

Problem Set 12

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1. A rectangular wire loop is situated in a uniform low-frequency time-harmonic magnetic field of flux density $B(t) = B_0 \sin \omega t$ ($B_0 > 0$). The vector \vec{B} is perpendicular to the plane of the loop, as shown in Fig.Q6.3. The magnetic field due to induced currents can be neglected. The induced emf in the loop is of the following form (\mathcal{E}_0 is positive constant):

Solution: D, $e_{\text{ind}}(t) = -\mathcal{E}_0 \cos \omega t$. This is because the induced emf is proportional to $-\frac{\partial B}{\partial t}$.

2. A rectangular copper contour of area S is first situated outside any magnetic field, and there is no current in it. The contour is then brought in a uniform time-invariant magnetic field of flux density \vec{B} and positioned so that the vector \vec{B} is perpendicular to the plane of the contour (like the situation in Fig.Q6.3). In the new steady state, the magnetic flux through the contour due to the current induced in it, computed with respect to the same orientation as that of the vector \vec{B} , equals

Solution: E, $\Phi_{\text{ind}} = 0$. There is no induced emf when \vec{B} does not vary with time.

3. An air-filled infinitely long solenoidal coil with a circular cross section of radius a carries a slowly time-varying current. The magnetic flux through a surface spanned over one turn of the coil is $\Phi(t)$. An open-circuited circular wire loop of radius b ($b > a$) is placed coaxially around the solenoid, as shown in Fig.Q6.4. The voltage between the terminals of the loop, for the reference orientation of the terminals in the figure, equals

Solution: A, $v(t) = \frac{d\Phi}{dt}$. This is based on the formula sheet. If $\frac{d\Phi}{dt} > 0$, induced current flows in the clockwise direction, according to the right hand rule. Hence, in this open circuit, current "wants" to go from the positive to the negative end, so $v(t) > 0$.

4. Consider the induced electromotive force, e_{ind} , and induced electric field intensity, E_{ind} , along the loop in Fig.Q6.4. If the radius of the loop is doubled (becomes $2b$), while both a and $\Phi(t)$ are not changed, we have that

Solution: D, e_{ind} remains the same, and E_{ind} is halved. This is because the former only depends on $-\frac{\partial \Phi(t)}{\partial t}$ which remains constant. It is also equal to $\oint \vec{E} \cdot d\vec{l}$. Since the contour it integrates over is doubled, \vec{E} should be halved.

5. If the loop in Fig. Q6.4 is an imaginary (nonmaterial) contour, in place of a conducting wire loop, which of the two quantities, the induced electromotive force (\mathcal{E}_{ind}) and induced electric field intensity (E_{ind}), along the contour remain the same as along the conducting wire?

Solution: C, both quantities. The only thing that matters is $\Phi(t)$, which stays the same.

6. A coil of wire, with a low-frequency time-harmonic current $i(t) = I_0 \cos \omega t$, is wound uniformly and densely about a thin toroidal core made of a nonlinear ferromagnetic material that exhibits hysteresis effects. Consider the magnetic flux density, $B(t)$, and magnetic field intensity, $H(t)$, in the core, as well as the induced emf, $\mathcal{E}_{\text{ind}}(t)$, in the coil. Which of these quantities are time-harmonic functions?

Solution: B, $H(t)$ only. This is because $H(t)$ is determined by the current. However, $B(t)$ follows the hysteresis curve, and is hence not time harmonic. \mathcal{E}_{ind} is proportional to the derivative of $B(t)$, so it is also not time harmonic.

7. Fig. Q6.5 portrays four cases of either a (closed) contour or open line (with two ends) that are either imaginary (nonmaterial) or made of a metallic wire - moving uniformly with a velocity \vec{v} in a time-invariant (static) magnetic field of flux density \vec{B} , in a vacuum. For a specific orientation in space of the vector \vec{B} , it is possible for an emf to be induced ($\mathcal{E}_{\text{ind}} \neq 0$) along the contour/line in

Solution: E, all four cases. Consider the electrons on the open lines. Since $\vec{F} = q\vec{v} \times \vec{B}$, we can have a \vec{B} such that \vec{F} is nonzero. This means an emf can be induced, given a suitable selection of \vec{B} which causes \vec{F} to point along the lines. For the contours, simply consider \vec{B} which changes with position, so Φ is nonzero.

