

ECEN-607: Advanced Analog IC Design

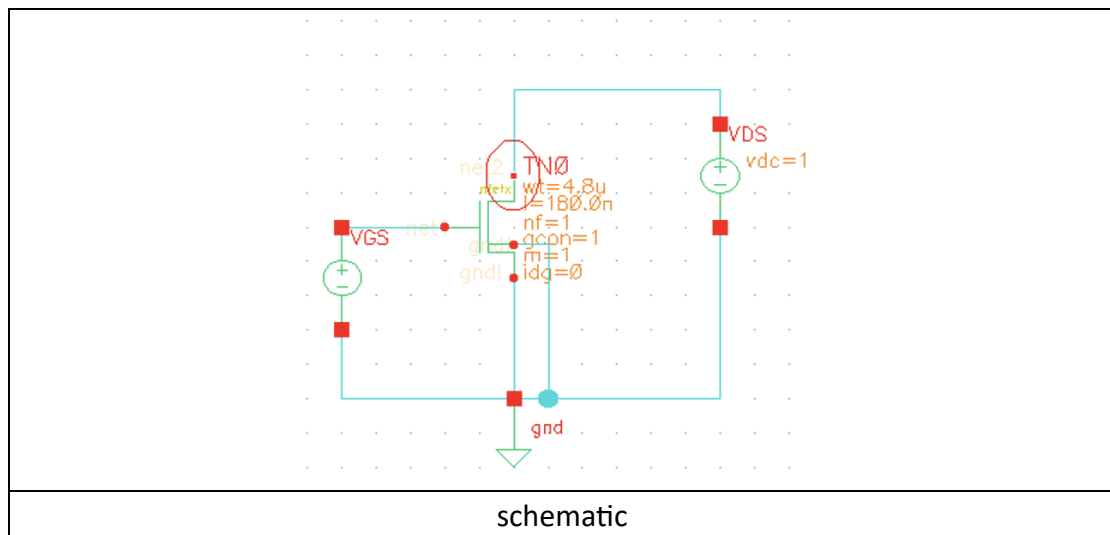
Assignment #1: Transistor Characterization

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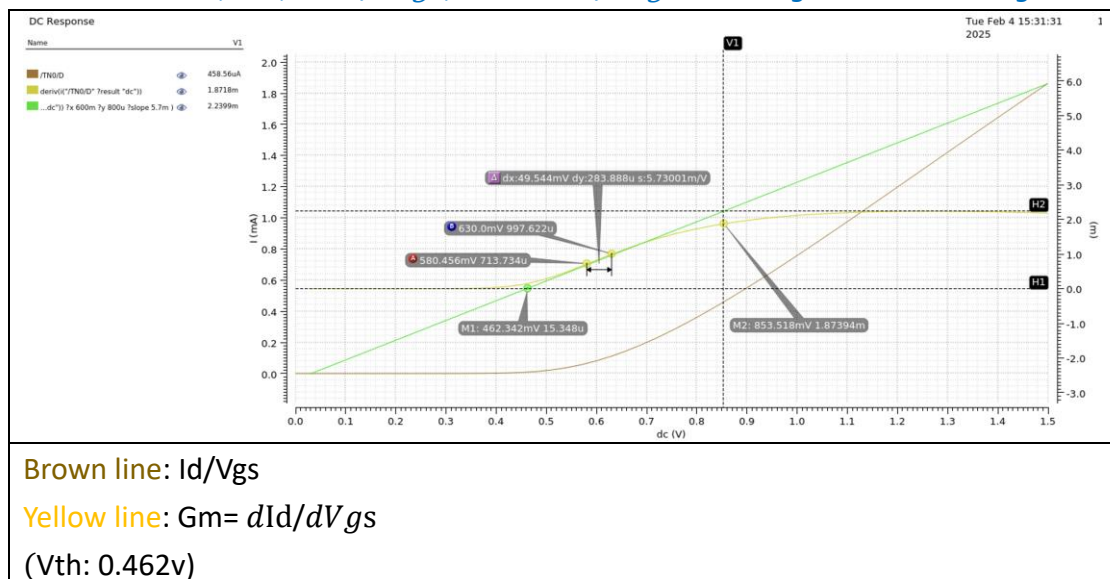
Due: 02/06/2025

