

EE206 - 2 STAGE OTA DESIGN ASSIGNMENT

YOUKTA MANDAVKAR 230108062

Technology used: TSMC 0.18 μm

Data: $V_{Tn} = 0.37\text{V}$ $\mu_{n\text{Cox}} = 230\mu\text{A/V}^2$ $V_{dd} = 1.8\text{V}$ $W_{\text{min}} = 0.27\mu\text{m}$
 $V_{Tp} = 0.39\text{V}$ $\mu_{p\text{Cox}} = 100\mu\text{A/V}^2$ $L_{\text{min}} = 0.18\mu\text{m}$

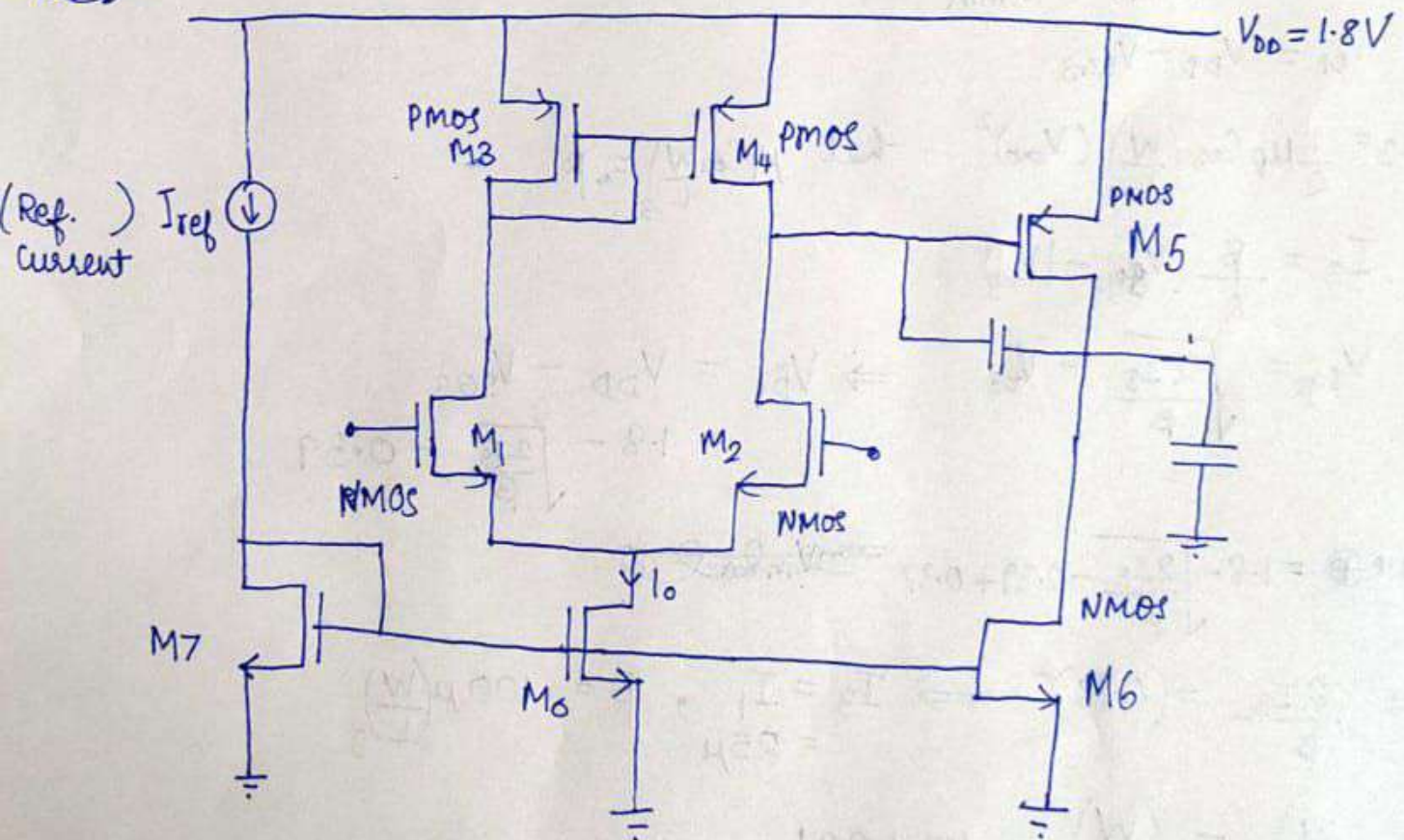
Specifications: (Chosen & given)

