SPEED CONTROL OF DC MOTOR USING NOVEL NEURAL NETWORK CONFIGURATION

A PROJECT THESIS SUBMITTED IN THE FUFILLMENT OF THE REQUIREMENTS FOR THE DEGREE OF

BACHELOR OF TECHNOLOGY

IN

ELECTRICAL ENGINEERING

BY

MANISH MISHRA

ROLL NO. 10502014



DEPARTMENT OF ELECTRICAL ENGINEERING
NATIONAL INSTITUTE OF TECHNOLOGY
ROURKELA

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UNDER THE GUIDANCE OF PROF. J.K SATHPATHY



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NATIONAL INSTITUTE OF TECHNOLOGY ROURKELA

CERTIFICATE

This is to certify that the progress report of the thesis entitled, "SPEED CONTROL OF DC MOTOR USING NOVEL NEURAL NETWORK CONFIGURATION" submitted by **Shri Manish Mishra** in partial fulfilment of the requirements for the award of Bachelor of Technology degree in Electrical Engineering at the National Institute of Technology Rourkela (Deemed University), is an authentic work carried out by him under my supervision and guidance.

To the best of my knowledge the matter embodied in the thesis has not been submitted to any other University/Institute for the award of any degree or diploma.

Prof. J.K SATHPATHY

Date: Department of Electrical Engineering

Place: National Institute of Technology Rourkela

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ABSTRACT

This paper uses Artificial Neural Networks (ANNs) in estimating speed and controlling it for a separately excited DC motor. The rotor speed of the dc motor can be made to follow an arbitrarily selected trajectory. The purpose is to achieve accurate trajectory control of the speed, especially when the motor and load parameters are unknown.

Such a neural control scheme consists of two parts. One is the neural identifier which is used to estimate the motor speed. The other is the neural controller which is used to generate a control signal for a converter. These two neural networks are trained by Levenberg-Marquardt back-propagation algorithm. ANNs used in this are the standard three layers feed-forward neural network with sigmoid activation functions in the input and hidden layers while linear activation function is employed for the output layer.

The conventional constant gain feedback controller fails to maintain the performance of the system at acceptable levels under unknown dynamics in load torque. On the other hand, ANNs act as an effective tool to implement the model and adaptive control in a complicated non-linear system having expansive allocations.

The adaptive learning algorithm is formed in such a way that the learning rate is as large as possible while maintaining the stability of the learning process. This simplifies the learning process in terms of computation time, which is of special importance in real-time implementation.

Chapter 1

INTRODUCTION

The development of high performance motor drives is very important in industrial applications. Generally, a high performance motor drive system must have good dynamic speed command tracking and load regulating response.

D.C motors have long been the primary means of electric traction. D.C motor is considered a SISO system having torque/speed characteristics compatible with most mechanical loads. This makes a D.C motor controllable over a wide range of speeds by proper adjustment of its terminal voltage. Recently, brushless D.C motors, induction motors, and synchronous motors have gained widespread use in electric traction. However, there is a persistent effort towards making them behave like dc motors through innovative design and control strategies. Hence dc motors are always a good proving ground for advanced control algorithm because the theory is extendable to other types of motors.

Many practical control issues (motor control problems):

- Variable and unpredictable inputs
- Noise propagation along a series of unit processes
- Unknown parameters
- Changes in load dynamics

Under these conditions, the conventional constant gain feedback controller fails to maintain the performance of the system at acceptable levels. The incorporation of feed forward in artificial neural networks is important for several reasons the dynamical properties of the system, and in practice it may improve the performance. They are generally present in most non-linear dynamical system and can be used to implement specific structures.

Advantages of using ANNs:

- Learning ability
- Massive parallelism
- Fast adaptation
- Inherent approximation capability
- High degree of tolerance

Speed control techniques in separately excited dc motor:

- Varying the armature voltage in the constant torque region.
- In the constant power region, field flux should be reduced to achieve speed above the rated speed.

Methods of speed control:

- Traditionally rheostat armature control method was used for low power dc motors.
- Use of conventional PID controllers.
- Neural network controllers (NNC).
- Constant power field weakening controller based on load-adaptive multi-input multioutput linearization technique (in high speed regimes).
- A single phase uniform PWM ac-dc buck-boost converter with only one switching device used for armature voltage control.
- Use of NARMA-L2 (Non-linear Auto-regressive Moving Average) controller in the constant torque region.

Through experience gained in designing trajectory controllers based on self-tuning and PID control, it is seen that the neural network controller gives comparable performance in speed tracking. In addition to those mentioned above, a unique advantage of the neural network

controller is its ability to cope with bad measurement data that occur during training and testing. However, a key drawback is the inadequate integral gain in the feedback loop, resulting in steady-state errors of the shaft position. Direct position tracking can alleviate this problem.

The traditional means adapted by the motion control industry with motor drives has been the approach of linearizing the system dynamics and designing a linear feedback controller. However, in high-performance motor drives such an approach is seldom satisfactory, as it results in poor speed and position tracking when sudden changes in load result in continuous acceleration or deceleration of the motor/load system. Adaptation is necessary to ensure optimal performance.

Chapter 2

BACKGROUND INFORMATION

2.1 OVERVIEW:

The neural network consists of junctions which are connected with LINKS, also called processing units. For each junction a number is ordered, this number is called weight. The weights are the tools for the long distance information storing in the neural network, the learning process occurring with the appropriate modification of weights. These weights are modified so that the network input/output behaviour is in consonance with the environment, which provide the input data.

The calculation algorithm consists of two basic steps:

- Calculation of the output of the network, with inputs and weights.
- Modification of weights with learning algorithm.

A single input neuron consists of a scalar input 'p' multiplied by the scalar weight 'w' to form 'wp' which is fed to the summer along with bias 'b' multiplied by '1'.

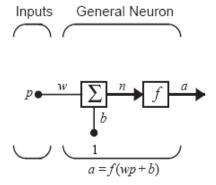


Figure 1: Basic Neural Network

The net input is 'wp+b' and the output 'a' is;

a=f(WP+b);

f- Transfer function

W & b can be adjusted by learning rule.

2.2 TRANSFER FUNCTION:

• <u>HARD-LIMIT TF</u>:

$$a = hardlim(n)$$

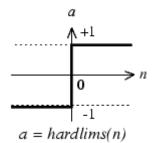


Figure 2: Symmetric Hard-limit Transfer Function

• <u>LINEAR TF</u>:

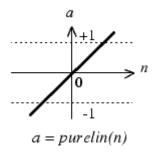


Figure 3: Linear Transfer Function

• LOG-SIGMOID TF:

$$a = logsig(n)$$

i.e.
$$a = 1/(1+\exp(-n));$$

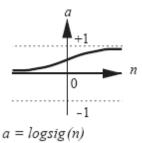


Figure 4: Log-Sigmoid Transfer Function

Used in multilayer n/w and trained using BPA as it is differentiable.

2.3 THREE-LAYER NETWORK:

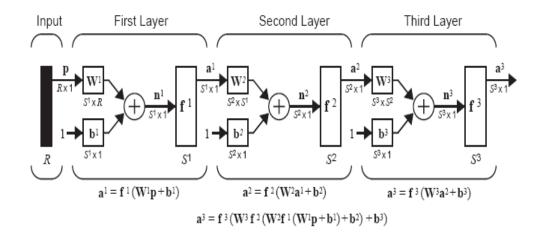


Figure 5: Three-Layer Network

 3^{rd} layer - OUTPUT LAYER $1^{st} \& 2^{nd}$ layer - HIDDEN LAYER

2.4 UNIVERSAL APPROXIMATORS:

$$f^{1}(n) = \frac{1}{1 + e^{-n}}$$
 and $f^{2}(n) = n$.

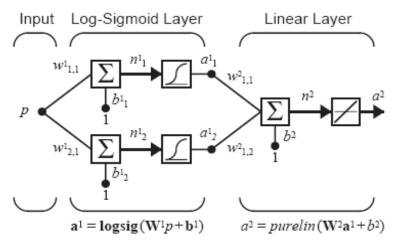


Figure 6: Universal Approximators

2.5 BACK PROPAGATION ALGORITHM:

- Procedure for selecting parameters- TRAINING the n/w.
- BPA is a method of TRAINING.
- Based on gradient descent.
- For a multilayer n/w, BPA is a gradient descent optimization procedure where we minimize a mean square error called <u>PERFORMANCE INDEX (PI)</u>.

 P_q – input to n/w

 $A_q - n/w$ output

 T_q – corresponding target output

$$F(\mathbf{x}) = \sum_{q=1}^{Q} e_q^2 = \sum_{q=1}^{Q} (t_q - a_q)^2.$$

$$e_q = T_q \text{-} A_q$$

X – Vector containing all n/w w & b.

Q- Total number of Errors in the network

F(x)- Performance Index

For Multiple outputs;

$$F(\mathbf{x}) = \sum_{q=1}^{Q} \mathbf{e}_{q}^{T} \mathbf{e}_{q} = \sum_{q=1}^{Q} (\mathbf{t}_{q} - \mathbf{a}_{q})^{T} (\mathbf{t}_{q} - \mathbf{a}_{q}).$$

Using stochastic approx.;

$$\hat{F}(\mathbf{x}) = (\mathbf{t}(k) - \mathbf{a}(k))^{T} (\mathbf{t}(k) - \mathbf{a}(k)) = \mathbf{e}^{T} (k) \mathbf{e}(k)$$

Where the expectation of the squared error has been replaced by the squared error at iteration 'k'.

2.5.1 STEEPEST DESCENT ALGORITHM FOR THE APPROX. MEAN SQUARE ERROR:

$$w_{i,j}^m(k+1) \, = \, w_{i,j}^m(k) - \alpha \frac{\partial \hat{F}}{\partial w_{i,j}^m} \, , \label{eq:wij}$$

$$b_i^m(k+1) = b_i^m(k) - \alpha \frac{\partial \ddot{F}}{\partial b_i^m} ,$$

where α is the learning rate.

i, j, m- Layers of neurons

F- Perfromance Index

w, b- respective weights and bias as per their sub-script and superscript.

Chapter 3

SEPARATELY EXCITED DC MOTOR

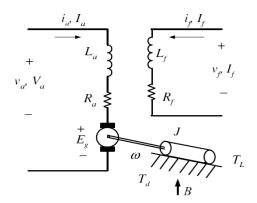


Figure 7: Separately Excited DC Motor

- The field windings are used to excite the field flux.
- Armature current is supplied to the rotor via brush and commutator for the mechanical work.
- Interaction of field flux and armature current in the rotor produces torque.

3.1 **OPERATION:**

- When a separately excited motor is excited by a field current of i_f and an armature current of i_a flows in the circuit, the motor develops a back emf and a torque to balance the load torque at a particular speed.
- The i_f is independent of the i_a . Each windings are supplied separately. Any change in the armature current has no effect on the field current.
- The i_f is normally much less than the i_a .

3.1.1 FIELD AND ARMATURE EQUATIONS:

Instantaneous field current:

$$v_f = R_f i_f + L_f \frac{di_f}{dt}$$

where R_f and L_f are the field resistor and inductor, respectively

Instantaneous armature current:

$$v_a = R_a i_a + L_a \frac{di_a}{dt} + e_g$$

where R_f and L_f are the armature resistor and inductor, respectively.

The motor back emf, which is also

known as speed voltage, is expressed as:

$$e_g = K_v \omega i_f$$

 K_v is the motor voltage constant (in V/A - rad/s) and ω is the motor speed (in rad/sec)

3.1.2 BASIC TORQUE EQUATION:

The torque develped by the motor is:

$$T_d = K_t i_f i_a$$

where $(K_t = K_v)$ is the torque constant.

Sometimes it is written as:

$$T_d = K_t \phi i_a$$

For normal operation, the developed torque must be equal to the load torque plus the friction and inertia, i.e.:

$$T_d = J\frac{d\omega}{dt} + B\omega + T_L$$

where

B: viscous friction constant, (N.m/rad/s)

 T_L : load torque (N.m)

J: inertia of the motor (kg.m²)

3.2 STEADY STATE OPERATION:

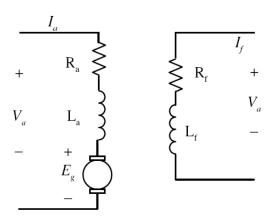


Figure 8: Separately Excited DC Motor In Steady State

Under steady - state operations, time derivatives is zero. Assuming the motor is not saturated.

For field circuit,

$$V_f = I_f R_f$$

The back emf is given by:

$$E_g = K_v \omega I_f$$

The armature circuit

$$V_a = I_a R_a + E_g = I_a R_a + K_v \omega I_f$$

3.2.1 STEADY-STATE TORQUE AND SPEED:

The motor speed can be easily derived:

$$\omega = \frac{V_a - I_a R_a}{K_v I_f}$$

If R_a is a small value (which is usual), or when the motor is lightly loaded, i.e. I_a is small,

$$\omega = \frac{V_a}{K_v I_f}$$

That is if the field current is kept constant, the motor speed depends only on the supply voltage.

