ELEC2146

Electrical Engineering Modelling and Simulation

Introduction to System Identification

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Overview

- Motivation
- The process of system ID
- Non-parametric approaches
 - Transient response
 - Frequency response
- Parametric approaches
 - Levy method
 - Parametric model structures
- Continuous and discrete time
- Model order

Motivation

Common problem in modelling:

- Have data from an experiment
 - Maybe inputs and outputs at different times, or for different conditions
 - Often have a reasonable amount of data → overdetermined equations
- Have no hypothesis about the model structure
 - To begin with
- Want to use the data and some assumptions to estimate the model structure and parameters

System Identification

Goes to heart of modelling

- Aims to provide most generally accurate explanation for observed data that is also compact
 - Caveat: in context of dynamic systems
 - Developed in the control systems context
- Solution space is infinite
- Model is only ever as good as the observed data used to estimate its parameters
- 'Generally accurate' ⇒ error criterion to be minimised
 - E.g. sum of squares



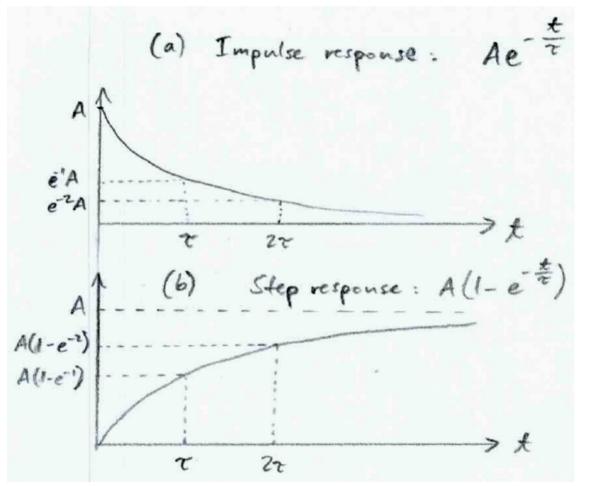
Process of System Identification

- Is it necessary?
 - If we are modelling a physical system
 - Do we already know enough about the system, from physics (mechanics, circuit theory, population dynamics, physiology etc) to guess the model structure?
 - e.g. LS lab question with height and time data; estimate gravity – can look up equation of motion
 - If yes, then we can guess at the form the model should take
 - Problem becomes parameter estimation
 - So far, have looked at least squares

Process of System Identification

- 1. Assemble prior knowledge of system
- 2. Design experiment likely to produce insight into system
- 3. Propose mathematical model
 - Choose fit criterion
 - Determine model parameters using data
 - Validate model using data
- 4. If model is not a good fit, return to 3
 - After varying the model order
- 5. Model still not good fit?
 - Return to 3 after varying the model structure