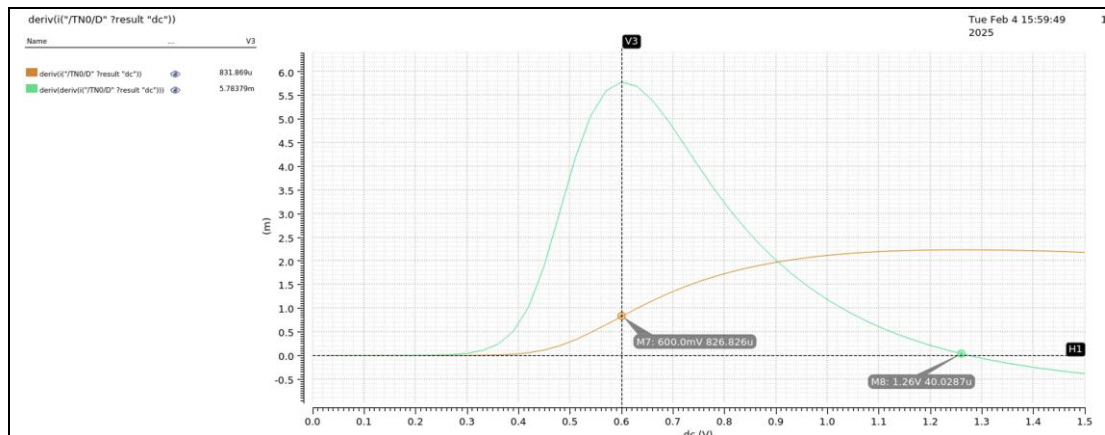
Instructor: Jose Silva-Martinez

Use the technology you are using in the lab and characterize a single N-type transistor employing $W=4.8\mu\text{m}$ and $L=0.18\mu\text{m}$. Use the IBM 0.18 technology you are using in the laboratory; please check it with your TA.



1. Set the drain-source voltage at 1V and sweep the gate-source voltage from 0 up to 1.5V. Plot i_{ds} , G_m , dG_m/dV_{gs} , and d^2G_m/dV_{gs}^2 versus gate-source voltage.