The developed torque is:

$$T_d = K_t I_f I_a = B\omega + T_L$$

The required power is:

$$P_d = T_d \omega$$

3.2.2 TORQUE AND SPEED CONTROL:

- From the derivation, several important facts can be deduced for steady-state operation of DC motor.
- For a fixed field current, or flux (I_f) , the torque demand can be satisfied by varying the armature current (I_a) .
- The motor speed can be varied by:
- controlling V_a (voltage control)
- controlling V_f (field control)
- These observations lead to the application of variable DC voltage for controlling the speed and torque of DC motor.

3.2.3 VARIABLE SPEED OPERATION:

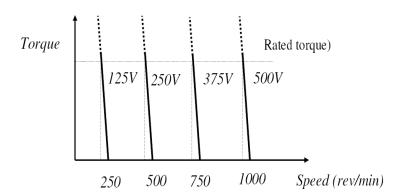


Figure 9: Torque Vs Speed Characteristic For Different Armature Voltages

- Family of steady-state torque speed curves for a range of armature voltage can be drawn as above.
- The speed of DC motor can simply be set by applying the correct voltage.
- Note that speed variation from no-load to full load (rated) can be quite small. It depends on the armature resistance.

3.2.4 BASE SPEED AND FIELD-WEAKENING:

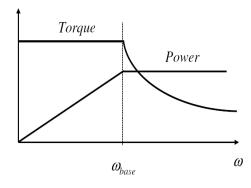


Figure 10: Torque Vs Speed And Power Vs Speed Characteristic Of Separately Excited DC Motor

• Base speed: (w_{base})

- the speed which correspond to the rated V_a , rated I_a and rated I_f .

- Constant Torque region ($w > w_{base}$)
- $-I_a$ and I_f are maintained constant to met torque demand. V_a is varied to control the speed. Power increases with speed.
- Constant Power region $(w > w_{base})$
- $-V_a$ is maintained at the rated value and i_f is reduced to increase speed. However, the power developed by the motor (= torque x speed) remains constant. This phenomenon is known as *field weakening*.

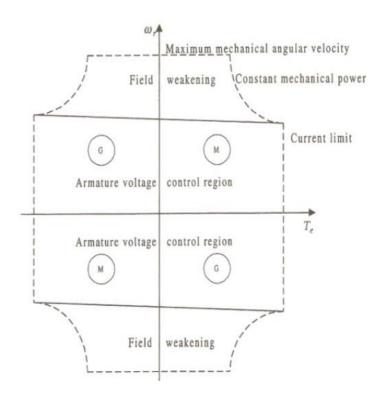


Figure 11: Typical Operating Regions Of Separately Excited DC Machines

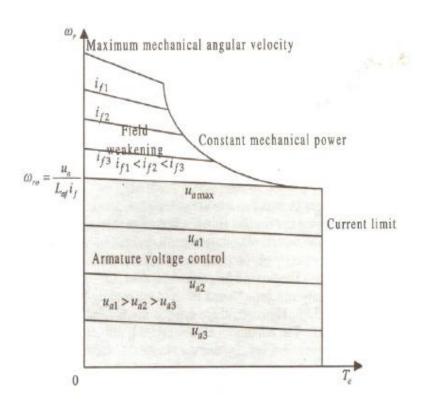


Figure 12: Steady-State Torque-Speed Operating Characteristics Of Separately Excited DC Motors

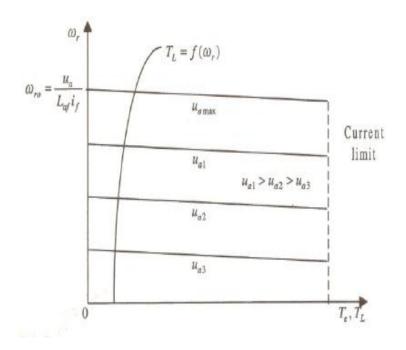


Figure 13: Torque-Speed Characteristic Curves For I_f=Const.

A high performance drive system consists of a motor, a converter, and a controller integrated to perform a precise mechanical manoeuvre. This requires the shaft speed and/or the motor to

closely follow a specified trajectory regardless of unknown load variations and other parameter uncertainties. One way to compensate for these uncertainties is to identify the motor/load dynamics through the parameters of a pre-defined model. These model parameters can then be manipulated using different control strategies to come up with the controller design.

If the unknown dynamics are non-stationary, the identification has to be performed online. However, if the dynamics are stationary, offline identification is adequate.

e.g. in self-tuning control, motor/load parameters are identified through a linear parametric (ARMAX) model using a Kalman Filter.

But identifying non-linear dynamics through a linear model does not guarantee an accurate functional representation.

The ability of a multi-layer perceptron type neural network to learn a large class of non-linear functions is well known. The neural network identifier evolves through the learning of a suitable time sequence of input/output patterns generated by the motor model. The ability to successfully train without explicit knowledge of the motor/load dynamics is the key advantage in this type of identification. Moreover the superior generalizing capability of the neural network allows accurate emulation of the motor dynamics for previously untrained inputs. The inherent noise rejection property of the neural network is useful in dealing with noisy input/output characteristics.

Chapter 4

OBJECTIVE

The neural network's role is to identify the unknown mapping between the voltage command and the speed of the motor. The trained neural network is then used for controller design.

4.1 SYSTEM DYNAMICS:

$$K\omega(t) = -R_aI_a(t) - L_a \left[di_a(t)/dt \right] + V_t(t)$$
 (1)

$$Ki_{a}(t) = J[d\omega(t)/dt] + D\omega(t) + T_{L}(t)$$
 (2)

Where,

 $\omega(t)$ - rotor speed (rad/s)

 $V_t(t)$ - terminal voltage (V)

I_a(t) - armature current (A)

 $T_L(t)$ - load torque (Nm)

J - Rotor inertia (Nm²)

K - Torque & back emf constant (Nm/A)

D - viscose friction coefficient (Nms)

 R_a - armature resistance (Ω)

L_a - armature inductance (H)

4.2 CONTROL SYSTEM APPLICATIONS:

- Predictive control method
- NARMA-L2 control method
- Model reference control method.

All are based on standard linear control architecture.

Two steps involved when used for control:

• System identification

- Control design
- SI stage, a neural network model of the plant that we want to control developed.
- Control design stage, the neural network plant model used to train the controller.

4.3 SYSTEM IDENTIFICATION:

It is to train a neural network to represent the forward dynamics of the plant. The prediction error between the plant output and the neural network output is used as the neural network training signal.

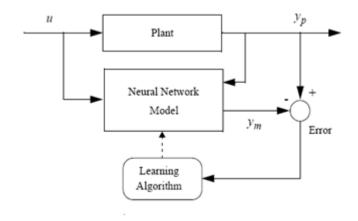


Figure 14: Plant Identification

The standard model used for non-linear identification in NARMA model.

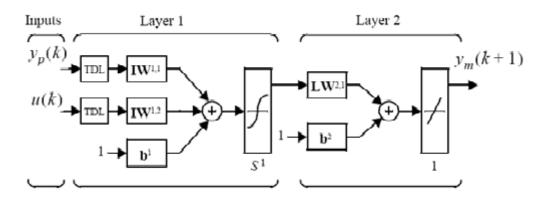


Figure 15: Neural Network Plant Model

TDL- Tapped Delay Lines that stores previous values of the input signal

IW (i, j) - Weight matrix from layer number 'i' to 'j'

IW (j, i) - Weight matrix from layer number 'j' to 'i'

4.4 CONTROL DESIGN:

We use Model reference Adaptive Control (MRAC) strategy. This architecture consists of two neural networks;

- Controller network
- Plant model network

After SI, the controller is trained so that the plant output follows the reference model output.

The controller training is done separately and requires the use of dynamic back-propagation.

DBP gets applied to a larger class of plant and hence the controller requires minimal online

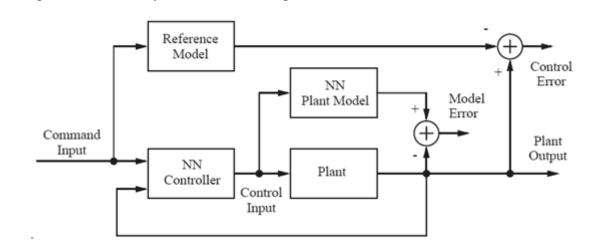


Figure 16: Model Reference Control Architecture

4.5 DISCRETE TIME DC MOTOR MODEL:

computation. Generally indirect MRAC is preferred.

$$T_L(t) = \mu W_P^2(t) \left[sign(W_p(t)) \right];$$

where μ is a constant.

The discrete time model speed equation governing the system dynamics is given by;

$$\begin{split} W_p(\mathbf{k}+1) &= \alpha \, W_p(k) + \, \beta \, W_p(k-1) + \, \gamma \, \left[sign \, \left(W_p(k) \right) \right] W_p^2(k) + \, \delta \, \left[sign \, \left(W_p(k-1) \right) \right] \\ W_p^2(k-1) &+ \, \xi \, V_t(k) \, ; \end{split}$$

4.6 IDENTIFICATION OF DC MOTOR MODEL:

The equation can be manipulated to the form;

$$V_t(k) = g[W_p(k+1), W_p(k), W_p(k-1)]$$

where the function g[.] is given by;

$$\begin{split} g[W_p(k+1),\ W_p(k),\ W_p(k-1)] &= \{\ W_p(k+1) - \alpha\ W_p(k) - \beta\ W_p(k-1) - \gamma\ [sign\ (W_p(k))] \\ W_p^{\ 2}(k) - \delta \left[sign\ (W_p(k-1)) \right] W_p^{\ 2}(k-1) \ \} / \ \xi \ ; \end{split}$$

and is assumed to be unknown. An ANN is trained to emulate the unknown function g[.]. However as $W_p(k+1)$ cannot be readily available.

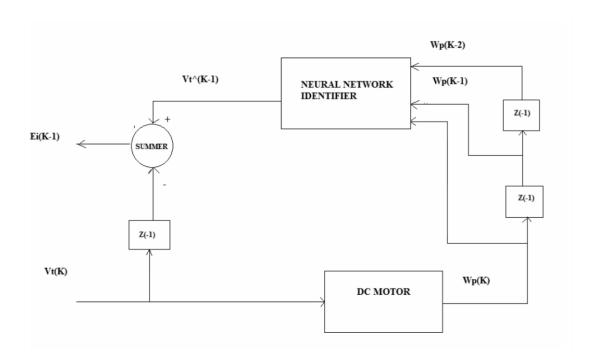


Figure 17: Structure Of The ANN Identifier

4.7 TRAJECTORY CONTROL OF DC MOTOR USING TRAINED ANN:

The objective of the control system is to drive the motor so that its speed $W_p(k)$, follows a pre-specified trajectory, $W_m(k)$. The following second order reference model is chosen;

$$W_m(k+1) = 0.6 W_m(k) + 0.2 W_m(k-1) + r(k)$$
;

For a given desired sequence $\{W_m(k)\}$, the corresponding control sequence $\{r(k)\}$ can be calculated using the above relation.

The speed at $(k+1)^{th}$ time step can be predicted from;

$$\widehat{W}_{P}(k+1) = 0.6 W_{p}(k) + 0.2 W_{p}(k-1) + r(k);$$

This result can be fed to the ANN to estimate the control input at \boldsymbol{k}^{th} time step using;

$$\widehat{V_t}(k-1) = N[W_p(k), W_p(k-1), W_p(k-2)];$$

Chapter 5

PROBLEM STATEMENT

A separately excited dc motor with name plate ratings of 1 hp, 220V, 550 rpm is used in all simulations. Following parameter values are associated with it.