- Transient response analysis
 - Assumes we can apply an impulse or step input



First-order system*: simple

- Directly estimate
 - A, τ or
- Use least squares

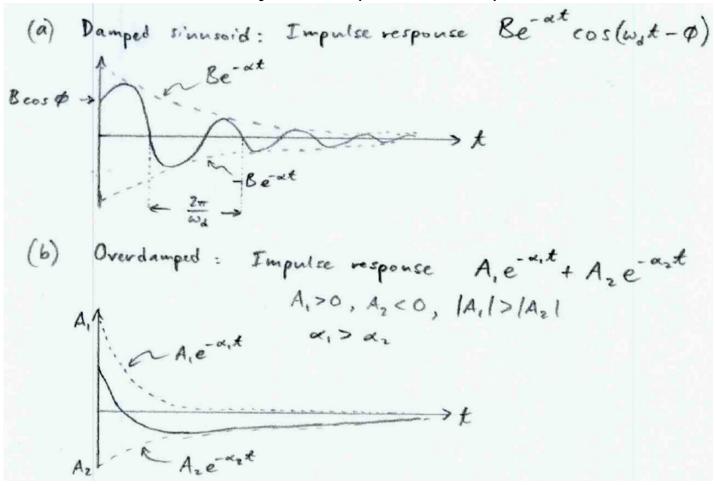
* assumption

Transient response analysis

- Second-order system (assumed)
- Need to know, or guess, the type of response
 - Overdamped, critically damped, underdamped, undamped
- This dictates the form of the solution
- Some forms can be estimated (roughly at least) directly
- Some can be partly estimated using LS
 - E.g. overdamped: use LS in 'early' and 'late' parts of response to estimate time constants
 - E.g. underdamped: pick peaks to estimate exponential decay and damped frequency
- Or use nonlinear LS
 - Convergence not guaranteed

Transient response analysis

Second-order system (assumed)



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Transient response analysis

- Second-order system (assumed)
- Sometimes effects of individual terms, like $A_1e^{-\alpha_1t}$ or $Be^{-\alpha t}$ can be measured
- Sometimes not
- E.g. $Ae^{-\alpha t}$, $(At+B)e^{-\alpha t}$ and $A_1e^{-\alpha_1 t}+A_2e^{-\alpha_2 t}$ all look quite similar
- When the order of the system is > 2
 - Even more problems
 - Often system is dominated by behaviour that can be captured by a low order (1, 2 or 3) model

- Problems with transient response analysis
 - Linear, stable systems only
 - Sampling rate must be fast enough to observe transients
 - Steady state behaviour can be difficult to observe
 - Quantisation, numerical accuracy
 - E.g. impulse response value \rightarrow 0 as $t \rightarrow \infty$
 - Noise dominates when t is large
 - Often can't apply an impulse input
 - Can't physically generate an impulse
 - Can generate one but can't apply it to the system

- Frequency response analysis
 - Just like frequency responses of amplifiers or filters in the electronics labs:

$$u(t) = A\sin(\omega_0 t)$$
 ? $y(t) = B\sin(\omega_0 t + \phi)$

– Transfer function magnitude at ω_0 is

$$\left|G(e^{j\omega_0 T})\right| = \frac{B}{A}$$

Amplitudes are often noisy (A and B are estimates)

- Problems with frequency response analysis
 - Need lots of measurements to know entire response
 - Reasonably long measurement time is needed
 - To reduce effect of transients
 - Assumes a sinusoidal input signal is actually possible
 - Only works for stable systems

Advantages

- Can guess order of system and rough positions of poles/zeroes
- Consult magnitude response sketching (earlier)

- Alternative method of frequency response analysis
 - Use 'spectrally rich' input signal
 - Also known as 'persistently exciting' of a high order
 - Contains many frequencies
 - Sample the input and output signals with frequency f_s (must have $f_s > 2 \times$ highest freq. in signal)
 - Take the discrete Fourier transform of each

$$u(nT) \stackrel{DFT}{\longleftrightarrow} U[k] \qquad y(nT) \stackrel{DFT}{\longleftrightarrow} Y[k]$$

Estimate the magnitude response as

$$|G[k]| \approx \frac{|Y[k]|}{|U[k]|}$$

- Alternative method of frequency response analysis
 - What is k?
 - k is a discrete frequency index, whose frequency in Hertz is

$$f = \frac{kf_s}{N}$$

- Where N is the number of samples of the signal used to compute the DFT
 - k = 0, 1, ..., N-1
 - But we only use k = 0, 1, ..., N/2, guided by the sampling Theorem

- Alternative method of frequency response analysis
 - What kinds of inputs are 'spectrally rich'?
 - White noise
 - Some systems cannot be excited with high-frequency input
 - Many systems low pass not much point exciting at high freqs.
 - Pseudo-random binary
 - Has high input power without large peak amplitudes
 - ... generally preferred
 - Probably more often feasible than other inputs
 - Basically just switching input on and off
 - Generate using white noise, filtered, and then clipped by taking the sign

General idea:

