

ADVANCED COMMUNICATION SYSTEMS

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Digital Modulation

1st Semester 2018

Material based on Chapters 2 & 3 of "Digital Communications" by Proakis & Salehi, 2008, and Chapter 7 of "Communication Systems Engineering" by Proakis & Salehi, 2002, and Chapter 5 of "Digital Communications—a Discrete-Time Approach" by Michael Rice, 2009

DIGITAL COMMUNICATION SYSTEM

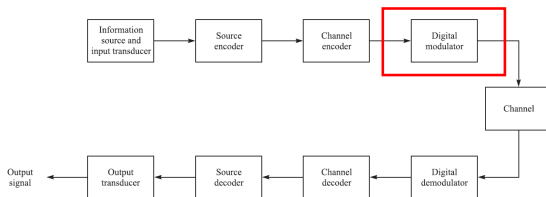


FIGURE 1.1-1
Basic elements of a digital communication system.

Digital modulation for AWGN channels

- Signal Space Representation
 - Baseband-bandpass signals
 - Signal space properties
 - Orthonormal bases
- Digital Modulation Schemes
 - One-dimensional modulation
 - Two-dimensional modulation
 - Multi-dimensional modulation

DIGITAL MODULATION

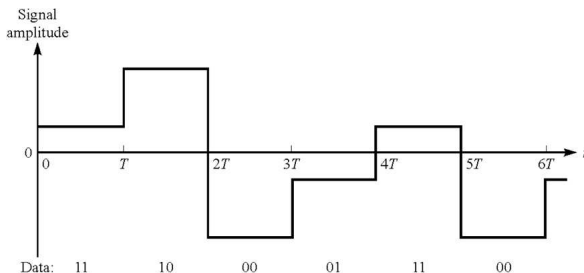


FIGURE 3.1-1

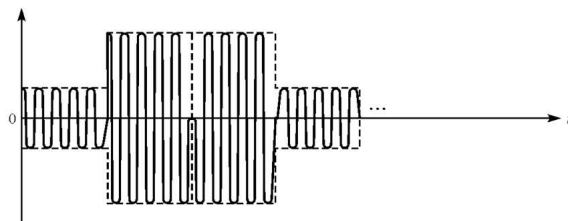
Block diagram of a memoryless digital modulation scheme.

- Modulation:** mapping *digital* information into *analog* signals suitable for transmission over physical channels.
 - requires **parsing** of the incoming bit sequence into a sequence of binary words of length k
 - each binary word of length k corresponds to a symbol; there are $M = 2^k$ possible symbols
 - each symbol corresponds to a **signaling interval** of length T
 - $1/T$ is the symbol rate; k/T is the bit rate
- Examples of channels:** Deep space, earth atmosphere, underwater acoustic channels, fibre optic cables, optical discs, etc.
- Different *channels* cause different types of *impairments* and require different types of modulation.

BASEBAND – BANDPASS SIGNALS



(a) Baseband PAM signal



(b) Bandpass PAM signal

BASEBAND – BANDPASS SIGNALS

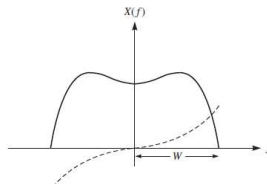


FIGURE 2.1-1

The spectrum of a real-valued lowpass (baseband) signal.

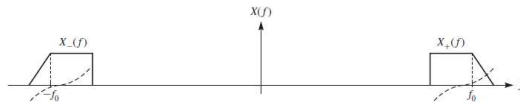


FIGURE 2.1-2

The spectrum of a real-valued bandpass signal.

- **Baseband channels:** Have frequency passbands that include zero frequency ($f = 0$). No need to use carrier waveforms to transmit source information.
- **Bandpass channels:** Have frequency passbands far removed from $f=0$. Digital information is impressed on higher frequency sinusoidal waveforms, i.e., carrier modulation.

SIGNAL SPACE

- To simplify analysis, use **geometric vector representation** for baseband and bandpass signals \Rightarrow signals have same properties as vectors. *Further Reading: Principles of Communication Engineering (1965) by Wozencraft and Jacobs*
- Vector Space:** A linear space or vector space L over a field F (usually $F = \mathbb{R}$ or $F = \mathbb{C}$) is a set that is closed under two operations of **addition** and **scalar multiplication**, and satisfies the following axioms:
 - Associative $\mathbf{u} + (\mathbf{v} + \mathbf{w}) = (\mathbf{u} + \mathbf{v}) + \mathbf{w}$
 - Commutative: $\mathbf{u} + \mathbf{v} = \mathbf{v} + \mathbf{u}$
 - Distributive: $a(\mathbf{u} + \mathbf{v}) = a\mathbf{u} + a\mathbf{v}$, $(a + b)\mathbf{v} = a\mathbf{v} + b\mathbf{v}$
 - Addition: $\mathbf{v} + (-\mathbf{v}) = -\mathbf{v} + \mathbf{v} = \mathbf{0}$, $\mathbf{0} + \mathbf{v} = \mathbf{v} + \mathbf{0} = \mathbf{v}$
 - Multiplication: $(ab)\mathbf{v} = a(b\mathbf{v})$, $1\mathbf{v} = \mathbf{v}$, $0\mathbf{v} = \mathbf{0}$,
- Examples of vector spaces:** \mathbb{R}^n , \mathbb{C}^n , function spaces, etc.

