

Today's Outline

8. Second Order Circuits

- the parallel RLC circuit
- underdamped, overdamped, and critically damped natural response



Overview

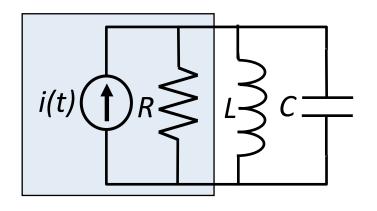
Second order circuit: a circuit composed of resistors, sources and two energy storage components, often one capacitor and one inductor. Some, not all, circuits with two capacitors or two inductors are second order circuits.

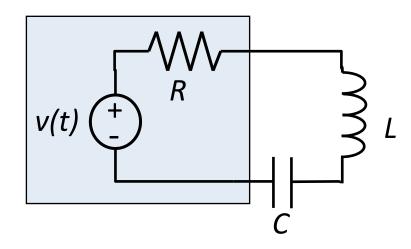
- RLC circuits include a resistor, an inductor and a capacitor
- "second order" refers to the second order differential equations that describe voltage and current variables, v(t) and i(t)
- RLC circuits are useful because of the time dependent response of such circuits

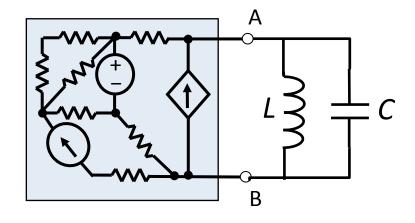


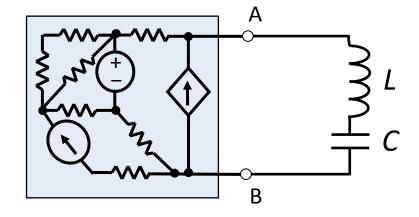
Overview

There are two classic forms of the *RLC* circuit: the *parallel RLC* and the *series RLC*.



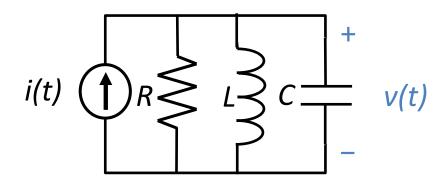








Parallel RLC



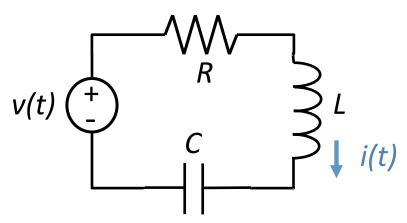
KCL:
$$-i + \frac{v}{1/sC} + \frac{v}{R} + \frac{v}{sL} = 0$$
 $-i + C\frac{dv}{dt} + \frac{v}{R} + \frac{1}{L}\int_{0}^{t} v(t')dt' + i_{L}(0) = 0$ $-si + s^{2}C \cdot v + \frac{s}{R} \cdot v + \frac{1}{L} \cdot v = 0$

Replacing s by
$$d/dt$$
:
$$\frac{d^2v}{dt^2} + \frac{1}{RC}\frac{dv}{dt} + \frac{1}{LC}v = \frac{1}{C}\frac{di}{dt}$$

This is an inhomogeneous linear second order differential equation.



Series RLC



KVL:
$$-v + R \cdot i + sL \cdot i + \frac{1}{sC} \cdot i = 0$$
 $-v + L \frac{di}{dt} + iR + \frac{1}{C} \int_{0}^{t} i(t') dt' + v_{c}(0) = 0$ $-sv + sR \cdot i + s^{2}L \cdot i + \frac{1}{C} \cdot i = 0$

Replacing s by
$$d/dt$$
:
$$\frac{d^2i}{dt^2} + \frac{R}{L}\frac{di}{dt} + \frac{1}{LC}i = \frac{1}{L}\frac{dv}{dt}$$

This is an inhomogeneous linear second order differential equation.



natural response

As in the case of first order circuits, it is useful to divide the response of a second order circuit into two parts.