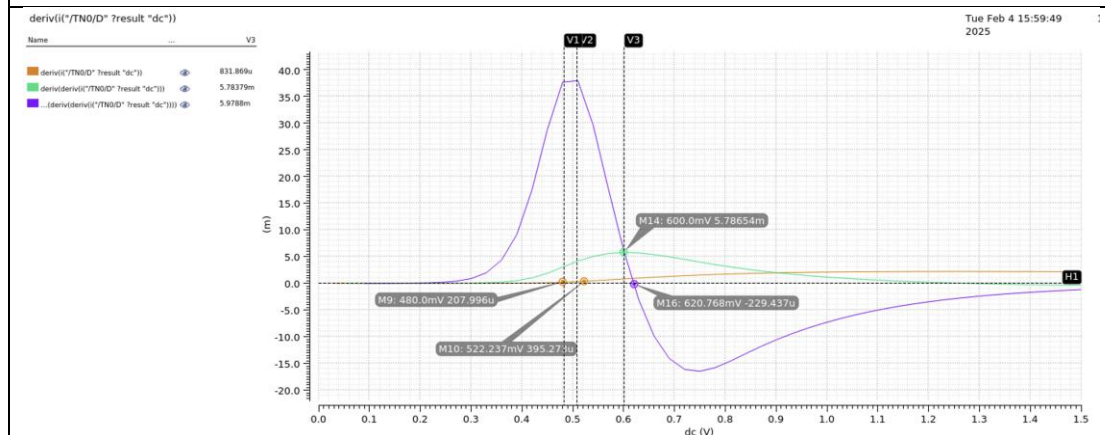




Brown line: $G_m = dI_d/dV_{gs}$

Green line: dG_m/dV_{gs}

When $V_{GS}=0.6v$, MOSFET gain is maximized rate of change



Brown line: $G_m = dI_d/dV_{gs}$

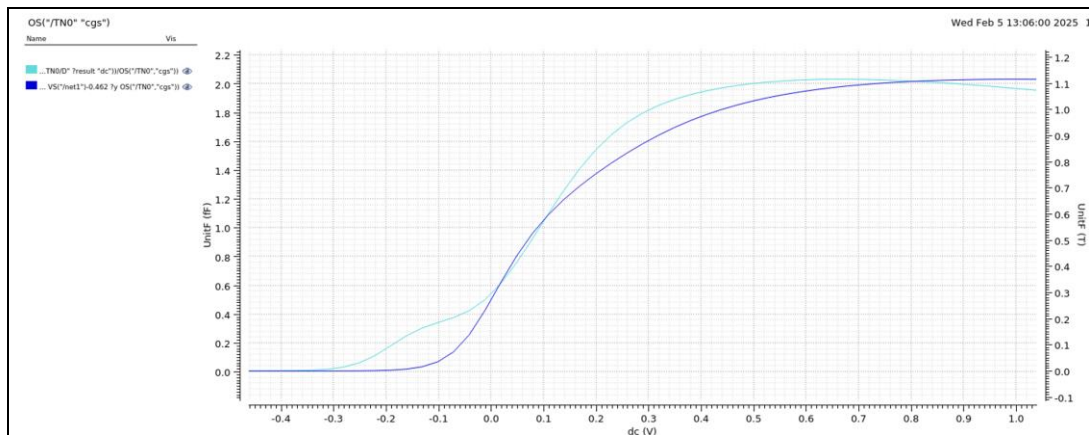
Green line: dG_m/dV_{gs}

Purple line: d^2G_m/dV_{gs}^2

When V_{GS} is around 0.522v, MOSFET gain is the most stable, meaning the best linearity.

When V_{GS} is over 0.62v, the MOSFET enters the non-linear region.

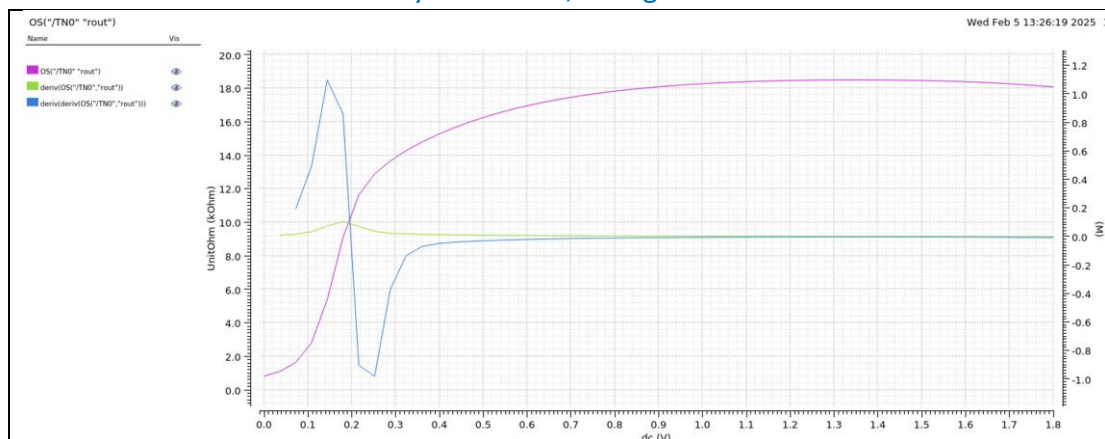
- $(d^3G_m/dV_{GS}^3 \text{ max})$ represents the MOSFET gain, which is the most stable and indicates the best linearity. (high linearity amplifiers, such as ADC preamplifiers.)
 - $(d^2G_m/dV_{GS}^2 \text{ max})$ indicates that the gain of the MOSFET is maximized; however, linearity begins to (high-gain amplifiers.)
2. For same conditions as i), plot C_{gs} and G_m/C_{gs} versus $V_{gs}-V_T$ (overdrive voltage); this parameter represent the transistor's f_t , which is quite relevant when designing fast circuits; G_m/C_{gs} is also known as the transistor's f_t .



The **bright blue line**: C_{gs} versus $V_{gs}-V_T$

The **dark blue line**: G_m/C_{gs} versus $V_{gs}-V_T$

- The **transition frequency** (f_t) of a MOSFET is defined as: $f_t = G_m / 2\pi C_{gs}$
3. Set the gate voltage such that the overdrive voltage $V_{gs}-V_T=200\text{mV}$, and sweep the drain voltage in the range 0-1.8V. Extract the transistor's output resistance and plot R_{ds} , dR_{ds}/dV_{ds} , and d^2R_{ds}/dV_{ds}^2 versus drain-source voltage. Notice that the derivatives of R_{ds} represent output resistor non-linearities. Certainly, R_{ds} is a second order effect and very non-linear, though!