SIGNAL SPACE

A signal space is a vector space consisting of **functions** $x(t)$ defined on a time set T ; addition and scalar multiplication are defined by

$(x_1 + x_2)(t) = x_1(t) + x_2(t)$ and $(\alpha x)(t) = \alpha x(t)$ where $\alpha \in \mathbb{C}$.

Main idea:

- represent a signal function by a vector
- represent this vector as a point in the signal space
- the modulation scheme is then visualized as a finite set of points, called the signal space diagram or **signal constellation**
- this approach enables a geometric interpretation, also it allows us to treat bandpass modulation in a similar way as baseband modulation

SIGNAL SPACE

Properties of signal functions: (here α^* denotes the conjugate of a complex number α)

- The **inner product** of two complex-valued signals is

$$\langle x_1(t), x_2(t) \rangle := \int_{-\infty}^{\infty} x_1(t) x_2^*(t) dt.$$

- Two signals $x_1(t)$ and $x_2(t)$ are called **orthogonal** if $\langle x_1(t), x_2(t) \rangle = 0$.
- The **norm** of $x(t)$ is

$$\|x(t)\| := \sqrt{\langle x(t), x(t) \rangle} = \sqrt{\int_{-\infty}^{\infty} |x(t)|^2 dt} = \sqrt{\mathcal{E}_x},$$

where \mathcal{E}_x is the **energy** in $x(t)$.

SIGNAL SPACE

- Distance between two signals is

$$d(x_1(t), x_2(t)) = \|x_1(t) - x_2(t)\|.$$

- Cauchy-Schwarz inequality for two signals is

$$|\langle x_1(t), x_2(t) \rangle| \leq \|x_1(t)\| \cdot \|x_2(t)\| = \sqrt{\mathcal{E}_{x_1} \mathcal{E}_{x_2}}$$

with equality when $x_1(t) = \alpha x_2(t)$, where α is any complex number.
Useful inequality which we will use in the topic "demodulation".

- Triangle inequality is

$$\|x_1(t) + x_2(t)\| \leq \|x_1(t)\| + \|x_2(t)\|.$$

SIGNAL SPACE

- A set of N signals $\{\phi_j(t), j = 1, 2, \dots, N\}$ **spans** a subspace S if any signal $s(t) \in S$ can be written as a **linear combination** of the N signals

$$s(t) = \sum_{j=1}^N s_j \phi_j(t),$$

where s_j are scalar-valued coefficients.

- A set of signals is **linearly independent** if *no signal in the set* can be represented as a linear combination of *the other signals in the set*.
- A **basis** for S is any linearly independent set that spans it.
- The **dimension** of S is the number of elements in *any basis for S* .

ORTHONORMAL BASES

Orthonormal Bases: A basis $\{\phi_j(t), j = 1, 2, \dots, N\}$ for a subspace S is an orthonormal basis if

$$\langle \phi_j(t), \phi_n(t) \rangle = \int_{-\infty}^{\infty} \phi_j(t) \phi_n^*(t) dt = \begin{cases} 1 & j = n \\ 0 & j \neq n \end{cases}$$

An orthonormal basis is a convenient way to represent any $s(t) \in S$ as

$$s(t) = \sum_{j=1}^N s_j \phi_j(t)$$

where s_j is the *projection* of $s(t)$ onto the basis vector $\phi_j(t)$, i.e.,

$$s_j = \langle s(t), \phi_j(t) \rangle = \int_{-\infty}^{\infty} s(t) \phi_j^*(t) dt.$$

ORTHONORMAL BASES

- Recall that modulation involves a signal set $\{s_1(t), \dots, s_M(t)\}$
- Each signal $s_m(t)$ (for $m = 1, \dots, M$) is represented in terms of the N basis signals as a **vector** given by

$$\mathbf{s}_m = [s_{m1}, s_{m2}, \dots, s_{mN}]^T$$

or equivalently as a **point** in the N -dimensional signal space.

- The plot of these M points is called a **signal space diagram** or a **signal constellation**, the following plots are $N = 2$ examples:

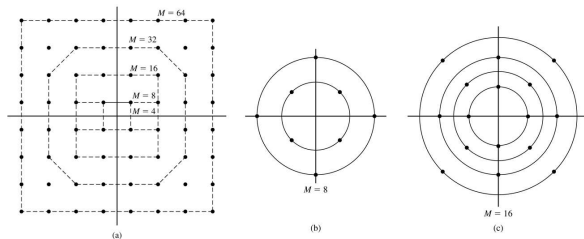


Figure 7.23

(a) Rectangular signal-space constellations for QAM.

Figure 7.23

(b, c) Examples of combined PAM-PSK signal-space constellations.

