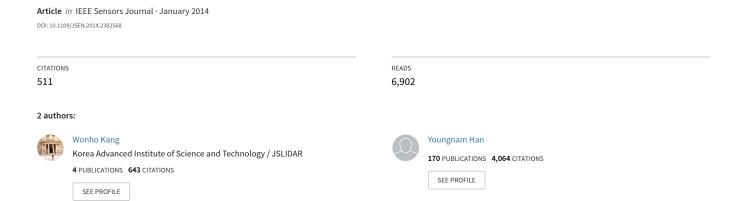
SmartPDR: Smartphone-Based Pedestrian Dead Reckoning for Indoor Localization



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Wonho Kang and Youngnam Han

Abstract—Indoor pedestrian tracking extends location-based services to indoor environments where GPS signal is rarely detected. Typical indoor localization method is Wi-Fi-based positioning system, which is practical showing accuracy and extending coverage. However, it involves significant costs of installing and managing wireless access points. A practical indoor pedestrian-tracking approach should consider the absence of any infrastructure or pretrained database. In this paper, we present a smartphone-based pedestrian dead reckoning, SmartPDR, which tracks pedestrians through typical dead reckoning approach using data from inertial sensors embedded in smartphones. SmartPDR does not require any complex and expensive additional device or infrastructure that most existing pedestrian tracking systems rely on. The proposed system was implemented on off-the-shelf smartphones and the performance was evaluated in several buildings. Despite inherent localization errors from low-cost noisy sensors and complicated human movements, SmartPDR successfully tracks indoor user's location, which is confirmed from the experimental results with reasonable location accuracy. Indoor pedestrian tracking system using smartphone inertial sensors can be a promising methodology validating its practical usage through real deployment.

Index Terms—Indoor pedestrian tracking, pedestrian dead reckoning, smartphone inertial sensor.

I. Introduction

OCATION-BASED services (LBS) rely on accurate and continuous localization of users. Typical LBS applications, such as navigation and content sharing, provide services based on user's current location. Thus, localization is essential function needed by location-aware applications in pervasive computing environments [1], [2]. Global Positioning System (GPS) has been contributing in this aspect by providing real-time location information. GPS is commonly used in outdoor environments and widely adopted in modern mobile devices such as smartphones [3], [4].

People spend most of their time indoors; therefore indoor pedestrian tracking becomes key technique required for indoor LBS in smartphone application market. Since the accuracy of GPS is degraded in indoor environments, active research has recently been done on indoor localization. However, no

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outstanding solution has been found due to practical issues that are related to complicated infrastructure requirements. Conventional techniques for indoor localization are based on various types of infrastructure support, which include infrared, narrowband radio, ultrasound, ultra-wideband (UWB), wireless fidelity (Wi-Fi) signal strength, radio-frequency identification (RFID), inertial measurement unit (IMU), vision, etc [1], [5], [6].

While the aforementioned methods are feasible in terms of locating accuracy, the implementation of most existing localization systems is based on infrastructure which is often difficult, if not impossible. For instance, the active badge location system [7] employed infrared beacons to find user location, but the limited range of infrared restricts localization in wide area. The Cricket system [8] and Active Bat system [9] were based on the use of costly ultrasonic devices for indoor localization in a limited space. Ubitag [10], [11] achieved reasonable localization accuracy by integrating time difference of arrival (TDoA) and angle of arrival (AoA) methods in UWB network, but the system requires high-cost UWB tag. Furthermore, signal interference problem must be solved to coexist with existing narrow band systems. Employing Wi-Fi signals has been widely adopted as estimating indoor location without expensive infrastructure cost [12]. However, Wi-Fi positioning system (WPS) requires signal training or indoor map. The training process should be performed by experts, which is time consuming and requires periodic management. An indoor map or floor plan is essential to create the database, but it does not typically exist or is not available to users for security reasons. There are also still many places having no or few Wi-Fi access points (APs), which makes localization difficult and becomes critical problem for WPS. Thus, a practical indoor pedestrian tracking method should consider indoor environments where pretrained database or floor plan is not available. This is the key reason to develop a system to locate indoor user effectively.

In this paper, we present SmartPDR, a smartphone-based pedestrian dead reckoning that tracks indoor user's location. SmartPDR employs typical dead reckoning approach, which is widely developed in localization industry to solve locating problems for anonymous places specifically indoor environments. SmartPDR is based on the use of accelerometer, magnetometer, and gyroscope in a smartphone, which are able to observe the pedestrian movement. SmartPDR provides an indoor localization model that computes the displacement through step event detection, heading direction estimation, and step length estimation. The main difficulty of this work

is coping with situations that the map database is unknown in advance, and available sensors are inaccurate. SmartPDR overcomes these issues of limited resources and inaccurate sensing capabilities and presents a lightweight localization model.

In comparison with previous scheme that used laptops, PDAs, or cell phones, our system is implemented on the latest smartphones that are equipped with inertial sensors. Our technique is feasible since the number of smartphones in use is increasing, and the devices are commonly equipped with various sensors. The proposed system can easily be used at any site because the system does not require any anchor or physical map information. Many indoor localization systems assume the availability of site map with which the location accuracy is improved by making use of a priori knowledge on paths and walls in the building. Obtaining a map for an anonymous building is, however, not always possible. We believe any realistic and generalized indoor localization system should be freed from this fundamental restriction.

The rest of the paper is organized as follow: In section II, we discuss previous works and related approaches on pedestrian dead reckoning which is considered as a candidate for indoor localization. Section III presents system architecture and core algorithms of SmartPDR for improving accuracy of pedestrian tracking. Novel methods are proposed while some existing methods are adopted. In section IV, the implementation of the proposed system is detailed, and the results of experiments are demonstrated to evaluate the performance of the proposed scheme. Finally, Section V concludes the paper to the latest research achievement and discusses future work to be conducted in the near future.

