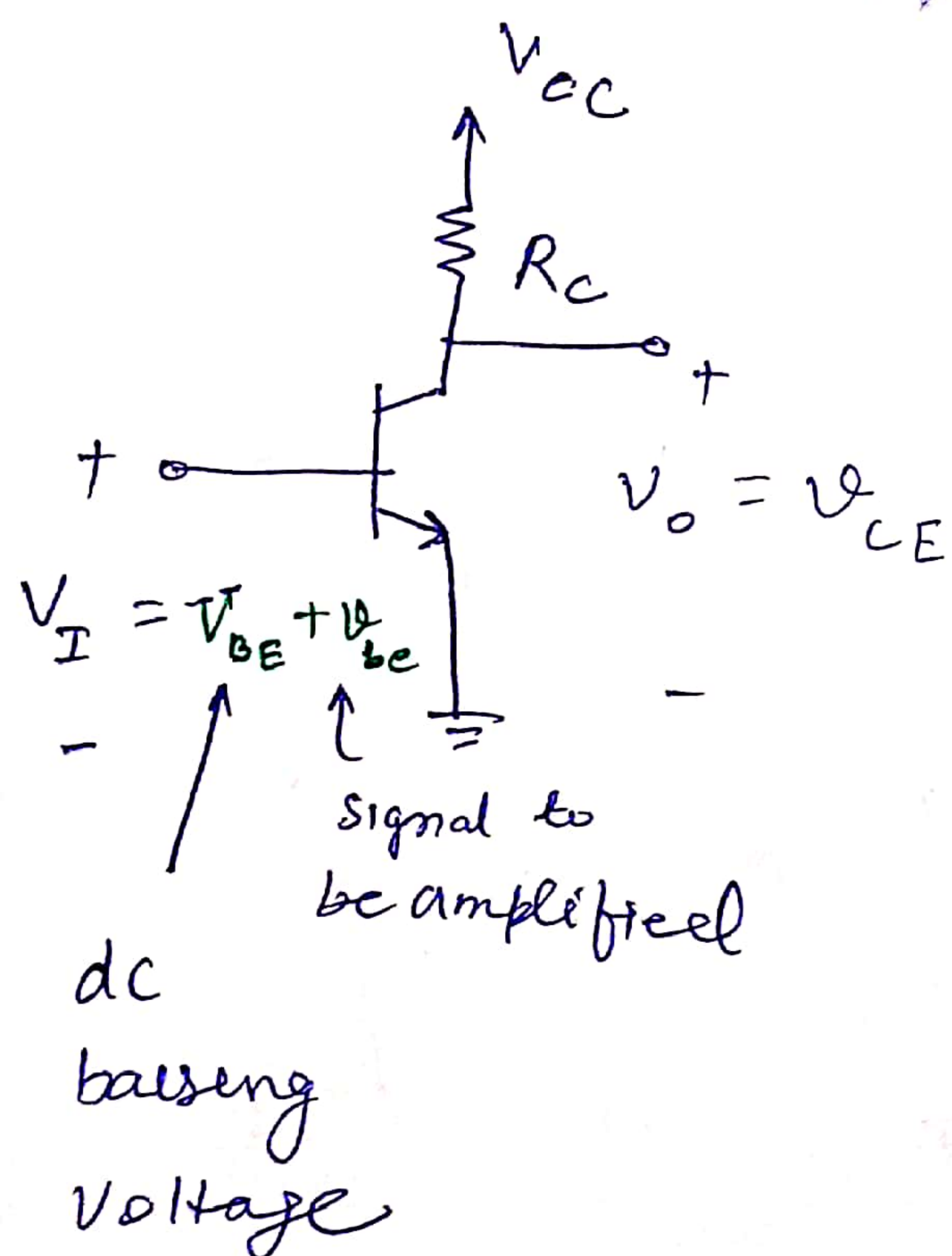
