TFE4188 - Introduction to Lecture 6

Oversampling and Sigma-Delta ADCs

Goal for today

Understand why there are different ADCs

Introduction to oversampling and delta-sigma modulators

1999, R. Walden: Analog-to-digital converter survey and analysis

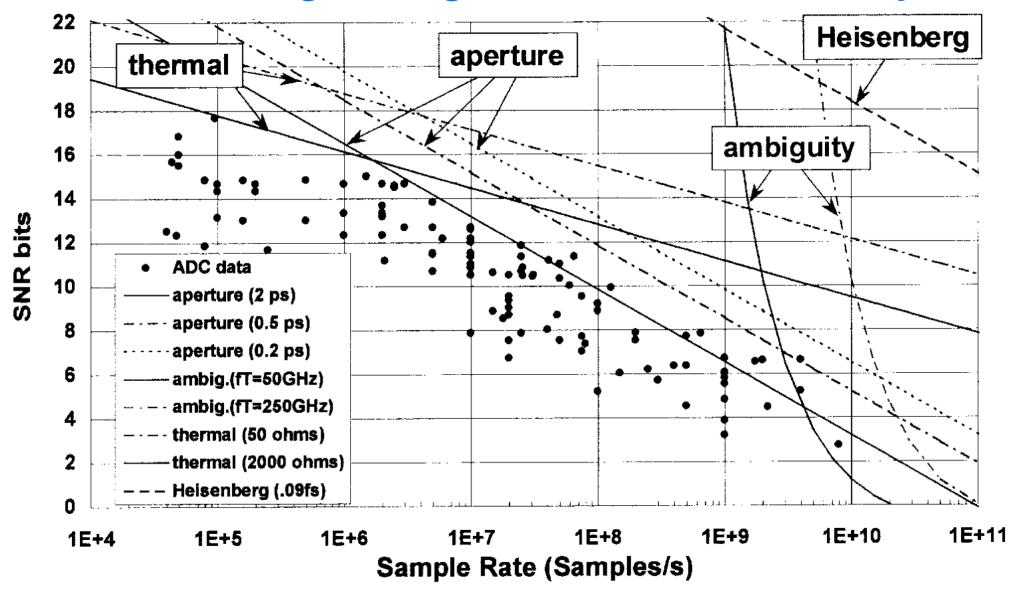


Fig. 7. Signal-to-noise ratio according to SNR-bits = (SNR(dB) - 1.76)/6.02. Three sets of curves show performance limiters due to thermal noise, aperture uncertainty, and comparator ambiguity. The Heisenberg limit is also displayed.

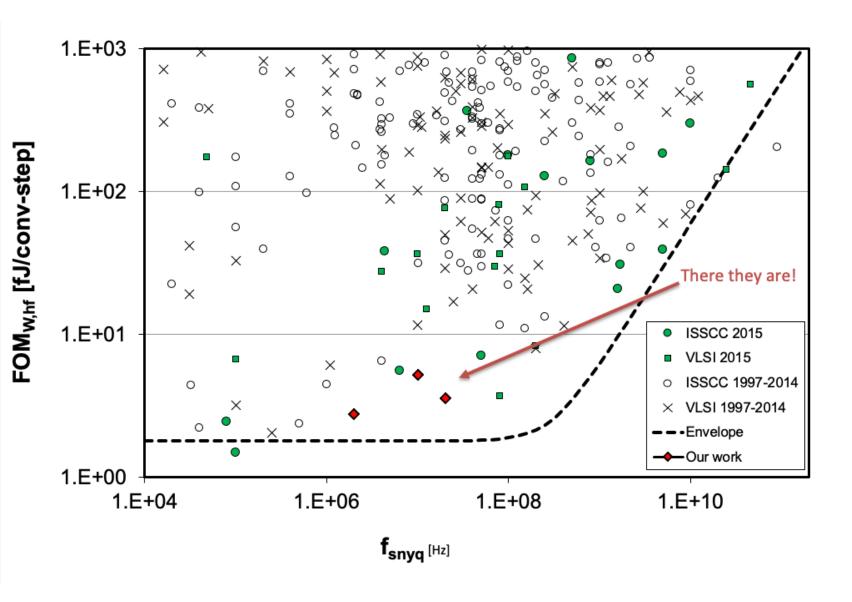
2.E+03 FOM_{w,hf} [fJ/conv-step] 2.E+02 2.E+01 **ISSCC 2021** 2.E+00 VLSI 2021 VLSI 1997-2020 - Envelope 2.E-01 1.E+05 1.E+08 1.E+04 1.E+06 1.E+07 1.E+09 1.E+10 f_{snyq} [Hz]

