

Proposal of an ultra-compact mode multiplexer using air-hole type photonic crystal waveguides

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Abstract: We propose an ultra-compact TE_0 - TE_1 mode-division multiplexer based on air-hole photonic crystal waveguides. The longitudinal sizes are only $2.05 \mu\text{m}$, which is $1/5$ compared with that based on conventional Si-wire waveguides.

Keywords: Photonic crystal, Mode multiplexer, Space division multiplexing, Mode division multiplexing

I. INTRODUCTION

With the rapid increase in Internet traffic, the demand for communication capacity expansion of optical fiber is increasing. Since the 1980s, optical fiber communication technology has experienced several technological innovations, and the development of multiplexing technologies such as wavelength division multiplexing (WDM) has increased the communication capacity of single-mode fiber. However, the communication capacity of conventional single-mode optical fiber is approaching its limit [1]. The mode division multiplexing (MDM) transmission, which is one of the space division multiplexing (SDM) technologies, has received attention [2]. MDM can further expand the transmission capacity by using multiple spatial modes propagating in one optical waveguide as transmission channels. Combining WDM and MDM technologies is effective in expanding transmission capacity from long-distance fiber communication to very-short-reach chip-based communication. WDM/MDM hybrid multiplexing technology that can realize wavelength and mode division multiplexing at the same time was proposed [3-5].

For chip communications, the size of the device is an important indicator to achieve high integration density. Nanophotonic technologies based on Si wire waveguides and photonic crystals can confine light to smaller devices due to the high refractive index difference of materials. These technologies have become candidates for reducing the size of optical devices [3-7]. Photonic crystals (PC) are widely studied because of their unique performance and high integration density [6,7]. In some studies of WDM/MDM hybrid multiplexers (MUXs), WDM parts adopt different structures, WDM parts use hole-type PC, and MDM use Si wire waveguides [3]. In this case, the loss will occur in the connection part of the PC and Si waveguide. Therefore, all PC mode MUX is desired to integrate all components for chip communications with PC waveguides (PCWs). However, at present, mode MUXs based on 2-D pillar-type PCWs have been investigated [4,5,8], which are not realistic from a manufacturing point of view.

In this study, we propose ultracompact mode MUX based on the air-hole type PCW which have more practical applications. By using asymmetric directional coupler (ADC),

it is possible to compose TE_0 - TE_1 mode MUX by changing the waveguides widths. The longitudinal sizes are only $2.05 \mu\text{m}$, which is significantly smaller than those based on Si-wire waveguides.

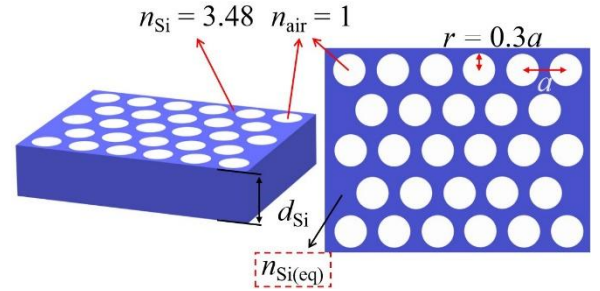


Fig. 1 The schematic diagrams of the 3D PC structure (left) and its plane view (right).

II. AIR-HOLE PHOTONIC CRYSTAL

The schematic diagrams of the 3D PC structure and its plane view considered in this study are shown in Fig. 1. It consists of Si plate with the thickness of d_{Si} . Air-holes with the radius of r are arranged in triangular lattice with the lattice constant of a . The refractive index of the 3D Si slab is set to $n_{\text{Si}} = 3.48$. Here, we examine an equivalent 2D structure with the equivalent refractive index $n_{\text{Si(eq)}}$, because the purpose of this work is to show the theoretical possibility of mode MUX based on air-hole PCWs, which have not been considered yet.