ORTHONORMAL BASES

- Each point corresponds to $k = \log_2 M$ bits of information.
- The square of the Euclidean distance of a point to the origin equals the energy of the corresponding signal

$$\mathcal{E}_{s_m} = s_{m1}^2 + s_{m2}^2 + \cdots + s_{mN}^2.$$

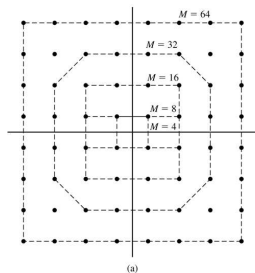
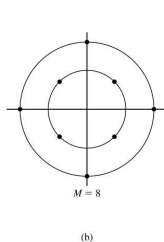
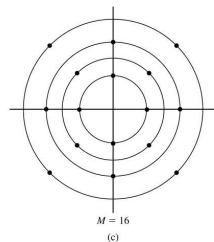


Figure 7.23

(a) Rectangular signal-space constellations for QAM.



(b, c) Examples of combined PAM-PSK signal-space constellations.



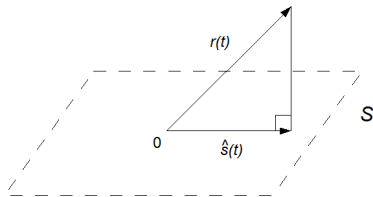
ORTHONORMAL BASES

Question:(useful for later topic of "demodulation")

- Given a received signal $r(t)$ outside a subspace S with orthonormal basis $\{\phi_j(t), j = 1, 2, \dots, N\}$, which $\hat{s}(t) = [s_1, \dots, s_N]$ in S is closest to $r(t)$? In other words, which $\hat{s}(t) \in S$ minimizes the distance $\|r(t) - \hat{s}(t)\|$?

Answer:

- $\hat{s}(t)$ is the projection of $r(t)$ onto the signal space S . More specifically, $\hat{s}(t) = [s_1, \dots, s_N]$ where $s_j = \langle r(t), \phi_j(t) \rangle$, is the projection of $r(t)$ onto each basis function $\phi_j(t)$ (for $j = 1, \dots, N$).



ORTHONORMAL BASES

- We can construct a set of orthonormal basis signals using the **Gram-Schmidt procedure**, starting from a set of signals $\{s_m(t), m = 1, 2, \dots, M\}$. The first orthonormal signal is simply

$$\phi_1(t) = \frac{s_1(t)}{\sqrt{\mathcal{E}_1}},$$

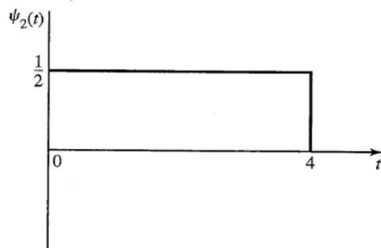
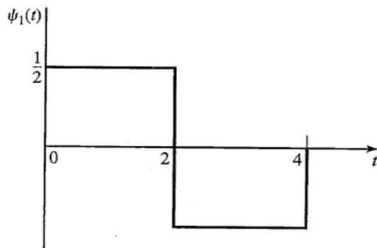
- The j -th basis signal can be found as $\phi_j(t) = \frac{\gamma_j(t)}{\sqrt{\mathcal{E}_j}}$ where $\gamma_j(t) = s_j(t) - \sum_{i=1}^{j-1} c_{ji} \phi_i(t)$, $c_{ji} = \langle s_j(t), \phi_i(t) \rangle$, and $\mathcal{E}_j = \int_{-\infty}^{\infty} \gamma_j^2(t) dt$. (See textbook Ch 2.2-4 for further details.)
- The procedure is continued until all the M signals have been exhausted and $N \leq M$ orthonormal signals have been constructed \Rightarrow Dimension of signal space is N .

N.B. In most cases we will be able to recognize orthonormal bases fairly easily, so that Gram-Schmidt is not needed.

SIGNAL SPACE

Questions:

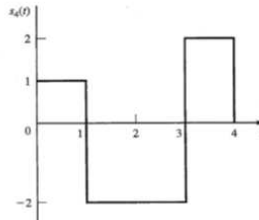
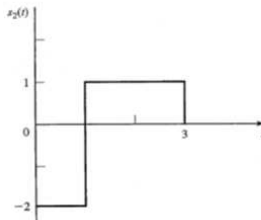
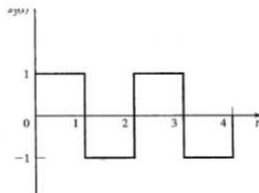
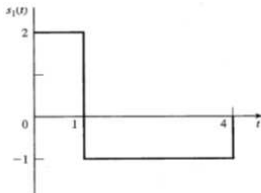
- What are the **norms** of the two signals below?
- Are they **orthogonal**?
- What is the **distance** between them?



SIGNAL SPACE

Question:

- What is the **dimension** of the subspace spanned by the signals below?



DIGITAL MODULATION



FIGURE 3.1–1

Block diagram of a memoryless digital modulation scheme.