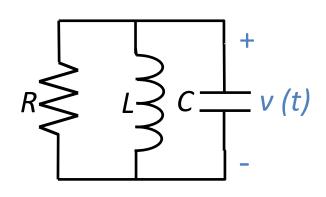
total response = transient (natural) response + steady state (forced) response

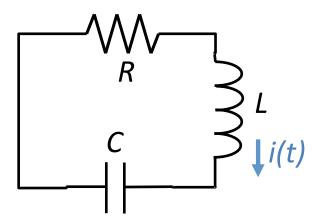
Solution to the homogeneous equation gives the "short-lived" transient or natural response.

Particular solution of the inhomogeneous equation gives the "long-lived" steady state response.



natural response





The differential equations that are to be solved are thus:

$$\frac{d^2v}{dt^2} + \frac{1}{RC}\frac{dv}{dt} + \frac{1}{LC}v = 0 \quad t > 0$$

$$i_L(0+) = I_0$$

$$v(0+) = V_0$$

$$\frac{d^{2}i}{dt^{2}} + \frac{1}{L/R} \frac{di}{dt} + \frac{1}{LC} i = 0 \quad t > 0$$

$$v_{c}(0+) = V_{0}$$

$$i(0+) = I_{0}$$



mathematical review

Consider the *homogeneous linear second order differential equation,* which corresponds to *unforced (natural)* behaviour:

$$a\frac{d^2x}{dt^2} + b\frac{dx}{dt} + cx = 0$$

Assume a solution of the form: $x(t) = K \exp(+st)$

Substitution returns an operator equation:

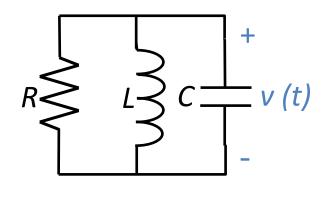
$$as^{2} \cdot x + bs \cdot x + c \cdot x = \left(as^{2} + bs + c\right) \cdot x = 0$$

The *characteristic equation* for the value of s is: $as^2 + bs + c = 0$

The roots of the characteristic equation are: $s_{1,2} = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$



parallel RLC



The differential equation to be solved is:

$$\frac{d^2v}{dt^2} + \frac{1}{RC}\frac{dv}{dt} + \frac{1}{LC}v = 0$$

The characteristic equation to be solved is:

$$s^2 + \frac{1}{RC}s + \frac{1}{LC} = 0$$

We identify the two coefficients as meaningful parameters:

$$s^2 + 2\alpha \cdot s + \omega_0^2 = 0$$

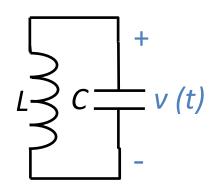
$$\alpha = \frac{1}{2RC}$$
 = damping rate

$$\alpha = \frac{1}{2RC}$$
 = damping rate
$$\omega_0 = \frac{1}{\sqrt{LC}}$$
 = resonant frequency

9 ECSE-200



undamped parallel RLC



Consider the special case where $R->\infty$, the damping rate α ->0 and the characteristic equation:

$$s^{2} + \omega_{0}^{2} = 0$$

$$s = \pm j\omega_{0} \qquad j = \sqrt{-1}$$

The solution to v(t) is:

$$\alpha = \frac{1}{2RC} \to 0$$

$$\omega_0 = \frac{1}{\sqrt{LC}}$$

$$v(t) = A_1 \exp(+j\omega_0 t) + A_2 \exp(-j\omega_0 t)$$

By Euler's theorem:

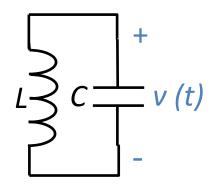
$$v(t) = B_1 \sin(\omega_0 t) + B_2 \cos(\omega_0 t)$$

The constants are determined by the initial conditions at t = 0+.