The equivalent 2D structure to the 3D structure is determined as follows. In this study, all the calculations were done with FDTD. Figure 2 (a) shows normalized frequencies (a/λ) of the upper edge, center, and lower edge of the photonic bandgap (PBG) for 2D PC as a function of $n_{\text{Si(eq)}}$. Figure 2 (b) shows the same one for 3D PC as a function of d_{Si} . Figure 2 (a) and (b) are calculated under the parameters of $a = 0.41 \mu\text{m}$ and $r = 0.3a$. For both Figures, the PBG widths are also plotted for the right axis. The PBG width and the position are changed with the parameters. Figure 3 (a) shows the 2D and 3D PBG width as a function of $n_{\text{Si(eq)}}$ (lower horizontal axis) and d_{Si} (upper horizontal axis). The 3D PBG width is not so changed with d_{Si} , while the 2D PBG width has its maximum around $n_{\text{Si(eq)}} = 3.037$, where the difference between 2D and 3D PBGs is small. To ensure that the higher-order mode and the fundamental mode can appear simultaneously in the PBG, we selected the widest 2D PBG when the $n_{\text{Si(eq)}} = 3.037$ as the parameter for subsequent calculation. Figure 3 (b) shows the 2D and 3D normalized frequency at the center of the PBGs as a function of $n_{\text{Si(eq)}}$ and d_{Si} . The center frequency of the 3D PC at $d_{\text{Si}} = 460 \text{ nm}$ is equal to the center frequency of the 2D PC at $n_{\text{Si(eq)}} = 3.037$,

where the PBG widths are also similar between 2D and 3D PCs. Therefore, a 3D PC with $d_{\text{Si}} = 460$ nm can be well approximated by a 2D PC with $n_{\text{Si}(\text{eq})} = 3.037$. PBG parameters for these 2D and 3D PCs are summarized in Table 1, and hereafter, we use them for the 2D equivalent PC. It should be noted that 3D PBG width is slightly larger for smaller values of d_{Si} , as shown in Fig. 3 (a) (although the difference is very small). Therefore, there is a possibility that thinner Si slab will lead to better performance in 3D design. However, as stated above, the purpose of this paper is to show mode multiplexing possibility in air-hole PCWs, and therefore, we used above parameters in this work. Full optimization of 3D structure will be reported elsewhere.

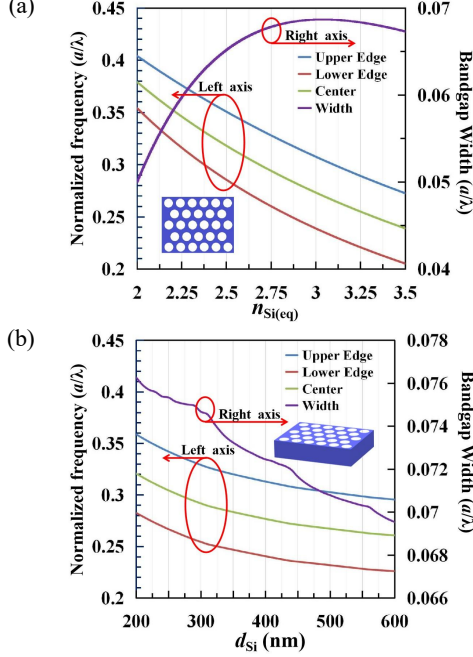


Fig. 2 (a) 2D PBG structure as a function of $n_{\text{Si}(\text{eq})}$ and (b) 3D PBG structure as a function of d_{Si} , where $a = 0.41 \mu\text{m}$ and $r = 0.3a$.

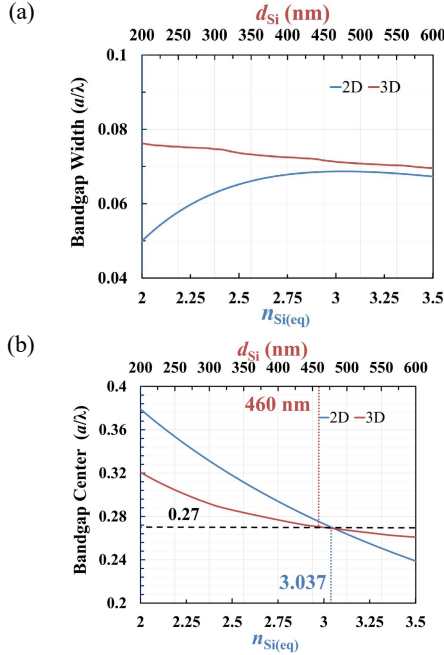


Fig. 3 (a) PBG width and (b) PBG center frequency of 2D and 3D PCs, where $a = 0.41 \mu\text{m}$ and $r = 0.3a$.