- Assume a model of a particular structure
 - e.g. *M* zeroes, *N* poles
- Estimate the parameters of this model structure

$$H(s) = \frac{b_M s^M + ... + b_1 s + b_0}{a_N s^N + ... + a_1 s + 1}$$

- See how well the model fits
 - Using the estimated parameters
- Change the structure (M and/or N) if the fit is not satisfactory
 - "satisfactory" according to some goodness of fit criterion like LS
 - More on this later in the course

- LS magnitude response fitting
 - Want to fit

$$\sum_{k} \left| H(j\omega_{k}) - \frac{Y(j\omega_{k})}{X(j\omega_{k})} \right|^{2}$$

where
$$H(j\omega) = \frac{Y(j\omega)}{X(j\omega)} = \frac{b_M (j\omega)^M + ... + b_1 j\omega + b_0}{a_N (j\omega)^N + ... + a_1 j\omega + 1}$$

- Given $H(j\omega_k)$ evaluated at frequency points ω_k
- By estimating parameters a_i , b_i
- Not possible using direct LS
- What about

$$\sum_{k} |X(j\omega_{k})H(j\omega_{k}) - Y(j\omega_{k})|^{2}$$

$$= \sum_{k} (X(j\omega_{k})H(j\omega_{k}) - Y(j\omega_{k}))^{*} (X(j\omega_{k})H(j\omega_{k}) - Y(j\omega_{k}))$$

Levy method

$$\sum_{k} |X(j\omega_k)H(j\omega_k) - Y(j\omega_k)|^2$$

Has a LS solution of the form

$$\mathbf{c} = [\mathbf{A}^* \mathbf{A}]^{-1} \mathbf{A}^* \mathbf{y}$$

- A* is conjugate transpose of A
- Can fit quite complicated frequency responses
- Problem: large values of ω_k are weighted very heavily

Sampling and discrete time

- Another class of method for parametric system ID estimate parameters from the sampled input and output signals
- First question: what should the sampling rate be?
 - Not too low, or we get aliasing $(\omega_s/2)$ well above 3dB point ω_B
 - Not too high, or discrete time poles are close to unit circle
- Practical choice:

$$10\omega_B \le \omega_s \le 30\omega_B$$

– Discrete time input:
$$x(n) = x(t)|_{t=nT}, n \in \mathfrak{I}$$

- Discrete time input:
$$x(n) = x(t)\Big|_{t=nT}, n \in \mathfrak{T}$$
- Discrete time output: $y(n) = y(t)\Big|_{t=nT}, n \in \mathfrak{T}$

• *n* is the discrete time sample index
• *T* is the sampling period
$$T = \frac{2\pi}{\omega_s} = \frac{1}{f_s}$$

- Sampling and discrete time
 - Inputs, outputs related via difference equation

$$y(n) = b_0 x(n) + b_1 x(n-1) + \dots + b_M x(n-M) - a_1 y(n-1) - \dots - a_N y(n-N)$$

– Apply z-transform:

$$Y(z) = b_0 X(z) + b_1 z^{-1} X(z) + \dots + b_M z^{-M} X(z) - a_1 z^{-1} Y(z) - \dots - a_N z^{-N} Y(z)$$

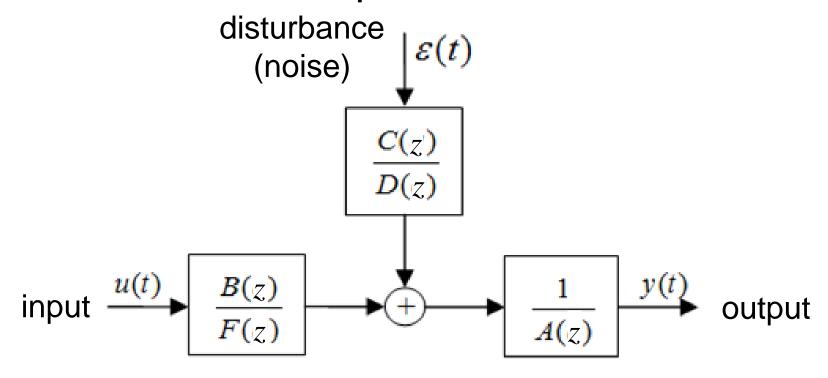
- Rearrange as
$$H(z) = \frac{Y(z)}{X(z)}$$