1. DG gain $\geq 40\text{ dB}$
2. Non-inverting gain = 2
3. GBW = 10 MHz
4. PM $\geq 60^\circ$
5. Slew Rate = ~~20~~ $\text{V}/\mu\text{s}$
6. ICMR+ = 1.6V
7. ICMR- = 0.8V
8. $C_L = 10\text{pF}$
9. $V_{dd} = 1.8\text{V}$
10. $I_{\text{ref}} = I_0/10$

Thumb Rule for PM $\geq 60^\circ$: $C_c \geq 0.22 C_L$
 $\geq 2.2\text{pF}$

Choosing $[C_c = 2.5\text{pF}]$

Diagram:



M_{1-2} : Input Differential pair
 M_{3-4} : Current mirror active loads
 M_5 : Stage 2 Amplifier

M_6 : Stage 2 current source
 M_7 : Current mirror MOSFET
 M_0 : Input stage current source

$$1. \text{ Slew Rate} = \frac{I_0}{C_c} \Rightarrow \left[I_0 = 16.67 \times 3 \text{ pF} = 50 \mu\text{A} \right] \quad \begin{matrix} I_0 = 20 \text{ V}/\mu\text{s} \times 2.5 \text{ pF} \\ [I_0 = 50 \mu\text{A}] \end{matrix}$$

$$2. g_{m1} = \text{GBW} \times 2\pi \times C_c = 10 \text{ MHz} \times 2\pi \times 2.5 \text{ pF} = 157.08 \mu\text{A}/\text{V}^2$$

$$\left(\frac{W}{L} \right)_1 = \frac{g_{m1}^2}{\mu_n C_{ox} 2 I_D} \quad I_D = \frac{I_0}{2} = \frac{50}{2} = 25 \mu\text{A}$$

$$= \frac{(157.08)^2}{230 \times 2 \times 25} = 2.14557 \Rightarrow \left[\left(\frac{W}{L} \right)_1 = \left(\frac{W}{L} \right)_2 = 2.14557 \right]$$

3. For M_3, M_4 (using ICMR \oplus)

M_3 is always in saturation $\therefore G, D$ connected.

\therefore To keep M_1 in saturation.

$$V_{D1} \geq V_{G1} - V_{t1}$$

$$V_{G1} \leq V_{D1} + V_{t1}$$

$$V_{in\max} \leq V_{D1\min} + V_{t1\min}$$

$$V_{D1} = V_{DD} - V_{SG3}$$

$$I_3 = \frac{1}{2} \mu_p C_{ox} \left(\frac{W}{L} \right)_3 (V_{ov})^2 \quad \text{let } \mu_p C_{ox} \left(\frac{W}{L} \right)_3 = \beta$$

$$\Rightarrow I_3 = \frac{\beta}{2} (V_{SG3} - |V_{t3}|)^2$$

$$V_{SG3} = \sqrt{\frac{2I_3}{\beta}} + V_{t3} \Rightarrow V_{D1} = V_{DD} - V_{SG3} = 1.8 - \sqrt{\frac{2I_3}{\beta}} - 0.39$$

$$\Rightarrow \text{ICMR}\oplus = 1.8 - \sqrt{\frac{2I_3}{\beta}} - 0.39 + 0.37 \Rightarrow \text{ICMR}\oplus = 1.8 - \sqrt{\frac{2I_3}{\beta}} - 0.02$$

$$\Rightarrow \frac{2I_3}{\beta} = (0.18)^2 \Rightarrow I_3 = I_1, \quad \beta = 100 \mu \left(\frac{W}{L} \right)_3 = 25 \mu$$

$$\Rightarrow \left(\frac{W}{L} \right)_3 = \left(\frac{W}{L} \right)_4 = 15.4321$$

