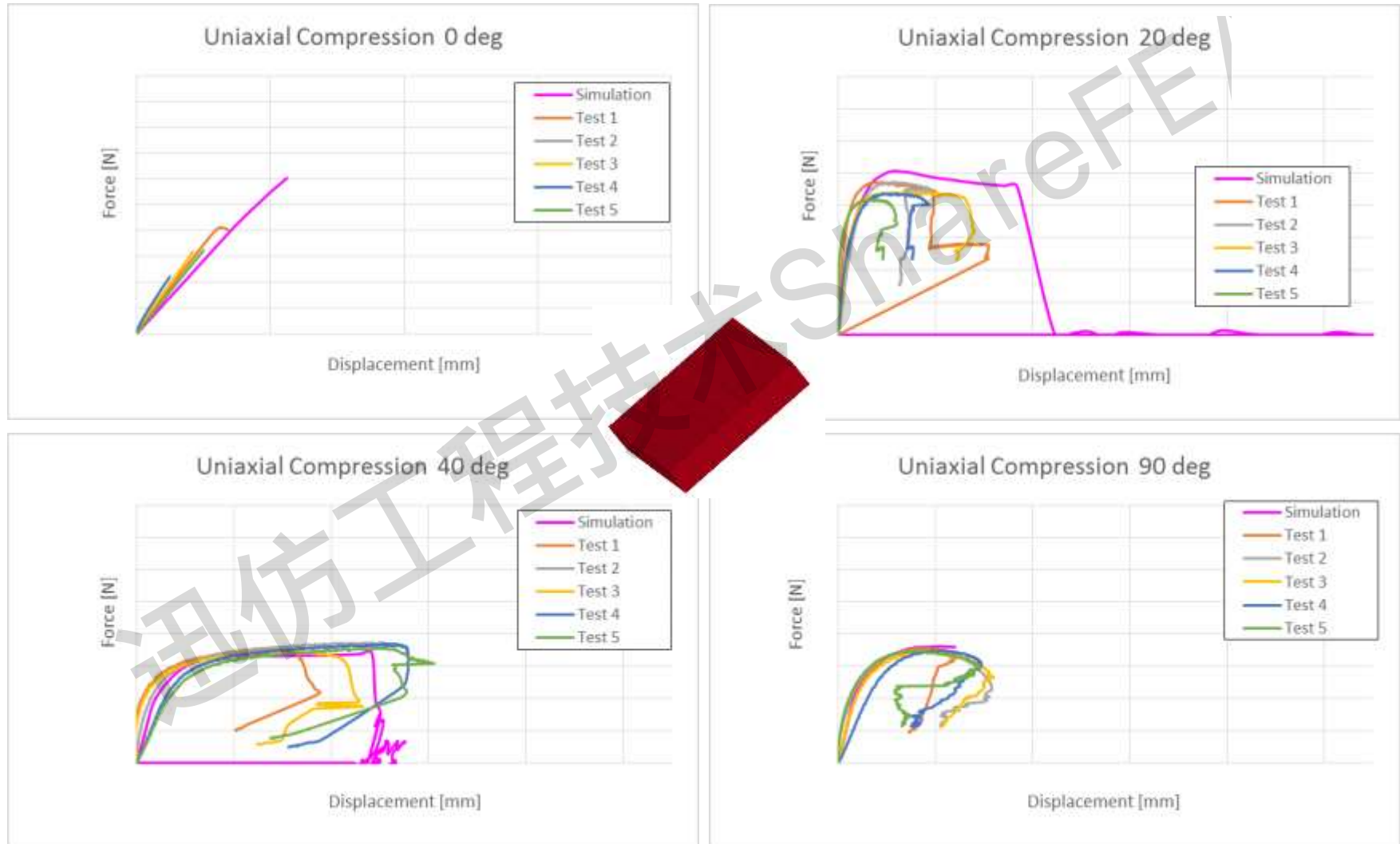
Relevant Modules

MF+GenYld CrachFEM		elastic behaviour	plastic behaviour	stress-space anisotropy	com- pressibility	normal fracture	shear fracture	stress-based criterion			
											
isotropic									 LS-Dyna		
orthotropic											
generally anisotropic											
strain-rate dependent											
strain dependent											
										 Abaqus	
											
											
											
										 PAM-Crash PAM-Stamp	
										 Radioss	

Tensile Tests (Different Orientations)



Compression Tests (Different Orientations)

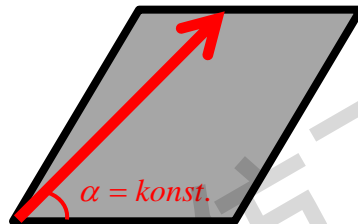
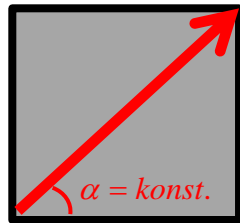


