

Example 1- simple national income model

Structural form:

$$Y = C + I_o + G_o$$

$$C = \alpha + \beta(Y - T), \quad (\alpha > 0; 0 < \beta < 1)$$

$$T = \gamma + \delta Y, \quad (\gamma > 0; 0 < \delta < 1)$$

or

$$Y - C = I_o + G_o$$

$$-\beta Y + C + \beta T = \alpha$$

$$-\delta Y + T = \gamma$$

or

$$Ax = d$$

with

$$A = \begin{pmatrix} 1 & -1 & 0 \\ -\beta & 1 & \beta \\ -\delta & 0 & 1 \end{pmatrix}, x = \begin{pmatrix} Y \\ C \\ T \end{pmatrix}, \text{ and } d = \begin{pmatrix} I_o + G_o \\ \alpha \\ \gamma \end{pmatrix}$$

Reduced form:

Solution to the system as indicated above (to address the problem of simultaneous equation bias)

$$x = A^{-1}d$$

$$A = \begin{pmatrix} 1 & -1 & 0 \\ -\beta & 1 & \beta \\ -\delta & 0 & 1 \end{pmatrix}, \text{ determinant: } |A| = \beta\delta - \beta + 1$$

$$x = A^{-1}d = \begin{pmatrix} \frac{\alpha}{-\beta+\beta\delta+1} - \beta \frac{\gamma}{-\beta+\beta\delta+1} + \frac{G_o+I_o}{-\beta+\beta\delta+1} \\ \frac{\alpha}{-\beta+\beta\delta+1} - \beta \frac{\gamma}{-\beta+\beta\delta+1} + (G_o + I_o) \frac{\beta-\beta\delta}{-\beta+\beta\delta+1} \\ \alpha \frac{\delta}{-\beta+\beta\delta+1} + \delta \frac{G_o+I_o}{-\beta+\beta\delta+1} + \gamma \frac{-\beta+1}{-\beta+\beta\delta+1} \end{pmatrix} = \begin{pmatrix} Y \\ C \\ T \end{pmatrix}$$

$$\begin{pmatrix} Y \\ C \\ T \end{pmatrix} = \begin{pmatrix} \frac{\alpha-\beta\gamma+G_o+I_o}{1-\beta+\beta\delta} \\ \frac{\alpha-\beta\gamma+(G_o+I_o)(\beta-\beta\delta)}{1-\beta+\beta\delta} \\ \frac{\alpha\delta+\delta(G_o+I_o)+\gamma(1-\beta)}{1-\beta+\beta\delta} \end{pmatrix} = \begin{pmatrix} \frac{\alpha-\beta\gamma}{1-\beta+\beta\delta} + \frac{1}{1-\beta+\beta\delta} G_o + \frac{1}{1-\beta+\beta\delta} I_o \\ \frac{\alpha-\beta\gamma}{1-\beta+\beta\delta} + \frac{(\beta-\beta\delta)}{1-\beta+\beta\delta} G_o + \frac{(\beta-\beta\delta)}{1-\beta+\beta\delta} I_o \\ \frac{\alpha\delta+\gamma(1-\beta)}{1-\beta+\beta\delta} + \frac{\delta}{1-\beta+\beta\delta} G_o + \frac{\delta}{1-\beta+\beta\delta} I_o \end{pmatrix}$$

or

$$\begin{pmatrix} Y \\ C \\ T \end{pmatrix} = \begin{pmatrix} \pi_{11} + \pi_{21}G_0 + \pi_{31}I_0 \\ \pi_{12} + \pi_{22}G_0 + \pi_{32}I_0 \\ \pi_{13} + \pi_{23}G_0 + \pi_{33}I_0 \end{pmatrix}, \text{ with}$$