4. $\left(\frac{W}{L}\right)_{M_0}$ using ICMR \ominus

$$\begin{aligned} V_{D0} &\geq V_{G0} - V_{th} \\ V_{D0} &= V_{in} - V_{gs1} \\ &= V_{dsat} \end{aligned} \quad \left| \quad \begin{aligned} V_{in} &\geq V_{gs1} + V_{dsat} \\ \Rightarrow \text{ICMR}\ominus &= V_{gs1} + V_{dsat} \end{aligned} \right.$$

$$I_{D0} = \frac{1}{2} \mu_n C_{ox} \left(\frac{W}{L}\right)_0 [V_{dsat}]^2 = I_0$$

$$\begin{aligned} \Rightarrow \text{ICMR}\ominus &= 0.8V = V_{ov} + V_{th} + V_{dsat} \\ &= \sqrt{\frac{2I_{D1}}{\beta_1}} + 0.37 + V_{dsat} \end{aligned}$$

$$\begin{aligned} \Rightarrow V_{dsat} &= 0.8 - \sqrt{\frac{2I_{D1}}{\beta_1}} - 0.37 \\ &= 0.8 - \sqrt{\frac{2 \times 25}{230 \times 2.14557}} - 0.37 \end{aligned}$$

$$V_{dsat} = 0.1117V$$

$$\Rightarrow I_D = \frac{1}{2} \mu_n C_{ox} \left(\frac{W}{L}\right)_0 (V_{dsat})^2$$

$$50 = \frac{1}{2} \times 230 \times \frac{W}{L} \times 0.0124$$

$$\left[\left(\frac{W}{L}\right)_0 = 34.85\right]$$

5. $M_5: 60^\circ = PM$

$$g_{m5} \geq 10 \cdot g_{m1} \quad g_{m5} \geq 1570.8 \mu A/V^2$$

$$I_D \propto \frac{W}{L} \propto g_m \quad \therefore \left(\frac{W}{L}\right)_5 = \frac{g_{m5}}{g_{m4}} \times \left(\frac{W}{L}\right)_4$$

$$g_{m4} = \mu_p C_{ox} \left(\frac{W}{L}\right)_4 (V_{gs} - V_{th})$$

$$= \sqrt{2 \cdot I_D \cdot \mu_p C_{ox} \left(\frac{W}{L}\right)_4} = \sqrt{2 \times 25 \times 100 \times 15.4321} = 277.77 \mu A/V^2$$

$$\Rightarrow \left(\frac{W}{L}\right)_5 = \frac{1570.8}{277.77} \times 15.4321 = [87.27 = \left(\frac{W}{L}\right)_5]$$

$$6. I_5 = \frac{(W/L)_5}{(W/L)_4} \times I_4 = 141.38 \mu A$$

$$\frac{I_6}{I_0} = \frac{(W/L)_6}{(W/L)_0} \Rightarrow \frac{141.38}{50} \times 34.85 = \left[98.54 = \left(\frac{W}{L} \right)_6 \right]$$

$$7. I_{ref} = \frac{I_0}{10} = 5 \mu A$$

$$\left(\frac{W}{L} \right)_7 = \frac{\left(\frac{W}{L} \right)_0}{10} = \left[3.485 = \left(\frac{W}{L} \right)_7 \right]$$

⇒ Summary of (W/L) Values:

$$\left(\frac{W}{L} \right)_0 = 34.85, \left(\frac{W}{L} \right)_{1,2} = 2.14557, \left(\frac{W}{L} \right)_{3,4} = 15.4321,$$

$$\left(\frac{W}{L} \right)_5 = 87.27, \left(\frac{W}{L} \right)_6 = 98.54, \left(\frac{W}{L} \right)_7 = 3.485$$

* Simulated Values:

Other values:

$$C_L = 10 \text{ pF} \quad C_c = 2.5 \text{ pF} \quad C_1 = 100 \mu F$$

* Gain = 2 in Feedback

$$\therefore 1 + \frac{R_f}{R_{in}} = 2 \Rightarrow \frac{R_f}{R_1} = \frac{R_{in}}{R_2} = 10 \text{ k}\Omega$$

