

**Problem 1.** We may deduce from eqns (6.7) and (6.9) that

$$t_i = -pn_i + \mu n_j \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

Show that it is identical to

$$\mathbf{t} = -p\mathbf{n} + \mu[2(\mathbf{n} \cdot \nabla)\mathbf{u} + \mathbf{n} \times (\nabla \times \mathbf{u})]$$

**Proof:** We utilize the Levi-Civita symbol, where

$$\begin{aligned} [\mathbf{n} \times (\nabla \times \mathbf{u})]_i &= \varepsilon_{ijk} n_j \left( \varepsilon_{kmn} \frac{\partial u_n}{\partial x_m} \right) = \varepsilon_{kij} \varepsilon_{kmn} n_j \frac{\partial u_n}{\partial x_m} \\ &= (\delta_{im} \delta_{jn} - \delta_{in} \delta_{jm}) n_j \frac{\partial u_n}{\partial x_m} \\ &= n_j \frac{\partial u_j}{\partial x_i} - n_j \frac{\partial u_i}{\partial x_j} \end{aligned}$$

Also, since we also have  $[(\mathbf{n} \cdot \nabla)\mathbf{u}]_i = n_j \frac{\partial u_i}{\partial x_j}$ , combining with the calculation above, we obtain that

$$\begin{aligned} t_i &= -pn_i + \mu \left( 2n_j \frac{\partial u_i}{\partial x_j} + n_j \frac{\partial u_j}{\partial x_i} - n_j \frac{\partial u_i}{\partial x_j} \right) \\ &= -pn_i + \mu n_j \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \end{aligned}$$

□

**Problem 2.** Show that the net force exerted on a finite blob of fluid by the surrounding fluid is

$$\int_S \mathbf{t} dS = \int_V (-\nabla p + \mu \nabla^2 \mathbf{u}) dV$$

where  $S$  is the surface of the blob and  $V$  is the region occupied by the blob. Deduce that if the blob is small the net force on it, excluded gravity, is  $-\nabla p + \mu \nabla^2 \mathbf{u}$  per unit volume.

**Proof:** Calculate

$$\left[ \int_S \mathbf{t} dS \right]_i = \int_S T_{ij} n_j dS = \int_S \mathbf{T}_i \cdot \mathbf{n} dS$$

where  $\mathbf{T}_i$  is the  $i$ -th row of the stress tensor, then by Divergence Theorem,

$$\begin{aligned} \left[ \int_S \mathbf{t} dS \right]_i &= \int_V \nabla \cdot \mathbf{T}_i dV = \int_V \frac{\partial T_{ij}}{\partial x_j} dV \\ &= \int_V -\frac{\partial p \delta_{ij}}{\partial x_j} + \mu \frac{\partial}{\partial x_j} \left( \frac{\partial u_j}{\partial x_i} + \frac{\partial u_i}{\partial x_j} \right) dV \\ &= \int_V -\frac{\partial p}{\partial x_i} + \mu \frac{\partial}{\partial x_i} \frac{\partial u_j}{\partial x_j} + \mu \frac{\partial^2 u_i}{\partial x_j^2} dV \end{aligned}$$

Since  $\nabla \cdot \mathbf{u} = 0$ ,  $\mu \frac{\partial}{\partial x_i} \frac{\partial u_j}{\partial x_j} = 0$ , we then obtain

$$\int_S \mathbf{t} dS = \int_V (-\nabla p + \mu \nabla^2 \mathbf{u}) dV$$

as desired. And when the volume is sufficiently small, we may approximate the integration by

$$(-\nabla p + \mu \nabla^2 \mathbf{u}) \cdot V$$

then the net force per unit volume is

$$\frac{1}{V} (-\nabla p + \mu \nabla^2 \mathbf{u}) \cdot V = -\nabla p + \mu \nabla^2 \mathbf{u}$$

□

**Problem 3.** Verify in the case of a simple shear flow,

$$\mathbf{u} = [u(y), 0, 0]$$

equation  $\mathbf{t} = -p\mathbf{n} + \mu[2(\mathbf{n} \cdot \nabla)\mathbf{u} + \mathbf{n} \times (\nabla \times \mathbf{u})]$  reduces, when  $\mathbf{n} = (0, 1, 0)$ , to

$$\mathbf{t} = \left[ \mu \frac{du}{dy}, -p, 0 \right]$$

**Proof:** Calculate  $\mathbf{t}$  component-wise,

$$\begin{aligned} t_1 &= \mu \left( \frac{\partial u_1}{\partial y} + \frac{\partial u_2}{\partial x} \right) = \mu \frac{du}{dy} \\ t_2 &= -p + 2\mu \frac{\partial u_2}{\partial y} = -p \\ t_3 &= \mu \left( \frac{\partial u_3}{\partial y} + \frac{\partial u_2}{\partial z} \right) = 0 \end{aligned}$$

□

**Problem 4.** Give an order of magnitude estimate of the Reynolds number for:

- (i). flow past the wing of a jumbo jet at  $150 \text{ ms}^{-1}$  (roughly half speed of sound).
- (ii). experiment in 1.1 with  $L = 2 \text{ cm}$  and  $U = 5 \text{ cm s}^{-1}$
- (iii). a thick layer of golden syrup draining of the spoon.
- (iv). a spermatozoa with a tail length of  $10^{-3} \text{ cm}$  swimming at  $10^{-2} \text{ cm s}^{-1}$  in water.