 $J=0.068\;Kgm^2$

 $K = 3.475 \text{ Nm A}^{-1}$

 $R_a = 7.56 \Omega$

 $L_a = 0.055 H$

D = 0.03475 Nms

 $\mu = 0.0039 \text{ Nms}^2$

T = 40 ms

As from the system dynamics equations, α , β and ξ are constant values based on the motor parameters J, K, D, R_a , L_a and the sampling period T. While γ and δ in addition to being functions of the above parameters are also functions of μ . The value k denotes the kth time step.

$$\begin{split} \alpha &= 2*(L_a\,J + R_a\,J + L_a\,D - R_a\,D\,T - K^2\,T)/(\,L_a\,J + 2*R_a\,J + 2*L_a\,D)\;;\\ \beta &= (\text{--})\,L_a\,J/(\,L_a\,J + 2*R_a\,J + 2*L_a\,D)\;;\\ \gamma &= (\text{--})\,2*\mu\;(L_a + R_a\,T)/(\,L_a\,J + 2*R_a\,J + 2*L_a\,D)\;;\\ \delta &= 2*L_a\,\mu/(\,L_a\,J + 2*R_a\,J + 2*L_a\,D)\;;\\ \xi &= 2*K*T/(\,L_a\,J + 2*R_a\,J + 2*L_a\,D)\;; \end{split}$$

Using the given values of the system parameters in the above stated equations we get;

 $\alpha = 0.0506$;

 $\beta = (-)0.003611$;

$$\gamma = (-)0.002692$$
;

$$\delta=0.000414 \; ;$$

$$\xi = 0.26795$$
;

The system equation becomes;

$$(K^2 + R_a \; D) \; W(t) = K \; V_t(t) - J \; L_a \frac{d^2 W}{dt^2} \; - (R_a \; J + L_a \; D) \; \frac{dW}{dt} - L_a \frac{dT_L}{dt} - R_a \; T_L(t) \; ; \label{eq:Kappa}$$

LIMITS TAKEN INTO CONSIDERATION:

$$-30.0 < W_P(k) < 30.0 \text{ rad/s}$$

-1.0
$$<$$
 $W_p(\mbox{k-}\mbox{1})$ - $W_p(\mbox{k})$ $<$ 1.0 rad/s

$$\text{-}100 \ v < V_t(k) < 100 \ v$$

Chapter 6

GENERATION OF THE SIGNAL

6.1 OVERVIEW:

$$\widehat{W}_{P}(k+1) = N [W_{p}(k), W_{p}(k-1)] + \xi V_{t}(k);$$

So, now the system dynamic equations get converted into two first order differential equations as follows:

$$\dot{\iota_a}(t) = (V_t(t) / L_a) - (R_a i_a(t) / L_a) - (K W(t) / L_a)$$
;

$$\dot{\mathcal{W}}(t) = \left(K \ i_a(t) \ / \ J\right) - \left(D \ W(t) \ / \ J\right) - \left(T_L(t) \ / \ J\right) \ ; \label{eq:Weight}$$

TAKING INITIAL VALUES AS,

$$W_p(0) = W(0) = 0;$$

$$i_a(0) = 0;$$

Substituting the values of the motor parameters in the above two equations along with the initial conditions, the above two equations get transformed into:

$$\dot{y_1} = 18.182 \text{ V}_t - 137.454 \text{ y}_1 - 63.182 \text{ y}_2 \text{ ;}$$

$$\dot{y_2} = 51.1 \text{ y}_1 - 0.511 \text{ y}_2 - 14.7 \text{ T}_L$$
;

Considering $y_1 = i_a(t)$ and $y_2 = W(t)$

$$V_t(k) = 50 \sin(2\pi kT/7) + 45 \sin(2\pi kT/3) \ \forall kT \in [0, 20]$$
 is assumed.

6.2 **RESULT**:

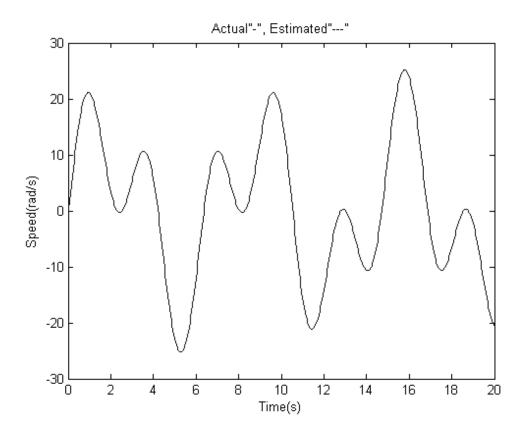


Figure 18: Actual And Estimated Rotor Speeds

Chapter 7

SYSTEM IDENTIFICATION

7.1 OVERVIEW:

The 3-layer feed-forward ANN used:

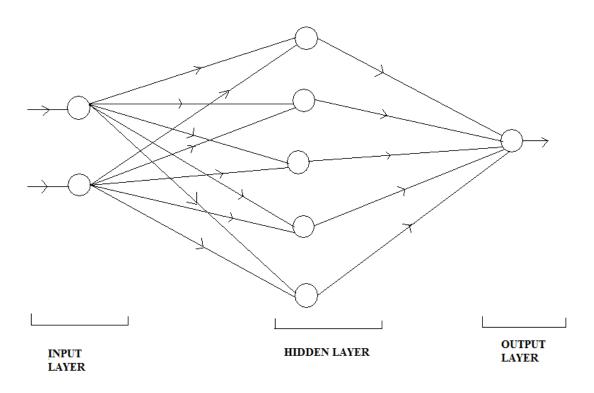


Figure 19: Three-Layer Feed forward ANN

As discussed earlier, the motor dynamics can be partitioned as;

$$W_p(k+1) = f[W_p(k), W_p(k-1)] + \xi V_t(k);$$

Where the function f[.] is given by;

$$\begin{split} & \text{f[} W_{p}(\mathbf{k}),W_{p}(\mathbf{k-1}) \text{]} = \alpha \, W_{p}(k) + \beta \, W_{p}(k-1) + \gamma \, \left[sign \, \left(W_{p}(k) \right) \right] W_{p}^{2}(k) + \\ & \delta \, \left[sign \, \left(W_{p}(k-1) \right) \right] \, W_{p}^{2}(k-1) \, ; \end{split}$$

which is supposed to be an UNKNOWN NON-LINEAR FUNCTION.

The values $W_p(k)$ and $W_p(k-1)$ which are the independent variables of f [.], are selected as the inputs to the ANN. The corresponding *ANN* output target f $[W_p(k), W_p(k-1)]$ is given by above equation.

The ANN is trained off-line using randomly generated input patterns of $[W_p(k), W_p(k-1)]$ and the corresponding target f $[W_p(k), W_p(k-1)]$. The choice of $W_p(k), W_p(k-1)$ has to satisfy the constraints as specified earlier.

The motor speed is estimated by the trained ANN predictor as

$$\widehat{W}_{P}(k+1) = N [W_{p}(k), W_{p}(k-1)] + \xi V_{t}(k);$$

Where N[.] denotes the ANN output for a given set of "." Inputs.

ANN topology and the training effort are briefly described by the following statistics:

Number of inputs	2
Number of outputs	1
Number of Hidden layers	1
Number of Hidden neurons	5
Number of training patterns 'P'	500
Number of training sweeps	1000
Learning Step 'η'	0.1
Momentum Gain 'α'	0.1
E_{total} threshold ' $arepsilon$ '	0.04

As mentioned earlier, except for the number of inputs/outputs of the *ANN*, all other design and learning parameters are selected by trial and error.

7.2 BLOCK DIAGRAM:

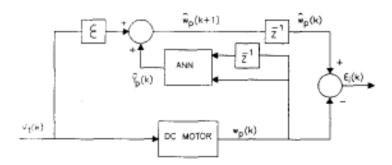


Figure 20: Structure Of The ANN For Identification Of The Dc Motor

The trained ANN is applied as a series-parallel type identifier to estimate the value of the function f [.]. \mathbf{z}^{-1} in any figure indicates a unit time delay. The performance of the trained ANN identifier is evaluated by comparing the actual and estimated speeds as calculated from the afore mentioned equations above for the following arbitrarily selected terminal voltage sequence,

$$V_t(k) = 50 \sin(2\pi kT/7) + 45 \sin(2\pi kT/3) \ \forall kT \in [0, 20]$$
.

7.3 C-CODE FOR TRAINING WITH BACK-PROPAGATION OF THE ANN:

A single neuron (i.e. processing unit) takes it total input *In* and produces an output activation *Out*. I shall take this to be the sigmoid function

Out =
$$1.0/(1.0 + \exp(-\ln I))$$
; /* Out = Sigmoid(In) */

though other activation functions are often used (e.g. linear or hyperbolic tangent). This has the effect of squashing the infinite range of *In* into the range 0 to 1. It also has the convenient property that its derivative takes the particularly simple form

Typically, the input In into a given neuron will be the weighted sum of output activations feeding in from a number of other neurons. It is convenient to think of the activations flowing through layers of neurons. So, if there are NumUnits1 neurons in layer 1, the total activation flowing into our layer 2 neuron is just the sum over Layer1Out[i]*Weight[i], where Weight[i] is the strength/weight of the connection between unit i in layer 1 and our unit in layer 2. Each neuron will also have a bias, or resting state, that is added to the sum of inputs, and it is convenient to call this weight[0]. We can then write

Normally layer 2 will have many units as well, so it is appropriate to write the weights between unit i in layer 1 and unit j in layer 2 as an array Weight[i][j]. Thus to get the output of unit j in layer 2 we have

Remember that in C the array indices start from zero, not one, so we would declare our variables as

Three layer networks are necessary and sufficient for most purposes, so our layer 2 outputs feed into a third layer in the same way as above

```
Layer3In[k] = Weight23[0][k] ; for(j = 1 ; j \le NumUnits2 ; j++) \{ Layer3In[k] += Layer2Out[j] * Weight23[j][k] ; \} Layer3Out[k] = 1.0/(1.0 + exp(-Layer3In[k])) ; \}
```

The code can start to become confusing at this point - I find that keeping a separate index *i*, *j*, *k* for each layer helps, as does an intuitive notation for distinguishing between the different layers of weights *Weight12* and *Weight23*. For obvious reasons, for three layer networks, it is traditional to call layer 1 the *Input* layer, layer 2 the *Hidden* layer, and layer 3 the *Output* layer.

Also, to save getting all the *In*'s and *Out*'s confused, we can write *LayerNIn* as *SumN*. Our code can thus be written

```
\label{eq:for_section} \begin{subarray}{ll} for( k = 1 \; ; \; k <= NumOutput \; ; \; k++ ) \; \{ & /* \; k \; loop \; computes \; output \; unit \; activations \\ */ & SumO[k] = WeightHO[0][k] \; ; \\ & for( \; j = 1 \; ; \; j <= NumHidden \; ; \; j++ ) \; \{ & SumO[k] \; += Hidden[j] \; * \; WeightHO[j][k] \; ; \\ & \} & Output[k] = 1.0/(1.0 + exp(-SumO[k])) \; ; \\ \end{subarray}
```

Generally we will have a whole set of *NumPattern* training patterns, i.e. pairs of input and target output vectors,

```
Input[p][i] , Target[p][k]
```

labelled by the index p. The network learns by minimizing some measure of the error of the network's actual outputs compared with the target outputs. For example, the sum squared error overall output unit's k and all training patterns p will be given by

```
\begin{split} & Error = 0.0 \ ; \\ & for(\ p = 1 \ ; \ p <= NumPattern \ ; \ p ++ \ ) \ \{ \\ & for(\ k = 1 \ ; \ k <= NumOutput \ ; \ k ++ \ ) \ \{ \\ & Error \ \ += \ \ 0.5 \ \ * \ \ (Target[p][k] \ \ - \ \ Output[p][k]) \ \ * \ \ (Target[p][k] \ \ - \ \ Output[p][k]) \ ; \\ & Output[p][k]) \ ; \\ & \} \end{split}
```

(The factor of 0.5 is conventionally included to simplify the algebra in deriving the learning algorithm.) If we insert the above code for computing the network outputs into the p loop of this, we end up with

```
Error = 0.0;
for(p = 1; p <= NumPattern; p++) { /* p loop over training patterns */
      for(j = 1; j \le NumHidden; j++) { /* j loop over hidden units */
             SumH[p][j] = WeightIH[0][j];
             for(i = 1; i \le NumInput; i++) {
                    SumH[p][j] += Input[p][i] * WeightIH[i][j];
              }
             Hidden[p][j] = 1.0/(1.0 + exp(-SumH[p][j]));
       }
      for(k = 1; k \le NumOutput; k++) { /* k loop over output units */
              SumO[p][k] = WeightHO[0][k];
             for(j = 1; j \le NumHidden; j++)
                    SumO[p][k] += Hidden[p][j] * WeightHO[j][k];
              }
             Output[p][k] = 1.0/(1.0 + \exp(-SumO[p][k]));
             Error += 0.5 * (Target[p][k] - Output[p][k]) * (Target[p][k] -
              Output[p][k]); /* Sum Squared Error */
       }
}
```