- ▶ Motivation
- ▶ MF-GenYld+CrachFEM for non-reinforced polymers
- ▶ MF-GenYld+CrachFEM for short fiber reinforced polymers
- ▶ MF-GenYld+CrachFEM for endless fiber reinforced polymers – Organic sheets
- ▶ MF-GenYld+CrachFEM for endless fiber reinforced composites (CFRP)
- ▶ **Current developments**
- ▶ Status of CrachFEM application

Tracking of directions for composite materials

Method 1

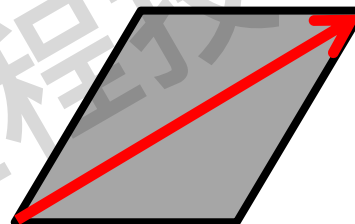
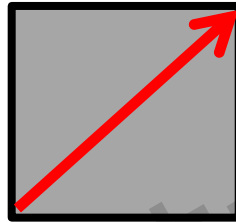
fixed angle between
element axis and fiber direction



- not precise in shear
- only one direction can be tracked

Method 2

shape functions
(e.g. PAMCRASH)

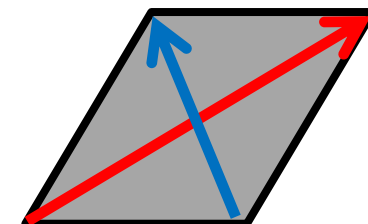
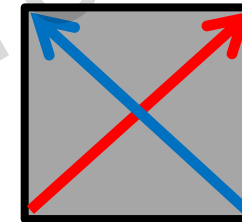


$$\begin{aligned} a_i &= x_{il} N_I^A \\ b_i &= x_{il} N_I^B \\ n^1 &= \frac{a}{|a|} \\ n^3 &= \frac{a \times b}{|a \times b|} \\ n^2 &= n^3 \times n^1 \end{aligned}$$

- precise
- Only one direction can be tracked

Method 3

deformation gradient



$$\begin{aligned} a &= F a^0 \\ b &= F b^0 \\ n^1 &= \frac{a}{|a|} \\ n^2 &= \frac{b}{|b|} \end{aligned}$$

- precise
- Multiple directions can be tracked

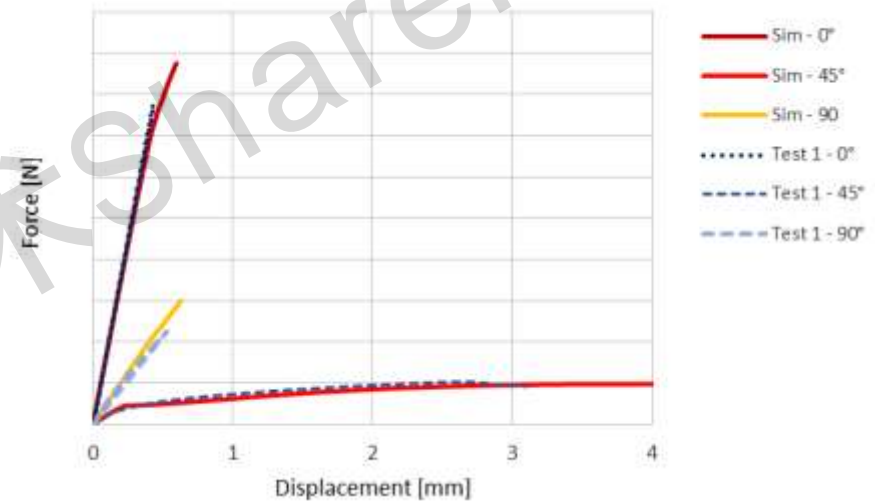
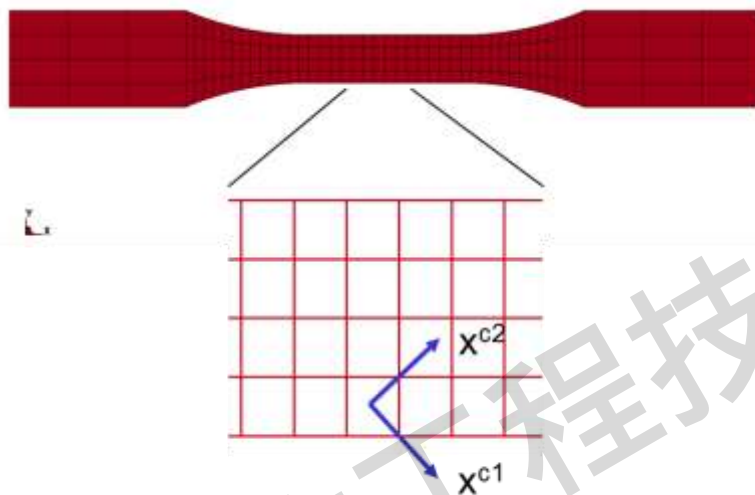
Source: G. Oberhofer, H. Dell, M. Vogler, H. Gese; Current solutions and open challenges in modeling organic sheets; Automotive CAE Grand Challenge April 12+13, 2016, Hanau