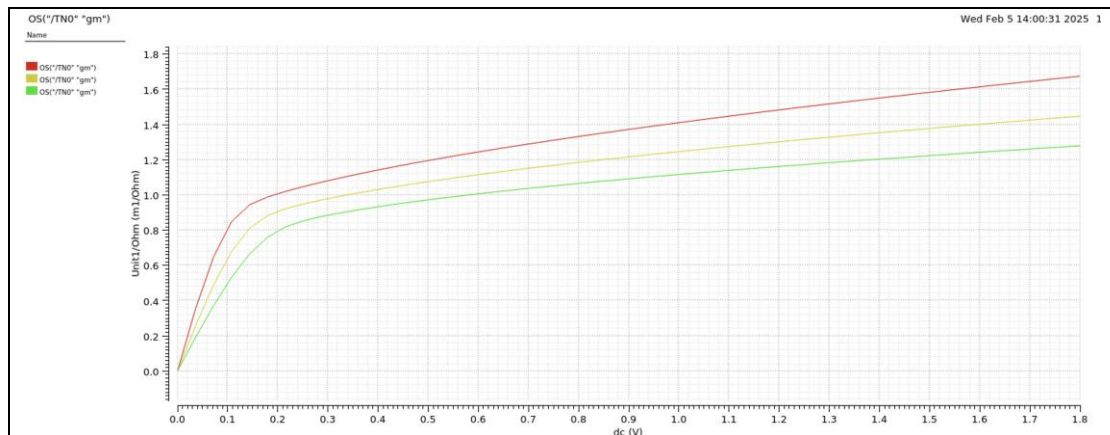


The **pink line**: R_{ds}

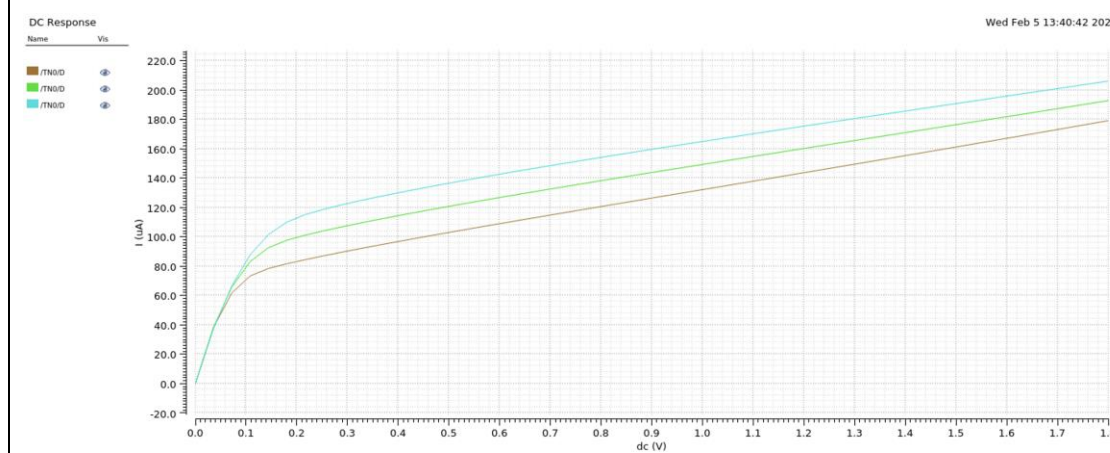
The **green line**: dR_{ds}/dV_{ds} ,

The **blue line**: d^2R_{ds}/dV_{ds}^2

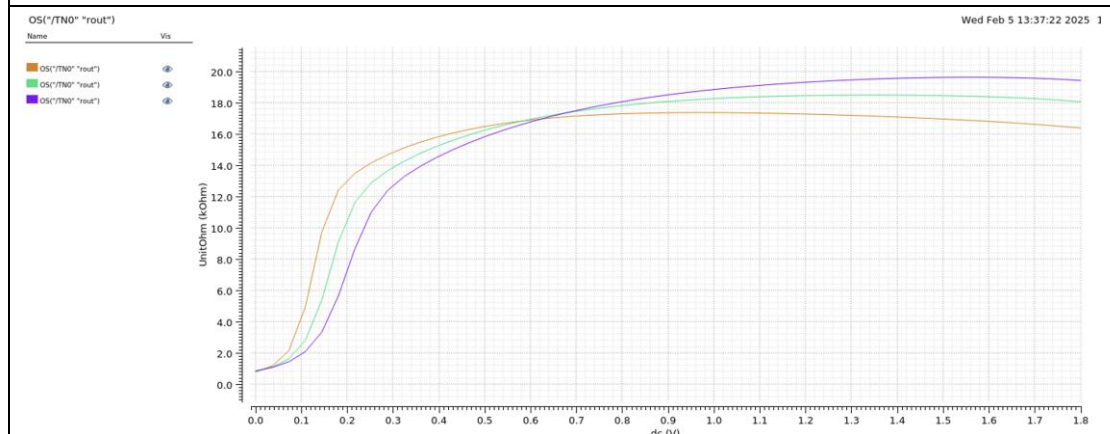
4. Repeat iii) for temperatures of -50, 27 and 100 degrees (Celsius). Make a table and compare I_d , G_m and R_{ds} for the 3 cases. For