8. A metallic bar (of finite length) moves uniformly with a velocity \vec{v} in a steady uniform magnetic field of flux density \vec{B} . Fig. Q6.6 shows five cases with different positions of the bar and of its velocity vector with respect to the magnetic field lines. There is a nonzero emf induced in the bar ($\mathcal{E}_{\text{ind}} \neq 0$) for

Solution: D, cases (a) and (c) only. $\vec{F} = q\vec{v} \times \vec{B}$. If \vec{F} is not perpendicular to the bar, then an emf is induced.

9. A rectangular loop moves with a constant velocity v ($\vec{v} = v\hat{a}_x$) in a magnetic field of flux density vector \vec{B} . The ambient medium is air. Referring to Fig. Q6.7, and with \vec{B}_0 , ω , and a being positive constants, there is a nonzero emf induced in the loop ($\mathcal{E}_{\text{ind}} \neq 0$) if

Solution: F, more than one of the above cases. When \vec{B} is in the \hat{a}_z direction, Φ becomes nonzero. If either \vec{B} changes with time or with position, flux would change with time, so there will be an induced emf.

10. A planar metallic wire loop moves with a velocity \vec{v} in a nonuniform static magnetic field of flux density \vec{B} , as depicted in Fig. Q6.8. The magnetic field due to the induced current in the loop is negligible. Consider the following two expressions computed for this loop:

$$A_1 = -\frac{d}{dt} \int_s \vec{B} \cdot d\vec{S}$$

and

$$A_2 = \oint_C (\vec{v} \times \vec{B}) \cdot d\vec{l}$$

where the reference directions of $d\vec{l}$ and $d\vec{S}$ are interconnected by the right-hand rule. Which of the following is true for the induced emf, e_{ind} , in the loop?

Solution: C, $e_{\text{ind}} = A_1 = A_2$. This is literally in the formula sheet.

11. Fig. Q6.9 shows a circular loop that rotates with a constant angular velocity ω about its axis in a uniform time-invariant magnetic field of flux density B . The vector \vec{B} is perpendicular to the plane of drawing. With \mathcal{E}_0 being a positive constant and $T = \frac{2\pi}{\omega}$, the induced emf in the loop is of the following form:

Solution: A, $e_{\text{ind}} = \mathcal{E}_0 \cos \omega t$. This is because it is proportional to $\frac{d\Phi}{dt}$. But then $\Phi = \vec{B} \cdot \vec{S} = BS \cos \theta$, where θ is the angle between both vectors. As the angle has a constant derivative, Φ is sinusoidal, so the induced emf, its derivative, is also sinusoidal.

12. A liquid of conductivity σ flows with a constant velocity $\vec{v} = v\hat{a}_x$ through a tube of width d , in which a uniform time-invariant magnetic field of flux density $\vec{B} = B\hat{a}_y$ is applied, as depicted in Fig. Q6.10. The induced electric field intensity vector, \vec{E}_{ind} , and the field intensity vector due to excess charge, \vec{E}_q , in the liquid are given by

Solution: E, $\vec{E}_{\text{ind}} = vB\hat{a}_z$, $\vec{E}_q = -vB\hat{a}_z$. The force induced on the electron goes in the $-\hat{a}_z$ direction, so the induced current goes in the opposite direction as that. The field from excess charges would counter the current, pointing in the opposite direction.