The next stage is to iteratively adjust the weights to minimize the network's error. A standard way to do this is by 'gradient descent' on the error function. We can compute how much the

error is changed by a small change in each weight (i.e. compute the partial derivatives d*Error*/d*Weight*) and shift the weights by a small amount in the direction that reduces the error.

```
Error = 0.0;
for(p = 1; p <= NumPattern; p++) { /* repeat for all the training patterns */
      for (j = 1; j \le NumHidden; j++) { /* compute hidden unit activations */
              SumH[p][j] = WeightIH[0][j];
              for(i = 1; i \le NumInput; i++) {
                     SumH[p][j] += Input[p][i] * WeightIH[i][j];
              }
              Hidden[p][j] = 1.0/(1.0 + exp(-SumH[p][j]));
       }
       for(k = 1; k \le NumOutput; k++) { /* compute output unit activations and
       errors */
              SumO[p][k] = WeightHO[0][k];
              for(j = 1; j \le NumHidden; j++) {
                     SumO[p][k] += Hidden[p][j] * WeightHO[j][k];
              }
              Output[p][k] = 1.0/(1.0 + \exp(-SumO[p][k]));
              Error += 0.5 * (Target[p][k] - Output[p][k]) * (Target[p][k] - Output[p][k]);
              DeltaO[k] = (Target[p][k] - Output[p][k]) * Output[p][k] * (1.0 -
              Output[p][k]);
       }
       for(j = 1; j \le NumHidden; j++) { /* 'back-propagate' errors to hidden layer */
```

```
SumDOW[j] = 0.0;
      for(k = 1; k \le NumOutput; k++) {
             SumDOW[j] += WeightHO[j][k] * DeltaO[k];
      }
      DeltaH[j] = SumDOW[j] * Hidden[p][j] * (1.0 - Hidden[p][j]);
}
for(j = 1; j \le NumHidden; j++) { /* update weights WeightIH */
      DeltaWeightIH[0][j] = eta * DeltaH[j] + alpha * DeltaWeightIH[0][j];
      WeightIH[0][j] += DeltaWeightIH[0][j] ;
      for(i = 1; i \le NumInput; i++) {
             DeltaWeightIH[i][j] = eta * Input[p][i] * DeltaH[j] + alpha *
             DeltaWeightIH[i][j];
             WeightIH[i][j] += DeltaWeightIH[i][j] ;
      }
}
for(k = 1; k \le NumOutput; k ++ ) { /* update weights WeightHO */
      DeltaWeightHO[0][k] = eta * DeltaO[k] + alpha * DeltaWeightHO[0][k];
      WeightHO[0][k] += DeltaWeightHO[0][k] ;
      for(j = 1; j \le NumHidden; j++) {
             DeltaWeightHO[j][k] = eta * Hidden[p][j] * DeltaO[k] + alpha *
             DeltaWeightHO[j][k]
             WeightHO[j][k] += DeltaWeightHO[j][k] ;
      }
}
```

}

he weight changes *DeltaWeightIH* and *DeltaWeightHO* are each made up of two components. First, the *eta* component that is the gradient descent contribution. Second, the *alpha* component that is a 'momentum' term which effectively keeps a moving average of the gradient descent weight change contributions, and thus smoothes out the overall weight changes. Fixing good values of the learning parameters *eta* and *alpha* is usually a matter of trial and error. Certainly *alpha* must be in the range 0 to 1, and a non-zero value does usually speed up learning. Finding a good value for *eta* will depend on the problem, and also on the value chosen for *alpha*. If it is set too low, the training will be unnecessarily slow. Having it too large will cause the weight changes to oscillate wildly, and can slow down or even prevent learning altogether.

The complete training process will consist of repeating the above weight updates for a number of epochs (using another *for* loop) until some error crierion is met, for example the *Error* falls below some chosen small number.

```
for( epoch = 1 ; epoch < LARGENUMBER ; epoch++ ) {
    /* ABOVE CODE FOR ONE ITERATION */
    if( Error < SMALLNUMBER ) break ;
}</pre>
```

If the training patterns are presented in the same systematic order during each epoch, it is possible for weight oscillations to occur. It is therefore generally a good idea to use a new random order for the training patterns for each epoch. If we put the NumPattern training pattern indices p in random order into an array ranpat[], then it is simply a matter of replacing our training pattern loop

```
for( p = 1 ; p <= NumPattern ; p++ ) {
```

with

```
for( np = 1; np \le NumPattern; np++) { p = ranpat[np];
```

Generating the random array *ranpat[]* is not quite so simple, but the following code will do the job

```
for(\ p=1\ ;\ p <= NumPattern\ ;\ p++\ )\ \{ \qquad \  \  \, /*\ set\ up\ ordered\ array\ */ ranpat[p] = p\ ; for(\ p=1\ ;\ p <= NumPattern\ ;\ p++\ )\ \{ \qquad \  \  \, /*\ swap\ random\ elements\ into\ each position\ */ np = p + rando()\ *\ (\ NumPattern\ + 1 - p\ )\ ; op = ranpat[p]\ ;\ ranpat[p] = ranpat[np]\ ;\ ranpat[np] = op\ ; \}
```

Naturally, one must set some initial network weights to start the learning process. Starting all the weights at zero is generally not a good idea, as that is often a local minimum of the error function. It is normal to initialize all the weights with small random values. If rando() is your favourite random number generator function that returns a flat distribution of random numbers in the range 0 to 1, and smallwt is the maximum absolute size of your initial weights, then an appropriate section of weight initialization code would be

```
for(\ i=0\ ;\ i<=NumInput\ ;\ i++\ )\ \{ DeltaWeightIH[i][j]=0.0\ ; WeightIH[i][j]=2.0\ *\ (\ rando()\ -\ 0.5\ )\ *\ smallwt\ ; \} for(\ k=1\ ;\ k<=NumOutput\ ;\ k++\ )\ \{ /* initialize WeightHO and DeltaWeightHO\ */ for(\ j=0\ ;\ j<=NumHidden\ ;\ j++\ )\ \{ DeltaWeightHO[j][k]=0.0\ ; WeightHO[j][k]=2.0\ *\ (\ rando()\ -\ 0.5\ )\ *\ smallwt\ ; \} \}
```

Chapter 8

TRAJECTORY CONTROL

8.1 OVERVIEW:

The objective of the control system is to drive the motor so that its speed, $W_p(k)$, follows a prespecified trajectory, $W_m(k)$. This is done by letting the dc motor follow the output of a selected reference model throughout the trajectory. The following second order reference model is selected;

$$W_m(k+1) = 0.6 W_m(k) + 0.2 W_m(k-1) + r(k)$$
;

 $\mathbf{r}(\mathbf{k})$ is the bounded input to the reference model. The coefficients are selected to ensure that its poles are within the unit circle and has the type of response that can be achieved by the dc motor. For a given desired sequence $(W_m(k))$ (trajectory), the corresponding control sequence $(\mathbf{r}(\mathbf{k}))$ can be calculated using the above equation.

The controller topology trained in the previous chapter is now used to estimate the motor terminal voltage $V_t(k)$ which enables accurate trajectory control of the shaft speed $W_p(k)$. Performance of the controller is simulated for arbitrarily selected speed tracks $(W_m \ (k))$. A graphical comparison of the specified and actual speed trajectories are hence presented.

Let's for a moment assume that the tracking error $E_c(k)$ is zero, and that the nonlinear function f[.] is known. The control input $V_t(k)$ to the motor at the k^{th} time step can be calculated as

$$V_t(k) = [-f[W_p(k), W_p(k-1)] + 0.6*W_p(k) + 0.2*W_p(k-1) + r(k)]/\xi$$
;

Hence the tracking error difference equation becomes

$$E_c(k+1) = 0.6*E_c(k) + 0.2*E_c(k-1)$$
;

Since the reference model is asymptotically stable, it follows that $\lim_{k\to\infty} E_c(\mathbf{k}+\mathbf{l}) = \mathbf{0}$ for arbitrary initial conditions. However since f[.] is not **known**, its estimated value from the *ANN* trained under the controller topology is used to estimate the controlled terminal voltage.

$$\widehat{V}_t(k) = [-N[W_p(k), W_p(k-1)] + 0.6*W_p(k) + 0.2*W_p(k-1) + r(k)]/\xi$$
;

The tracking control capability of the model was investigated for different arbitrarily specified trajectories. Only a specific result is shown for brevity. In this case, the specified speed trajectory is defined by

$$W_{m}(k) = 10*Sin(2.0*\pi kT/4) + 16*Sin(2.0*\pi kT/7) \forall kT \in [0,20];$$

For the above trajectory, the corresponding (r(k)) is derived by using the first equation. This is applied to the model shown below. The matrix α_m^T corresponds to the reference model coefficients [0.6 0.2].

8.3 PLOTS:

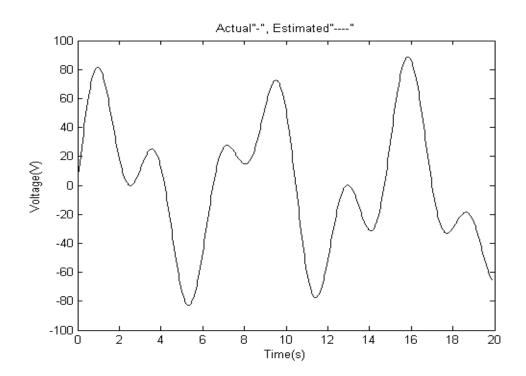


Figure 21: Actual And Estimated Terminal Voltage Of The DC Motor

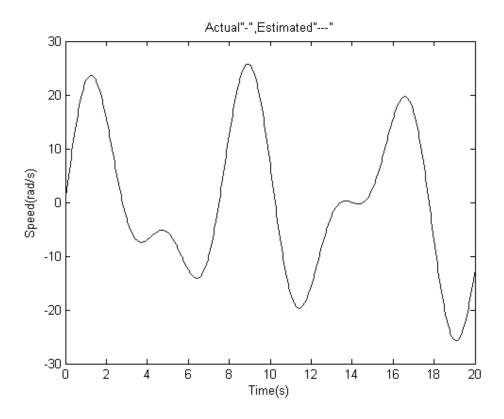


Figure 22: Tracking Performance For A Sinusoidal Reference Track

8.4 OVERALL CONTROLLER STRUCTURE:

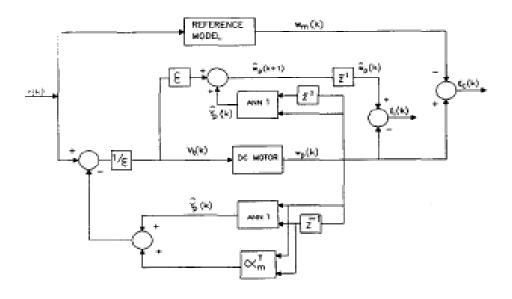


Figure 23: The Overall Structure Of The Controller In Topology

The maximum tracking error is 0.55 rad/s.

Both the ANN is the Block Diagram can be trained using the C-code mentioned in **Section** 7.4.

The overall structure of the identification and control system is displayed in Figure 20.

Chapter 9

RESULTS

9.1 TABLE OF OUTPUTS FOR COMPARISON:

KT	$W_p(k)$	$\widehat{W_p}(k+1)$	RMS ERROR	W _m (k)	$V_t(k)$	$\widehat{V_t}(\mathbf{k})$	W _p (k)
0	0	0	0	0	0	0	0
0.04	0.4478	0	0.4478	1.2022	5.5603	0	0
0.08	1.6429	1.5126	0.1303	2.4013	11.0919	7.1898	1.9486
0.12	3.0828	3.0041	0.0787	3.5939	16.5662	10.8739	2.988
0.16	4.5727	4.4738	0.0989	4.7769	21.9551	15.6482	4.3185
0.2	6.0509	5.919	0.1319	5.9471	27.231	20.7295	5.7224
0.24	7.4945	7.3335	0.161	7.1014	32.367	25.8374	7.1229
0.28	8.8921	8.7104	0.1817	8.2368	37.3371	30.8718	8.4934
0.32	10.2362	10.0428	0.1934	9.3503	42.1166	35.7857	9.8221
0.36	11.5206	11.324	0.1966	10.4389	46.6817	40.5486	11.1015
0.4	12.7401	12.5478	0.1923	11.4998	51.0103	45.1353	12.3261
0.44	13.8896	13.7082	0.1814	12.5303	55.0816	49.5232	13.4908
0.48	14.9648	14.7996	0.1652	13.5277	58.8768	53.6916	14.5913
0.52	15.9619	15.8168	0.1451	14.4895	62.3785	57.621	15.6236
0.56	16.8774	16.7554	0.122	15.4132	65.5715	61.2935	16.5841
0.6	17.7082	17.611	0.0972	16.2966	68.4425	64.6931	17.4695
0.64	18.4521 19.1069	18.3802 19.06	0.0719 0.0469	17.1374 17.9338	70.9802 73.1756	67.8052 70.6172	18.2773 19.0049
0.08	19.1009	19.6478	0.0409	18.6837	75.1730	73.1186	19.0049
0.72	20.144	20.1419	0.0021	19.3855	76.5142	75.3006	20.2126
0.70	20.5248	20.5409	-0.0161	20.0376	77.6504	77.1566	20.6902
0.84	20.8136	20.8443	-0.0307	20.6386	78.4303	78.6822	21.0826
0.88	21.0108	21.052	-0.0412	21.1872	78.856	79.8748	21.3897
0.92	21.1172	21.1646	-0.0474	21.6825	78.9319	80.734	21.6116
0.96	21.1342	21.1833	-0.0491	22.1234	78.6646	81.2614	21.7489
1	21.0634	21.1098	-0.0464	22.5093	78.0627	81.4605	21.8027
1.04	20.9073	20.9465	-0.0392	22.8396	77.1371	81.3367	21.7742
1.08	20.6684	20.6962	-0.0278	23.1139	75.9006	80.8977	21.6654
1.12	20.3501	20.3625	-0.0124	23.3321	74.3677	80.1531	21.4783
1.16	19.9556	19.9493	0.0063	23.4941	72.5548	79.1143	21.2158
1.2	19.4888	19.4609	0.0279	23.6001	70.4801	77.7939	20.8806
1.24	18.954	18.9023	0.0517	23.6504	68.1631	76.2061	20.4759
1.28	18.3559	18.2787	0.0772	23.6455	65.6248	74.3667	20.0054
1.32	17.6994	17.5958	0.1036	23.586	62.8873	72.2931	19.473
1.36	16.9896	16.8595	0.1301	23.4729	59.974	70.0038	18.883
1.4	16.2323	16.0761	0.1562	23.3071	56.9089	67.5177	18.2398
1.44	15.4331	15.2521	0.181	23.0897	53.7168	64.8554	17.5482
1.48	14.5982	14.3942	0.204	22.8221	50.4232	62.0378	16.8132
1.52	13.7338	13.5093	0.2245	22.5057	47.0539	59.0865	16.0401
1.56	12.8462	12.6042	0.242	22.1421	43.6346	56.0235	15.2342
1.6	11.9421	11.6859	0.2562	21.733	40.1915	52.8713	14.4011
1.64	11.028	10.7614	0.2666	21.2803	36.75	49.6521	13.5466
1.68	10.1105	9.8377	0.2728	20.786	33.3357	46.3886	12.6764
1.72	9.1966	8.9214 8.0193	0.2752	20.252	29.9733	43.1025	11.7963
1.76	8.2928		0.2735	19.6806	26.6868	39.8165	10.9123
1.8	7.4055	7.1377	0.2678	19.0741	23.4993	36.5515	10.0303