all these simulations keep constant the gate-source voltage; evidently V_{dsat} will not be constant due to V_T variations.



Gm: -50, 27, 100 degrees (Celsius)



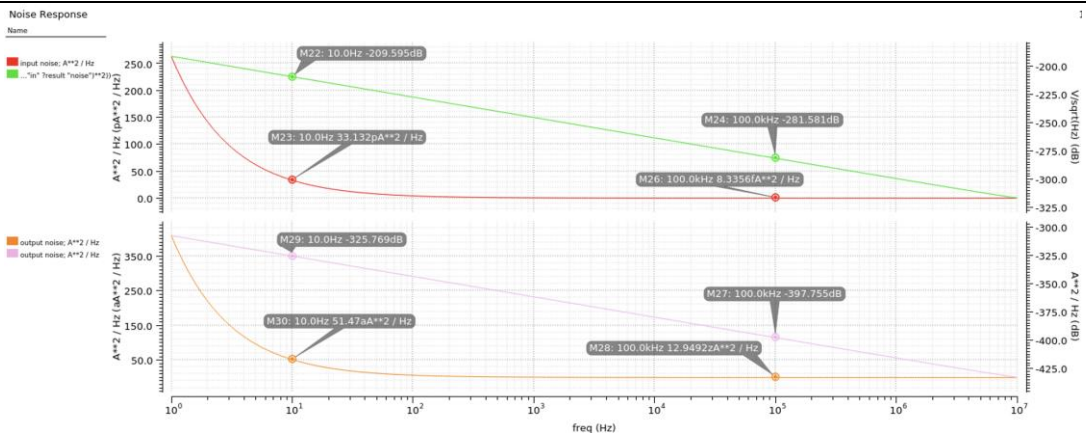
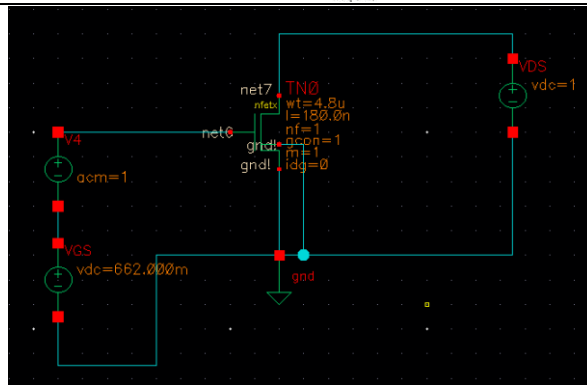
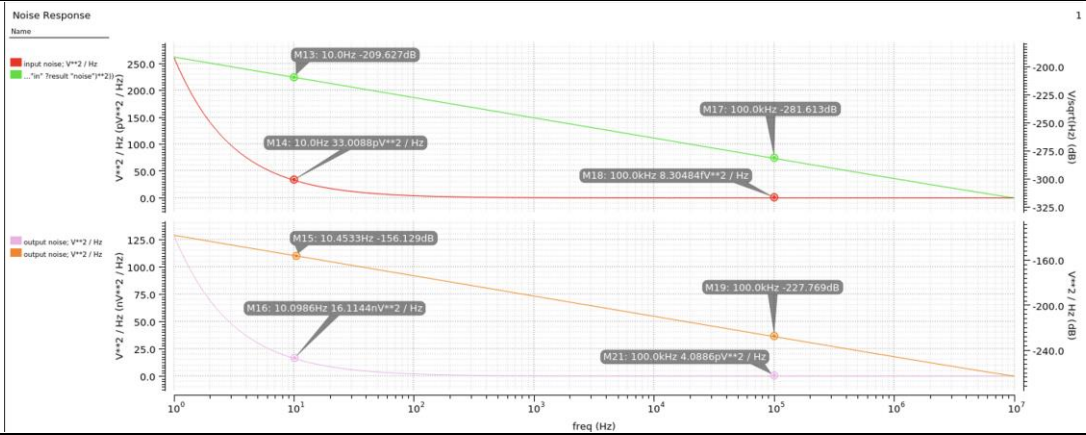
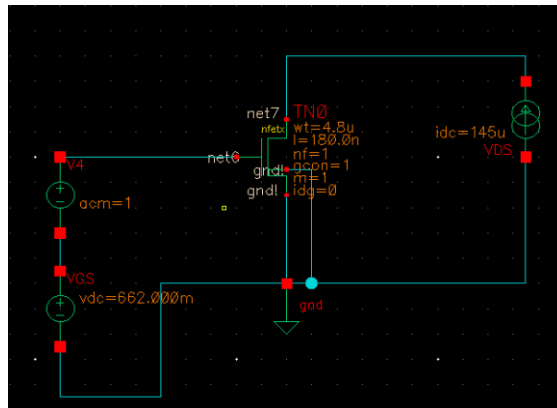
Id: -50, 27, 100 degrees (Celsius)