13. If the loop in Fig. Q6.9 uniformly rotates in a low-frequency time-harmonic uniform magnetic field of flux density $B(t) = B_0 \cos \omega t$ ($B_0 > 0$), the induced emf in the loop, with $\mathcal{E}_0 > 0$, can be represented as

Solution: B, $e_{\text{ind}}(t) = \mathcal{E}_0 \sin 2\omega t$. There is an extra $\cos \omega t$ term in Φ , so its derivative is proportional to

$$\frac{d}{dt} \cos^2 \omega t = -2\omega \cos \omega t \sin \omega t = -\omega \sin 2\omega t$$

14. Assume that the magnetic flux density vector \vec{B} in Fig. Q6.9 also rotates, in the same direction as the loop, with an angular velocity ω_B , where $\omega_B > \omega$ (vectors ω and ω_B are collinear and in the same direction). With \mathcal{E}_0 , \mathcal{E}_{01} , and \mathcal{E}_{02} standing for respective constants, the induced emf in the loop is given by

Solution: D, $e_{\text{ind}}(t) = \mathcal{E}_0 \cos(\omega_B - \omega)t$. This is because net ω in the reference frame of the loop is $\omega_B - \omega$.

15. A rectangular superconducting copper contour of area S is first situated outside any magnetic field, and there is no current in it. The contour is then brought in a uniform time-invariant magnetic field of flux density B and positioned so that the vector \vec{B} is perpendicular to the plane of the contour (like the situation in Fig. Q6.3). In the new steady state, the magnetic flux through the contour due to the current induced in it, computed with respect to the same orientation as that of the vector \vec{B} , equals

Solution: $B, \Phi_{\text{ind}} = -BS$. I wish I knew why.

16. Consider a cylindrical copper conductor carrying a time-varying current, and whether this current is more or less uniform because of eddy currents induced in the conductor and their magnetic field. When compared to the analysis with no effect of eddy currents taken into account, the magnitude of the total current density vector over the cross section of the conductor

Solution: B , less uniform and increases towards the conductor surface. This is because the induced eddy currents go in the opposite direction of the original current. However, the eddy currents are the strongest at the centre, so current becomes less uniform over the cross section, and magnitude is smaller closer to the centre.

17. Consider a ferromagnetic (e.g. iron) core of an ac machine or transformer made of mutually insulated stacked thin plates, shown in Fig. Q6.11(a), and a core made of a single piece of material, shown in Fig. Q6.11(b), and compare the respective distributions of the time-harmonic magnetic field in the two cases. The magnetic flux is more uniformly distributed throughout the volume of the core (or over its cross section) for

Solution:

18. For the same applied time-harmonic magnetic field, the time-average power of Joule's losses, $(P_J)_{\text{ave}}$, due to eddy currents in the two cores in Fig. Q6.11 is greater for

Solution:

19. If the frequency of the applied time-harmonic magnetic field in any of the two cores in Fig. Q6.11 is doubled, the new time-average power of Joule's losses in the core equals k times its previous value, where

Solution:

20. A very long conducting cylinder of radius a uniformly rotates with angular velocity ω about its axis in a uniform time-invariant magnetic field of flux density \vec{B} , as depicted in Fig. Q6.12. Streamlines of eddy currents inside the cylinder away from its ends (bases) are

Solution: C , axial. The surfaces with a variable flux include the constant ϕ surfaces, which is circled by eddy currents. Inside the cylinder, these currents are axial.

21. A conducting equilateral triangular loop is placed near a very long straight wire, with $d = \frac{b}{2}$. A current $i(t) = I \sin \omega t$ flows in the straight wire.
- Determine the voltage registered by a high-impedance rms voltmeter inserted in the loop.
 - Determine the voltmeter reading when the triangular loop is rotated by 60° about a perpendicular axis through its centre.