1.84	6.5413	6.283	0.2583	18.4347	20.433	33.3286	9.156
1.88	5.7063	5.461	0.2453	17.765	17.5087	30.1678	8.2952
1.92	4.9067	4.6773	0.2294	17.0674	14.7459	27.0884	7.4535
1.96	4.1481	3.937	0.2111	16.3445	12.1626	24.1089	6.6363
2	3.4359	3.2451	0.1908	15.5988	9.7753	21.2467	5.8489
2.04	2.775	2.6059	0.1691	14.8331	7.5984	18.5178	5.0961
2.08	2.1701	2.0234	0.1467	14.0499	5.6448	15.9369	4.3825
2.12	1.6252	1.5008	0.1244	13.2519	3.9255	13.5179	3.7124
2.16	1.1436	1.0411	0.1025	12.4418	2.4492	11.2729	3.0898
2.2	0.7287	0.6468	0.0819	11.6223	1.2229	9.2124	2.518
2.24	0.3824	0.3195	0.0629	10.796	0.2512	7.3459	2.0002
2.28	0.1068	0.0605	0.0463	9.9656	-0.4632	5.6808	1.5387
2.32	-0.0972	-0.1294	0.0322	9.1336	-0.9199	4.2232	1.1357
2.36	-0.229	-0.2503	0.0213	8.3027	-1.1205	2.9773	0.7925
2.4	-0.2889	-0.3024	0.0135	7.4753	-1.0689	1.9454	0.5102
2.44	-0.278	-0.287	0.009	6.6539	-0.7708	1.1295	0.2891
2.48	-0.1978	-0.2055	0.0077	5.8409	-0.2343	0.5291	0.1289
2.52	-0.0507	-0.0601	0.0094	5.0385	0.5309	0.1412	0.0289
2.56	0.1608	0.1465	0.0143	4.249	1.5129	-0.0387	-0.0122
2.6	0.4332	0.4111	0.0221	3.4745	2.6982	-0.0167	0.0038
2.64	0.7626	0.7302	0.0324	2.7171	4.0715	0.2008	0.0746
2.68	1.1443	1.0996	0.0447	1.9786	5.6159	0.6048	0.1976
2.72	1.5735	1.5147	0.0588	1.2608	7.3131	1.1848	0.3693
2.76	2.0448	1.9707	0.0741	0.5654	9.1434	1.9288	0.5862
2.8	2.5523	2.4624	0.0899	-0.106	11.0861	2.8237	0.8442
2.84	3.0902	2.984	0.1062	-0.752	13.1193	3.8549	1.1389
2.88	3.652	3.5298	0.1222	-1.3712	15.2203	5.0068	1.4657
2.92	4.2313	4.0937	0.1376	-1.9626	17.3657	6.2626	1.8197
2.96	4.8216	4.6693	0.1523	-2.5251	19.5318	7.6046	2.1959
3	5.4161	5.2504	0.1657	-3.0579	21.6942	9.0146	2.589
3.04	6.0083	5.8304	0.1779	-3.5601	23.8286	10.4735	2.9937
3.08	6.5911	6.4028	0.1883	-4.0312	25.9108	11.962	3.4047
3.12	7.1583	6.9611	0.1972	-4.4707	27.9166	13.4597	3.8164
3.16	7.7033	7.4988	0.2045	-4.8783	29.8224	14.947	4.2235
3.2	8.2199	8.0095	0.2104	-5.254	31.605	16.4038	4.6208
3.24	8.7018	8.4871	0.2147	-5.5976	33.2421	17.8104	5.0031
3.28	9.1434	8.9256	0.2178	-5.9092	34.7122	19.147	5.3652
3.32	9.5392	9.3191	0.2201	-6.1892	35.9949	20.3946	5.7023
3.36	9.8837	9.6623	0.2214	-6.4379	37.0713	21.535	6.0096
3.4	10.1723	9.95	0.2223	-6.6559	37.9235	22.5504	6.2827
3.44	10.4001	10.1774	0.2227	-6.8439	38.5353	23.4241	6.5174
3.48	10.5634	10.3403	0.2231	-7.0025	38.8923	24.1403	6.7096
3.52	10.6584	10.4347	0.2237	-7.1327	38.9816	24.6849	6.8557
3.56	10.6815	10.4572	0.2243	-7.2355	38.7923	25.0448	6.9523
3.6	10.6303	10.4049	0.2254	-7.3121	38.3156	25.208	6.9964
3.64	10.5021	10.2753	0.2268	-7.3636	37.5444	25.1647	6.9852
3.68	10.2951	10.0667	0.2284	-7.3914	36.474	24.9062	6.9165
3.72	10.0078	9.7778	0.23	-7.3968	35.1017	24.4256	6.7882
3.76	9.6394	9.4078	0.2316	-7.3815	33.427	23.7178	6.5987
3.8	9.1892	8.9566	0.2326	-7.3468	31.4516	22.7794	6.3467

3.84	8.6575	8.4248	0.2327	-7.2944	29.1795	21.6088	6.0314
3.88	8.0445	7.8133	0.2312	-7.226	26.6167	20.2061	5.6523
3.92	7.3515	7.124	0.2275	-7.1433	23.7715	18.5735	5.2094
3.96	6.58	6.3589	0.2211	-7.0481	20.6541	16.7146	4.7029
4	5.7319	5.521	0.2109	-6.9421	17.277	14.635	4.1337
4.04	4.8097	4.6135	0.1962	-6.8272	13.6544	12.342	3.5028
4.08	3.8166	3.6403	0.1763	-6.7052	9.8028	9.8442	2.8118
4.12	2.756	2.6059	0.1501	-6.5778	5.7399	7.1525	2.0626
4.16	1.6319	1.515	0.1169	-6.447	1.4856	4.2786	1.2577
4.2	0.4488	0.373	0.0758	-6.3144	-2.9389	1.2357	0.3997
4.24	-0.7879	-0.8145	0.0266	-6.1819	-7.5111	-1.9615	-0.5082
4.28	-2.0663	-2.0412	-0.0251	-6.0512	-12.2071	-5.3086	-1.4622
4.32	-3.3742	-3.301	-0.0732	-5.9241	-17.0019	-8.8219	-2.4543
4.36	-4.7023	-4.5872	-0.1151	-5.8021	-21.8697	-12.4678	-3.4751
4.4	-6.0428	-5.893	-0.1498	-5.6869	-26.7837	-16.2198	-4.517
4.44	-7.3881	-7.2112	-0.1769	-5.5799	-31.7168	-20.0556	-5.5736
4.48	-8.73	-8.5344	-0.1956	-5.4827	-36.6413	-23.9547	-6.6389
4.52	-10.0622	-9.8555	-0.2067	-5.3967	-41.5293	-27.894	-7.7067
4.56	-11.376	-11.1667	-0.2093	-5.323	-46.353	-31.8537	-8.7718
4.6	-12.6646	-12.4607	-0.2039	-5.263	-51.0847	-35.8092	-9.8279
4.64	-13.9215	-13.73	-0.1915	-5.2177	-55.697	-39.7376	-10.8693
4.68	-15.1394	-14.9672	-0.1722	-5.1881	-60.163	-43.6175	-11.8907
4.72	-16.3117	-16.1652	-0.1465	-5.1751	-64.4566	-47.4253	-12.8866
4.76	-17.4326	-17.3169	-0.1157	-5.1795	-68.5526	-51.1379	-13.8517
4.8	-18.4963	-18.4156	-0.0807	-5.2019	-72.4267	-54.7335	-14.7811
4.84	-19.4972	-19.4547	-0.0425	-5.2429	-76.0561	-58.1911	-15.6701
4.88	-20.4302	-20.428	-0.0022	-5.3028	-79.4191	-61.4899	-16.5143
4.92	-21.2907	-21.3298	0.0391	-5.3821	-82.4956	-64.61	-17.3094
4.96	-22.0744	-22.1547	0.0803	-5.4807	-85.2673	-67.5326	-18.0514
5	-22.7773	-22.8976	0.1203	-5.5988	-87.7175	-70.2399	-18.7368
5.04	-23.396	-23.5542	0.1582	-5.7363	-89.8316	-72.7158	-19.3621
5.08	-23.9276	-24.1205	0.1929	-5.8929	-91.5967	-74.9454	-19.9245
5.12	-24.3696	-24.5931	0.2235	-6.0683	-93.0023	-76.9154	-20.4211
5.16	-24.7197	-24.969	0.2493	-6.262	-94.0399	-78.6142	-20.8497
5.2	-24.9765	-25.2461	0.2696	-6.4733	-94.7031	-80.0318	-21.2082
5.24	-25.1388	-25.4225	0.2837	-6.7016	-94.9881	-81.1602	-21.4951
5.28	-25.2058	-25.4974	0.2916	-6.9459	-94.8931	-81.993	-21.7089
5.32	-25.1774	-25.4701	0.2927	-7.2054	-94.4186	-82.5257	-21.8487
5.36	-25.0537	-25.3409	0.2872	-7.4788	-93.5675	-82.756	-21.914
5.4	-24.8356	-25.1105	0.2749	-7.765	-92.345	-82.683	-21.9044
5.44	-24.5241	-24.7803	0.2562	-8.0628	-90.7585	-82.3081	-21.8201
5.48	-24.1207	-24.3523	0.2316	-8.3706	-88.8174	-81.6344	-21.6615
5.52	-23.6276	-23.8291	0.2015	-8.687	-86.5336	-80.6666	-21.4293
5.56	-23.047	-23.2138	0.1668	-9.0103	-83.9207	-79.4113	-21.1247
5.6	-22.3821	-22.5102	0.1281	-9.3391	-80.9943	-77.8768	-20.7492
5.64	-21.6363	-21.7224	0.0861	-9.6713	-77.7722	-76.0734	-20.3045
5.68	-20.8131	-20.8553	0.0422	-10.0054	-74.2734	-74.0131	-19.793
5.72	-19.9167	-19.9139	-0.0028	-10.3394	-70.5188	-71.7085	-19.217
5.76	-18.9517	-18.904	-0.0477	-10.6714	-66.5308	-69.1739	-18.5793
5.8	-17.923	-17.8315	-0.0915	-10.9994	-62.3329	-66.4253	-17.883