II. PEDESTRIAN DEAD RECKONING

Recent development of microelectromechanical systems (MEMS) allows of integrating multiple sensors, including accelerometer, magnetometer, and gyroscope in a compact inertial sensor module. The technology is becoming cheaper and thus affordable for more applications. All the information needed for the detection of human movement is in the signals generated by accelerometer, magnetometer and gyroscope. This fact is employed in extensive research on pedestrian dead reckoning (PDR) and its applications [13]-[16]. Most PDR systems detect the number of step events using pedometer or accelerometer and move the location forward by the step length in the direction that is determined by magnetometer or gyroscope [17]–[19]. The average step length is adjusted for the walking speed and then used to calculate the user's location. More sophisticated systems analyze accelerometer signals to estimate step lengths. PDR can be treated as an application of inertial navigation technology. Limited by the size and weight, the gimbaled inertial navigation system is not suitable for applications like pedestrian tracking. Instead, the strapdown inertial navigation system (INS) using inertial measurement unit (IMU) becomes a proper candidate for the applications that require mobility.

A. IMU-Based Localization

Many IMU-based localization systems have been developed, especially in robotics area, to track the locations of mobile robots. Applying these techniques to human tracking poses a new challenge because human behavior, compared to robots, is dynamic. Moreover, a subtle motion of human movement should be carefully considered to obtain reasonable tracking accuracy. Godha and Lachapelle [20] proposed a pedestrian navigation system that achieves reasonable accuracy in both indoor and outdoor environments by integrating GPS and IMU. Klingbeil and Wark [21] proposed a Monte-Carlo-based localization system that uses accelerometer for step event detection and magnetometer to track heading direction, however, the system exploits physical map information with anchors at known locations.

IMU-based pedestrian tracking can be divided into acceleration integration approach and step counting approach. The acceleration integration method first subtracts the gravity component, and the location is then estimated by integrating remaining acceleration. This scheme is, however, difficult to implement on smartphones because the performance of accelerometers in smartphones is limited. The step counting method detects step events directly with acceleration. Steps are recognized by reading the inertial force, and a periodically observed series of signal patterns on inertial force trigger step events. This approach is appropriate for smartphone usage since it does not require high accuracy or precision of accelerometers.

B. Smartphone-Based Pedestrian Dead Reckoning

Sensors in smartphones have been used to understand the status of users, such as activity and location. Many contextaware applications have been developed in diverse fields, such as healthcare, dietary monitoring, social networking, and education. These applications monitor individuals' contexts to understand users' activity, such as running, walking, or sitting [22], [23]. Strapdown usage of accelerometer has been studied to track users, and foot-mounted inertial sensors have been used to detect step event [24], [25]. CompAcc [24] introduced a practical system that tracks pedestrian course without relying on Wi-Fi infrastructure. CompAcc records pedestrian walking pattern using accelerometer and magnetometer in a smartphone and matches it to a possible path from a map. Although CompAcc provides human-scale localization, the system is designed for outdoor environments, and it employs map information.

The Wi-Fi-based positioning technique allows new opportunities for location-aware services, and research on fingerprinting methods has proved their accuracy and robustness using correlations between locations and radio-signal patterns [26]. The approach constructs a database that associates ambient radio signals (fingerprints) with physical locations in offline training phase and searches the current location through finding the received fingerprint in the database most similar to that which a device currently observes in positioning phase. This method provides indoor localization within a few meters of accuracy with wide coverage. However, the training process

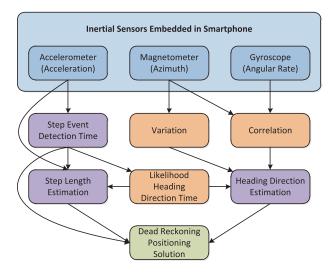


Fig. 1. Overall system architecture of SmartPDR.

should be performed by experts, which is time consuming and requires periodic management. Furthermore, a map or floor plan is necessary to create the database where an indoor map typically does not exist or is not available to users for security reasons. There are also still many places having no or few Wi-Fi APs, which makes localization difficult.

While the abovementioned approaches are feasible in terms of localization accuracy, the critical problem is that they are not practical due to the requirement of additional infrastructure such as foot-mounted inertial sensors, wireless APs, pretrained database, map information, etc. Since the realization of selfcontained, stand-alone localization is the main goal of our research, we specifically propose a practical indoor pedestrian tracking system for smartphones. It will be discussed how to solve the problem of tracking complicated human walking in the following section.

III. SmartPDR: SMARTPHONE-BASED PEDESTRIAN DEAD RECKONING FOR INDOOR LOCALIZATION

SmartPDR is a solution to pedestrian dead reckoning problem. Specifically designed for smartphones, it tracks the user's movement with inertial sensors embedded in smartphones. We first describe the system architecture of SmartPDR and then describe the details of each core algorithm.

A. System Architecture

SmartPDR is a middleware for mobile application that tracks pedestrian movement. We previously conducted studies about detecting step event as well as estimating heading direction in [27]. In this work, we extend the previous idea and enhance the system performance through improvement of each algorithm. Fig. 1 illustrates the overall structure of the proposed system. To estimate the movement of the user, SmartPDR reads step event and calculates step length with three-axis accelerometer, and determines heading direction with both three-axis magnetometer and three-axis gyroscope. This approach is practical since recent smartphones are usually equipped with accelerometer, magnetometer, and gyroscope. The system estimates the next possible location by adding step

length to previous location in the direction of heading at the stepping point of time. The core process of SmartPDR repeats four steps: step event detection, heading direction estimation, step length estimation, and location estimation. In the following, the procedures of these processes are explained in detail.