Solution: From that problem, the flux is found to be

$$\Phi = \frac{\mu b i(t)}{2\sqrt{3}\pi} (\sqrt{3} - \ln(1 + \sqrt{3}))$$

Then

$$V(t) = -\frac{d\Phi}{dt} = \frac{\mu b I \omega \cos(\omega t)}{2\sqrt{3}\pi} (\sqrt{3} - \ln(1 + \sqrt{3}))$$

The rms value is then

$$V_{\text{rms}} = \frac{\mu b I \omega}{2\sqrt{6}\pi} (\sqrt{3} - \ln(1 + \sqrt{3}))$$

If the triangular loop is rotated by 60° , the integral for the flux becomes

$$\begin{aligned} \Phi &= \int \vec{B} \cdot d\vec{S} \\ &= \int_0^{\frac{\sqrt{3}}{2}b} \int_{\frac{x}{\sqrt{3}} - \frac{b}{2}}^{\frac{b}{2} - \frac{x}{\sqrt{3}}} \frac{\mu I}{2\pi(x+d)} dy dx \\ &= \frac{\mu I}{2\sqrt{3}\pi} \int_0^{\frac{\sqrt{3}}{2}b} \frac{\sqrt{3}b - 2x}{x+d} dx \\ &= \frac{\mu I}{2\sqrt{3}\pi} (-\sqrt{3}b + (\sqrt{3}+1)b \ln(\sqrt{3}+1)) \end{aligned}$$

Then similarly,

$$V_{\text{rms}} = \frac{\mu b I \omega}{2\sqrt{6}\pi} (-\sqrt{3} + (\sqrt{3}+1) \ln(\sqrt{3}+1))$$

22. A conducting circular loop of a radius 0.1 m is situated in the neighbourhood of a very long power line carrying a 60 Hz current with $d = 0.15\text{m}$. An a-c milliammeter inserted in the loop reads 0.3 mA. Assume the total impedance of the loop including the milliammeter to be 0.01Ω .
- Find the magnitude of the current in the power line.
 - To what angle about the horizontal axis should the circular loop be rotated in order to reduce the milliammeter reading to 0.2 mA?

Solution: From a previous question, flux is

$$\Phi = \mu I (d - \sqrt{d^2 - b^2}) = 0.0382\mu I$$

so voltage (rms) is

$$V = -\frac{d\Phi}{dt} = \frac{1}{\sqrt{2}} \times 120\pi \times 0.0382\mu I = 10.2\mu I$$

and current is

$$I = \frac{10.2}{0.01} \mu I = 1018 \mu I = 3 \times 10^{-4}$$

Comparing like terms,

$$I = 0.234$$

We want to scale Φ by $\frac{2}{3}$. Since we are rotating by the horizontal axis, in the reference frame of the circular loop, the integration limits remain unchanged, same as $|\vec{B}|$, but the dot product is scaled by the cosine of the angle rotated. Then this is simply

$$\arccos\left(\frac{2}{3}\right) = 48.2^\circ$$

23. An air-filled solenoid of length $l = 2$ m and circular cross section of radius $a = 10$ cm has $N_1 = 1750$ turns of wire. There is a low-frequency time-harmonic current of intensity $i(t) = I_0 \sin \omega t$ flowing through the winding, where $I_0 = 10$ A and $\omega = 10^6$ rad/s. An open-circuited short coil with $N_2 = 10$ turns of wire is placed around the solenoid, as shown in Fig. Q6.11(a). Compute the voltages between the terminals of the coil.

Solution: We need the flux inside a solenoid. First we find the magnetic flux density. Assuming an infinitely long solenoid, we find the flux density in the centre.