Transfer function (discrete-time)

$$H(z) = \frac{b_0 + b_1 z^{-1} + \dots + b_M z^{-M}}{1 + a_1 z^{-1} + \dots + a_N z^{-N}}$$

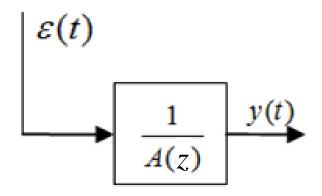
- Compare with continuous time: $H(s) = \frac{b_M s^M + ... + b_1 s + b_0}{a_{11} s^N + ... + a_1 s + 1}$ Poles, zeroes similar

General form of parametric models



 Different combinations of transfer functions produce different models

AR (autoregressive) model



- Has poles only, no zeroes
- No input u(t)?
 - Like a bell that has been struck
- Time-domain form:

$$y(t) + a_1 y(t-T) + \dots + a_N y(t-NT) = \varepsilon(t)$$

- AR (autoregressive) model
 - Suppose we take m+N-1 samples of the output y, spaced by T (the sampling period)
 - $\rightarrow m$ equations

$$y(t_{1}) + a_{1}y(t_{1} - T) + ... + a_{N}y(t_{1} - NT) = \varepsilon(t_{1})$$

$$y(t_{2}) + a_{1}y(t_{2} - T) + ... + a_{N}y(t_{2} - NT) = \varepsilon(t_{2})$$

$$\vdots$$

$$y(t_{m}) + a_{1}y(t_{m} - T) + ... + a_{N}y(t_{m} - NT) = \varepsilon(t_{m})$$

- AR (autoregressive) model
 - Rearranging:

$$y(t_{1}) = -a_{1}y(t_{1} - T) - \dots - a_{N}y(t_{1} - NT) + \varepsilon(t_{1})$$

$$y(t_{2}) = -a_{1}y(t_{2} - T) - \dots - a_{N}y(t_{2} - NT) + \varepsilon(t_{2})$$

$$\vdots$$

$$y(t_{m}) = -a_{1}y(t_{m} - T) - \dots - a_{N}y(t_{m} - NT) + \varepsilon(t_{m})$$

$$y = Xc + \varepsilon$$

AR (autoregressive) model

$$y = Xc + \varepsilon$$

where

$$\mathbf{X} = \begin{bmatrix} -y(t_1 - T) & -y(t_1 - 2T) & \cdots & -y(t_1 - NT) \\ -y(t_2 - T) & -y(t_2 - 2T) & \cdots & -y(t_2 - NT) \\ \vdots & \vdots & & \vdots \\ -y(t_m - T) & -y(t_m - 2T) & \cdots & -y(t_m - NT) \end{bmatrix}$$

$$\mathbf{y} = \begin{bmatrix} y(t_1) \\ y(t_2) \\ \vdots \\ y(t_m) \end{bmatrix} \qquad \mathbf{c} = \begin{bmatrix} a_1 \\ a_2 \\ \vdots \\ a_N \end{bmatrix} \qquad \mathbf{\varepsilon} = \begin{bmatrix} \varepsilon(t_1) \\ \varepsilon(t_2) \\ \vdots \\ \varepsilon(t_m) \end{bmatrix}$$