10



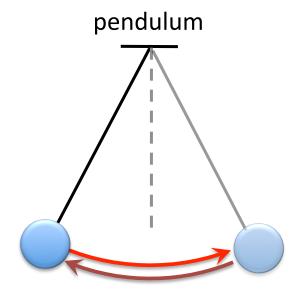
undamped parallel RLC

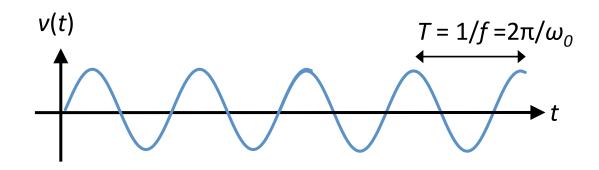


The solution is an undamped oscillation, like that of an undamped mechanical pendulum.

$$v(t) = B_1 \sin(\omega_0 t) + B_2 \cos(\omega_0 t) \qquad \omega_0 = \frac{1}{\sqrt{LC}}$$

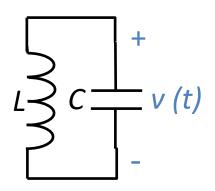
The angular frequency ω_0 is called the **undamped resonant frequency** of the *LC* circuit.



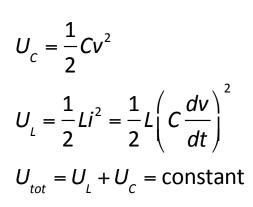


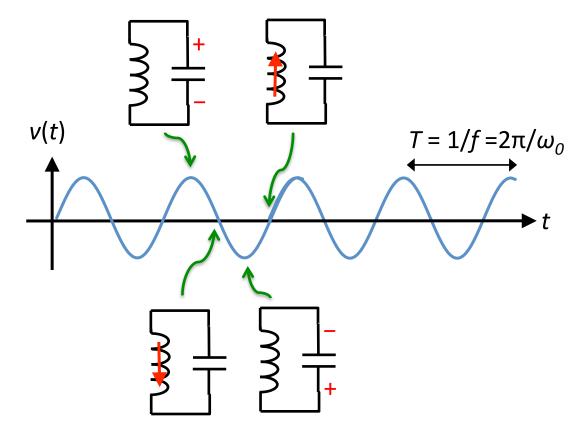


undamped parallel RLC



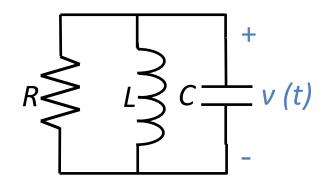
Energy oscillates between electric energy stored in *C* and magnetic energy stored in *L*. Without *R*, there is no energy lost to heat.







parallel RLC



$$\alpha = \frac{1}{2RC}$$
 $\omega_0 = \frac{1}{\sqrt{IC}}$

The case of non-zero damping gives:

$$s^2 + 2\alpha \cdot s + \omega_0^2 = 0$$

The general solution to the roots are:

$$s = -\alpha \pm \sqrt{\alpha^2 - \omega_0^2}$$

These roots can are in general complex numbers, with three classes of solution:

$$\alpha < \omega_0$$
 $s = -\alpha \pm j\sqrt{\omega_0^2 - \alpha^2}$

$$\alpha = \omega_0$$
 $S = -\alpha$

$$\alpha > \omega_0$$
 $s = -\alpha \pm \sqrt{\alpha^2 - \omega_0^2}$

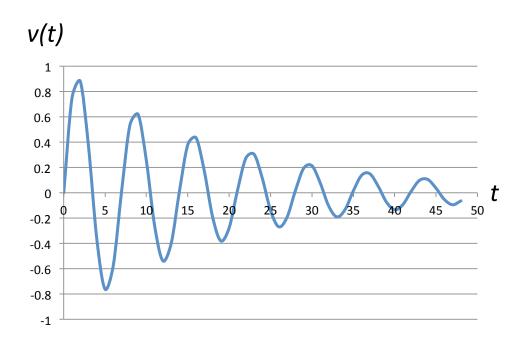
WcGill underdamped natural response

underdamped response: $\alpha < \omega_0$

The roots are complex:

$$S = -\alpha \pm j\sqrt{\omega_0^2 - \alpha^2}$$
$$= -\alpha \pm j\omega_d$$

The natural response has an oscillation at the damped frequency $\omega_{\rm d}$, decaying with time constant α .