B. Murmann, ADC Performance Survey 1997-2021 (ISSCC & VLSI Symposium)

$$FOM_W = rac{P}{2^B f_s}$$

Below 10 fJ/conv.step is good

Below 1 fJ/conv.step is extreme



People from NTNU have made some of the worlds best ADCs

A Compiled 9-bit 20-MS/s 3.5-fJ/conv.step SAR ADC in 28-nm FDSOI for Bluetooth Low Energy Receivers

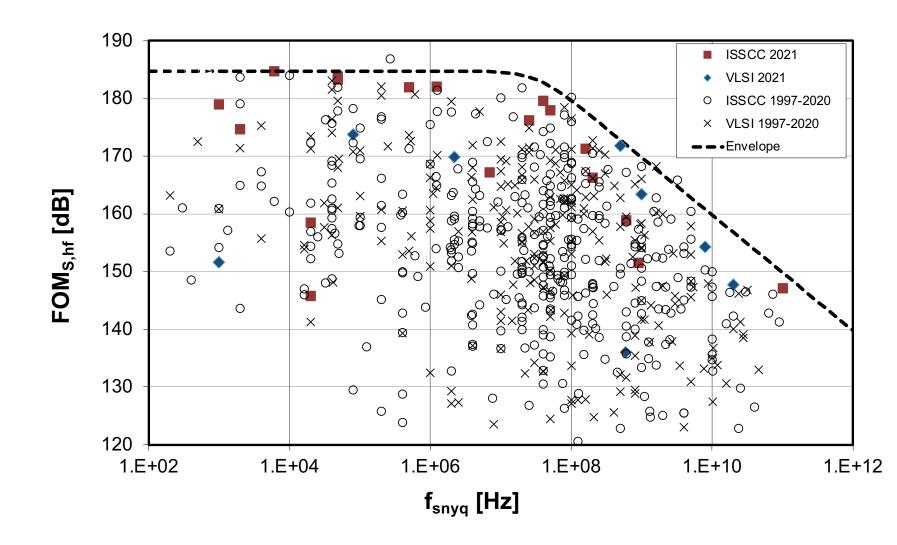
A 68 dB SNDR Compiled Noise-Shaping SAR ADC With On-Chip CDAC Calibration