$$\begin{aligned} \pi_{11} &= \frac{\alpha - \beta\gamma}{1 - \beta + \beta\delta}, \pi_{21} = \frac{1}{1 - \beta + \beta\delta}, \pi_{31} = \frac{1}{1 - \beta + \beta\delta} \\ \pi_{12} &= \frac{\alpha - \beta\gamma}{1 - \beta + \beta\delta}, \pi_{22} = \frac{(\beta - \beta\delta)}{1 - \beta + \beta\delta}, \pi_{32} = \frac{(\beta - \beta\delta)}{1 - \beta + \beta\delta} \\ \pi_{13} &= \frac{\alpha\delta + \gamma(1 - \beta)}{1 - \beta + \beta\delta}, \pi_{23} = \frac{\delta}{1 - \beta + \beta\delta}, \pi_{33} = \frac{\delta}{1 - \beta + \beta\delta} \end{aligned}$$

The objective is to estimate the structural form parameters via estimating the reduced form. We will have estimates for $\pi_{11}, \dots, \pi_{33}$ and need to use these to estimate the structural form parameters.

How?

For instance: $\delta = \frac{\pi_{33}}{\pi_{31}}$ or $\frac{\pi_{23}}{\pi_{21}}$, $\beta = ???$ is it possible?????

The answer to the above lies in the identification of the system and the individual equations

Comparative static analysis:

Comparative static results with respect to G_0 :

$$\begin{pmatrix} \frac{\partial Y}{\partial G_0} \\ \frac{\partial C}{\partial G_0} \\ \frac{\partial T}{\partial G_0} \end{pmatrix} = \begin{pmatrix} \frac{1}{1 - \beta + \beta\delta} \\ \frac{\beta - \beta\delta}{1 - \beta + \beta\delta} \\ \frac{\delta}{1 - \beta + \beta\delta} \end{pmatrix}$$

Comparative static results with respect to I_0 :

$$\begin{pmatrix} \frac{\partial Y}{\partial I_0} \\ \frac{\partial C}{\partial I_0} \\ \frac{\partial T}{\partial I_0} \end{pmatrix} = \begin{pmatrix} \frac{1}{1 - \beta + \beta\delta} \\ \frac{\beta - \beta\delta}{1 - \beta + \beta\delta} \\ \frac{\delta}{1 - \beta + \beta\delta} \end{pmatrix}$$

Example 2- identified system

Consider the following structural form:

$$y_1 = a + bx_1 + cy_2 + u_1$$

$$y_2 = d + ex_2 + fy_1 + u_2$$

with y_1 and y_2 endogenous, and x_1 and x_2 exogenous

or

$$\begin{aligned} y_1 - cy_2 &= a + bx_1 + u_1 \\ -fy_1 + y_2 &= d + ex_2 + u_2 \end{aligned}$$

or

$$A = \begin{pmatrix} 1 & -c \\ -f & 1 \end{pmatrix}, |A| = \begin{vmatrix} 1 & -c \\ -f & 1 \end{vmatrix} = 1 - cf$$

The reduced form only exists if $cf \neq 1$

$$g = \begin{pmatrix} y_1 \\ y_2 \end{pmatrix} \text{ and } r = \begin{pmatrix} a + bx_1 + u_1 \\ d + ex_2 + u_2 \end{pmatrix}$$

Thus $Ag = r$ and therefore $g = A^{-1}r$

(Note that $g = A^{-1}r$ is the reduced form)

$$A = \begin{pmatrix} 1 & -c \\ -f & 1 \end{pmatrix} A^{-1} = \begin{pmatrix} -\frac{1}{cf-1} & -\frac{c}{cf-1} \\ -\frac{f}{cf-1} & -\frac{1}{cf-1} \end{pmatrix}$$

$$g = A^{-1} \begin{pmatrix} a + bx_1 + u_1 \\ d + ex_2 + u_2 \end{pmatrix} = \begin{pmatrix} \frac{1}{1-cf}(a + u_1 + bx_1) + \frac{c}{1-cf}(d + u_2 + x_2e) \\ \frac{1}{1-cf}(d + u_2 + x_2e) + \frac{f}{1-cf}(a + u_1 + bx_1) \end{pmatrix}$$