$$v(t) = \exp(-\alpha t) \left[A_1 \exp(+j\omega_d t) + A_2 \exp(-j\omega_d t) \right]$$
$$= \exp(-\alpha t) \left[B_1 \sin(\omega_d t) + B_2 \cos(\omega_d t) \right]$$

The coefficients can be found:

$$v(0+) = B_2$$

$$\frac{dv}{dt}(0+) = -\alpha B_2 - \omega_d B_1$$

14 ECSE-200



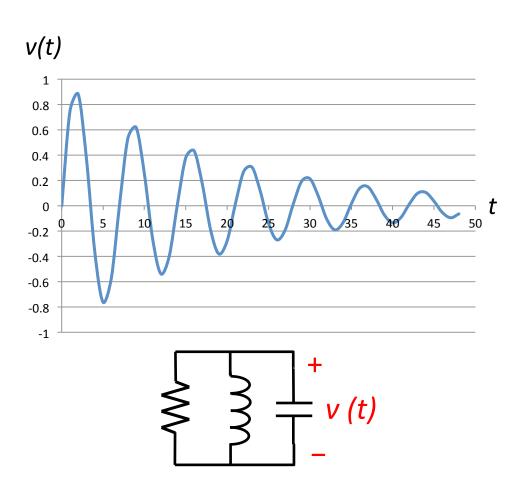
WCGill underdamped natural response

underdamped response: $\alpha < \omega_0$

$$s = -\alpha \pm j\omega_d$$

By analogy, an underdamped pendulum oscillates, losing a fraction of the initially stored energy during each oscillation (eg. by friction).

pendulum



The resistor dissipates energy at each moment that $v(t) \neq 0$.

ECSE-200 15



critically damped natural response

critically damped response: $\alpha = \omega_0$

The roots are identical:

$$s = -\alpha = -\omega_0$$

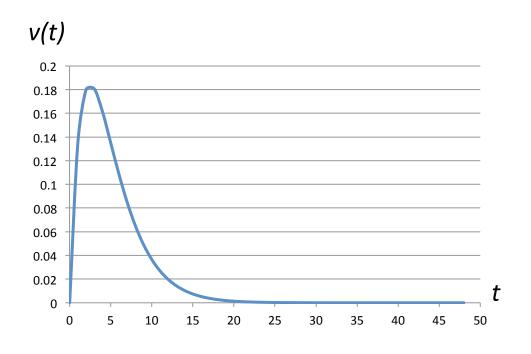
The natural response has the form*:

$$v(t) = \exp(-\alpha t) \left[A_1 t + A_2 \right]$$

The coefficients can be found by using the initial conditions:

$$v(0+) = A_2$$

$$\frac{dv}{dt}(0+) = A_1 + sA_2$$



^{*}refer to theory of ordinary differential equations for explanation

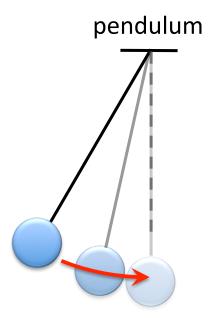


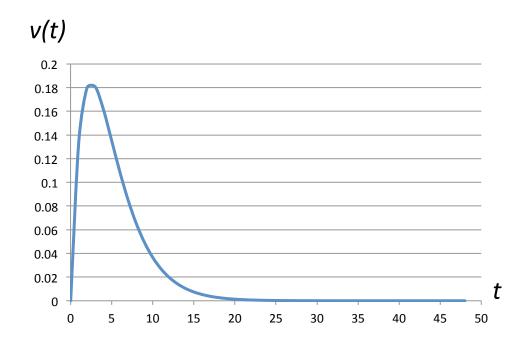
critically damped natural response

critically damped response: $\alpha = \omega_0$

$$s = -\alpha = -\omega_0$$

By analogy, a critically damped pendulum does not oscillate, but approaches rest.