- **Symbol generator:** maps a sequence of blocks of k bit values into a sequence of symbols. There are $M = 2^k$ possible symbols.
- **Modulator:** maps a symbol sequence into a continuous time signal $s(t)$.
 - Binary modulation: $k = 1, M = 2$ symbols
 - 4-ary modulation: $k = 2, M = 4$ symbols
 - M -ary modulation: $k > 1, M = 2^k$ symbols

ONE-DIMENSIONAL MODULATION: OOK

One of the simplest binary modulation schemes is **On Off Keying (OOK)**.

- a baseband OOK modulator maps a binary symbol sequence $a(n)$ to a continuous time signal $s(t)$ given by

$$s(t) = \sum_{n \in \mathbb{Z}} a(n)p(t - nT) \quad t \in \mathbb{R},$$

where $1/T$ is the symbol rate and $p(t)$ is a pulse signal, for example:

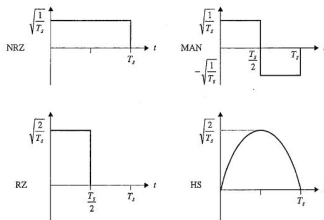


Figure A.1.1 The non-return-to-zero (NRZ), the return-to-zero (RZ), Manchester (MAN), and half-sine (HS) pulse shapes as shown.

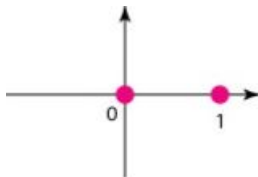
Thus on the signaling interval $(0, T]$ baseband OOK modulation produces a signal of the form

$$s_m(t) = A_m p(t), \quad \text{for } m = 1, 2, \quad A_1 = 1, A_2 = 0.$$

Bandpass OOK employs a carrier frequency f_c —on the signaling interval $(0, T]$ it produces a signal of the form

$$s_m(t) = A_m g(t) \cos(2\pi f_c t), \quad \text{for } m = 1, 2, \quad A_1 = 1, A_2 = 0.$$

where the pulse signal is now denoted by $g(t)$. The OOK signal constellation is one-dimensional and given by

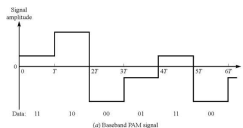


ONE-DIMENSIONAL MODULATION: PAM

Similar as OOK, a baseband PAM modulator maps a symbol sequence $a(n)$ to a continuous time signal $s(t)$ given by

$$s(t) = \sum_{n \in \mathbb{Z}} a(n)p(t - nT) \quad t \in \mathbb{R},$$

for example



On the signaling interval $(0, T]$ baseband PAM modulation produces a signal of the form

$$s_m(t) = A_m p(t), \quad 1 \leq m \leq M,$$

where $\{A_1, A_2, \dots, A_M\}$ is the set of possible amplitudes.

Some example constellations are shown below:

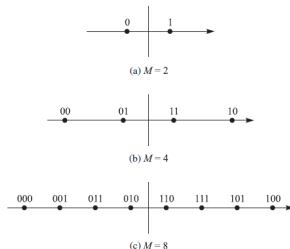


FIGURE 3.2-1

Constellation for PAM signaling.

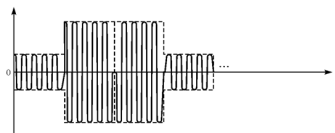
- The **energy** per constellation point equals

$$\mathcal{E}_m = \|s_m(t)\|^2 = \int_0^T A_m^2 p^2(t) dt = A_m^2 \mathcal{E}_p$$

where \mathcal{E}_p is the energy in $p(t)$.

- An orthonormal basis vector for PAM is given by

$$\phi(t) = \frac{p(t)}{\sqrt{\mathcal{E}_p}}$$



(b) Bandpass PAM signal

- For carrier-modulated PAM signals, we have

$$s_m(t) = A_m g(t) \cos(2\pi f_c t), \quad 1 \leq m \leq M, \quad 0 \leq t < T$$

- the bandpass PAM **energy** per constellation point equals

$$\begin{aligned} \mathcal{E}_m &= \|s_m(t)\|^2 = \int_0^T A_m^2 g^2(t) \cos^2(2\pi f_c t) dt \\ &= \frac{A_m^2}{2} \int_0^T g^2(t) dt + \underbrace{\frac{A_m^2}{2} \int_0^T g^2(t) \cos(4\pi f_c t) dt}_{\approx 0 \text{ for large } f_c} \approx \frac{A_m^2}{2} \mathcal{E}_g \end{aligned}$$

- binary bandpass PAM is also called Binary Phase Shift Keying (**BPSK**) because the symbol values inform the phase of $s_m(t)$. More precisely: $A_1 = 1 \leftrightarrow \text{phase } 0$ and $A_2 = -1 \leftrightarrow \text{phase } \pi$.