$$\begin{aligned}
\begin{pmatrix} y_1 \\ y_2 \end{pmatrix} &= \begin{pmatrix} \frac{a+bx_1+u_1}{1-cf} + c \frac{d+ex_2+u_2}{1-cf} \\ \frac{d+ex_2+u_2}{1-cf} + f \frac{a+bx_1+u_1}{1-cf} \end{pmatrix} = \begin{pmatrix} \frac{a+u_1}{1-cf} + \frac{bx_1}{1-cf} + c \frac{d+u_2}{1-cf} + c \frac{ex_2}{1-cf} \\ \frac{d+u_2}{1-cf} + \frac{ex_2}{1-cf} + f \frac{a+u_1}{1-cf} + f \frac{bx_1}{1-cf} \end{pmatrix} \\
&= \begin{pmatrix} \frac{a+u_1}{1-cf} + c \frac{d+u_2}{1-cf} + \frac{bx_1}{1-cf} + c \frac{ex_2}{1-cf} \\ \frac{d+u_2}{1-cf} + f \frac{a+u_1}{1-cf} + f \frac{bx_1}{1-cf} + \frac{ex_2}{1-cf} \end{pmatrix} \\
&= \begin{pmatrix} \frac{a+u_1+c(d+u_2)}{1-cf} + \frac{bx_1}{1-cf} + c \frac{ex_2}{1-cf} \\ \frac{d+u_2+f(a+u_1)}{1-cf} + f \frac{bx_1}{1-cf} + \frac{ex_2}{1-cf} \end{pmatrix} = \begin{pmatrix} \frac{a+cd}{1-cf} + \frac{b}{1-cf}x_1 + \frac{ce}{1-cf}x_2 + \frac{u_1+cu_2}{1-cf} \\ \frac{d+fa}{1-cf} + \frac{fb}{1-cf}x_1 + \frac{e}{1-cf}x_2 + \frac{u_2+fu_1}{1-cf} \end{pmatrix} \\
&= \begin{pmatrix} \pi_{11} + \pi_{21}x_1 + \pi_{31}x_2 + u_1^* \\ \pi_{12} + \pi_{22}x_1 + \pi_{32}x_2 + u_2^* \end{pmatrix}
\end{aligned}$$

with

$$\pi_{11} = \frac{a+cd}{1-cf}, \pi_{21} = \frac{b}{1-cf}, \pi_{31} = \frac{ce}{1-cf}, \pi_{12} = \frac{d+fa}{1-cf}, \pi_{22} = \frac{fb}{1-cf}, \pi_{32} = \frac{e}{1-cf}$$

The comparative static results for a change in x_1 is given by

$$\begin{aligned}
\frac{\partial y_1}{\partial x_1} &= \pi_{21} = \frac{b}{1-cf} \\
\frac{\partial y_2}{\partial x_1} &= \pi_{22} = \frac{fb}{1-cf}
\end{aligned}$$

The comparative static results for a change in x_2 is given by

$$\begin{aligned}
\frac{\partial y_2}{\partial x_1} &= \pi_{31} = \frac{ce}{1-cf} \\
\frac{\partial y_2}{\partial x_2} &= \pi_{32} = \frac{e}{1-cf}
\end{aligned}$$

The structural form parameters are estimated by the following:

$$\begin{aligned}
f &= \frac{\pi_{22}}{\pi_{21}}, c = \frac{\pi_{31}}{\pi_{32}} \\
b &= \pi_{21}(1 - cf) = \pi_{21}\left(1 - \frac{\pi_{31}}{\pi_{32}} \frac{\pi_{22}}{\pi_{21}}\right), \\
e &= \pi_{32}(1 - cf) = \pi_{32}\left(1 - \frac{\pi_{31}}{\pi_{32}} \frac{\pi_{22}}{\pi_{21}}\right), \\
\pi_{11} &= \frac{a+cd}{1-cf} = \frac{a + \frac{\pi_{31}}{\pi_{32}}d}{1 - \frac{\pi_{31}}{\pi_{32}} \frac{\pi_{22}}{\pi_{21}}}, \text{ and} \\
\pi_{12} &= \frac{d+fa}{1-cf} = \frac{d + \frac{\pi_{22}}{\pi_{21}}a}{1 - \frac{\pi_{31}}{\pi_{32}} \frac{\pi_{22}}{\pi_{21}}}
\end{aligned}$$