* DC gain = 51.68756 dB

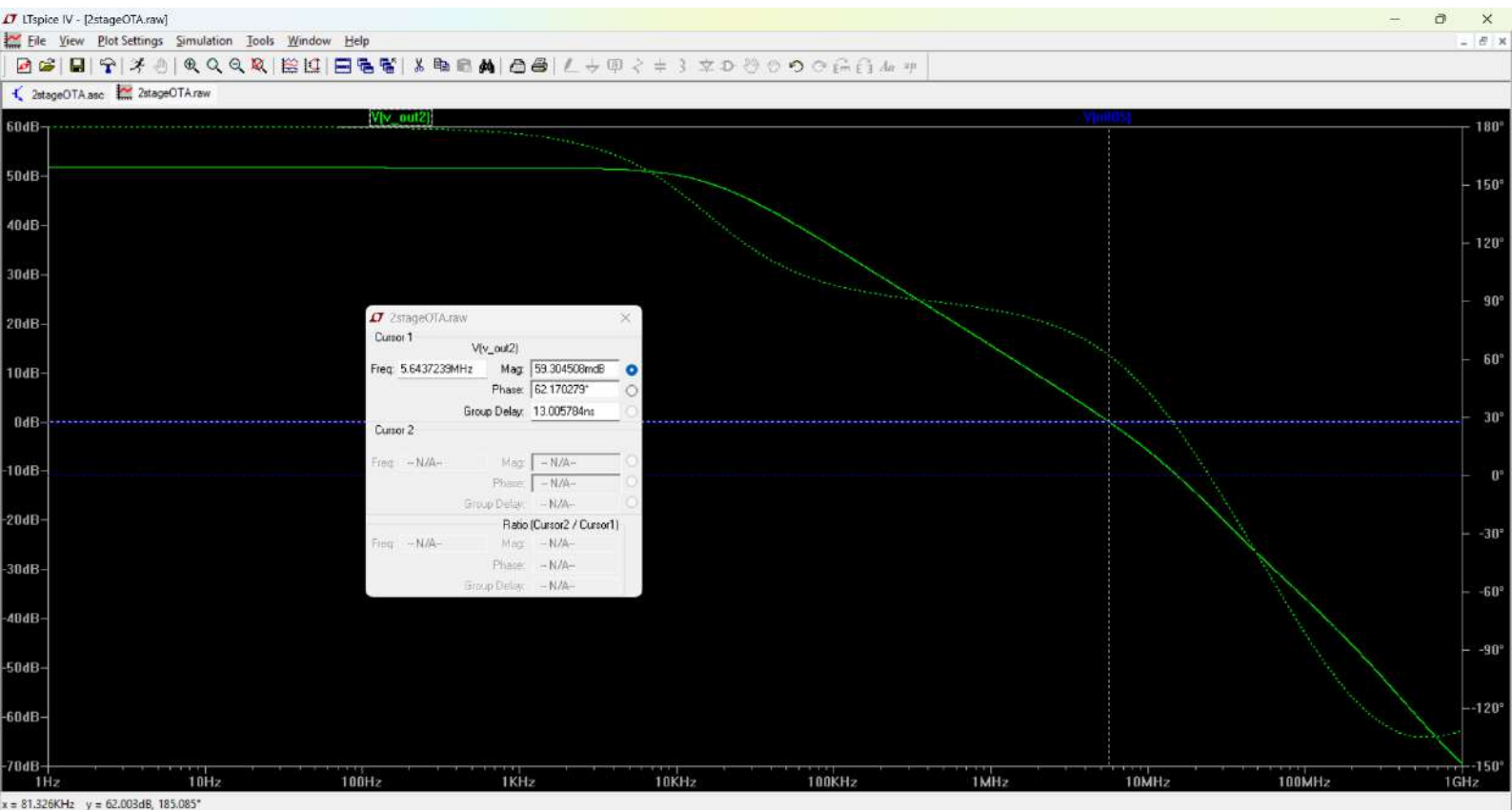
$$* \text{ Power dissipation} = 1.8 \text{ V} (50 \mu A + 2 \times 1.95 \times 10^{-5} \text{ A} + 1.18 \times 10^{-4} \text{ A})$$

$$[\text{Power max} = 291 \mu W]$$

$$P_{calc} = 1.8 [50 \mu A + 141.39 \mu A + 5 \mu A]$$

$$[= 353.502 \mu W]$$

AC Analysis



DC gain = 51.6875 dB

Phase Margin = 62.170279 deg

Transient Analysis