5.84	-16.8358	-16.7028	-0.133	-11.3214	-57.9499	-63.4792	-17.1317
5.88	-15.6958	-15.5246	-0.1712	-11.6354	-53.4074	-60.3535	-16.3288
5.92	-14.5088	-14.3039	-0.2049	-11.9395	-48.7321	-57.0667	-15.4786
5.96	-13.2809	-13.0477	-0.2332	-12.2314	-43.9509	-53.638	-14.5851
6	-12.0187	-11.7635	-0.2552	-12.5093	-39.0916	-50.0874	-13.6529
6.04	-10.7289	-10.4585	-0.2704	-12.7711	-34.1818	-46.435	-12.6866
6.08	-9.4183	-9.1404	-0.2779	-13.0147	-29.2496	-42.7014	-11.6913
6.12	-8.0939	-7.8165	-0.2774	-13.2382	-24.3226	-38.9075	-10.6719
6.16	-6.7628	-6.4944	-0.2684	-13.4397	-19.4284	-35.0734	-9.6338
6.2	-5.4326	-5.1813	-0.2513	-13.6172	-14.5938	-31.2195	-8.5822
6.24	-4.1103	-3.8846	-0.2257	-13.769	-9.8452	-27.3667	-7.5229
6.28	-2.8031	-2.6113	-0.1918	-13.8932	-5.208	-23.5341	-6.4611
6.32	-1.5184	-1.3682	-0.1502	-13.9882	-0.7067	-19.7409	-5.4024
6.36	-0.2634	-0.1618	-0.1016	-14.0524	3.6354	-16.0057	-4.3525
6.4	0.954	1.0016	-0.0476	-14.0842	7.7966	-12.3466	-3.3169
6.44	2.1206	2.1162	0.0044	-14.0823	11.7562	-8.764	-2.3016
6.48	3.2265	3.1766	0.0499	-14.0453	15.4954	-5.2548	-1.3159
6.52	4.266	4.178	0.088	-13.9719	18.9971	-1.8575	-0.3683
6.56	5.2349	5.1156	0.1193	-13.8612	22.2461	1.4047	0.5359
6.6	6.1298	5.9855	0.1443	-13.7122	25.2288	4.5152	1.3931
6.64	6.9479	6.7839	0.164	-13.5239	27.934	7.4603	2.2004
6.68	7.6872	7.508	0.1792	-13.2958	30.3524	10.2281	2.9557
6.72	8.3457	8.1551	0.1906	-13.0273	32.4767	12.8086	3.6569
6.76	8.9223	8.7234	0.1989	-12.7179	34.3021	15.1929	4.3024
6.8	9.4166	9.2114	0.2052	-12.3675	35.8256	17.3742	4.8913
6.84	9.8284	9.6185	0.2099	-11.9758	37.0468	19.3476	5.4227
6.88	10.1578	9.9445	0.2133	-11.5429	37.9671	21.1099	5.8964
6.92	10.406	10.1898	0.2162	-11.0691	38.5904	22.659	6.3122
6.96	10.5742	10.3553	0.2189	-10.5546	38.9224	23.9951	6.6706
7	10.6642	10.4428	0.2214	-10	38.9711	25.1204	6.9723
7.04	10.6784	10.4542	0.2242	-9.4059	38.7465	26.0376	7.2184
7.08	10.6194	10.3924	0.227	-8.7732	38.2604	26.7523	7.4102
7.12	10.4905	10.2604	0.2301	-8.1028	37.5265	27.2708	7.5496
7.16	10.2952	10.062	0.2332	-7.3959	36.5601	27.6011	7.6386
7.2	10.0375	9.8013	0.2362	-6.6537	35.3782	27.7527	7.6796
7.24	9.7218	9.4829	0.2389	-5.8776	33.9993	27.7362	7.6753
7.28	9.3527	9.1116	0.2411	-5.0692	32.4431	27.5635	7.6286
7.32	8.9355	8.6929	0.2426	-4.2303	30.7305	27.2475	7.5428
7.36	8.4754	8.2324	0.243	-3.3626	28.8835	26.8021	7.4213
7.4	7.9781	7.736	0.2421	-2.4682	26.9248	26.2419	7.2678
7.44	7.4494	7.2097	0.2397	-1.549	24.8778	25.5825	7.0863
7.48	6.8955	6.6599	0.2356	-0.6074	22.7664	24.8397	6.8809
7.52	6.3227	6.093	0.2297	0.3543	20.615	24.0299	6.6558
7.56	5.7374	5.5155	0.2219	1.3338	18.4477	23.1698	6.4155
7.6	5.1461	4.934	0.2121	2.3285	16.2889	22.2764	6.1644
7.64	4.5554	4.3549	0.2005	3.3359	14.1628	21.3663	5.9071
7.68	3.9718	3.7847	0.1871	4.3531	12.0928	20.4566	5.6484
7.72	3.4019	3.2298	0.1721	5.3776	10.1021	19.5635	5.3927
7.76	2.8521	2.6963	0.1558	6.4065	8.2129	18.7034	5.1447
7.8	2.3288	2.1902	0.1386	7.4368	6.4466	17.892	4.9091

7.84	1.8379	1.7172	0.1207	8.4659	4.8234	17.1443	4.6901
7.88	1.3856	1.2828	0.1028	9.4906	3.3624	16.4749	4.4922
7.92	0.9771	0.8919	0.0852	10.508	2.0811	15.8975	4.3194
7.96	0.6178	0.5494	0.0684	11.5152	0.9956	15.4247	4.1757
8	0.3124	0.2596	0.0528	12.5093	0.1204	15.0683	4.0646
8.04	0.0651	0.0262	0.0389	13.4872	-0.5318	14.839	3.9896
8.08	-0.12	-0.1473	0.0273	14.4461	-0.9502	14.7463	3.9535
8.12	-0.2398	-0.2581	0.0183	15.3831	-1.1259	14.7983	3.9589
8.16	-0.2915	-0.3037	0.0122	16.2952	-1.052	15.002	4.0082
8.2	-0.2733	-0.2823	0.009	17.1797	-0.7237	15.3639	4.1031
8.24	-0.1838	-0.1927	0.0089	18.0339	-0.1382	15.8884	4.2447
8.28	-0.0221	-0.0341	0.012	18.855	0.705	16.5779	4.4338
8.32	0.212	0.1936	0.0184	19.6405	1.8045	17.433	4.6707
8.36	0.5179	0.4899	0.028	20.3879	3.1565	18.4537	4.9554
8.4	0.8943	0.854	0.0403	21.0948	4.7553	19.6392	5.2871
8.44	1.3393	1.2841	0.0552	21.7588	6.593	20.986	5.6645
8.48	1.8502	1.7783	0.0719	22.3779	8.6597	22.4894	6.0861
8.52	2.4241	2.3338	0.0903	22.9499	10.9435	24.143	6.5494
8.56	3.057	2.9475	0.1095	23.473	13.4308	25.9392	7.052
8.6	3.7447	3.6157	0.129	23.9454	16.106	27.8687	7.5906
8.64	4.4825	4.3343	0.1482	24.3654	18.9519	29.9206	8.1618
8.68	5.265	5.0985	0.1665	24.7315	21.9497	32.0829	8.7616
8.72	6.0866	5.9034	0.1832	25.0425	25.0793	34.3425	9.386
8.76	6.9415	6.7436	0.1979	25.2971	28.3191	36.6845	10.0303
8.8	7.8233	7.6133	0.21	25.4945	31.6465	39.0932	10.6899
8.84	8.7254	8.5064	0.219	25.6337	35.0379	41.5519	11.3598
8.88	9.6411	9.4167	0.2244	25.7141	38.4689	44.0427	12.0349
8.92	10.5639	10.3375	0.2264	25.7352	41.9144	46.5466	12.7098
8.96	11.4867	11.2621	0.2246	25.6969	45.3489	49.0453	13.3795
9	12.4027	12.1837	0.219	25.5988	48.7464	51.5186	14.0385
9.04	13.3052	13.0953	0.2099	25.4413	52.0811	53.9462	14.6815
9.08	14.187	13.99	0.197	25.2244	55.3271	56.3086	15.3035
9.12	15.0419	14.8608	0.1811	24.9486	58.4589	58.5842	15.8989
9.16	15.8635	15.7009	0.1626	24.6145	61.4512	60.7535	16.463
9.2	16.6454	16.5035	0.1419	24.223	64.2795	62.7969	16.991
9.24	17.3815	17.262	0.1195	23.775	66.9203	64.6946	17.4782
9.28	18.0661	17.9701	0.096	23.2716	69.3506	66.4273	17.92
9.32	18.6939	18.6216	0.0723	22.7142	71.549	67.9768	18.3122
9.36	19.2597	19.2108	0.0489	22.1042	73.4951	69.3259	18.6509
9.4	19.7588	19.7322	0.0266	21.4433	75.1702	70.4585	18.9325
9.44	20.1868	20.1807	0.0061	20.7333	76.5569	71.3596	19.1536
9.48	20.5398 20.8142	20.5517	-0.0119 -0.0268	19.9761 19.1737	77.6396 78.4048	72.0155 72.4137	19.3113 19.4027
9.52	20.8142	21.045	-0.0268	18.3284	78.4048	72.5436	19.4027
9.36	21.0067	21.1605	-0.0363	17.4426	78.9373	72.3436	19.4233
9.64	21.1147	21.1848	-0.0438	16.5186	78.6872	72.3939	19.3777
9.68	21.1338	21.1159	-0.049	15.5592	78.0848	71.9031	19.2570
9.08	20.9108	20.9524	-0.0476	14.5668	77.1269	70.2219	18.7957
9.76	20.6625	20.6934	-0.0309	13.5444	75.8125	68.9082	18.4526
9.70	20.3226	20.3386	-0.0309	12.4947	74.1427	67.2986	18.0344
7.0	20.3220	20.3360	-0.010	14.474/	/+.144/	07.2700	10.0344