RECALL FROM EARLIER SUBJECTS (SIGNALS & SYSTEMS):

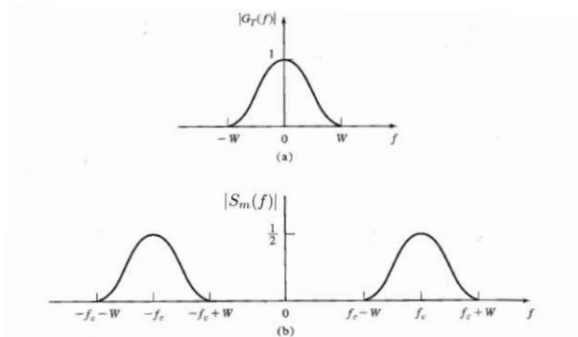


Figure 7.9 Spectra of (a) baseband and (b) amplitude-modulated signals.

- Modulating the signal waveform $s_m(t)$ with carrier $\cos(2\pi f_c t)$ **shifts the spectrum** of the baseband signal by f_c , i.e.,

$$S_m(f) = \frac{A_m}{2}(G_T(f - f_c) + G_T(f + f_c))$$

- For bandpass PAM signaling, the orthonormal basis vector is given by

$$\phi(t) = \sqrt{\frac{2}{\mathcal{E}_g}} g(t) \cos(2\pi f_c t)$$

which results in $s_m(t) = A_m \sqrt{\frac{\mathcal{E}_g}{2}} \phi(t)$.

- Bandpass PAM has the same signal space diagram as baseband PAM but with a different basis vector

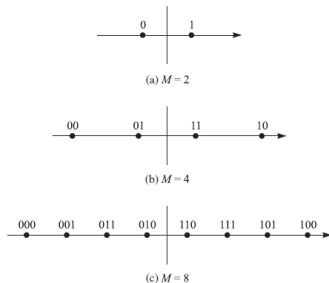
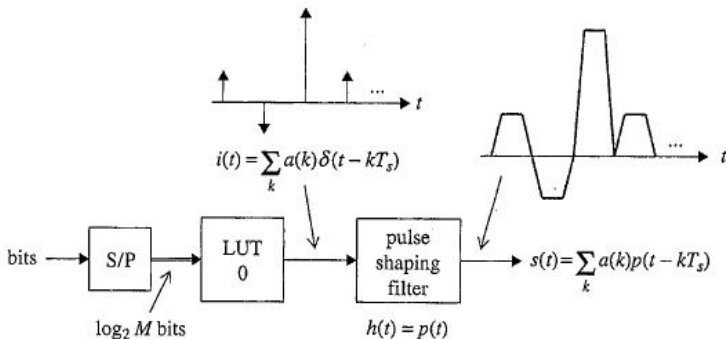


FIGURE 3.2-1

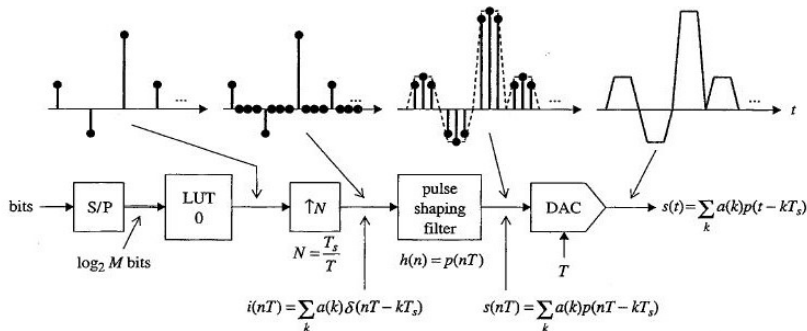
Constellation for PAM signaling.

PAM MODULATOR IMPLEMENTATION

(in the next two figures the signaling interval is not denoted by T but by T_s)
PAM modulation, using a continuous-time pulse shaping filter:



PAM modulation, using a discrete-time FIR pulse shaping filter:



we see that this involves an upsampler as well as a digital-to-analog converter.

TWO-DIMENSIONAL MODULATION

- **Orthogonal signaling:** Modulation using two signals $\phi_1(t)$ and $\phi_2(t)$ that are orthonormal, i.e.,

$$s(t) = s_1\phi_1(t) + s_2\phi_2(t)$$

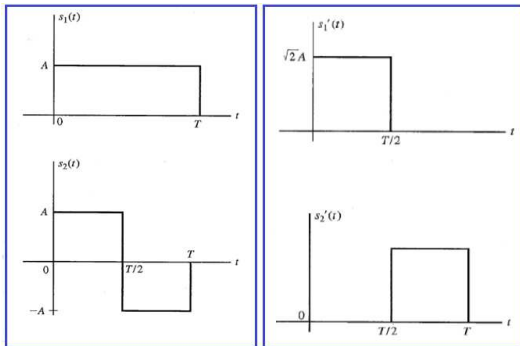
- We can denote the modulated signals as a vector $s(t) = (s_1, s_2)$ where s_1 and s_2 are the *projections* of $s(t)$ onto the basis vectors $\phi_1(t)$ and $\phi_2(t)$, i.e.,

$$s_j = \langle s(t), \phi_j(t) \rangle = \int_{-\infty}^{\infty} s(t)\phi_j(t)dt, \quad j \in \{1, 2\}.$$

Question: What are the geometric vector representations for the two sets of signals below given orthonormal basis functions

$$\phi_1(t) = \begin{cases} \sqrt{2/T} & 0 \leq t < T/2 \\ 0 & T/2 \leq t < T \end{cases}$$

$$\phi_2(t) = \begin{cases} 0 & 0 \leq t < T/2 \\ \sqrt{2/T} & T/2 \leq t < T \end{cases}$$



Question: What are the signals for $M = 4$ bi-orthogonal signal constellation below using the same basis functions $\{\phi_1(t), \phi_2(t)\}$?