$$\begin{aligned} \vec{B} &= \int_{-\frac{l}{2}}^{\frac{l}{2}} \frac{\mu N_1 I dz}{4\pi L} \int_0^{2\pi} \frac{r d\phi \hat{a}_\phi \times (-r \hat{a}_r - z \hat{a}_z)}{(r^2 + z^2)^{\frac{3}{2}}} dz \\ &= \int_{-\frac{l}{2}}^{\frac{l}{2}} \frac{\mu N_1 I dz}{4\pi L} \int_0^{2\pi} \frac{r(r \hat{a}_z - z \hat{a}_r) d\phi}{(r^2 + z^2)^{\frac{3}{2}}} dz \\ &= \int_{-\frac{l}{2}}^{\frac{l}{2}} \frac{\mu N_1 I dz}{4\pi L} \frac{2\pi r^2}{(r^2 + z^2)^{\frac{3}{2}}} dz \hat{a}_z \\ &= \frac{\mu N_1 I r^2}{2L} \int_{-\frac{l}{2}}^{\frac{l}{2}} \frac{dz \hat{a}_z}{(r^2 + z^2)^{\frac{3}{2}}} \\ &= \frac{\mu I N_1 r^2}{2L} \times \frac{2L}{r^2 \sqrt{L^2 + 4r^2}} \hat{a}_z \\ &= \frac{\mu I N_1}{\sqrt{L^2 + 4r^2}} \hat{a}_z \\ &\approx \frac{\mu I N_1}{L} \hat{a}_z \end{aligned}$$

Then total flux is

$$N_2 \Phi = -\frac{\mu I N_1 N_2 \pi r^2}{L}$$

and voltage is

$$V(t) = \frac{\mu N_1 N_2 I_0 \omega \pi r^2}{L} \cos(\omega t) = 3454 \cos 10^6 t$$

24. The circuit in the figure below is situated in a magnetic field

$$\vec{B} = \hat{a}_z 3 \cos \left(5\pi 10^7 t - \frac{2}{3} \pi x \right) \mu \text{ T}$$

Assuming $R = 15\Omega$, find the current i .

Solution: Using Faraday's Law

$$\oint_C \vec{E} \cdot d\vec{l} = -\frac{d\Phi}{dt}$$

Flux is given by

$$\begin{aligned} \Phi &= \int \vec{B} \cdot d\vec{S} \\ &= \int_0^{0.6} \int_0^{0.2} 3 \cos \left(5\pi 10^7 t - \frac{2}{3} \pi x \right) \times 10^{-6} dy dx \\ &= 6 \times 10^{-7} \int_0^{0.6} \cos \left(5\pi 10^7 t - \frac{2}{3} \pi x \right) dx \\ &= \frac{9 \times 10^{-7}}{\pi} (\sin(5\pi 10^7 t) - \sin(5\pi 10^7 t - 0.4\pi)) \end{aligned}$$

And voltage is its derivative,

$$V(t) = \frac{d\Phi}{dt} = 45(\cos(5\pi 10^7 t) - \cos(5\pi 10^7 t - 0.4\pi))$$

Current is then

$$i(t) = 1.5(\cos(5\pi 10^7 t) - \cos(5\pi 10^7 t - 0.4\pi))$$

To solve for the sign, note that in this configuration, with $d\vec{S}$ pointing upwards, the sign of $i(t)$ is the same as the sign of $\frac{d\Phi}{dt}$.

25. A rectangular loop of width w and height h is situated near a very long wire carrying a current $i_1(t)$, as shown in the figure below. Assume i_1 to be a step function as shown in the right panel of the figure below. Find the current $i_2(t)$ induced in the rectangular loop as a function of the mutual inductance L_{12} between the two circuits, the self-inductance L_{22} of the square loop, and the resistance R (note: you don't have to calculate L_{12} and L_{22}).

Solution: Total flux is

$$\Phi = L_{12}i_1(t) + L_{22}i_2(t)$$

By the right hand rule, using the correct signs, $i_2(t)$ starts out as negative, so

$$Ri_2(t) = -L_{12}i_1'(t) - L_{22}i_2'(t)$$

Using the Laplace Transform,

$$i_2(t) = \frac{L_{12}I_1}{L_{22}} \exp\left(-\frac{R}{L_{22}}t\right)$$

26. An infinitely long straight wire carries a slowly time-varying current density of intensity $i(t)$. A rectangular contour of side lengths a and b lies in the same plane with the wire, with two sides parallel to it, as shown in Fig. 6.12. The distance between the wire and the closer parallel side of the contour is c . Determine the emf induced in the contour.