$r = 0.3a$	2D structure	3D structure
	$n_{\text{Si}(\text{eq})} = 3.037$	$d_{\text{Si}} = 460$ nm
Upper edge	0.30463	0.30605
Lower edge	0.23596	0.23465
Center	0.27029	0.27035
Width	0.06868	0.07141

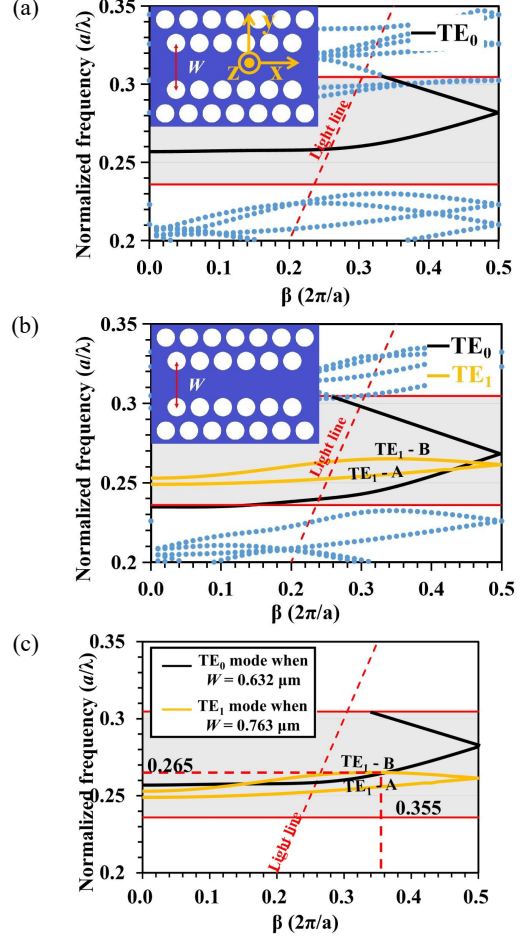


Fig. 4 Dispersion curves of the PCW with $W =$ (a) $0.632 \mu\text{m}$, (b) $0.763 \mu\text{m}$, and (c) the dispersion curves of PCWs in Fig. 4 (a) and (b) superimposed on the same Figure, where $a = 0.41 \mu\text{m}$.

III. AIR-HOLE PHOTONIC CRYSTAL WAVEGUIDES

Once the PC structure is determined, the next task is to investigate the guided modes. A line defect with the width of W is introduced into a complete PC by removing an array of air holes, forming a PCW. Hereafter, the lattice constant is set to $a = 0.41 \mu\text{m}$. For this lattice constant, normalized frequency of 0.265 corresponds to a wavelength of 1550 nm. Figure 4 (a) shows the dispersion curve of the PCW with $W = 0.632 \mu\text{m}$. The hatched area is the PBG. The waveguide is single-mode for the normalized frequency from 0.259 to 0.282 under the light line. Here, we define the xyz coordinate as shown in the inset of Fig. 4(a), and TE mode is defined as the modes, whose principal electromagnetic components are H_z , E_x , and E_y . Figure 4 (b) shows the dispersion curve of the PCW with $W = 0.763 \mu\text{m}$. By increasing the width, a higher-order mode (TE_1) appears in the PBG. There are two curves for the mode and labeled as $\text{TE}_1\text{-A}$ and -B modes. They are also under the light line and can be used for the guided mode. Figure 4 (c) shows the dispersion curves of PCWs with $W = 0.632$ and $0.763 \mu\text{m}$ superimposed on the same Figure (Here,

we only focus on the TE₀ mode when $W = 0.632 \mu\text{m}$ and the TE₁ modes when $W = 0.763 \mu\text{m}$). The TE₀ mode of the single-mode waveguide and the TE₁-B mode of the multimode waveguide have an intersection point at the normalized frequency of 0.265, and the propagation constant β of the two modes are both 0.355. Therefore, the TE₁ mode can be excited by using the phase matching conditions [9].

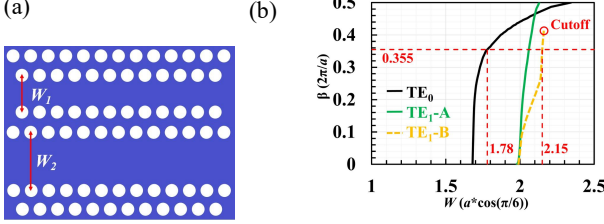


Fig. 5 (a) Mode multiplexer structure. (b) Relationship between propagation constant β and the waveguide width W at $a/\lambda = 0.265$.