9.88 19.3693 19.3435 0.0258 10.3254 69.7536 63.1998 9.92 18.7572 18.7058 0.0514 9.2118 67.048 60.7208 9.96 18.0567 17.9774 0.0793 8.083 64.0145 57.9648 10 17.2695 17.1609 0.1086 6.9421 60.6653 54.9413 10.04 16.3982 16.2597 0.1385 5.7923 57.0149 51.6615 10.08 15.4454 15.2777 0.1677 4.6367 53.0793 48.1384 10.12 14.4145 14.2193 0.1952 3.4784 48.8769 44.3864 10.16 13.3092 13.0895 0.2197 2.3206 44.4273 40.4217 10.2 12.1337 11.8935 0.2402 1.1664 39.7522 36.2614 10.28 9.5908 9.3268 0.264 -1.1187 29.8181 27.4303	17.5411 16.9734 16.3322 15.619 14.8354 13.9835 13.0657 12.0848 11.044 9.9468 8.7971
9.92 18.7572 18.7058 0.0514 9.2118 67.048 60.7208 9.96 18.0567 17.9774 0.0793 8.083 64.0145 57.9648 10 17.2695 17.1609 0.1086 6.9421 60.6653 54.9413 10.04 16.3982 16.2597 0.1385 5.7923 57.0149 51.6615 10.08 15.4454 15.2777 0.1677 4.6367 53.0793 48.1384 10.12 14.4145 14.2193 0.1952 3.4784 48.8769 44.3864 10.16 13.3092 13.0895 0.2197 2.3206 44.4273 40.4217 10.2 12.1337 11.8935 0.2402 1.1664 39.7522 36.2614 10.24 10.8925 10.6372 0.2553 0.019 34.8744 31.9245 10.28 9.5908 9.3268 0.264 -1.1187 29.8181 27.4303	16.3322 15.619 14.8354 13.9835 13.0657 12.0848 11.044 9.9468 8.7971
9.96 18.0567 17.9774 0.0793 8.083 64.0145 57.9648 10 17.2695 17.1609 0.1086 6.9421 60.6653 54.9413 10.04 16.3982 16.2597 0.1385 5.7923 57.0149 51.6615 10.08 15.4454 15.2777 0.1677 4.6367 53.0793 48.1384 10.12 14.4145 14.2193 0.1952 3.4784 48.8769 44.3864 10.16 13.3092 13.0895 0.2197 2.3206 44.4273 40.4217 10.2 12.1337 11.8935 0.2402 1.1664 39.7522 36.2614 10.24 10.8925 10.6372 0.2553 0.019 34.8744 31.9245 10.28 9.5908 9.3268 0.264 -1.1187 29.8181 27.4303	15.619 14.8354 13.9835 13.0657 12.0848 11.044 9.9468 8.7971
10 17.2695 17.1609 0.1086 6.9421 60.6653 54.9413 10.04 16.3982 16.2597 0.1385 5.7923 57.0149 51.6615 10.08 15.4454 15.2777 0.1677 4.6367 53.0793 48.1384 10.12 14.4145 14.2193 0.1952 3.4784 48.8769 44.3864 10.16 13.3092 13.0895 0.2197 2.3206 44.4273 40.4217 10.2 12.1337 11.8935 0.2402 1.1664 39.7522 36.2614 10.24 10.8925 10.6372 0.2553 0.019 34.8744 31.9245 10.28 9.5908 9.3268 0.264 -1.1187 29.8181 27.4303	14.8354 13.9835 13.0657 12.0848 11.044 9.9468 8.7971
10.04 16.3982 16.2597 0.1385 5.7923 57.0149 51.6615 10.08 15.4454 15.2777 0.1677 4.6367 53.0793 48.1384 10.12 14.4145 14.2193 0.1952 3.4784 48.8769 44.3864 10.16 13.3092 13.0895 0.2197 2.3206 44.4273 40.4217 10.2 12.1337 11.8935 0.2402 1.1664 39.7522 36.2614 10.24 10.8925 10.6372 0.2553 0.019 34.8744 31.9245 10.28 9.5908 9.3268 0.264 -1.1187 29.8181 27.4303	13.9835 13.0657 12.0848 11.044 9.9468 8.7971
10.08 15.4454 15.2777 0.1677 4.6367 53.0793 48.1384 10.12 14.4145 14.2193 0.1952 3.4784 48.8769 44.3864 10.16 13.3092 13.0895 0.2197 2.3206 44.4273 40.4217 10.2 12.1337 11.8935 0.2402 1.1664 39.7522 36.2614 10.24 10.8925 10.6372 0.2553 0.019 34.8744 31.9245 10.28 9.5908 9.3268 0.264 -1.1187 29.8181 27.4303	13.0657 12.0848 11.044 9.9468 8.7971
10.12 14.4145 14.2193 0.1952 3.4784 48.8769 44.3864 10.16 13.3092 13.0895 0.2197 2.3206 44.4273 40.4217 10.2 12.1337 11.8935 0.2402 1.1664 39.7522 36.2614 10.24 10.8925 10.6372 0.2553 0.019 34.8744 31.9245 10.28 9.5908 9.3268 0.264 -1.1187 29.8181 27.4303	12.0848 11.044 9.9468 8.7971
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10.24 10.8925 10.6372 0.2553 0.019 34.8744 31.9245 10.28 9.5908 9.3268 0.264 -1.1187 29.8181 27.4303	8.7971
10.28 9.5908 9.3268 0.264 -1.1187 29.8181 27.4303	
	7.5989
10.32 8.2338 7.9688 0.265 -2.2437 24.6089 22.8	6.3567
10.36 6.8275 6.57 0.2575 -3.3529 19.2731 18.0552	5.0755
10.4 5.378 5.1376 0.2404 -4.4436 13.838 13.2182	3.7601
10.44 3.8919 3.6789 0.213 -5.513 8.3315 8.3119	2.4161
10.48 2.3758 2.2014 0.1744 -6.5583 2.782 3.3598	1.049
10.52 0.837 0.7128 0.1242 -7.5769 -2.782 -1.6151	-0.3355
10.56 -0.7166 -0.7794 0.0628 -8.5664 -8.3315 -6.5889	-1.7313
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11.6 -20.519 -20.5396 0.0206 -19.231 -75.1702 -76.0089 -	20.3612
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12 -14.1693 -13.9547 -0.2146 -15.5988 -48.7464 -54.5409 -14.8 12.04 -13.2925 -13.0588 -0.2337 -15.0887 -45.3489 -51.5077 -14.6 12.08 -12.3958 -12.1462 -0.2496 -14.5608 -41.9144 -48.3979 -13.1 12.12 -11.4858 -11.224 -0.2618 -14.0174 -38.4689 -45.2339 -12.3 12.16 -10.5693 -10.299 -0.2703 -13.4609 -35.0379 -42.0381 -10.661 12.2 -9.6528 -9.3782 -0.2746 -12.8937 -31.6465 -38.8326 -10.6 12.24 -8.743 -8.4682 -0.2748 -12.3181 -28.3191 -35.6392 -9.7 12.28 -7.8466 -7.5755 -0.2711 -11.7364 -25.0793 -32.4793 -8.5 12.32 -6.9701 -6.7066 -0.2635 -11.1509 -21.9497 -29.3736 -8 12.36 -6.1197 -5.8675
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12.72 -0.5468 -0.4746 -0.0722 -5.5489 -0.705 -5.1769 -1.4 12.76 -0.2357 -0.1814 -0.0543 -5.0548 0.1382 -3.7443 -1.0 12.8 0.0042 0.0431 -0.0389 -4.579 0.7237 -2.5272 -0.6 12.84 0.1721 0.1985 -0.0264 -4.1225 1.052 -1.5293 -0.4 12.88 0.2679 0.2849 -0.017 -3.6864 1.1259 -0.7525 -0 12.92 0.2922 0.3031 -0.0109 -3.2716 0.9502 -0.1976 -0.0 12.96 0.2464 0.2544 -0.008 -2.8791 0.5318 0.1361 0.0 13 0.1325 0.1406 -0.0081 -2.5093 -0.1204 0.2518 0.0 13.04 -0.0472 -0.0357 -0.0115 -2.1629 -0.9956 0.1549 0.0 13.08 -0.2897 -0.2718 -0.0179 -1.8402 -2.0811 </td
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13.84	-9.7181	-9.4973	-0.2208	0.1969	-36.5601	-26.6868	-7.3893
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14.32	-8.9335	-8.7007	-0.2328	-0.2848	-30.3524	-27.7831	-7.6868
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14.56	-4.3218	-4.1349	-0.1869	0.0029	-11.7562	-15.3979	-4.3115
14.6	-3.2945	-3.1305	-0.164	0.1162	-7.7966	-12.5237	-3.5166
14.64	-2.2017	-2.0672	-0.1345	0.2509	-3.6354	-9.4454	-2.6605
14.68	-1.0475	-0.95	-0.0975	0.4076	0.7067	-6.1768	-1.746
14.72	0.1634	0.2154	-0.052	0.5871	5.208	-2.733	-0.7764
14.76	1.4227	1.4233	-0.0006	0.79	9.8452	0.8701	0.2447
14.8	2.7171	2.6674	0.0497	1.0165	14.5938	4.6479	1.3114
14.84	4.0362	3.9412	0.095	1.2669	19.4284	8.5859	2.4139
14.88	5.3715	5.2381	0.1334	1.5415	24.3226	12.6501	3.5432
14.92	6.7154	6.551	0.1644	1.8402	29.2496	16.8156	4.692
14.96	8.0601	7.8726	0.1875	2.1629	34.1818	21.0602	5.854
15	9.3983	9.1957	0.2026	2.5093	39.0916	25.3603	7.0227
15.04	10.7218	10.5127	0.2091	2.8791	43.9509	29.6934	8.1919
15.08	12.0238	11.8163	0.2075	3.2716	48.7321	34.034	9.3551
15.12	13.2975	13.0989	0.1986	3.6864	53.4074	38.3584	10.5062
15.16	14.5357	14.353	0.1827	4.1225	57.9499	42.6433	11.6395
15.2	15.7316	15.5715	0.1601	4.579	62.3329	46.8641	12.7491
15.24	16.879	16.7473	0.1317	5.0548	66.5308	50.9958	13.8291
15.28	17.9719	17.8733	0.0986	5.5489	70.5188	55.0146	14.8739
15.32	19.0049	18.943	0.0619	6.0599	74.2734	58.8977	15.8785
15.36	19.9725	19.9499	0.0226	6.5863	77.7722	62.6228	16.8379
15.4	20.8698	20.8882	-0.0184	7.1267	80.9943	66.1682	17.7474
15.44	21.6924	21.7522	-0.0598	7.6794	83.9207	69.513	18.6025
15.48	22.4362	22.5367	-0.1005	8.2427	86.5336	72.6378	19.3991
15.52	23.0974	23.237	-0.1396	8.8148	88.8174	75.5244	20.1334
15.56	23.6729	23.8489	-0.176	9.3936	90.7585	78.1561	20.8019
15.6	24.16	24.3687	-0.2087	9.9773	92.345	80.5177	21.4014
15.64	24.5562	24.7933	-0.2371	10.5638	93.5675	82.5958	21.9292
15.68	24.8599	25.12	-0.2601	11.1509	94.4186	84.3785	22.3829
15.72	25.0695	25.347	-0.2775	11.7364	94.8931	85.8559	22.7603
15.76	25.1842	25.4727	-0.2885	12.3181	94.9881	87.0201	23.0598
15.8	25.2035	25.4965	-0.293	12.8937	94.7031	87.8649	23.28

15.92 24.6914 24.9577 -0.2663 14.5608 91.5967 88.4518 15.96 24.3338 24.5784 -0.2446 15.0887 89.8316 87.9978 16 23.8852 24.1024 -0.2172 15.5988 87.7175 87.2234 16.04 23.348 23.5327 -0.1847 16.0889 85.2673 86.1343 16.08 22.7249 22.8728 -0.1479 16.5565 82.4956 84.7376 16.12 22.0191 22.1265 -0.1074 16.9995 79.4191 83.0427 16.16 21.2341 21.2985 -0.0644 17.4156 76.0561 81.061 16.2 20.3737 20.3935 -0.0198 17.8026 72.4267 78.8049 16.24 19.4425 19.4172 0.0253 18.1585 68.5526 76.288 16.28 18.445 18.3752 0.0698 18.4812 64.4566 73.5261 16.32 17.3864 17.2738 0.1126 18.7687	23.42 23.4793 23.4575 23.3549 23.172 22.9098 22.5693 21.661 21.0976 20.4648 19.7658 19.7658 19.0038 18.1826 17.3063 16.379 15.4055 14.3905 13.339
15.92 24.6914 24.9577 -0.2663 14.5608 91.5967 88.4518 15.96 24.3338 24.5784 -0.2446 15.0887 89.8316 87.9978 16 23.8852 24.1024 -0.2172 15.5988 87.7175 87.2234 16.04 23.348 23.5327 -0.1847 16.0889 85.2673 86.1343 16.08 22.7249 22.8728 -0.1479 16.5565 82.4956 84.7376 16.12 22.0191 22.1265 -0.1074 16.9995 79.4191 83.0427 16.16 21.2341 21.2985 -0.0644 17.4156 76.0561 81.061 16.2 20.3737 20.3935 -0.0198 17.8026 72.4267 78.8049 16.24 19.4425 19.4172 0.0253 18.1585 68.5526 76.288 16.28 18.445 18.3752 0.0698 18.4812 64.4566 73.5261 16.32 17.3864 17.2738 0.1126 18.7687	23.4575 23.3549 23.172 22.9098 22.5693 22.1523 21.661 21.0976 20.4648 19.7658 19.0038 18.1826 17.3063 16.379 15.4055
15.96 24.3338 24.5784 -0.2446 15.0887 89.8316 87.9978 16 23.8852 24.1024 -0.2172 15.5988 87.7175 87.2234 16.04 23.348 23.5327 -0.1847 16.0889 85.2673 86.1343 16.08 22.7249 22.8728 -0.1479 16.5565 82.4956 84.7376 16.12 22.0191 22.1265 -0.1074 16.9995 79.4191 83.0427 16.16 21.2341 21.2985 -0.0644 17.4156 76.0561 81.061 16.2 20.3737 20.3935 -0.0198 17.8026 72.4267 78.8049 16.24 19.4425 19.4172 0.0253 18.1585 68.5526 76.288 16.28 18.445 18.3752 0.0698 18.4812 64.4566 73.5261 16.32 17.3864 17.2738 0.1126 18.7687 60.163 70.5358 16.36 16.2721 16.1195 0.1526 19.0192	23.3549 23.172 22.9098 22.5693 22.1523 21.661 21.0976 20.4648 19.7658 19.0038 18.1826 17.3063 16.379 15.4055 14.3905
16 23.8852 24.1024 -0.2172 15.5988 87.7175 87.2234 16.04 23.348 23.5327 -0.1847 16.0889 85.2673 86.1343 16.08 22.7249 22.8728 -0.1479 16.5565 82.4956 84.7376 16.12 22.0191 22.1265 -0.1074 16.9995 79.4191 83.0427 16.16 21.2341 21.2985 -0.0644 17.4156 76.0561 81.061 16.2 20.3737 20.3935 -0.0198 17.8026 72.4267 78.8049 16.24 19.4425 19.4172 0.0253 18.1585 68.5526 76.288 16.28 18.445 18.3752 0.0698 18.4812 64.4566 73.5261 16.32 17.3864 17.2738 0.1126 18.7687 60.163 70.5358 16.36 16.2721 16.1195 0.1526 19.0192 55.697 67.3349 16.4 15.1078 14.9191 0.1887 19.231 <	23.172 22.9098 22.5693 22.1523 21.661 21.0976 20.4648 19.7658 19.0038 18.1826 17.3063 16.379 15.4055 14.3905
16.04 23.348 23.5327 -0.1847 16.0889 85.2673 86.1343 16.08 22.7249 22.8728 -0.1479 16.5565 82.4956 84.7376 16.12 22.0191 22.1265 -0.1074 16.9995 79.4191 83.0427 16.16 21.2341 21.2985 -0.0644 17.4156 76.0561 81.061 16.2 20.3737 20.3935 -0.0198 17.8026 72.4267 78.8049 16.24 19.4425 19.4172 0.0253 18.1585 68.5526 76.288 16.28 18.445 18.3752 0.0698 18.4812 64.4566 73.5261 16.32 17.3864 17.2738 0.1126 18.7687 60.163 70.5358 16.36 16.2721 16.1195 0.1526 19.0192 55.697 67.3349 16.4 15.1078 14.9191 0.1887 19.231 51.0847 63.9422 16.48 12.6537 12.4087 0.245 19.5318	22.9098 22.5693 22.1523 21.661 21.0976 20.4648 19.7658 19.0038 18.1826 17.3063 16.379 15.4055 14.3905
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16.28 18.445 18.3752 0.0698 18.4812 64.4566 73.5261 16.32 17.3864 17.2738 0.1126 18.7687 60.163 70.5358 16.36 16.2721 16.1195 0.1526 19.0192 55.697 67.3349 16.4 15.1078 14.9191 0.1887 19.231 51.0847 63.9422 16.44 13.8995 13.6798 0.2197 19.4024 46.353 60.3775 16.48 12.6537 12.4087 0.245 19.5318 41.5293 56.6609 16.52 11.3768 11.1131 0.2637 19.6179 36.6413 52.8136 16.56 10.0758 9.8007 0.2751 19.6593 31.7168 48.8569	19.7658 19.0038 18.1826 17.3063 16.379 15.4055 14.3905
16.32 17.3864 17.2738 0.1126 18.7687 60.163 70.5358 16.36 16.2721 16.1195 0.1526 19.0192 55.697 67.3349 16.4 15.1078 14.9191 0.1887 19.231 51.0847 63.9422 16.44 13.8995 13.6798 0.2197 19.4024 46.353 60.3775 16.48 12.6537 12.4087 0.245 19.5318 41.5293 56.6609 16.52 11.3768 11.1131 0.2637 19.6179 36.6413 52.8136 16.56 10.0758 9.8007 0.2751 19.6593 31.7168 48.8569	19.0038 18.1826 17.3063 16.379 15.4055 14.3905
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16.4 15.1078 14.9191 0.1887 19.231 51.0847 63.9422 16.44 13.8995 13.6798 0.2197 19.4024 46.353 60.3775 16.48 12.6537 12.4087 0.245 19.5318 41.5293 56.6609 16.52 11.3768 11.1131 0.2637 19.6179 36.6413 52.8136 16.56 10.0758 9.8007 0.2751 19.6593 31.7168 48.8569	17.3063 16.379 15.4055 14.3905
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16.6 8.7574 8.4787 0.2787 19.6549 26.7837 44.8125	12.2566
16.64 7.4287 7.1548 0.2739 19.6036 21.8697 40.702	11.1484
16.68 6.0971 5.8363 0.2608 19.5047 17.0019 36.5471	10.0202
16.72 4.77 4.5305 0.2395 19.3573 12.2071 32.3692	8.8778
16.76 3.4543 3.2446 0.2097 19.1609 7.5111 28.1902	7.727
16.8 2.1575 1.9855 0.172 18.9151 2.9389 24.03	6.5737
16.84 0.8868 0.76 0.1268 18.6197 -1.4856 19.9092	5.4238
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16.92 -1.5444 -1.5653 0.0209 17.8797 -9.8028 11.8612	3.1579
16.96 -2.6815 -2.6535 -0.028 17.4354 -13.6544 7.936	2.0559
17 -3.7549 -3.685 -0.0699 16.9421 -17.277 4.1012	0.9872
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17.2	-3.6701
17.24	-4.4425
17.28 -9.1798 -8.9775 -0.2023 12.1873 -35.1017 -18.3722	-5.1568
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17.6 -10.5635 -10.335 -0.2285 4.4436 -37.9235 -31.5898	-8.7066
17.64 -10.4009 -10.1693 -0.2316 3.3529 -37.0713 -32.2553	-8.8855
17.68 -10.1739 -9.9392 -0.2347 2.2437 -35.9949 -32.7184	-9.01
17.72	-9.0825
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17.8 -9.1498 -8.9079 -0.2419 -1.1664 -31.605 -32.9904	-9.0823