B. Transformation of Coordinate Systems

In order to describe the components of a vector of arbitrary orientation in the global coordinate system (GCS) with respect to the local coordinate system (LCS), a coordinate transformation must be performed. The transformation from LCS to GCS is accomplished by sequential rotations about three axes where these angular rotations can be represented as Euler angles. A convenient way of describing these rotations is using a rotation matrix. The rotation matrices along each of the three axes at time t are mentioned below:

$$R_{\phi,t} = \begin{bmatrix} \cos \phi_t, & 0, & \sin \phi_t \\ 0, & 1, & 0 \\ -\sin \phi_t, & 0, & \cos \phi_t \end{bmatrix}$$
(1a)

$$R_{\theta,t} = \begin{bmatrix} 1, & 0, & 0 \\ 0, & -\cos \theta_t, & \sin \theta_t \\ 0, & \sin \theta_t, & \cos \theta_t \end{bmatrix}$$
(1b)

$$R_{\psi,t} = \begin{bmatrix} \cos \psi_t, & \sin \psi_t, & 0 \\ -\sin \psi_t, & \cos \psi_t, & 0 \\ 0, & 0, & 1 \end{bmatrix}$$
(1c)

$$R_{\theta,t} = \begin{bmatrix} 1, & 0, & 0\\ 0, & -\cos\theta_t, & \sin\theta_t\\ 0, & \sin\theta_t, & \cos\theta_t \end{bmatrix}$$
(1b)

$$R_{\psi,t} = \begin{bmatrix} \cos \psi_t, & \sin \psi_t, & 0\\ -\sin \psi_t, & \cos \psi_t, & 0\\ 0, & 0, & 1 \end{bmatrix}$$
 (1c)

where the rotations are performed by ϕ_t rotation about y-axis denoted as $R_{\phi,t}$, θ_t rotation about x-axis as $R_{\theta,t}$, and ψ_t rotation about z-axis as $R_{\psi,t}$. These rotated angles that are a specific kind of Euler angles are called roll ϕ_t , pitch θ_t , and yaw ψ_t , respectively. The rows of rotation matrices are actually the projections of GCS on LCS, and the columns are those of LCS on GCS. One of the key properties of the rotation matrices is orthogonality. The orthogonality of the rotation matrices in mathematical term means that any pair of columns (or rows) of the matrices are perpendicular, and that the sum of the squares of the elements in each column (or row) is equal to one. The final rotation matrix R_t that transforms a vector from LCS to GCS is simply obtained by multiplying the above three rotation matrices sequentially, resulting

$$R_{t} = R_{\psi,t} R_{\theta,t} R_{\phi,t}$$

$$= \begin{bmatrix} c \psi c \phi - s \psi s \theta s \phi, & -s \psi c \theta, & c \psi s \phi + s \psi s \theta c \phi \\ -s \psi c \phi - c \psi s \theta s \phi, & -c \psi c \theta, & -s \psi s \phi + c \psi s \theta c \phi \\ -c \theta s \phi, & s \theta, & c \theta c \phi \end{bmatrix}$$
(2)

where c stands for cos and s does for sin functions. Note that ϕ , θ , and ψ are the short terms of ϕ_t , θ_t , and ψ_t , respectively.

C. Step Event Detection

Pedestrian distance traveled is represented by the number of step event, therefore it is necessary to detect step event accurately in order to get better estimation. To detect step event, we use accelerometer sensor that actually indicates three-axis acceleration relative to the smartphone itself. A user's steps are counted by reading the inertial force, and a periodically

observed series of signal patterns on inertial force trigger step events. Basically, the strongest indication of the step specific peak signature is featured on the vertical axis relative to ground. However, the vertical signal component may be distributed among all three accelerometer axes depending on the present orientation and attitude of a smartphone. Therefore, the acceleration in LCS is projected to GCS to obtain the acceleration values in vertical axis by multiplying the rotation matrix R_t as

$$a_t^{GCS} = R_t a_t^{LCS} \tag{3}$$

where a_t^{GCS} and a_t^{LCS} are the acceleration in GCS and LCS, respectively. This process is usually performed to resolve the arbitrary placement of smartphone. The acceleration is then filtered to remove the influence of the Earth's gravity. Because it is a low-frequency component causing an offset about 9.8 m/s², a simple high-pass filter (HPF) is applied to the acceleration on z-axis in GCS, which is implemented with the following equations [28]:

$$g_{z,t} = \alpha g_{z,t-1} + (1 - \alpha) a_{z,t}^{GCS}$$
 (4)
 $a_t^{HPF} = a_{z,t}^{GCS} - g_{z,t}$ (5)

$$a_t^{HPF} = a_{z,t}^{GCS} - g_{z,t} \tag{5}$$

where $g_{z,t}$ is the gravity component, and α is the parameter for HPF. Note that the common value used for α is in the range of $0.9 \le \alpha \le 1.0$. The resulting output a_t^{HPF} only contains highfrequency components with zero mean. To reduce random noise, low-pass filtering (LPF) is then processed by a moving average filter as

$$a_t^{step} = a_t^{LPF} = \frac{1}{W} \sum_{i = -\frac{W-1}{2}}^{\frac{W-1}{2}} a_{t+i}^{HPF}$$
 (6)

where average-filtered output a_t^{LPF} is used as step acceleration a_t^{step} in the next step counting procedure. W is moving window $(W = 2j - 1, j \in \mathbb{N})$, which is the number of points used in moving average. In this way, most of high-frequency noise is filtered out, but the signal retains its low-frequency attributes. A peak step counting algorithm is then applied to mark the candidate stepping points of time that have the possibility of user walking. We employ three conditions on step acceleration to detect a valid step event as following sets:

$$t^{peak} = \left\{ t \middle| a_{t}^{step} > a_{t+i}^{step}, \right.$$

$$a_{t}^{step} > a_{\tau}^{peak}, \quad |i| \leq \frac{N}{2}, \quad i \neq 0 \right\}$$

$$t^{pp} = \left\{ t \middle| \max\left(a_{t}^{step} - a_{t-i}^{step}\right) > a_{\tau}^{pp}, \right.$$

$$\max\left(a_{t}^{step} - a_{t+i}^{step}\right) > a_{\tau}^{pp}, \quad 1 \leq i \leq \frac{N}{2} \right\}$$

$$t^{slope} = \left\{ t \middle| \frac{2}{N} \sum_{i=t-\frac{N}{2}}^{t-1} \left(a_{i+1}^{step} - a_{i-1}^{step}\right) > 0, \right.$$

$$\left. \frac{2}{N} \sum_{i=t+1}^{t+\frac{N}{2}} \left(a_{i}^{step} - a_{i-1}^{step}\right) < 0 \right\}$$

$$(7c)$$

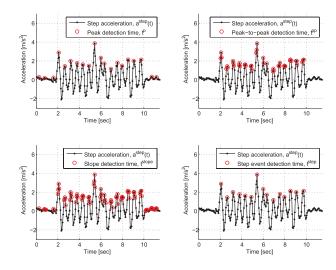


Fig. 2. Peak step event detection in step acceleration through the intersection of three time point sets at the example of 15 steps.

where N is the total number of samples for the comparison $(N=2j,\ j\in\mathbb{N})$. t^{peak} is the peak point of time exceeding the threshold a_{τ}^{peak} . t^{pp} is the set of time point that the largest difference between the current peak and both of previous and next valley (peak-to-peak) is greater than the threshold a_{τ}^{pp} . t^{slope} is the point of time that shows increment (positive slope) on the frontside and decrement (negative slope) on the backside. In this paper, we set the thresholds a_{τ}^{peak} to be 0.5 m/s^2 and $a_{\tau}^{pp^2}$ to be 1.0 m/s². The resulting step event time t^{step} is obtained from the intersection of above three sets of time points as

$$t^{step} = t^{peak} \cap t^{pp} \cap t^{slope} \tag{8}$$

where the k^{th} step event time t_k^{step} is the k^{th} smallest element in the set t^{step} . Fig. 2 shows the step event time t^{step} and three sets of time point, t^{peak} , t^{pp} , and t^{slope} , which are marked with red circles at the example of 15 steps. Through the proposed approach, we eliminated insignificant peaks and generated rightful step event time free from random noise as confirmed in the figure.

D. Heading Direction Estimation

Now, we discuss issues with regard to how to obtain walking direction information. Once a step is detected, it is important to know which direction the step was taken because the major source of location error is the distortion of heading direction. Unlike foot-mounted IMU, the placement of smartphone is unstable and this results in practical difficulty in finding the heading direction of user movement. The tilt of axes are always changing, and smartphone cannot stay horizontal. Errors caused by tilt angles could be large if not compensated. To handle the tilts of smartphone when it is in an arbitrary position, LCS is transformed into GCS through the rotation matrix provided in equation (2).

Magnetometer can provide the heading direction of pedestrian h_t^{mag} using the x-axis and y-axis components of the Earth's magnetic field outputs in GCS as following equations:

$$m_t^{GCS} = R_t m_t^{LCS} (9)$$

$$h_t^{mag} = \operatorname{atan2}\left(-m_{y,t}^{GCS}, m_{x,t}^{GCS}\right) \tag{10}$$

where $m_{x,t}^{GCS}$ and $m_{y,t}^{GCS}$ are the magnetic measurements on x-axis and y-axis in GCS. The function atan2 (y, x) is defined in mathematical term as

atan2
$$(y, x) = 2\tan^{-1}\left(\frac{y}{\sqrt{x^2 + y^2} + x}\right)$$
. (11)

The angle calculated in equation (10) is actually a compass reading, i.e., the azimuth relative to magnetic north. To get the value of true north, the magnetic declination must be deduced from the compass reading as

$$h_t^{mag} = \operatorname{atan2}\left(-m_{y,t}^{GCS}, m_{x,t}^{GCS}\right) - h_{\Delta}^{decline}$$
 (12)

where $h_{\Lambda}^{decline}$ is the difference between magnetic north and true north. This difference is caused by the tilt of the Earth's magnetic field generator relative to the Earth's spin axis.

The gyroscope gives angular velocity outputs of pitch θ , roll ϕ , and yaw ψ which are the rotations on x-axis, y-axis, and z-axis, respectively. There exists a drift offset error of gyroscope in each of the axes. The accuracy of heading direction will decay with time if this error is not removed. Therefore, the drift caused by gyroscope bias should be compensated as

$$\hat{\omega}_{i,t} = \omega_{i,t}^{LCS} - b_i^{gyro}, \quad i \in \{x, y, z\}$$
 (13)

where $\hat{\omega}_{i,t}$ is corrected angular velocity, $\omega_{i,t}^{LCS}$ is the raw value obtained from gyroscope, and b_i^{gyro} is the angular drift correction on i-axis. The angular velocities acquired from equation (13) are the representations of LCS, which should be transformed to GCS. To obtain angular velocity on z-axis in GCS $\omega_{z,t}^{GCS}$, the transformation from LCS to GCS is performed through the scalar projection of angular velocity vector $\hat{\omega}_t$ onto gravity vector g_t as

$$\omega_{z,t}^{GCS} = \frac{\hat{\omega}_t \cdot g_t}{|g_t|} = \frac{\hat{\omega}_t^T g_t}{|g_t|} \tag{14}$$