overdamped natural response

overdamped response: $\alpha > \omega_0$

Two real roots are found.

$$s = -\alpha \pm \sqrt{\alpha^2 - \omega_0^2}$$

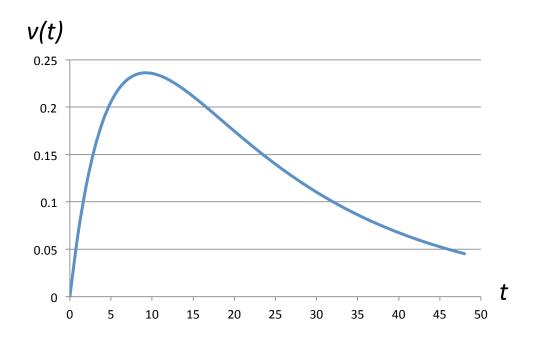
The natural response is:

$$v(t) = A_1 \exp(s_1 t) + A_2 \exp(s_2 t)$$

The coefficients can be found by using the initial conditions:

$$v(0+) = A_1 + A_2$$

$$\frac{dv}{dt}(0+) = s_1 A_1 + s_2 A_2$$





overdamped natural response

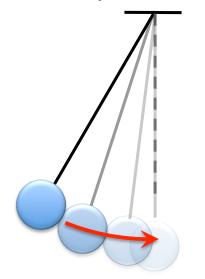
overdamped response: $\alpha > \omega_0$

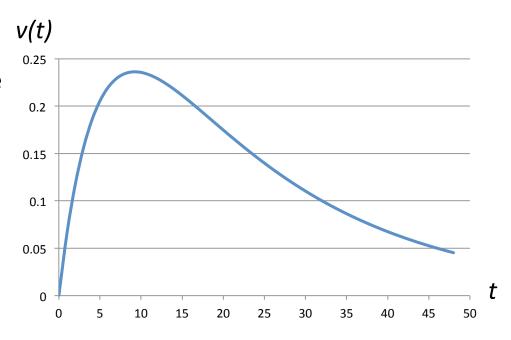
Two real roots are found.

$$s = -\alpha \pm \sqrt{\alpha^2 - \omega_0^2}$$

By analogy, an overdamped pendulum approaches rest at a rate dominated by damping (eg. as if placed in a highly viscous fluid)

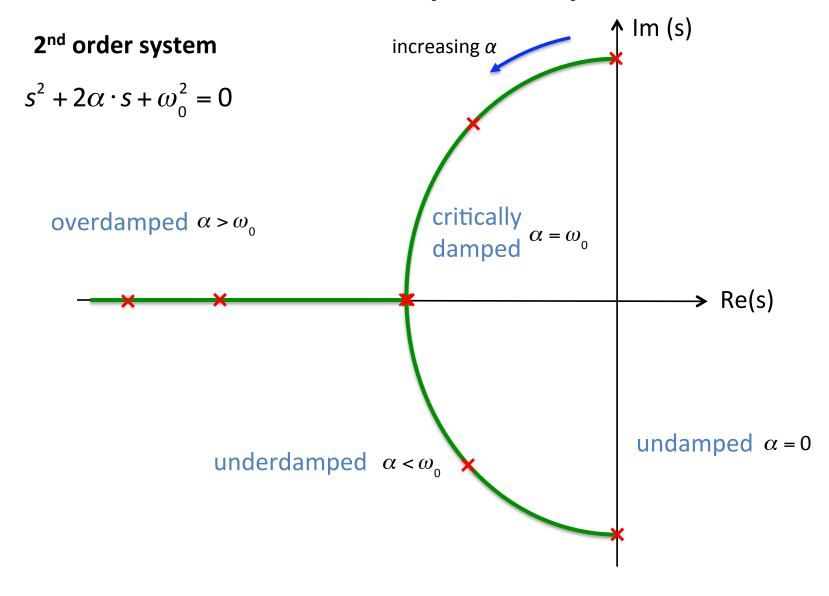
pendulum







the complex s-plane





the complex s-plane

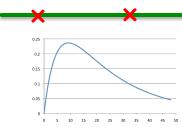
increasing α

2nd order system

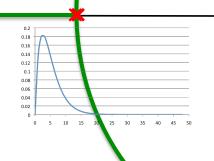
$$s^2 + 2\alpha \cdot s + \omega_0^2 = 0$$