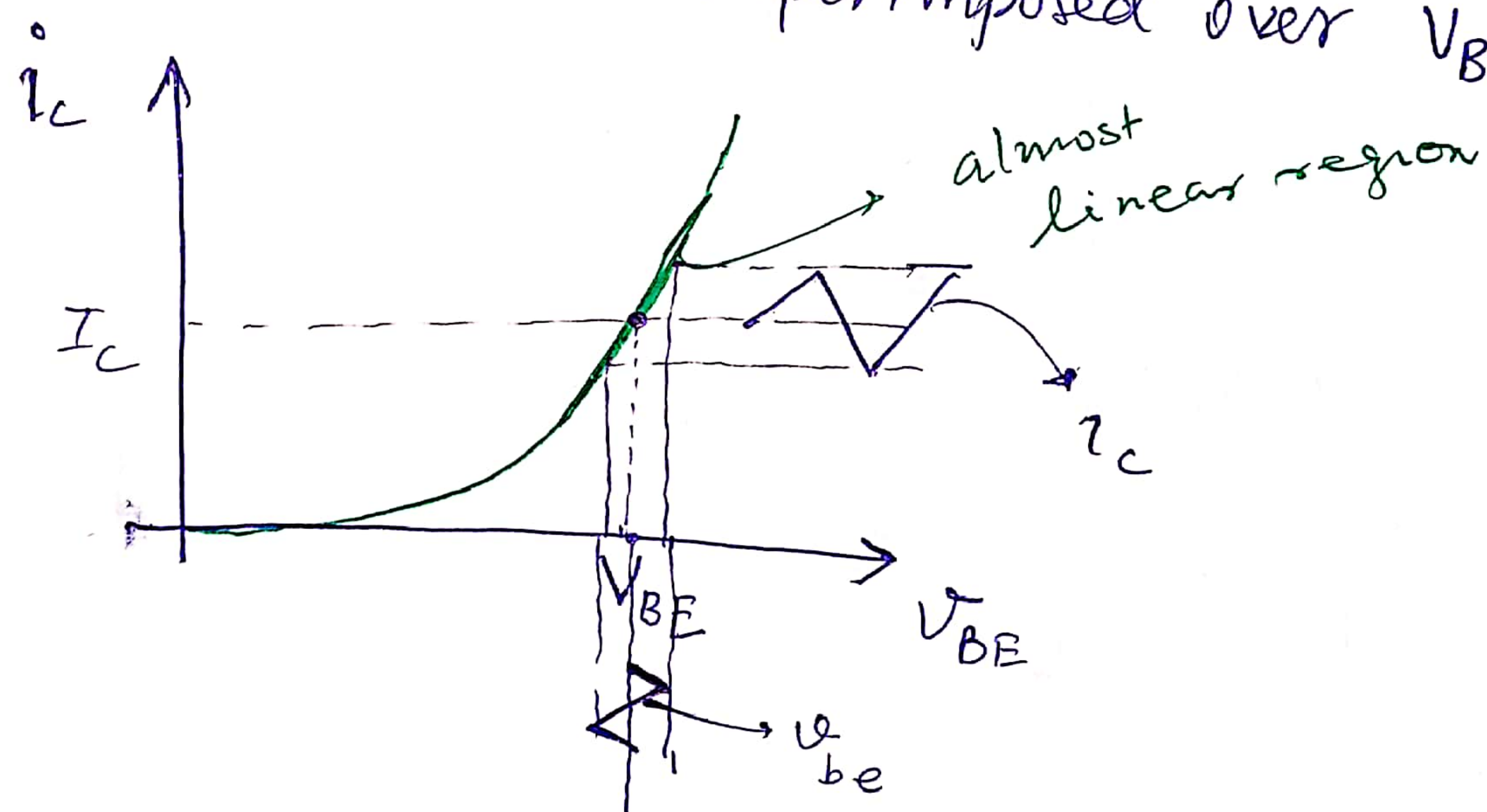