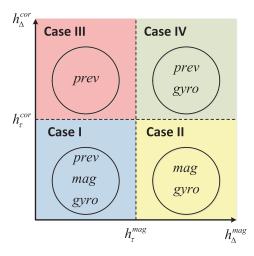
where the gravity vector g_t can be obtained by

$$g_t = R_t^{-1} \begin{bmatrix} 0 \\ 0 \\ g_{z,t} \end{bmatrix} = R_t^T \begin{bmatrix} 0 \\ 0 \\ g_{z,t} \end{bmatrix}, \tag{15}$$

and $\hat{\omega}_t = \begin{bmatrix} \hat{\omega}_{x,t} & \hat{\omega}_{y,t} & \hat{\omega}_{z,t} \end{bmatrix}^T$. The pedestrian heading direction from gyroscope can be determined through the integration. Since the sampling intervals for the sensors in smartphone are discrete, we treat this integration as its equivalent summation. The corresponding heading direction of pedestrian movement by gyroscope h_t^{gyro} is obtained as

$$h_t^{gyro} = \sum_t -\omega_{z,t}^{GCS} \tag{16}$$

where the negative sign of $\omega_{z,t}^{GCS}$ arises because the positive measurement of gyroscope indicates negative angular change by axial definition.



The heading direction estimation algorithm that selects heading direction sources based on the correlation and the variation of the sources.

The heading directions determined from magnetometer and gyroscope are noisy due to sensing capability, user movement, magnetic disturbance, etc. Deciding appropriate heading direction from these noisy values is crucial to enhance the localization accuracy. Therefore, we establish a new algorithm that uses measurements from magnetometer and gyroscope together to find the reasonable heading direction h_t of a user. The key concept of algorithm is to select reliable heading direction sources among previous estimate, magnetometer, and gyroscope based on the variation of magnetometer as well as the correlation between magnetometer and gyroscope. The proposed algorithm is visualized in Fig. 3 and expressed in the following equation:

$$h_{t} = \begin{cases} w^{pmg} \left(w^{prev} h_{t-1} + w^{mag} h_{t}^{mag} + w^{gyro} h_{t}^{gyro} \right), \\ \text{for } h_{\Delta}^{cor} \leq h_{\tau}^{cor}, h_{\Delta}^{mag} \leq h_{\tau}^{mag} \end{cases}$$
(17a)
$$w^{mg} \left(w^{mag} h_{t}^{mag} + w^{gyro} h_{t}^{gyro} \right), \\ \text{for } h_{\Delta}^{cor} \leq h_{\tau}^{cor}, h_{\Delta}^{mag} > h_{\tau}^{mag} \end{cases}$$
(17b)
$$h_{t-1}, \text{ for } h_{\Delta}^{cor} > h_{\tau}^{cor}, h_{\Delta}^{mag} \leq h_{\tau}^{mag} \end{cases}$$
(17c)
$$w^{pg} \left(w^{prev} h_{t-1} + w^{gyro} h_{t}^{gyro} \right), \\ \text{for } h_{\Delta}^{cor} > h_{\tau}^{cor}, h_{\Delta}^{mag} > h_{\tau}^{mag} \end{cases}$$
(17d)

where

$$w^{pmg} = (w^{prev} + w^{mag} + w^{gyro})^{-1}$$
 (18a)

$$w^{mg} = (w^{mag} + w^{gyro})^{-1} (18b)$$

$$w^{pg} = \left(w^{prev} + w^{gyro}\right)^{-1} \tag{18c}$$

$$h_{\Delta}^{cor} = \left| h_t^{mag} - h_t^{gyro} \right|$$

$$h_{\Delta}^{mag} = \left| h_t^{mag} - h_{t-1}^{mag} \right|$$
(19a)
$$(19b)$$

$$h_{\Delta}^{mag} = \left| h_t^{mag} - h_{t-1}^{mag} \right| \tag{19b}$$

Note that w^{prev} , w^{mag} , and w^{gyro} are weighting parameters on previous heading direction estimate, current magnetometerbased direction, and current gyroscope-based output, respectively. In this paper, the ratio of weighting parameters are set to $w^{prev}: w^{mag}: w^{gyro} = 2:1:2$. The threshold h_{τ}^{cor} and h_{τ}^{mag} are used to determine the correlation h_{Δ}^{cor} and magnetometer variation h_{Λ}^{mag} , respectively. The values used in this paper are

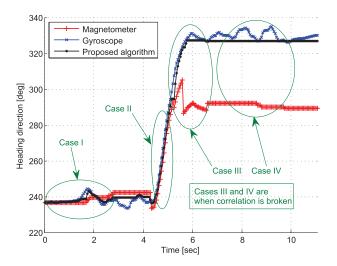


Fig. 4. The result of turning at a 90-degree corner having magnetic disturbances which shows each corresponding condition of heading direction source selection.

 $h_{\tau}^{cor}=5$ degrees and $h_{\tau}^{mag}=2$ degrees. As inferred from the equation and the figure, the proposed algorithm employs magnetometer and gyroscope together when they have similar outputs (Case I is for going straight, and Case II is for turning). In contrast, when they show different values, the algorithm uses previous estimate only (Case IV is for going straight because magnetometer is stable), or with gyroscope (Case III is for turning because magnetometer changes). The effectiveness of the proposed algorithm is confirmed at the example of turning at a 90-degree corner suffering magnetic disturbances where the result is depicted in Fig. 4. In the figure, the proposed novel algorithm successfully estimates heading direction with four categorized conditions resolving the drawbacks of magnetometer and gyroscope.