overdamped $\alpha > \omega_0$

$$S = -\alpha \pm \sqrt{\alpha^2 - \omega_0^2}$$

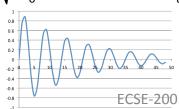


critically damped $\alpha = \omega_0$ $s = -\alpha$



underdamped $\alpha < \omega_0$

$$S = -\alpha \pm j\sqrt{\omega_0^2 - \alpha^2} = -\alpha \pm j\omega_d$$



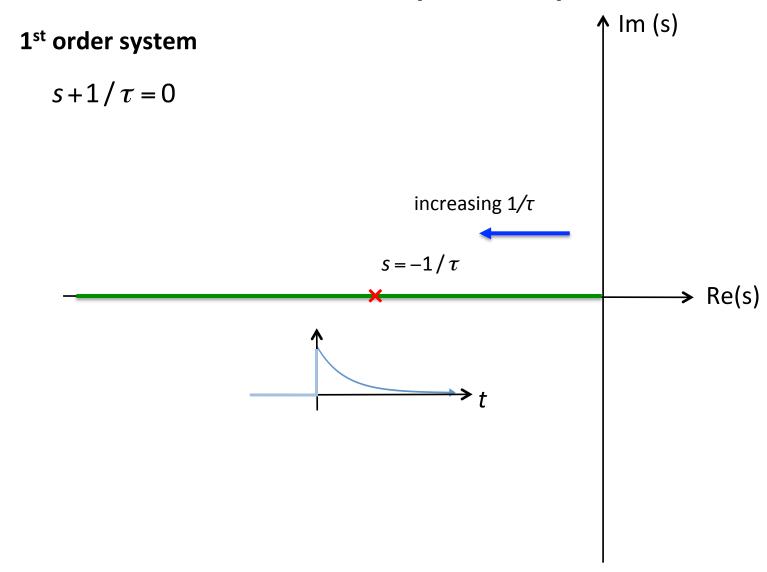
undamped $\alpha = 0$ $s = \pm j\omega_0$

→ Re(s)

Im (s)



the complex s-plane





RLC natural response: general procedure

step #1: Find the initial value and initial deritvative of the circuit variable of interest, x(0+) and dx/dt(0+), using circuit analysis and continuity of capacitor voltage and inductor current.

step #2: Using the operator method, or by directly writing down the equation, determine the characteristic equation coefficients α and ω_0 in terms of R, L, C.

$$s^2 + 2\alpha s + \omega_0^2 = 0$$

step #3: Find the roots of the characteristic equation:

$$S_{1,2} = -\alpha \pm \sqrt{\alpha^2 - \omega_0^2}$$

step #4: Construct the solution, using the over-/critical/under-damped nature of the response: $x(t) = A_1 \exp(s_1 t) + A_2 \exp(s_2 t)$

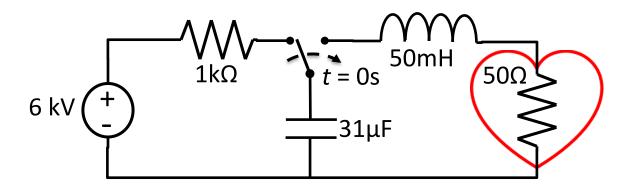
$$x(t) = \exp(-\alpha t) \left[A_1 t + A_2 \right]$$

$$x(t) = \exp(-\alpha t) \left[B_1 \sin(\omega_d t) + B_2 \cos(\omega_d t) \right]$$