BJT as an Amplifier :-

We know that BJT in active mode acts as a voltage controlled current source. i.e. the change in V_{BE} gives rise to change in collector current, I_C . If we allow to pass the I_C through a resistor R_C then we will be able to obtain an output voltage $I_C R_C$ that can be used as voltage amplification.

However, since BJT is a highly non-linear device
 \therefore Since $I_C = I_S e^{V_{BE}/V_T} \Rightarrow I_C$ depends exponentially with V_{BE} , the transistor must be biased at a dc base-emitter voltage V_{BE} and then the signal, V_{be} to be amplified will be superimposed over V_{BE} .



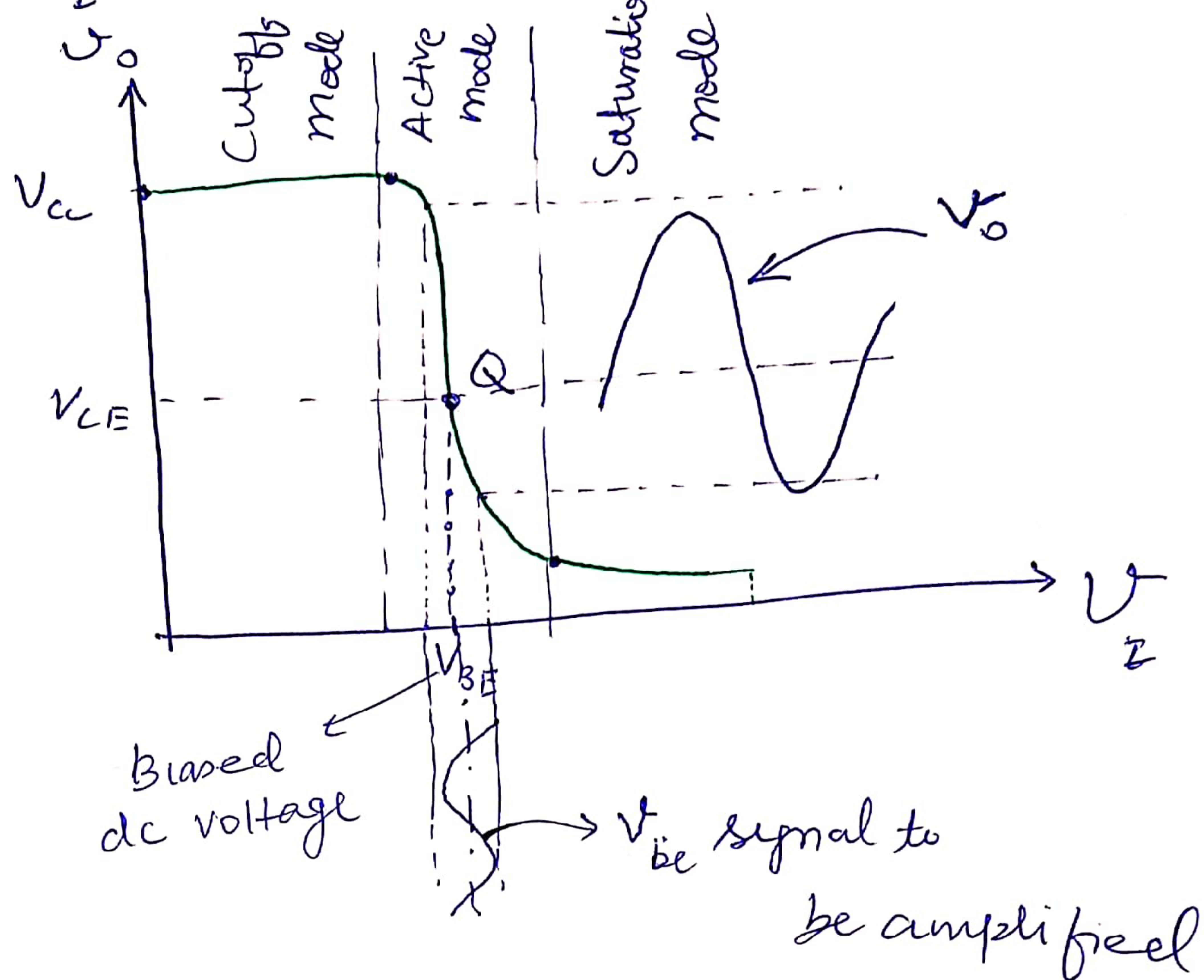
Basic structure of commonly used common-emitter BJT amplifier

The output V_O can be written as

$$V_O = V_{CE} = V_{CC} - R_C i_C$$

$$= V_{CC} - R_C I_S e^{V_I/V_T}$$

The V_o vs V_i is known as transfer characteristics



We can see here in the transfer characteristics, that by biasing ^{input} voltage at V_{BE} , the transistor operation can be ensured in active region, where we can have a desired linear amplification as shown in figure.