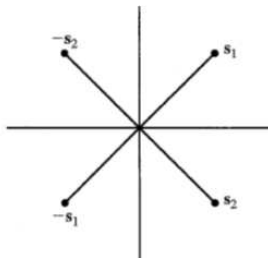
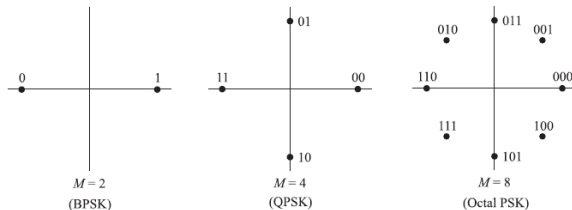


Figure 7.15 Signal constellation for $M = 4$ biorthogonal signals.

TWO-DIMENSIONAL BANDPASS MODULATION: MPSK

- **M -ary phase-shift keying (PSK):** All M bandpass signals are constrained to have the same energy, i.e., signal constellation points lie on a circle
- **Examples:**



- **Gray encoding:** Adjacent phases differ by only 1 bit. This leads to a better average bit error rate (BER). Indeed, in case the demodulator mistakes a symbol for its neighbour then this results in only 1 bit error. And this is the most likely demodulator error scenario.

- Signals with M -PSK modulation can be represented, for $m = 1, 2, \dots, M$, as

$$\begin{aligned}
 s_m(t) &= g(t) \cos(2\pi f_c t + \theta_m), \\
 &= \operatorname{Re} (g(t) e^{j\theta_m} e^{j2\pi f_c t}), \\
 &= g(t) \cos(\theta_m) \cos(2\pi f_c t) - g(t) \sin(\theta_m) \sin(2\pi f_c t)
 \end{aligned}$$

where $g(t)$ is the signal pulse shape and $\theta_m = \frac{2\pi}{M}(m-1)$ is the phase that conveys the transmitted information.

- An orthonormal basis for the signal space is

$$\{\phi_1(t), \phi_2(t)\} = \left\{ \sqrt{\frac{2}{\mathcal{E}_g}} g(t) \cos(2\pi f_c t), -\sqrt{\frac{2}{\mathcal{E}_g}} g(t) \sin(2\pi f_c t) \right\}$$

where basis functions are unit norm, i.e., $\|\phi_1(t)\| = \|\phi_2(t)\| = 1$

INTERPRETATION:

- the transmitted information is impressed on 2 orthogonal carrier signals, namely the in-phase carrier signal $\cos(2\pi f_c t)$ and the quadrature carrier signal $\sin(2\pi f_c t)$

$$s_m(t) = g(t) \cos(\theta_m) \cos(2\pi f_c t) - g(t) \sin(\theta_m) \sin(2\pi f_c t)$$

- its lowpass equivalent signal equals

$$s_m^{lowpass}(t) = g(t)e^{j\theta_m} = I(t) + jQ(t),$$

where $I(t) := g(t) \cos \theta_m$ is the in-phase component and $Q(t) := g(t) \sin \theta_m$ is the quadrature component of $s_m(t)$.

QPSK

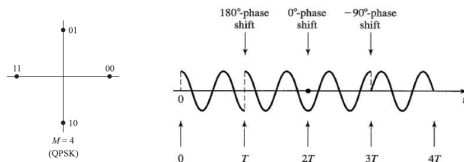


Figure 7.18 Example of a four PSK signal.

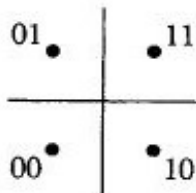
In quadrature/quaternary PSK (QPSK), the $M = 4$ signal points are differentiated via phase shifts by multiples of $\pi/2$, i.e., the corresponding bandpass signals are, for $t \in (0, T]$ given by

$$s_m(t) = g(t) \cos \left(2\pi f_c t + \frac{\pi}{2}(m-1) \right), \quad m = 1, 2, 3, 4$$

In the above figure we see how a QPSK modulator maps a sequence $a(n)$ of dibits into a continuous-time waveform $s(t)$.

QPSK

Equivalently, the signal constellation can be rotated:

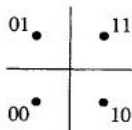


Denote the first bit of the dibit $a(n)$ by $a_1(n)$; denote the second bit of the dibit $a(n)$ by $a_2(n)$. Then the corresponding QPSK modulator maps the two binary symbol sequences $a_1(n)$ and $a_2(n)$ to a continuous-time waveform $s(t)$ given on the next page.