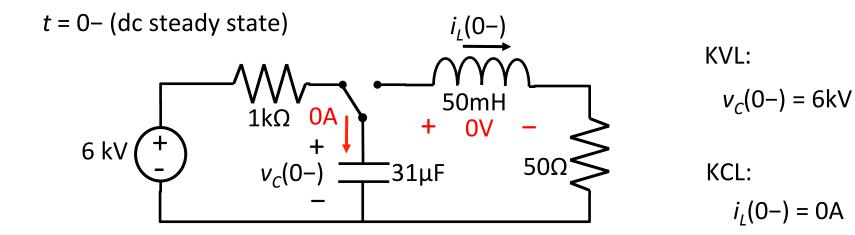


Find the voltage versus time on the heart, crudely approximated as a 50Ω resistor. The circuit is in dc steady state for t < 0, and the switch moves instantaneously at t = 0s.

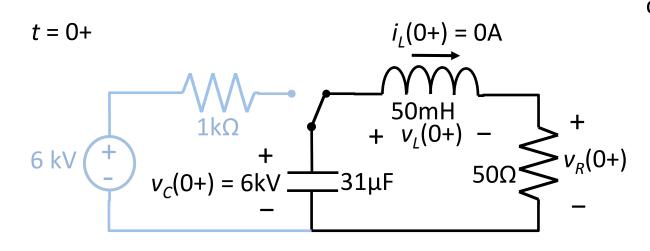
The circuit has been designed to deliver a voltage pulse to the human heart, with shape and amplitude that have the desired physiological effect.



step #1 : initial conditions



step #1 : initial conditions



continuity:

$$v_C(0+) = v_C(0-) = 6kV$$

$$i_L(0+) = i_L(0-) = 0A$$

Ohm:
$$v_R(0+) = i_I(0+) 50\Omega = 0V$$

KVL:
$$0 = -v_C(0+) + v_L(0+) + v_R(0+)$$

$$v_L(0+) = v_C(0+) - v_R(0+) = 6kV$$



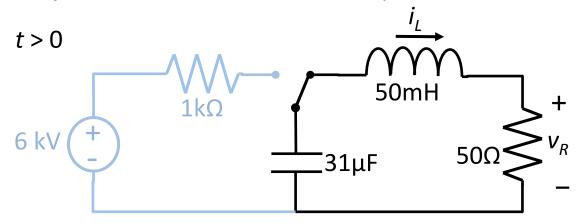
initial conditions:

$$\begin{vmatrix} v_R(0+) = 0 \text{ V} \\ \frac{dv_R}{dt} \Big|_{t=0+} = 6 \text{ MV/s}$$

Ohm, inductor:
$$\left. \frac{dv_R}{dt} \right|_{t=0+} = 50\Omega \cdot \frac{di_L}{dt} \bigg|_{t=0+} = 50\Omega \cdot \frac{v_L(0+)}{50\text{mH}} = 6 \text{ MV/s}$$



step #2: find the characteristic equation



Note that the natural response of v_R and i_L are determined by the same characteristic equation. Why?

mesh equation:
$$0 = i_L \cdot sL + i_L \cdot R + i_L \cdot \frac{1}{sC}$$

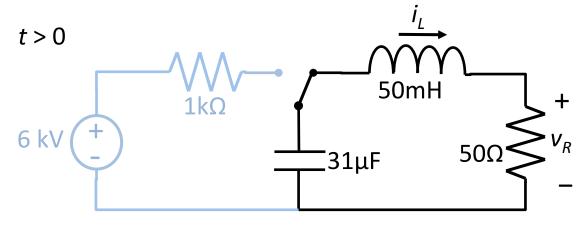
$$0 = \left(sL + R + \frac{1}{sC}\right) \cdot i_L$$

$$i_{L} \neq 0 \qquad \therefore 0 = sL + R + \frac{1}{sC} \implies 0 = s^{2} + s \cdot \frac{R}{L} + \frac{1}{LC}$$

$$0 = s^{2} + s \cdot \frac{50\Omega}{50\text{mH}} + \frac{1}{50\text{mH} \cdot 31\mu\text{F}}$$