We then focus on the fact that the heading direction is usually determined between two consecutive steps. Upon each detected step event and estimated heading direction, we try to find which point of time represents the direction of current user movement. In other words, we selects the most likelihood time for each heading direction where the likelihood heading direction time for the k^{th} step event t_k^{head} is

$$t_k^{head} = \underset{t_{k-1}^{step} < t < t_k^{step}}{\arg \min} a_t^{step}$$
 (20)

where it is equivalent to the point of time that has valley acceleration as described in Fig. 5. The corresponding heading direction at the k^{th} step event h_k is

$$h_k = h_t|_{t=t_k^{head}}. (21)$$

E. Step Length Estimation

Total traveled distance can be calculated by estimating step length in every valid step event. Generally, there are two approaches for estimating step length: static model and dynamic model. Static model assumes that any valid step has the same length. The k^{th} step length l_k in static model can be determined through the following equation:

$$l_k = l, \quad \forall k$$
 (22)

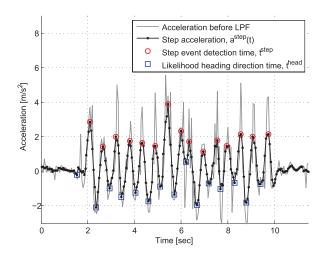


Fig. 5. The likelihood heading direction time from step event detection time which is equivalent to the valley point of time on step acceleration at the example of 15 steps.

where the constant l depends on the users using the system. In contrary, dynamic model assumes any valid step has different length because step length varies from step to step even for the same person. As mentioned before, the performance of accelerometer in smartphones is not enough to calculate the displacement through the integration of acceleration. To overcome this problem, the step length should be estimated using certain approach, such as one proposed in [29]. It assumes that vertical impact occurred from walking activity is proportional to step length. The vertical impact, which is the difference between the current peak and the previous valley of step acceleration in a step event interval $a_{pp,t}^{step}$, is obtained as

$$a_{pp,t}^{step} = a_{peak,t}^{step} - a_{valley,t}^{step}$$
 (23)

where

$$a_{peak,t}^{step} = a_t^{step} \Big|_{t=t_b^{step}}$$
 (24)

and

$$a_{valley,t}^{step} = a_t^{step} \Big|_{t=t_t^{head}}.$$
 (25)

The k^{th} step length l_k is then calculated through the vertical impact as following equation:

$$l_k = \beta \sqrt[4]{a_{pp,t}^{step}} + \gamma \tag{26}$$

where β is a scale factor, and γ is an offset. By the way, we consider employing logarithm instead of principal fourth root as

$$l_k = \beta \log \left(a_{pp}^{step} \right) + \gamma. \tag{27}$$

We conducted a simulation to compare two step length estimation algorithms, and the estimated step length of each algorithm is displayed in Fig. 6 with respect to reference step length from 0.4 meter to 1.0 meter and corresponding peak-to-peak step acceleration.

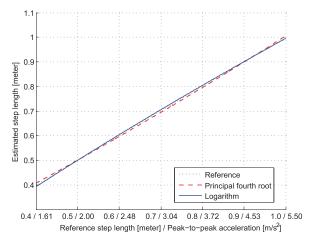


Fig. 6. Step length comparison estimated based on principal fourth root and logarithm with respect to the reference step length and peak-to-peak acceleration.

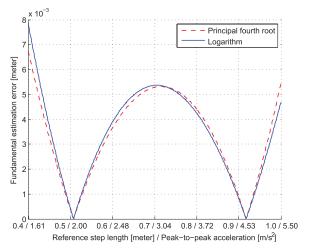


Fig. 7. Fundamental step length estimation error from the slopes of principal fourth root and logarithm functions.

The results of these two algorithms are almost same, but the difference is found in Fig. 7, which depicts fundamental estimation error of each algorithm. The error comes from the slopes of the two functions that are slightly different. It is observed from the figure that logarithm-based step length estimation is a little more accurate than principal fourth root-based one as reference step length becomes larger. For this reason, we combine two equations as

$$l_{k} = \begin{cases} \beta \sqrt[4]{a_{pp,t}^{step}} + \gamma, & \text{for } a_{pp}^{step} < a_{\tau}^{step} \\ \beta \log \left(a_{pp}^{step} \right) + \gamma, & \text{for } a_{pp}^{step} \ge a_{\tau}^{step} \end{cases}$$
(28)

which is proposed for step length estimation in this paper. The threshold a_{τ}^{step} is used to select estimation algorithm, which is $3.230 \, \text{m/s}^2$ in the paper. In the above equations, the parameters β and γ for each function are $\beta=1.479$ and $\gamma=-1.259$ for principal fourth root, and $\beta=1.131$ and $\gamma=0.159$ for logarithm.

F. Location Estimation

The pedestrian movement is represented as indoor location on a two-dimensional plane. The movement consists of

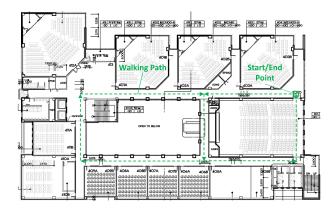


Fig. 8. Indoor layout of testbed building with walking path.

walking distance and heading direction. Thus, the current user position at the $k^{\rm th}$ step s_k^{user} is computed by adding the estimated current step length l_k to the previous location s_{k-1}^{user} in the estimated heading direction h_k at the $k^{\rm th}$ step event time t_k^{step} according to

$$s_k^{user} = \begin{bmatrix} x_k^{GCS} \\ y_k^{GCS} \end{bmatrix} = \underbrace{\begin{bmatrix} x_{k-1}^{GCS} \\ y_{k-1}^{GCS} \end{bmatrix}}_{s_k^{user}} + l_k \begin{bmatrix} \sin(h_k) \\ \cos(h_k) \end{bmatrix}$$
(29)

where x_k^{GCS} and y_k^{GCS} represent the displacement on x-axis (East) and that on y-axis (North) in GCS at the k^{th} step, respectively. The localization error in this paper is defined as the Euclidean norm of the difference between user location and reference location in two dimension defined as

$$d_k^{error} = \left\| s_k^{ref} - s_k^{user} \right\| \tag{30}$$

where s_k^{ref} is the reference location point at the k^{th} step. As a result, we simplified the localization problem to be deterministic such that pedestrian movement is modeled as step event detection, heading direction estimation, and step length estimation.