Amplifier Gain (V_o/V_i)

The Amplifier gain A_v , defined by $A_v = \frac{V_o}{V_i}$ can be is the slope of the transfer curve at bias point-Q.

$$\begin{aligned}
 A_v &\equiv \left. \frac{dV_o}{dV_i} \right|_{V_i = V_{BE}} \\
 &= \left. \frac{d}{dV_i} [V_{cc} - R_c I_s e^{V_i/V_T}] \right|_{V_i = V_{BE}} \\
 &= -\frac{1}{V_T} I_s e^{V_{BE}/V_T} R_c
 \end{aligned}$$

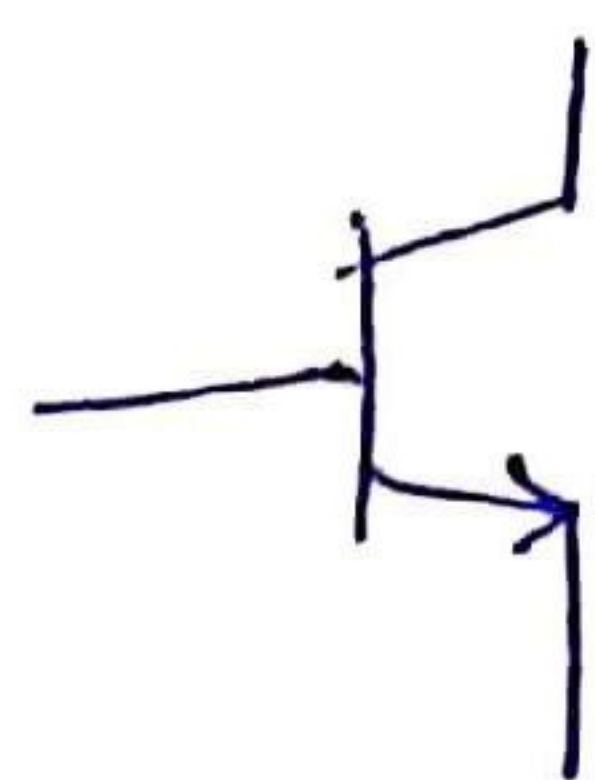
$$A_v = -\frac{I_c R_c}{V_T} = -\frac{V_{R_c}}{V_T}$$