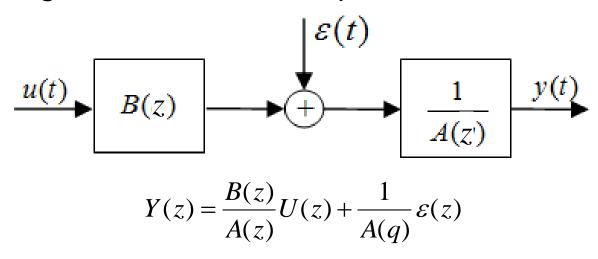
- AR (autoregressive) model
 - If N < m,

$$\hat{\mathbf{c}}_{LS} = \left[\mathbf{X}^T \mathbf{X} \right]^{-1} \mathbf{X}^T \mathbf{y}$$

- Current output is linear combination of previous outputs
 - Linear prediction
- Order N

ARX model

Autoregressive with extra input



- Poles and zeroes
- Time-domain form:

$$y(t) + a_1 y(t-T) + ... + a_N y(t-NT) = b_1 u(t-T) + ... + b_M u(t-MT) + \varepsilon(t)$$

ARX model

- Suppose we take m+N-1 samples of the output and m+M-1 samples of the input, spaced by T (the sampling period)
 - \blacksquare \rightarrow *m* equations

$$y(t_{1}) + a_{1}y(t_{1} - T) + \dots + a_{N}y(t_{1} - NT) = b_{1}u(t_{1} - T) + \dots + b_{M}u(t_{1} - MT) + \varepsilon(t_{1})$$

$$y(t_{2}) + a_{1}y(t_{2} - T) + \dots + a_{N}y(t_{2} - NT) = b_{1}u(t_{2} - T) + \dots + b_{M}u(t_{2} - MT) + \varepsilon(t_{2})$$

$$\vdots$$

$$y(t_{m}) + a_{1}y(t_{m} - T) + \dots + a_{N}y(t_{m} - NT) = b_{1}u(t_{m} - T) + \dots + b_{M}u(t_{m} - MT) + \varepsilon(t_{m})$$

ARX model

$$y = Xc + \varepsilon$$

where

$$\mathbf{X} = \begin{bmatrix} -y(t_1 - T) & -y(t_1 - 2T) & \cdots & -y(t_1 - NT) & u(t_1 - T) & u(t_1 - 2T) & \cdots & u(t_1 - MT) \\ -y(t_2 - T) & -y(t_2 - 2T) & \cdots & -y(t_2 - NT) & u(t_2 - T) & u(t_2 - 2T) & \cdots & u(t_2 - MT) \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\ -y(t_m - T) & -y(t_m - 2T) & \cdots & -y(t_m - NT) & u(t_m - T) & u(t_m - 2T) & \cdots & u(t_m - MT) \end{bmatrix}$$

$$\mathbf{y} = \begin{bmatrix} y(t_1) \\ y(t_2) \\ \vdots \\ y(t_m) \end{bmatrix} \qquad \mathbf{c} = \begin{bmatrix} a_1 \\ a_2 \\ \vdots \\ a_N \\ b_1 \\ b_2 \\ \vdots \\ b \end{bmatrix} \qquad \mathbf{\varepsilon} = \begin{bmatrix} \varepsilon(t_1) \\ \varepsilon(t_2) \\ \vdots \\ \varepsilon(t_m) \end{bmatrix}$$

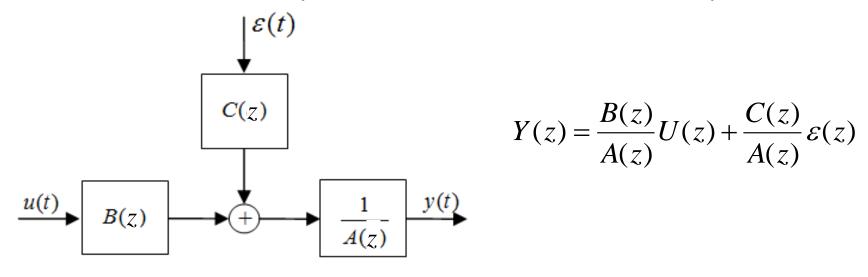
- ARX model
 - If N+M < m,

$$\hat{\mathbf{c}}_{LS} = \left[\mathbf{X}^T \mathbf{X} \right]^{-1} \mathbf{X}^T \mathbf{y}$$