**Solution:** (i).  $Re = \frac{UR}{\nu} = \frac{15000 \times 10^3}{0.15} = 10^7$ .

(ii). If we approximate the viscosity of salty water as pure water, then  $Re = \frac{5 \times 2}{0.01} = 10^3$ .

(iii).  $Re = \frac{1 \times 1}{1200} = 8 \times 10^{-3}$ .

(iv).  $Re = \frac{10^{-3} \times 10^{-2}}{0.01} = 10^{-3}$ .

**Problem 5.** The problem of 2 - D steady viscous flow past a circular cylinder of radius  $a$  involves finding a velocity field  $\mathbf{u} = [u(x, y), v(x, y), 0]$  which satisfies

$$(\mathbf{u} \cdot \nabla) \mathbf{u} = -\frac{1}{\rho} \nabla p + \nu \nabla^2 \mathbf{u}, \quad \nabla \cdot \mathbf{u} = 0$$

together with the boundary conditions

$$\mathbf{u} = 0 \text{ on } x^2 + y^2 = a^2; \quad \mathbf{u} \rightarrow (U, 0, 0) \text{ as } x^2 + y^2 \rightarrow \infty$$

Rewrite the problem in dimensionless form by using the dimensionless variables

$$\mathbf{x}' = \mathbf{x}/a, \quad \mathbf{u}' = \mathbf{u}/U, \quad p' = p/\rho U^2$$

Without solving the problem, show that the streamline pattern can depend on  $\nu, a, U$  only in the combination  $R = Ua/\nu$ , so that flows at equal Reynolds numbers are geometrically similar.

**Proof:** We calculate each term in the original equation

$$(\mathbf{u}' \cdot \nabla') \mathbf{u}' = \left( \frac{\mathbf{u}}{U} \cdot a \nabla \right) \frac{\mathbf{u}}{U} = \frac{a}{U^2} (\mathbf{u} \cdot \nabla) \mathbf{u}$$

Second term

$$\nabla' p' = a \nabla \left( \frac{p}{\rho U^2} \right) = \frac{a}{\rho U^2} \nabla p$$

thus

$$\frac{1}{\rho} \nabla p = \frac{U^2}{a} \nabla' p'$$

Third term

$$\nu \nabla'^2 \mathbf{u}' = \nu \frac{a^2}{U} \nabla^2 \mathbf{u}$$

Thus, by calculating the boundary condition, we transform the problem into

$$\begin{cases} (\mathbf{u}' \cdot \nabla') \mathbf{u}' = \nabla' p' + \frac{\nu}{U_a} \nabla'^2 \mathbf{u}' \\ \nabla' \cdot \mathbf{u}' = 0 \\ \mathbf{u}' = 0 \text{ on } x'^2 + y'^2 = 1 \\ \mathbf{u}' \rightarrow (1, 0, 0) \text{ as } x'^2 + y'^2 \rightarrow \infty \end{cases}$$

and notice that the solution to this question depends on  $\mathbf{x}'$  and  $R$ , then at each fixed  $\mathbf{x}'$ , the direction will only depend on  $R$ , so for same  $R$  (Reynolds number), the flow is geometrically similar.  $\square$

**Problem 6.** *Viscous fluid flow between two stationary rigid boundaries  $y = \pm h$  under a constant pressure gradient  $P = -dp/dx$ . Show that*

$$u = \frac{P}{2\mu}(h^2 - y^2), \quad v = w = 0$$

**Proof:** We seek solution to Navier-Stokes equation of the form  $\mathbf{u} = (u(y), 0, 0)$ , then consider N-S equation at  $x$ -component

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = -\frac{1}{\rho} \frac{\partial p}{\partial x} + \mu \nabla^2 u$$

Notice that since  $v = w = 0$ , and by  $\nabla \cdot \mathbf{u} = 0$ , we have  $\frac{\partial u}{\partial x} = 0$ . By some simple cancellation, we obtain

$$\mu \frac{d^2 u}{dy^2} = -\frac{P}{\rho}$$

the solution to this ODE is  $u = -\frac{P}{2\mu\rho}y^2 + C_1y + C_2$ , plugging in two boundary values ( $u = 0$  at  $y = \pm h$ ),  $C_1 = 0, C_2 = \frac{P}{2\mu\rho}h^2$ , thus the solution is

$$\mathbf{u} = \left( \frac{P}{2\mu}(h^2 - y^2), 0, 0 \right)$$

as desired.  $\square$