$V_{R_c} \equiv$ Voltage across R_c

BJT as a Switch



open

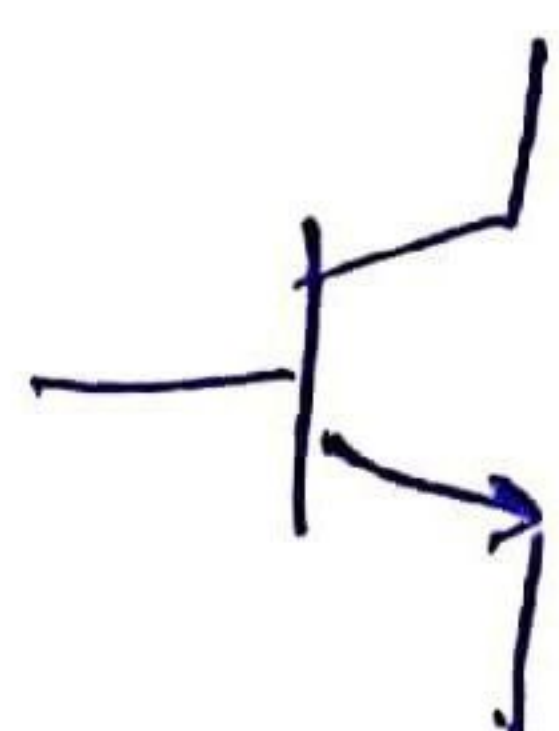


\Rightarrow



open switch

In Cutoff mode



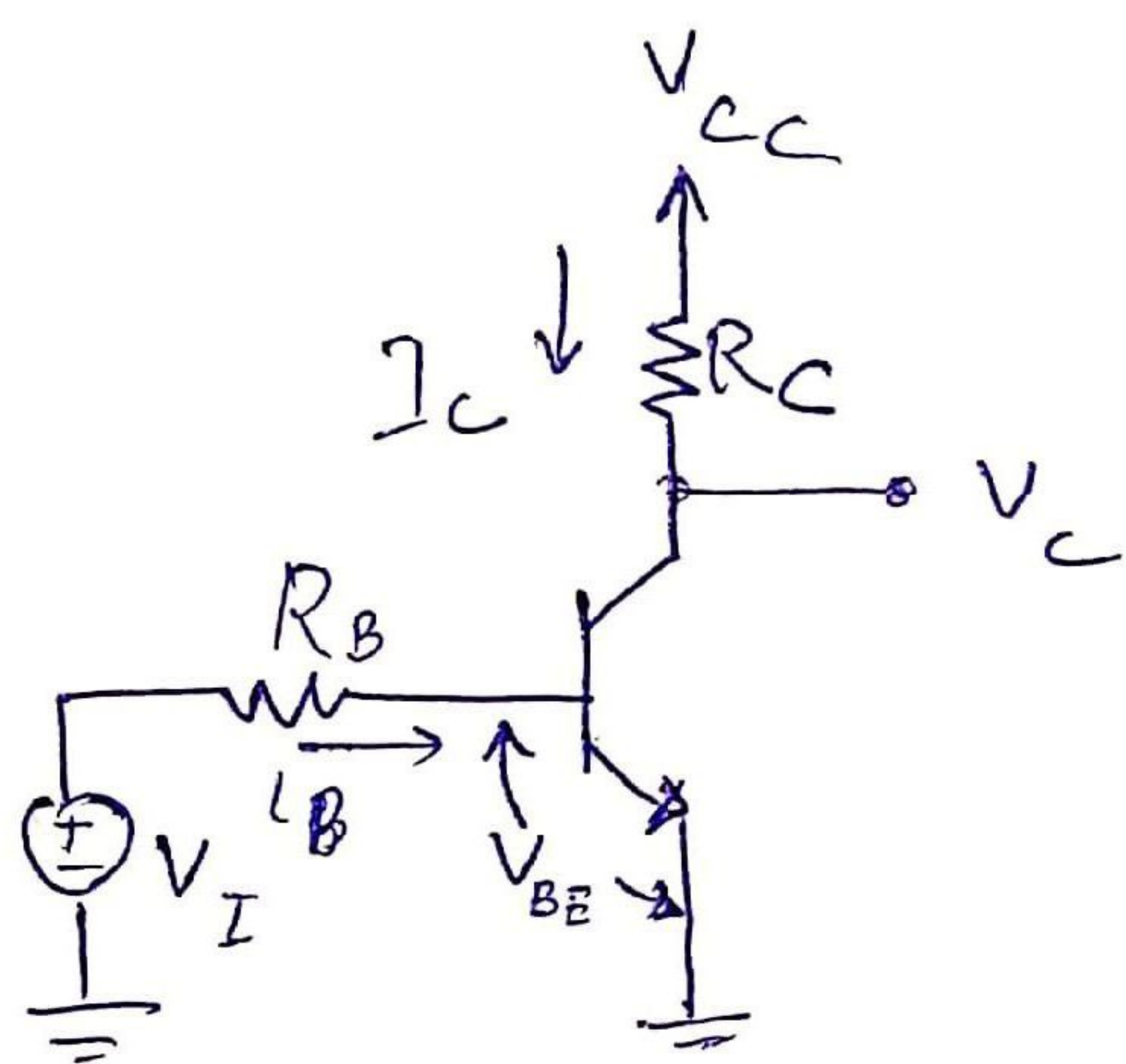
\Rightarrow



Closed
Switch

In Saturation mode

Consider the common-emitter circuit as shown below



For $V_I < 0.5 \text{ V}$

The transistor is in cutoff region
i.e. $I_B = 0$, $I_C = 0$, $V_C = V_{CC}$

The node C is disconnected from the ground and the switch is in open position.

For $V_I > 0.5 \text{ V}$

As V_I increases, $V_{BE} \uparrow$ and when V_{BE} reaches 0.7 V , EBJ is fwd. biased, ~~the~~ I_B starts flowing into base

$$I_B = \frac{V_I - V_{BE}}{R_B}$$

$$\& \quad I_C = \beta I_B \Rightarrow$$

$$\& \quad V_C = V_{CC} - I_C R_C$$

As V_I increases, I_B (and hence I_C) increases therefore V_C decreases.

When V_C becomes lower than V_B by 0.4 V , CBJ becomes forward ~~bias~~^{bias}, and transistor leaves active region and enters the saturation region.

As V_I is increased further transistor goes deeper into the saturation region. The V_{CE} decreases only slightly. When $V_{CE} \approx V_{CEsat} (\approx 0.2\text{ V})$, the collector current I_C then remains nearly constant at I_{Csat} given by

$$I_{sat} = \frac{V_{CC} - V_{CEsat}}{R_C}$$

In this state, the switch is closed with a closure resistance R_{CEsat} .