define

$$z_1 = \pi_{11}\left(1 - \frac{\pi_{31}}{\pi_{32}} \frac{\pi_{22}}{\pi_{21}}\right), \text{ and } z_2 = \pi_{12}\left(1 - \frac{\pi_{31}}{\pi_{32}} \frac{\pi_{22}}{\pi_{21}}\right)$$

$$z_1 = a + cd, \text{ or } a = z_1 - cd$$

$$z_2 = d + fa = d + f(z_1 - cd) = d + fz_1 - fcd$$

$$d - fcd = z_2 - fz_1$$

$$d(1 - fc) = z_2 - fz_1$$

$$d = \frac{z_2 - fz_1}{1 - fc} = \frac{\pi_{12}(1 - \frac{\pi_{31}}{\pi_{32}} \frac{\pi_{22}}{\pi_{21}}) - \pi_{11} \frac{\pi_{22}}{\pi_{21}} (1 - \frac{\pi_{31}}{\pi_{32}} \frac{\pi_{22}}{\pi_{21}})}{1 - \frac{\pi_{22}}{\pi_{21}} \frac{\pi_{31}}{\pi_{32}}} = \pi_{12} - \pi_{11} \frac{\pi_{22}}{\pi_{21}}$$

$$\begin{aligned} a &= \pi_{11} \left(1 - \frac{\pi_{31}}{\pi_{32}} \frac{\pi_{22}}{\pi_{21}}\right) - \frac{\pi_{31}}{\pi_{32}} \frac{\pi_{12}(1 - \frac{\pi_{31}}{\pi_{32}} \frac{\pi_{22}}{\pi_{21}}) - \pi_{11} \frac{\pi_{22}}{\pi_{21}} (1 - \frac{\pi_{31}}{\pi_{32}} \frac{\pi_{22}}{\pi_{21}})}{1 - \frac{\pi_{31}}{\pi_{32}} \frac{\pi_{22}}{\pi_{21}}} \\ &= \pi_{11} \left(1 - \frac{\pi_{31}}{\pi_{32}} \frac{\pi_{22}}{\pi_{21}}\right) - \frac{\pi_{31}}{\pi_{32}} (\pi_{12} - \pi_{11} \frac{\pi_{22}}{\pi_{21}}) \\ &= \pi_{11} - \frac{\pi_{31}}{\pi_{32}} \pi_{12} \end{aligned}$$

How do we estimate the standard errors of the structural form parameters?

Example 3- SAS Example (Example 2 continued)

The REG Procedure
 Model: MODEL1
 Dependent Variable: y1

Analysis of Variance					
Source	DF	Sum of Squares	Mean Square	F Value	Pr > F
Model	2	39244291	19622145	137.30	<.0001
Error	97	13862788	142915		
Corrected Total	99	53107079			

Root MSE	378.04146	R-Square	0.7390
Dependent Mean	3977.51000	Adj R-Sq	0.7336
Coeff Var	9.50448		

Parameter Estimates					
Variable	DF	Parameter Estimate	Standard Error	t Value	Pr > t
Intercept	1	1008.85165	210.44972	4.79	<.0001
x1	1	20.63740	1.32274	15.60	<.0001
x2	1	9.76651	1.08785	8.98	<.0001

The REG Procedure
 Model: MODEL1
 Dependent Variable: y2

Analysis of Variance					
Source	DF	Sum of Squares	Mean Square	F Value	Pr > F
Model	2	273834386	136917193	293.59	<.0001
Error	97	45236258	466353		
Corrected Total	99	319070645			