17.84	-8.7105	-8.4675	-0.243	-2.3206	-29.8224	-32.7476	-9.0156
17.88	-8.231	-7.9883	-0.2427	-3.4784	-27.9166	-32.36	-8.909
17.92	-7.7173	-7.4762	-0.2411	-4.6367	-25.9108	-31.8424	-8.7662
17.96	-7.1752	-6.9373	-0.2379	-5.7923	-23.8286	-31.21	-8.5912
18	-6.6111	-6.3782	-0.2329	-6.9421	-21.6942	-30.4787	-8.388
18.04	-6.0312	-5.8052	-0.226	-8.083	-19.5318	-29.665	-8.161
18.08	-5.4421	-5.2248	-0.2173	-9.2118	-17.3657	-28.7854	-7.9145
18.12	-4.8502	-4.6437	-0.2065	-10.3254	-15.2203	-27.8571	-7.6532
18.16	-4.2623	-4.0683	-0.194	-11.4208	-13.1193	-26.8968	-7.3817
18.2	-3.6847	-3.5049	-0.1798	-12.4947	-11.0861	-25.9213	-7.1046
18.24	-3.1241	-2.96	-0.1641	-13.5444	-9.1434	-24.9474	-6.8267
18.28	-2.5867	-2.4394	-0.1473	-14.5668	-7.3131	-23.9914	-6.5526
18.32	-2.0789	-1.9492	-0.1297	-15.5592	-5.6159	-23.0693	-6.287
18.36	-1.6066	-1.4948	-0.1118	-16.5186	-4.0715	-22.1962	-6.0345
18.4	-1.1755	-1.0816	-0.0939	-17.4426	-2.6982	-21.3871	-5.7993
18.44	-0.791	-0.7144	-0.0766	-18.3284	-1.5129	-20.6559	-5.5858
18.48	-0.4581	-0.3977	-0.0604	-19.1737	-0.5309	-20.0155	-5.3978
18.52	-0.1812	-0.1356	-0.0456	-19.9761	0.2343	-19.4782	-5.2392
18.56	0.0354	0.0682	-0.0328	-20.7333	0.7708	-19.0548	-5.1133
18.6	0.1883	0.2107	-0.0224	-21.4433	1.0689	-18.7556	-5.0231
18.64	0.2743	0.2891	-0.0148	-22.1042	1.1205	-18.5887	-4.9715
18.68	0.2913	0.3015	-0.0102	-22.7142	0.9199	-18.5623	-4.9608
18.72	0.2375	0.2461	-0.0086	-23.2716	0.4632	-18.6832	-4.9926
18.76	0.112	0.122	-0.01	-23.775	-0.2512	-18.956	-5.0684
18.8	-0.0859	-0.0711	-0.0148	-24.223	-1.2229	-19.3834	-5.189
18.84	-0.356	-0.3332	-0.0228	-24.6145	-2.4492	-19.967	-5.3549
18.88	-0.6974	-0.6636	-0.0338	-24.9486	-3.9255	-20.708	-5.5661
18.92	-1.1084	-1.0609	-0.0475	-25.2244	-5.6448	-21.6055	-5.8219
18.96	-1.5867	-1.5234	-0.0633	-25.4413	-7.5984	-22.6571	-6.1214
19	-2.1295	-2.0486	-0.0809	-25.5988	-9.7753	-23.8584	-6.4629
19.04	-2.7335	-2.6336	-0.0999	-25.6969	-12.1626	-25.2043	-6.8444
19.08	-3.3943	-3.2751	-0.1192	-25.7352	-14.7459	-26.6876	-7.2633
19.12	-4.1077	-3.969	-0.1387	-25.7141	-17.5087	-28.2996	-7.7168
19.16	-4.8685	-4.711	-0.1575	-25.6337	-20.433	-30.0305	-8.2016
19.2	-5.6713	-5.4962	-0.1751	-25.4945	-23.4993	-31.8693	-8.7141
19.24	-6.5103	-6.3195	-0.1908	-25.2971	-26.6868	-33.8032	-9.2502
19.28	-7.3794	-7.1751	-0.2043	-25.0425	-29.9733	-35.8186	-9.8057
19.32	-8.2722	-8.0573	-0.2149	-24.7315	-33.3357	-37.9005	-10.3763
19.36	-9.182	-8.9598	-0.2222	-24.3654	-36.75	-40.0333	-10.9572
19.4	-10.1021	-9.8762	-0.2259	-23.9454	-40.1915	-42.1996	-11.5435
19.44	-11.0256	-10.7997	-0.2259	-23.473	-43.6346	-44.382	-12.1304
19.48	-11.9459	-11.7237	-0.2222	-22.9499	-47.0539	-46.5625	-12.7128
19.52	-12.856	-12.6412	-0.2148	-22.3779	-50.4232	-48.7225	-13.286
19.56	-13.749	-13.5452	-0.2038	-21.7588	-53.7168	-50.8429	-13.8449
19.6	-14.6182	-14.4288	-0.1894	-21.0948	-56.9089	-52.9043	-14.3845
19.64	-15.4572	-15.2851	-0.1721	-20.3879	-59.974	-54.8869	-14.9
19.68	-16.2598	-16.1073	-0.1525	-19.6405	-62.8873	-56.7724	-15.3868
19.72	-17.0195	-16.8886	-0.1309	-18.855	-65.6248	-58.5419	-15.8404
19.76	-17.7306	-17.6227	-0.1079	-18.0339	-68.1631	-60.1765	-16.2564
19.8	-18.3874	-18.3033	-0.0841	-17.1797	-70.4801	-61.6581	-16.6306

19.84	-18.9848	-18.9243	-0.0605	-16.2952	-72.5548	-62.9699	-16.9592
19.88	-19.5178	-19.4803	-0.0375	-15.3831	-74.3677	-64.0956	-17.2384
19.92	-19.982	-19.9658	-0.0162	-14.4461	-75.9006	-65.0202	-17.4649
19.96	-20.373	-20.3761	0.0031	-13.4872	-77.1371	-65.7295	-17.6357
20	-20.687	-20.7068	0.0198	-12.5093	-78.0627		

9.2 PLOT OF TRAINED ANN FROM SYSTEM IDENTIFICATION CODING:

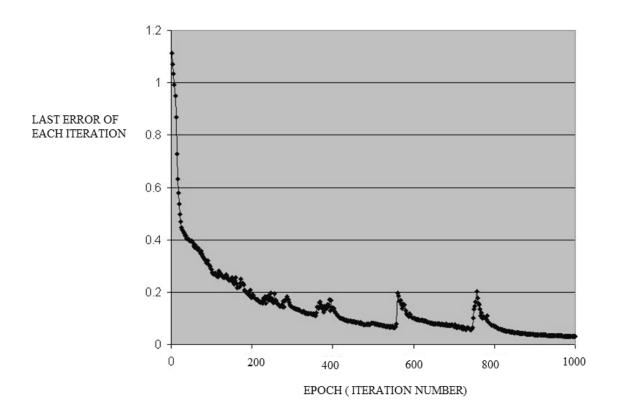


Figure 24: Trend of root-mean-squared (RMS) error for the entire training set over several training iterations

Chapter 10

CONCLUSION

10.1 DISCUSSIONS:

The speed trajectory of a dc motor has been successfully controlled by using a neural network based model reference adaptive control (MRAC) technique. A multi-layer perceptron is used to identify the motor dynamics. The trained neural network is then used to derive the appropriate control voltage for trajectory control of the rotor speed.

The controller design does not require explicit knowledge of the motor/load dynamics which is a useful feature when dealing with parameter and load uncertainties. The actual tuning of the controller only involves minimal effort. The motor displays good tracking performance for different speed trajectories. The robustness of the controller is positively established by evaluating its performance under noisy loading conditions. The controller remains stable for a wide range of sampling frequencies.

It is believed that better control performance can be obtained by training the neural network on-line. However, the resulting increased computational overhead at each sampling instant calls for a faster and more efficient software/hardware arrangement.

The unknown, time invariant, nonlinear operating characteristics of the dc motor and its load have been successfully captured by an ANN. The concepts of model reference adaptive control have been used in conjunction with the trained ANN to achieve trajectory control of the rotor speed.

10.2 FUTURE SCOPE:

The ability to deal with a noisy operating environment is always an important consideration for electric drives control. Noise can be introduced due to several reasons. Two main causes are motor-load parameter drift and quantization and resolution errors of the speed and/or position encoders. A high performance drive controller should be robust enough to maintain accurate tracking performance regardless of the noisy operating environment. *ANN*

based controllers have the inherent noise rejection capability of the ANN built into them.

Therefore *ANN* based controllers are expected to display superior performance under noisy operating environments.

The investigation of the controller performance under noise can be a cruitial phenomenon that can be studied through the necessary simulations.

Chapter 11

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