- Current output is linear combination of previous outputs
- Also known as an equation error model structure
 - $\varepsilon(t)$ is a direct error in the equation: $A(z)Y(z) = B(z)U(z) + \varepsilon(z)$

ARMAX model

- Adds a model for noise
 - To account for possible "coloured noise", i.e. not flat spectrum



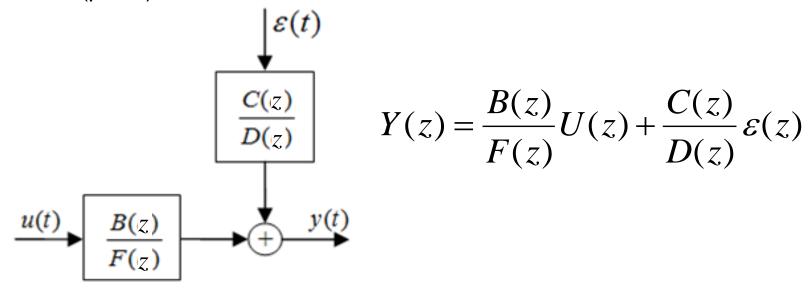
$$y(t) + a_1 y(t-T) + ... + a_N y(t-NT)$$

= $b_1 u(t-T) + ... + b_M y(t-MT) + \varepsilon(t) + c_1 \varepsilon(t-T) + ... + c_{n_c} \varepsilon(t-n_cT)$

Solution via instrumental variable methods

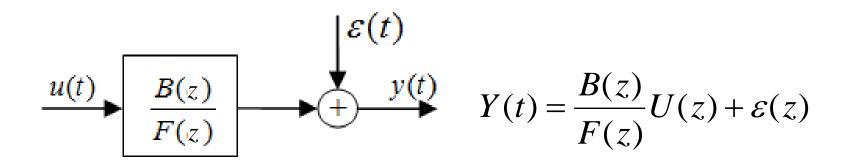
Box-Jenkins model

- Noise model is more detailed, decoupled from input
 - ARMAX assumes noise and input are subject to same 'dynamics' (poles)

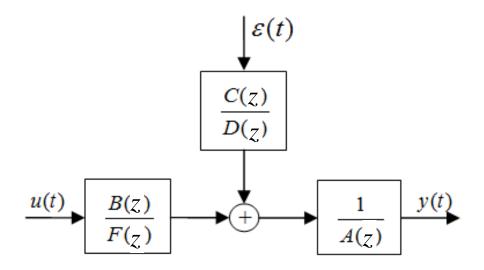


- Noise is contributed early in process: ARMAX
- Noise is contributed late in process: Box-Jenkins

- Output error model
 - Noise occurs directly at output



General model structure



- More parameters ⇒
 - More detailed model
 - More difficulty estimating parameters accurately

- Mapping back to s-plane
 - These models are all discrete time
 - To go back to continuous time:
 - Impulse invariant pole mapping (all-pole models only)

$$\frac{1}{s+b} \leftrightarrow \frac{1}{1-e^{-bT}z^{-1}}$$

Bilinear transform

$$z^{-1} = \frac{1 - \frac{sT}{2}}{1 + \frac{sT}{2}}$$

Model Order

- Have to guess N, M
- Evaluate model (after estimating parameters), find order that produces a 'good' fit
 - According to some desired criterion
- In practise
 - Often simpler model structures are sufficient to describe the main system effects
 - — ∴ polynomial orders tend to be low

Process of System Identification

- 1. Assemble prior knowledge of system
- 2. Design experiment likely to produce insight into system
- 3. Propose mathematical model
 - Choose fit criterion
 - Determine model parameters using data
 - Validate model using data
- 4. If model is not a good fit, return to 3
 - After varying the model order
- 5. Model still not good fit?
 - Return to 3 after varying the model structure