QPSK

$$s(t) = I(t)\sqrt{2}\cos 2\pi f_c t - Q(t)\sqrt{2}\sin 2\pi f_c t,$$

- $I(t) = \sum_n a_1(n)g(t - nT)$ is the **in-phase** component of $s(t)$
- $Q(t) = \sum_n a_2(n)g(t - nT)$ is the **quadrature** component of $s(t)$
- Note that $I(t)$ and $Q(t)$ are binary PAM pulse trains. In fact, this QPSK signal constellation can be interpreted as two PAM signal constellations, one on the in-phase component (ϕ_1 -axis), the other on the quadrature component (ϕ_2 -axis).



QPSK IMPLEMENTATION

Using a continuous-time pulse shaping filter:

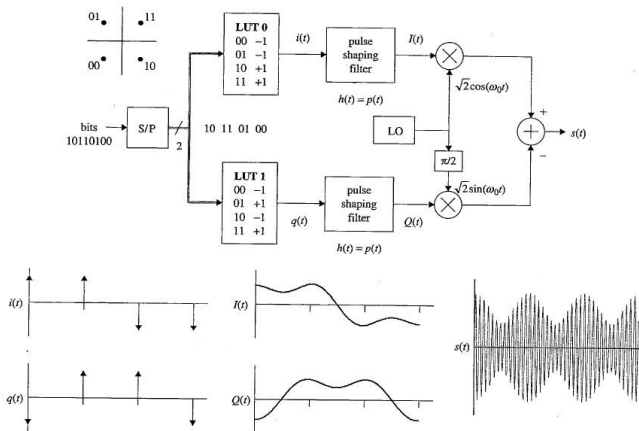


Figure 5.3.12 An example of a QPSK signal corresponding to the bit sequence 10110100.

DMPSK

Differential MPSK (DMPSK) modulation involves precoding of the information symbol sequence $b(n)$ into a symbol sequence $\delta(n)$ that is then input to a MPSK modulator.

- in MPSK each symbol value determines the actual value of the phase, but in DMPSK it determines the **phase change** from the previous signalling interval's symbol
- thus DMPSK is **modulation with memory**
- in which situations is differential modulation needed? If the MPSK demodulator's errors are always of the same type, determined by a **fixed** (or slowly varying) **phase mismatch** ϕ , the value of which we do not know (it may even be zero).
- how does differential modulation help? It leads to a better symbol error performance since it is robust against a fixed unknown phase mismatch.

EXAMPLE: DBPSK MODULATION

- Example: a symbol value of 0 causes a 0° phase change and a symbol value of 1 causes a 180° phase change

Data Bit	1	0	1	0	0	1
BPSK phase	0°	180°	0°	180°	180°	0°
DBPSK phase	180°	0°	0°	180°	180°	180°

- *Exercise:* Assume that the BPSK demodulator is able to reconstruct the DBPSK values without error. How to retrieve the original data bit sequence?
- *Exercise:* Assume that the BPSK demodulator's phase mismatch $\phi = 180^\circ$ (so it always picks 1 when it should have picked 0 and vice versa, in other words all the DBPSK values are demodulated in error). Convince yourself that your data retrieval method of the previous exercise still works.

TWO-DIMENSIONAL BANDPASS MODULATION: QAM

- **Quadrature amplitude modulation (QAM)**: Allow signals to have different amplitudes; impress separate information bits on each of the **quadrature carriers**
- Important performance parameters are **average energy** and **minimum distance** in the signal constellation

N.B. Note that averaging is needed because the symbols to be modulated are uncertain, one needs a probabilistic attitude

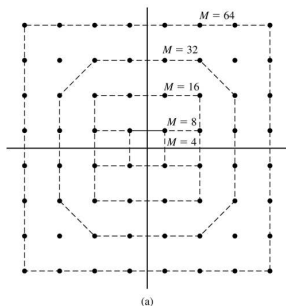


Figure 7.23

(a) Rectangular signal-space constellations for QAM.

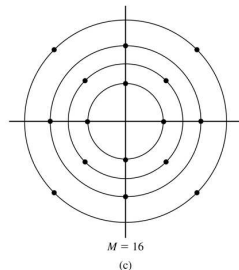
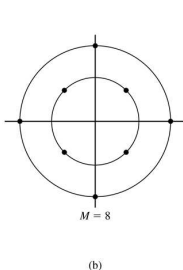


Figure 7.23

(b, c) Examples of combined PAM-PSK signal-space constellations.