IV. EXPERIMENTS AND EVALUATION

We first describe the platform design and experimental environments. The performance of the proposed system is then compared with the ground-truth reference path as well as conventional pedestrian dead reckoning approaches.

A. Experimental Setup

To evaluate the proposed scheme in real environments, we implemented the proposed system on Google Android platform. Our system was tested on Samsung Galaxy Note and Note II smartphones equipped with accelerometer, magnetometer, and gyroscope where the sampling rate of each inertial sensor was 20 Hz. The experiments were conducted in Creative Learning Hall (CLH) at Korea Advanced Institute of Science and Technology (KAIST), the indoor layout of which is shown in Fig. 8. To evaluate the quality of path estimation, we tracked a walking path with a step counter. We explored the corridors of our testbed building

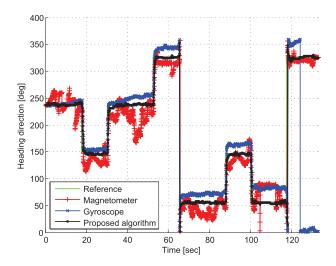


Fig. 9. Heading direction estimation with respect to the ground-truth reference heading direction.

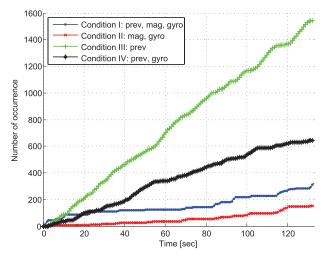


Fig. 10. The cumulative occurred number of heading direction estimation conditions.

(i.e., the two closed rectangles in Fig. 8) multiple times. The testbed consisted of eight-shaped path in an office environment with total length of 168.55 m. It took about two minutes to walk along under normal walking speed with around 215 steps. The experiment was run for 50 times with 5 participants, and the average results are presented. The actual distance covered and time taken for walking varies across different trials.

In the experiments, a smartphone is held on hand, in front along the corridor. This hand-held position of smartphone is reasonable because the user who wants to know current location should regularly check the information on the screen of smartphone. In this position, the direction of smartphone is almost same as that of the user even though there is some trembling. We also performed simulations to understand the signal characteristics of inertial sensors generated in different walking styles of users and to quantify the performance of the proposed system with various parameters. We logged steps and the observation with smartphones and simulated the log. The simulation was conducted on Matlab computer program with exactly the same operating systems that run on smartphones. We also run the realtime application on each smartphone. The main goal of the experiment was to verify the accuracy of indoor localization by applying the proposed algorithm.

B. Experimental Results

The proposed system estimates a pedestrian path from measured sensor data. We identified an acceleration signature by human walking steps and measured the magnetic azimuth as well as angular rate for heading direction. We configured the parameters of the system based on our previous work [27].

Fig. 9 shows the estimated heading direction of pedestrian from magnetometer, gyroscope, and the proposed algorithm. The changes of direction with 90 degree explain the turnings at corners. It is inferred from the wavy direction of magnetometer in the figure that magnetic distortion is found at many points. The magnetic field is influenced, for example, by working machines and a metal gate in

the vicinity. Unstable placement of the device also affects the measurement of the magnetic force such that a smartphone held in a hand is easily shaken during walking. The direction of gyroscope is almost same with the reference direction; however the accumulated bias error arises after few turns. The proposed heading estimation algorithm utilizes the correlation between magnetometer and gyroscope as well as the variation of magnetometer. The obtained heading direction is almost same with the ground-truth reference heading direction. It means that the reliable heading direction is obtained with the proposed algorithm resolving the drawback of each sensor.

Fig. 10 describes how the heading direction of the proposed algorithm is calculated with the cumulative occurred number of each condition of heading direction estimation. In the figure, the case III and case IV mostly happened with 58.01% and 24.23% while the case I and case II rarely happened with 12.11% and 5.65%, respectively. Note that the sum probability of four cases equals to 100%. The result from the figure explains that heading direction outputs of magnetometer and gyroscope are mostly different, and this is confirmed by the condition of the case III and case IV with the total probability of 82.24%. Furthermore, the variation of magnetometer can be effectively utilized which is supported by the case I and case III with the sum probability of 70.12%. In the proposed algorithm, the previous estimate, magnetometer, and gyroscope are used for heading direction estimation as 94.35%, 17.76%, and 41.99%, respectively.

Fig. 11 displays the measurement error on heading direction estimation when the heading direction of likelihood heading time is employed. Because the user rarely turns 90-degree corner at once, the peaks arise on the figure at the time of turning. It is cleared from the figure that there is magnetic distortion at many points in this experiment environment, and the accumulated error of gyroscope caused bias offset after few turns. The heading direction error of the proposed algorithm is almost less than 5 degrees in the whole experimental period. Specifically, the average heading direction error of the

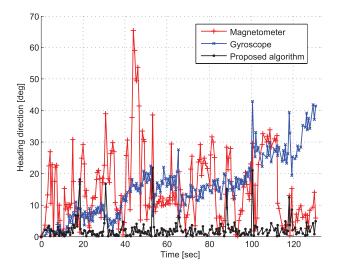


Fig. 11. Heading direction estimation error with respect to the ground-truth reference heading direction where the data of the likelihood heading direction time is applied.