Root MSE	682.90056	R-Square	0.8582
Dependent Mean	4459.52000	Adj R-Sq	0.8553
Coeff Var	15.31332		

Parameter Estimates					
Variable	DF	Parameter Estimate	Standard Error	t Value	Pr > t
Intercept	1	2668.42257	380.15998	7.02	<.0001
x1	1	50.72257	2.38941	21.23	<.0001
x2	1	-12.89939	1.96512	-6.56	<.0001

The REG Procedure
 Model: MODEL1
 Dependent Variable: y1

Analysis of Variance					
Source	DF	Sum of Squares	Mean Square	F Value	Pr > F
Model	2	39244291	19622145	137.30	<.0001
Error	97	13862788	142915		
Corrected Total	99	53107079			

Root MSE	378.04146	R-Square	0.7390
Dependent Mean	3977.51000	Adj R-Sq	0.7336
Coeff Var	9.50448		

Parameter Estimates					
Variable	Label	DF	Parameter Estimate	Standard Error	t Value
Intercept	Intercept	1	3029.19452	109.52448	27.66
x1		1	59.04098	4.75556	12.42
y2h	Predicted Value of y2	1	-0.75713	0.08433	-8.98

Parameter Estimates				
Variable	Label	DF	Pr > t	
Intercept	Intercept	1	<.0001	
x1		1	<.0001	
y2h	Predicted Value of y2	1	<.0001	

The REG Procedure
 Model: MODEL2
 Dependent Variable: y2

Analysis of Variance					
Source	DF	Sum of Squares	Mean Square	F Value	Pr > F
Model	2	273834386	136917193	293.59	<.0001
Error	97	45236258	466353		
Corrected Total	99	319070645			

Root MSE	682.90056	R-Square	0.8582
Dependent Mean	4459.52000	Adj R-Sq	0.8553
Coeff Var	15.31332		

Parameter Estimates					
Variable	Label	DF	Parameter Estimate	Standard Error	t Value
Intercept	Intercept	1	188.86879	463.24042	0.41
x2		1	-36.90351	2.03272	-18.15
ylh	Predicted Value of y1	1	2.45780	0.11578	21.23

Parameter Estimates				
Variable	Label	DF	Pr > t	
Intercept	Intercept	1	0.6844	
x2		1	<.0001	
ylh	Predicted Value of y1	1	<.0001	

Therefore:

$$\pi_{11} = 1008.85165$$

$$\pi_{21} = 20.63740$$

$$\pi_{31} = 9.76651$$

$$\pi_{12} = 2668.42257$$

$$\pi_{22} = 50.72257$$

$$\pi_{32} = -12.89939$$

yielding estimates:

$$f = \frac{\pi_{22}}{\pi_{21}} = 2.4578$$

$$c = \frac{\pi_{31}}{\pi_{32}} = -0.75713$$

$$b = \pi_{21} \left(1 - \frac{\pi_{31}}{\pi_{32}} \frac{\pi_{22}}{\pi_{21}} \right) = 59.041$$

$$e = \pi_{32} \left(1 - \frac{\pi_{31}}{\pi_{32}} \frac{\pi_{22}}{\pi_{21}} \right) = -36.904$$

$$d = \pi_{12} - \pi_{11} \frac{\pi_{22}}{\pi_{21}} = 188.87$$

$$a = \pi_{11} - \frac{\pi_{31}}{\pi_{32}} \pi_{12} = 3029.2$$

The estimates of the structural model equations are:

$$\hat{y}_1 = a + bx_1 + cy_2 = +3029.2 + 59.041x_1 - 0.75713y_2$$

$$\hat{y}_2 = d + ex_2 + fy_1 = 188.87 - 36.904x_2 + 2.4578y_1$$

This method of estimation is known as Indirect Least Squares (ILS)