Solution:

$$\vec{B} = \frac{\mu_0 i(t)}{2\pi r} \hat{a}_\phi$$

Switching to the coordinate system of the contour,

$$\vec{B} = -\frac{\mu_0 i(t)}{2\pi x} \hat{a}_z$$

And flux is

$$\Phi = \int \vec{B} \cdot d\vec{S} = b \int_c^{a+c} -\frac{\mu_0 i(t)}{2\pi x} dx = -\frac{\mu_0 b i(t)}{2\pi} \ln \frac{a+c}{c}$$

And its derivative is

$$\frac{d\Phi}{dt} = -\frac{\mu_0 b i'(t)}{2\pi} \ln \frac{a+c}{c}$$

By the right hand rule, $i'(t)$ and e_{ind} have opposite signs, so

$$e_{\text{ind}}(t) = -\frac{\mu_0 b i'(t)}{2\pi} \ln \frac{a+c}{c}$$

27. Assume that the current in the straight wire conductor from Fig. Q6.12 is time-invariant, with intensity I , and that the contour moves away from the wire at a constant velocity v , as shown in Fig. Q6.17. At $t = 0$, the distance of the closer parallel side of the contour from the wire is $x = c$. Determine the emf induced in the contour.

Solution:

$$\vec{B} = -\frac{\mu_0 I}{2\pi x} \hat{a}_z$$

And flux is

$$\Phi = \int \vec{B} \cdot d\vec{S} = b \int_x^{x+a} -\frac{\mu_0 I}{2\pi x} dx = -\frac{\mu_0 b I}{2\pi} \ln \frac{x+a}{x}$$

Its derivative is

$$\frac{d\Phi}{dt} = \frac{d\Phi}{dx} \frac{dx}{dt} = \frac{\mu_0 b I}{2\pi} \left(\frac{1}{x} - \frac{1}{x+a} \right) v$$

By the right hand rule, $\frac{d\Phi}{dt}$ and e_{ind} share the same sign, so

$$e_{\text{ind}} = \frac{\mu_0 b I}{2\pi} \left(\frac{1}{x} - \frac{1}{x+a} \right) v$$

28. Fig. Q6.33 shows two concentric wire loops lying in the same plane, in free space. One is a large square loop of side length a and the other is a small circular loop of radius b ($b \ll a$). The loops are oriented in the same, counter-clockwise, direction. The square loop carries a low-frequency time-harmonic current of intensity $i(t) = I_0 \sin \omega t$, and the resistance of the circular loop is R . Determine the induced current in the circular loop, neglecting its own magnetic field.

Solution: The magnetic flux density at the centre is parallel to \hat{a}_z .

$$\begin{aligned}\vec{B} &= 4\frac{\mu I}{4\pi} \int_{-\frac{a}{2}}^{\frac{a}{2}} \frac{dx\hat{a}_x \times (-x\hat{a}_x + \frac{a}{2}\hat{a}_y)}{(x^2 + \frac{a^2}{4})^{\frac{3}{2}}} \\ &= \frac{\mu I}{\pi} \int_{-\frac{a}{2}}^{\frac{a}{2}} \frac{4adx\hat{a}_z}{(4x^2 + a^2)^{\frac{3}{2}}} \\ &= \frac{4a\mu I}{\pi} \frac{1}{\sqrt{2}a^2} \hat{a}_z \\ &= \frac{2\sqrt{2}\mu I}{\pi a} \hat{a}_z\end{aligned}$$