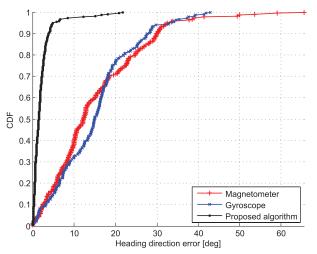


Fig. 12. Cumulative heading direction error distribution with respect to the ground-truth reference heading direction.

proposed algorithm is 2.28 degrees with the standard deviation of 3.63 degrees.

The result of measurement error on heading direction estimation is summarized as the cumulative distribution in Fig. 12. As expected, the proposed heading direction estimation algorithm shows the best performance utilizing the advantages of magnetometer and gyroscope. The result of heading direction estimation will be confirmed in localization process showing that errors in degrees could cause errors in meters.

Fig. 13 is the screenshots of the proposed localization system, SmartPDR on Galaxy Note which is an Android application containing proposed algorithms. The figure explains the installation of application on smartphone and the result of pedestrian tracking. The trajectory is displayed on Google Maps by converting displacement into latitude and longitude information. All the sensor values used for algorithm and the localization result outputs are logged, and the performance of the proposed algorithm is evaluated on Matlab computer program.

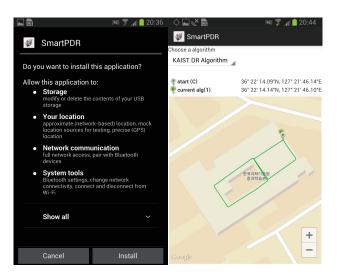


Fig. 13. The screenshots of SmartPDR on Galaxy Note from installation to localization where the proposed algorithms are built in.

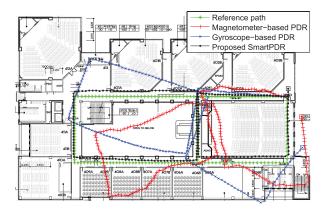


Fig. 14. Localization trajectories with respect to the ground-truth reference path that are constructed on Matlab computer program with logged data file from the smartphone.

Fig. 14 depicts the trajectories built with the logged data file from smartphone application. The trajectory of the proposed system is compared with magnetometer-based PDR and gyroscope-based PDR where the heading direction of likelihood heading direction time is employed. In the figures, we see the detected steps and their location corresponding to each heading direction estimation where starting and finishing points are remarked as circles and squares for each scheme.

It is proved from Figs. 13 and 14 that the proposed Smart-PDR successfully draws the corridors of the building that is almost same with ground-truth reference path. In contrast, the movement path of magnetometer-based PDR was twisted due to the magnetic distortion in this indoor environment, and that of gyroscope-based PDR became inaccurate with accumulated error of drift bias in gyroscope readings.

Fig. 15 shows the localization error with respect to the walking distance. In the figure, the locating error of SmartPDR was less than 2 meters in the whole experimental period. Specifically, the average location error of SmartPDR was 1.35 meters. The localization error generally increases as the walked distance increases due to the cumulative error on step

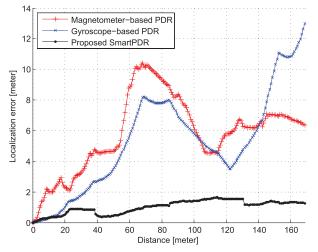


Fig. 15. Localization error with respect to the ground-truth reference path.

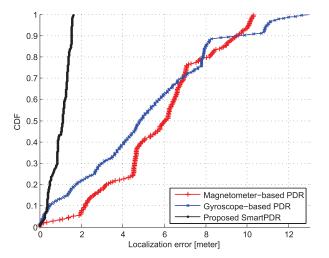


Fig. 16. Localization error CDF with respect to the ground-truth reference path.

event detection and heading direction estimation. However, the error in our experiment did not always increase and even decreased at some points of the path. This is because the walking path has many turning points and has the shape of closed loop in our experiment setup.

The result of localization error is summarized as the cumulative distribution in Fig. 16. The proposed SmartPDR gives the best performance with the largest locating error of 1.62 meters.

In our experiment analysis, we used only two types of smartphones, Samsung Galaxy Note and Note II. However, diverse types of smartphones would have different performance characteristics on inertial sensors that may influence the performance of the proposed system. Especially, different inertial chipsets can cause localization error due to the gap of sensor values. We plan to consider this kind of problem to apply our system in the future work.

V. CONCLUSION

SmartPDR is a smartphone-based pedestrian dead reckoning solution that tracks users in anonymous buildings. By exploring the inside of a building with a smartphone, SmartPDR estimates the current location of the user on Google Maps.

In the experiment, the system successfully draws the corridor outline of the building.

Our work makes two important contributions to the research on indoor localization. First, we extended the field of pedestrian tracking systems to indoor environments. SmartPDR introduces a method to track users with pervasive mobile devices. Second, we designed a complete system that runs on the smartphone device and verified its robustness. We implemented all the components of PDR in a real device and verified the robustness of the proposed scheme. It is important to note that SmartPDR is a PDR technology on a smartphone without any other infrastructure. These contributions validate that self-contained pedestrian tracking system based on smartphone inertial sensors, instead of wireless or other technologies, can indeed be achievable, which is the key for the success of such a system. Our system can be used to enable the deployment of various location-based applications such as indoor navigation system in a large shopping center. For the future work, we plan to improve the proposed system in several aspects.

The current experiment with SmartPDR represents a method to track a pedestrian in indoor environment with inaccurate sensors in a smartphone. Based on experiments done to date, the accuracy of the system is acceptable in measuring displacement of a pedestrian. Now, we will study a complete system including floor recognition. A further set of large-scale experiments in diverse indoor environments is planned to understand the practical usage of the system. Finally, we plan to implement a seamless localization system by detecting the precise entrance position of the building, which was assumed to be known in the current work. This is beyond the scope of this paper at this stage of development.

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