General Anisotropy for Composite Materials

- ▶ Superposition of two or multiple transversely-isotropic components or
- ▶ Structural tensors (implementation according to Ph.D. thesis of M. Vogler)

Superposition of two or multiple transversely-isotropic components

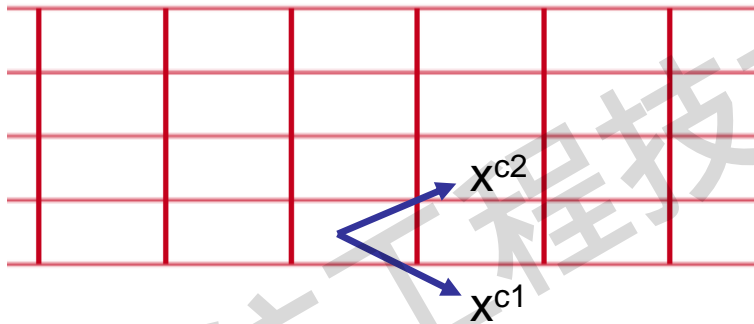
Example: $\pm 45^\circ$ tensile test of organic sheet:



Source: G. Oberhofer, H. Dell, M. Vogler, H. Gese; Current solutions and open challenges in modeling organic sheets; Automotive CAE Grand Challenge April 12+13, 2016, Hanau

Superposition of two or multiple transversely-isotropic components

Example: +/- 45° tensile test of organic sheet:

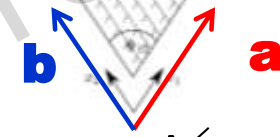
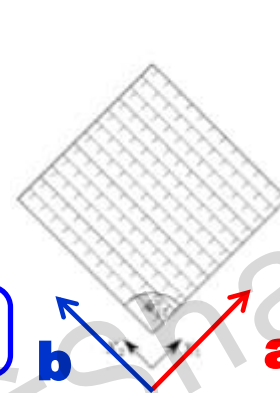


- Relative rotation of the x-axes of the two components: x^{c1} and x^{c2}

Source: G. Oberhofer, H. Dell, M. Vogler, H. Gese; Current solutions and open challenges in modeling organic sheets; Automotive CAE Grand Challenge April 12+13, 2016, Hanau

Structural tensors (implementation according to Ph.D. thesis of M. Vogler)

$$\mathbf{B} = \mathbf{b} \otimes \mathbf{b}$$



$$\mathbf{A} = \mathbf{a} \otimes \mathbf{a}$$

➔ \mathbf{a} and \mathbf{b} not necessarily perpendicular to each other! $\mathbf{a} \not\perp \mathbf{b}$

➔ Monoclinic material behavior (not orthotropic anymore)!

$$f = \hat{f}(\boldsymbol{\sigma}, \bar{\varepsilon}^p, \mathbf{A}, \mathbf{B}) = \alpha_1 I_1 + \alpha_2 I_2 + \alpha_3 I_3 + \underline{\alpha_7 I_7} - 1$$

- Mixed Invariant $I_7 := \underline{\text{tr} [\mathbf{A}\mathbf{B} (\boldsymbol{\sigma}^{\text{pind}})^2]}$ has to be regarded in the yield surface formulation and in the elasticity law
- Additional anisotropy parameter $\underline{\alpha_7}$
 - ... which physical meaning?
 - ... how to determine?

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Benefits for users of MF GenYld+CrachFEM

- ▶ One material model for different FEA codes
- ▶ Improved modelling of advanced materials (e.g. with anisotropic hardening)
- ▶ CrachFEM also predictive in case of non-linear strain path (isotropic-kinematic hardening of algorithm Crach; tensorial description of damage in fracture models)
- ▶ FLC prediction and fracture prediction also possible for orthotropic materials
- ▶ MATFEM offers also experimental material characterization for material model => material model development is motivated and directly supported by material tests
- ▶ MATFEM is partner in research projects to include new innovative features in MF GenYld+CrachFEM

Benefits for users of MF GenYld+CrachFEM

- ▶ Further development is driven by a growing number of licensees from different industrial branches (aerospace, automotive, consumer products, medical devices, currently approx. 50 users worldwide)
- ▶ MF GenYld+CrachFEM is in wide use in industry. Customers include: Airbus Operations, BMW AG, Ford, Hyundai-Mobis, Mercedes-Benz AG, ThyssenKrupp Steel Europe AG, ...