COMPARISON OF PAM, PSK AND QAM

■ TABLE 3.2-1
Comparison of PAM, PSK, and QAM

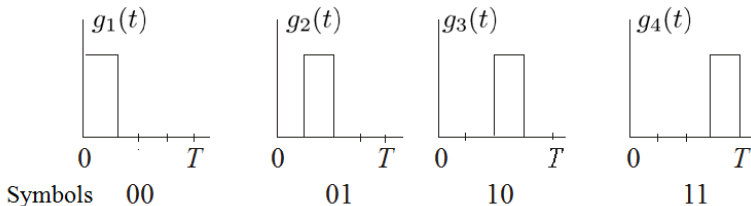
Signaling Scheme	$s_m(t)$	s_m	E_{avg}	E_{bavg}	d_{min}
Baseband PAM	$A_m p(t)$	$A_m \sqrt{\mathcal{E}_p}$	$\frac{2(M^2-1)}{3} \mathcal{E}_p$	$\frac{2(M^2-1)}{3 \log_2 M} \mathcal{E}_p$	$\sqrt{\frac{6 \log_2 M}{M^2-1}} \mathcal{E}_{\text{bavg}}$
Bandpass PAM	$A_m g(t) \cos 2\pi f_c t$	$A_m \sqrt{\frac{\mathcal{E}_g}{2}}$	$\frac{M^2-1}{3} \mathcal{E}_g$	$\frac{M^2-1}{3 \log_2 M} \mathcal{E}_g$	$\sqrt{\frac{6 \log_2 M}{M^2-1}} \mathcal{E}_{\text{bavg}}$
PSK	$g(t) \cos \left[2\pi f_c t + \frac{2\pi}{M}(m-1) \right]$	$\sqrt{\frac{\mathcal{E}_g}{2}} \left(\cos \frac{2\pi}{M}(m-1), \sin \frac{2\pi}{M}(m-1) \right)$	$\frac{1}{2} \mathcal{E}_g$	$\frac{1}{2 \log_2 M} \mathcal{E}_g$	$2 \sqrt{\log_2 M \sin^2 \left(\frac{\pi}{M} \right)} \mathcal{E}_{\text{bavg}}$
QAM	$A_{mi} g(t) \cos 2\pi f_c t - A_{mq} g(t) \sin 2\pi f_c t$	$\sqrt{\frac{\mathcal{E}_g}{2}} (A_{mi}, A_{mq})$	$\frac{M-1}{3} \mathcal{E}_g$	$\frac{M-1}{3 \log_2 M} \mathcal{E}_g$	$\sqrt{\frac{6 \log_2 M}{M-1}} \mathcal{E}_{\text{bavg}}$

MULTI-DIMENSIONAL MODULATION

- Can use **time** domain and/or **frequency** domain to increase the number of dimensions
- **Orthogonal Signaling (Baseband)**: e.g. Pulse position modulation (PPM)

$$s_m(t) = A_m g(t - \tau_m), \quad \tau_m \leq t < \tau_{m+1}$$

where $1 \leq m \leq M$ and $g(t)$ is a pulse of duration T/M .



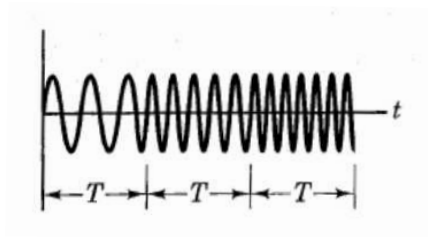
Four-dimensional PPM

- **Orthogonal Signaling (Bandpass):** e.g. Frequency shift-keying (FSK)

$$s_m(t) = \sqrt{\frac{2\mathcal{E}}{T}} \cos(2\pi(f_c + m\Delta f)t), \quad 0 \leq m \leq M-1, \quad 0 \leq t \leq T$$

where Δf is the frequency separation between successive frequencies.

- For orthogonality, we need to have minimal frequency separation of $\Delta f = 1/(2T)$ (see Tutorial problem)



- **Bi-Orthogonal Signaling:** A set of $M = 2^k$ bi-orthogonal signals is constructed from $\frac{1}{2}M$ orthogonal signals and their negatives

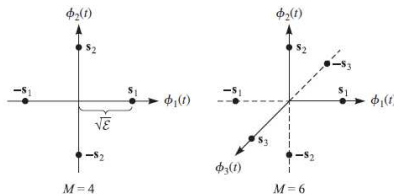


FIGURE 3.2-8

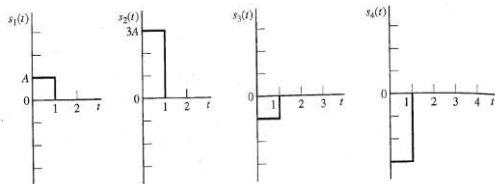
Signal space diagram for $M = 4$ and $M = 6$ biorthogonal signals.

N.B. Many other possible modulation schemes. See textbook Chapter 3 for further details.

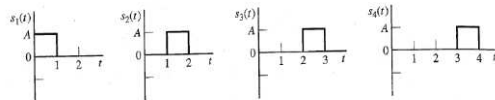
QUIZ

Question: Which set of signals corresponds to the following modulations?

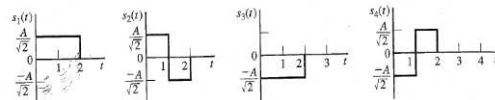
1. Orthogonal signalling
2. PAM
3. Bi-orthogonal signalling



Set I



Set II



Set III