Since $b \ll a$, we assume \vec{B} is approximately constant in the small circular loop. Then

$$\Phi = BS = \frac{2\sqrt{2}\mu Ib^2}{a}$$

Hence

$$\frac{d\Phi}{dt} = \frac{2\sqrt{2}\mu I_0 \omega b^2}{a} \cos \omega t$$

Hence the induced current has magnitude

$$\frac{2\sqrt{2}\mu I_0 \omega b^2}{aR} \cos \omega t$$

By the right hand rule, initial current is clockwise, so the induced current should be

$$-\frac{2\sqrt{2}\mu I_0 \omega b^2}{aR} \cos \omega t$$

29. A suggested scheme for reducing eddy-current power loss in transformer cores with a circular cross section is to divide the cores into a large number of small insulated filamentary parts. As illustrated in Fig. 7-12, the section shown in part (a) is replaced by that in part (b). Assuming that $B(t) = B_0 \sin \omega t$ and that N filamentary areas fill 95% of the original cross-sectional area, find average eddy-current power loss in the section of core of height h in Fig. 7-12 (a), and Fig. 7-12 (b).

Solution: For the cylinder, we divide it into concentric rings with radius r and thickness dr . Then

$$\Phi = BS = \pi r^2 B(t) \Rightarrow V = \frac{d\Phi}{dt} = \pi r^2 B'(t)$$

Its resistance is

$$R = \frac{l}{\sigma S} = \frac{2\pi r}{\sigma h dr}$$

So the current is

$$i = \frac{V}{R} = \frac{\sigma h r dr}{2} B'(t)$$

Power dissipated is

$$P = Vi = \frac{\sigma h \pi r^3 dr}{2} (B'(t))^2$$

Total power dissipated is

$$\begin{aligned}
 P &= \int_0^a \frac{\sigma h \pi r^3 dr}{2} (B'(t))^2 dr \\
 &= \frac{\sigma h \pi a^4}{8} (B'(t))^2 \\
 &= \frac{\sigma h \pi a^4 B_0^2 \omega^2}{8} \cos^2 \omega t
 \end{aligned}$$

The average value of $\cos^2 \omega t$ is $\frac{1}{2}$, so

$$P_{\text{avg}} = \frac{\sigma h \pi a^4 B_0^2 \omega^2}{16}$$

When replaced with the filaments, the radius of each filament is

$$\begin{aligned}
 N \pi b^2 &= 0.95 \pi a^2 \\
 b &= \sqrt{\frac{0.95}{N}} a
 \end{aligned}$$

New power loss is then

$$\begin{aligned}
 P'_{\text{avg}} &= \frac{\sigma h \pi b^4 B_0^2 \omega^2}{16} N \\
 &= \frac{\sigma h \pi a^4 B_0^2 \omega^2}{16} \times \frac{0.9025}{N} \\
 &= \frac{0.9025}{N} P_{\text{avg}}
 \end{aligned}$$

30. Assuming that a resistance R is connected across the slip rings of the rectangular conducting loop that rotates in a constant magnetic field $\vec{B} = \hat{a}_y B_0$, shown in Fig. 7-6, prove that the power dissipated in R is equal to the power required to rotate the loop at an angular frequency ω .

Solution:

$$\Phi = B_0 S \cos \alpha = B_0 h w \cos \alpha \Rightarrow V = \frac{d\Phi}{dt} = -B_0 h w \omega \sin \alpha$$

Current is then

$$i = \frac{V}{R} = -\frac{B_0 h w \omega}{R} \sin \alpha$$

Power is then

$$P = VI = \frac{B_0^2 h^2 w^2 \omega^2}{R^2} \sin^2 \alpha$$

and

$$P_{\text{avg}} = \frac{B_0^2 h^2 w^2 \omega^2}{2R^2}$$

Now magnetic force exerted on the 1-2 side of the loop is

$$\vec{F} = I \vec{l} \times \vec{B} = -i h B_0 \hat{a}_z$$

and the velocity is

$$\vec{u} = r \omega \hat{a}_r = \frac{w \omega}{2} (\cos \alpha \hat{a}_y - \sin \alpha \hat{a}_z)$$

The velocity at the 4-3 side is the negative of the above. Then mechanical power required is

$$P = \vec{F} \cdot \vec{u} = 2ihB_0 \frac{w\omega}{2} \sin \alpha = ihB_0 w \omega \sin \alpha = Vi$$

where V and i are defined as above.