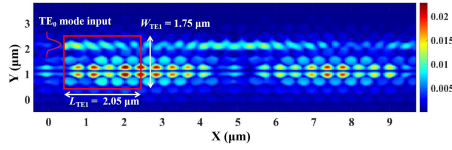


Fig. 6 Magnetic field distribution $|H_z|$ of TE₀-TE₁ mode MUX at $a/\lambda = 0.265$.

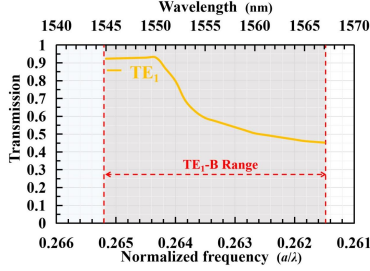


Fig. 7 Transmission spectrum of TE₁ mode MUX.

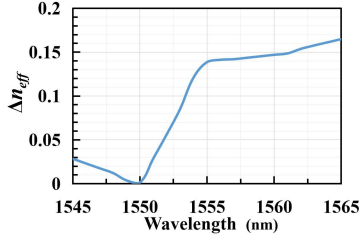


Fig. 8 Δn_{eff} spectrum.

IV. ULTRACOMPACT PHOTONIC CRYSTAL MODE MULTIPLEXER

Here, we consider a mode MUX based on an ADC. It consists of a single-mode waveguide with the width of W_1 and a multi-mode waveguide with the width of W_2 arranged in parallel as shown in Fig. 5(a). Two rows of air-holes are placed between two waveguides and the separation between two waveguides is $0.355 \mu\text{m}$. Figure 5 (b) shows the propagation constant β of TE₀ and TE₁ modes as a function of the waveguide width W at $a/\lambda = 0.265$ ($\lambda = 1550 \text{ nm}$ for $a = 0.41 \mu\text{m}$). For the TE₀ mode with $W_1 = 1.78 \cdot (a \cdot \cos(\pi/6)) = 0.632 \mu\text{m}$, the phase matching conditions are satisfied for TE₁ mode with $W_2 = 2.15 \cdot (a \cdot \cos(\pi/6)) = 0.763 \mu\text{m}$. Figure 6 shows the field distribution of TE₀-TE₁ mode MUX, where W_1 and W_2 are 0.632 and $0.763 \mu\text{m}$, at the wavelength 1550 nm . As we can see, the TE₀ mode launched from narrow waveguide is coupled to the TE₁ mode of wide waveguide.

The coupling length is only $2.05 \mu\text{m}$ for the lattice constant $a = 0.41 \mu\text{m}$. The typical coupling length for the ADC based on Si-wire waveguides with the waveguide separation of 200 nm around 1550 nm is about $10 \mu\text{m}$ [10]. Here, the coupling length of proposed PCW ADC is 1/5 even though the waveguide separation is increased to $0.355 \mu\text{m}$. Figure 7 shows the calculated transmission spectrum of the TE₁ mode MUX for the lattice constant $a = 0.41 \mu\text{m}$. Since the TE₁-B mode only exists in the normalized frequency range of $a/\lambda = 0.2615 \sim 0.2652$, we only show the results in the range, where the TE₁-B mode exists. The transmissions of the TE₁ mode at the wavelength of 1550 nm are greater than 90%. However, the transmissions at other wavelengths are degraded, especially for longer wavelength region. This partly comes from that the phase matching condition is not satisfied for the other wavelength region. Figure 8 shows the effective index difference, Δn_{eff} spectrum between TE₀ and TE₁-B modes. Δn_{eff} is zero at 1550 nm and is not zero for other wavelengths, and the value is large for longer wavelength side. Therefore, the phase mismatch seems to be the dominant factor for longer wavelength side degradation.

V. CONCLUSIONS

We proposed an ultra-compact air-hole PC mode MUX using waveguide phase matching principle. It was shown that the two mode (TE₀ and TE₁ modes) multiplexing is possible, the size of the MUX can be reduced to 1/5 compared with those of Si-wire based mode MUX, and more than 90% transmission is possible at the wavelength of 1550 nm .

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