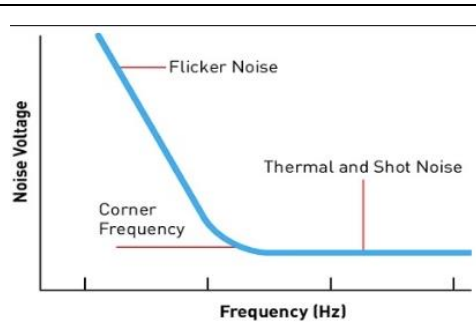


rds: -50, 27, 100 degrees (Celsius)

5. Simulate the transistor and report the input and output referred noise density. Include a screen shot showing the noise density in the frequency range of 1Hz up to 10MHz; use log10 scale in the x-axis and y-axis to visualize the flicker noise level (voltage) and the thermal noise level (current). Check these values with the theoretical values. The easiest way to do this is by biasing the gate voltage with a DC voltage source such that $V_{gs}-V_T=200\text{mV}$ in series with an AC voltage source. Connect at amplifier's drain terminal a power supply such that V_{DS} is set at 1V. The

DC voltage source operates as short circuit for AC analyss and current can be measured.





The relationship between $I_o (\text{noise})^2 = V_i (\text{noise})^2 * G_M^2$, which is at 10Hz, $51.47 \text{aA}^2 / 33 \text{pV}^2$ $G_m = 1.24 \text{m}$ at 10Hz

Flicker Noise (Low-Frequency Noise), the gate-referred noise voltage is given by $V_g^2(f) = k/fWL C_{ox}$

Thermal Noise (White Noise, Frequency-Independent)

The drain current noise is given by: $4KT * 2/3 * G_m$

By those condition on the top we can rewrite the input noise as $V_i^2(f) = 8kT/3g_m + k/fWL C_{ox}$, by this formula and the picture on the top we can calculate the flicker noise (in low freq) and thermal noise (at high freq), not matter Input out Output ($V_i^2 * G_m^2 = I_o^2$).

Conclusion:

- $(d3G_m/dV_{GS3} \text{ max})$ represents the MOSFET gain, which is the most stable and indicates the best linearity.(high linearity amplifiers, such as ADC preamplifiers.)
- $(d2G_m/dV_{GS} \text{ max})$ indicates that the gain of the MOSFET is maximized; however, linearity begins to (high-gain amplifiers.)
- The relationship between $I_o (\text{noise})^2 = V_i (\text{noise})^2 * G_M^2$
- The input noise can be written as $8kT/3g_m + k/fWL C_{ox}$, which means low frequency is dominate by flicker noise and high frequency is dominate by thermal noise.