$$0 = s^2 + s \cdot 1000 + 645161$$

step #3: find the roots of the characteristic equation



$$0 = a \cdot s^{2} + b \cdot s + c$$
$$= s^{2} + s \cdot 1000 + 645161$$

$$s_{1,2} = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

$$= \frac{-1000 \pm \sqrt{(1000)^2 - 4 \cdot 1 \cdot 645161}}{2 \cdot 1} = -500 \pm i \cdot 629 \quad [s^{-1}] \text{ units}$$

step #4 : construct the solution

$$v_R(0+) = 0 \text{ V}$$
 $\frac{dv_R}{dt}\Big|_{t=0+} = 6 \text{ MV/s}$ $s_{1,2} = -500 \pm i \cdot 629 \text{ [s}^{-1}\text{]}$

Two complex roots correspond to *underdamped* natural response.

$$v_{R}(t) = A_{1} \exp(s_{1}t) + A_{2} \exp(s_{2}t)$$

$$= \exp(-500s^{-1} \cdot t) \left[B_{1} \cos(629s^{-1} \cdot t) + B_{2} \sin(629s^{-1} \cdot t) \right]$$

Apply first of two initial conditions:

$$v_{R}(0+) = 1 \cdot \left[B_{1} \cdot 1 + B_{2} \cdot 0 \right] = B_{1}$$

$$0 \lor = B_{1}$$



step #4 : construct the solution

$$V_R(t) = B_2 \cdot \exp(-500s^{-1} \cdot t) \cdot \sin(629s^{-1} \cdot t)$$

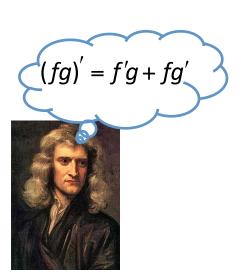
Apply second of two initial conditions:

$$\frac{dv_R}{dt} = B_2 \cdot \left[-500s^{-1} \exp(-500s^{-1} \cdot t) \right] \cdot \sin(629s^{-1} \cdot t)$$
$$+B_2 \cdot \exp(-500s^{-1} \cdot t) \cdot \left[629s^{-1} \cos(629s^{-1} \cdot t) \right]$$

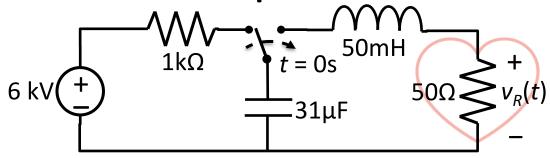
$$\frac{dv_{R}}{dt}\bigg|_{t=0+} = B_{2} \cdot \left[-500s^{-1} \cdot 1 \right] \cdot 0 + B_{2} \cdot 1 \cdot \left[629s^{-1} \cdot 1 \right]$$

$$6MV/s = B_{2} \cdot 629s^{-1}$$

$$B_{2} = 9.54 \text{ kV}$$

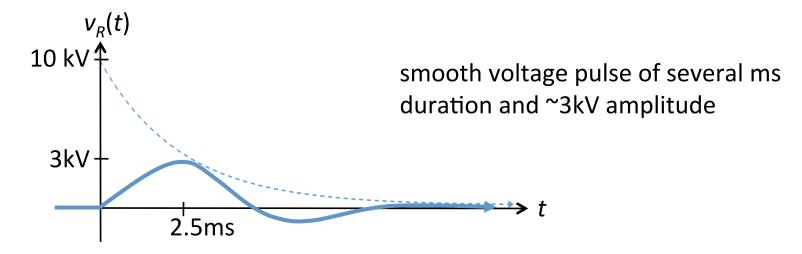






solution:

$$v_R(t) = 9.54 \text{kV} \cdot \exp(-500 \text{s}^{-1} \cdot t) \cdot \sin(629 \text{s}^{-1} \cdot t)$$
 $t > 0$



The energy delivered to the heart is:

$$U = \frac{1}{2}C \ v_c^2(0) = \frac{1}{2} \cdot 31 \mu F \cdot (6kV)^2 = 558 J$$