Carsten Wulff 2023 5

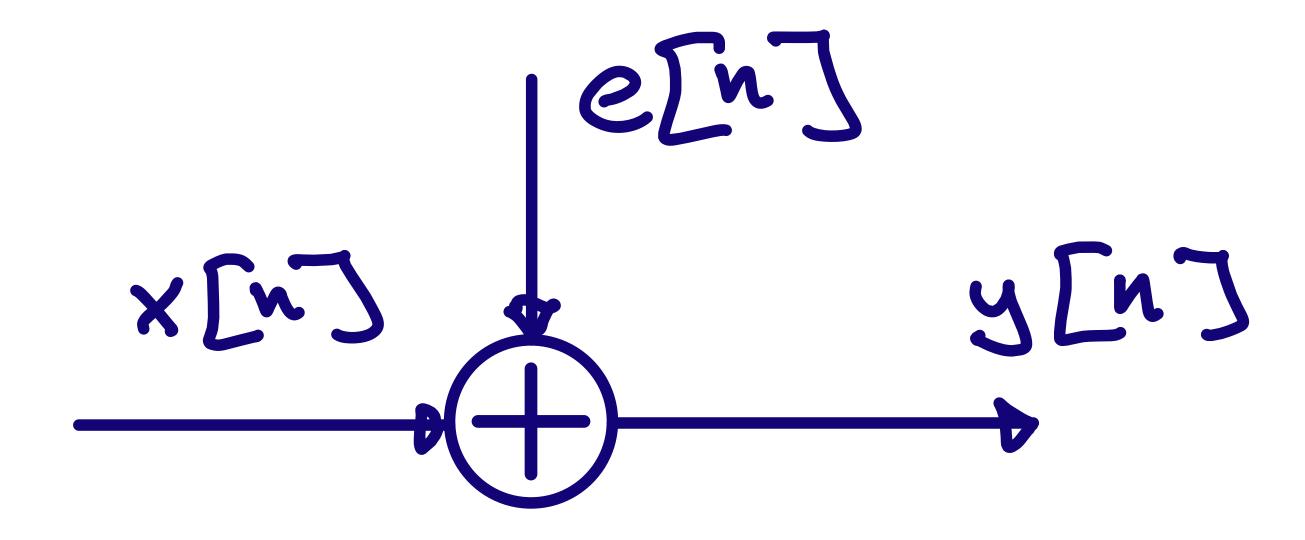
B. Murmann, ADC Performance Survey 1997-2021 (ISSCC & VLSI Symposium)

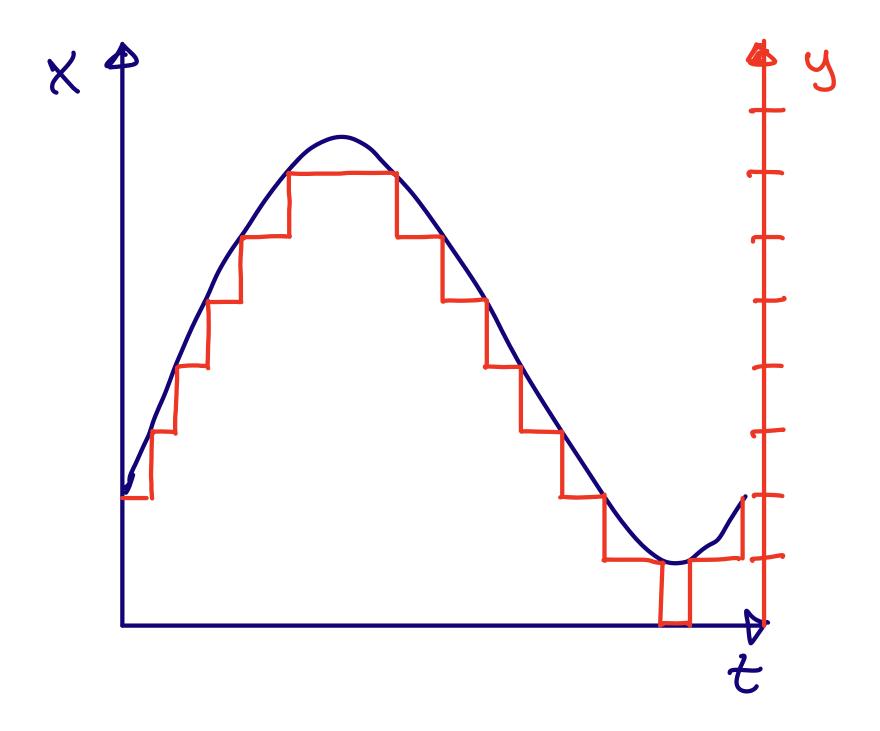
$$FOM_S = SNDR + 10\logigg(rac{f_s/2}{P}igg)$$

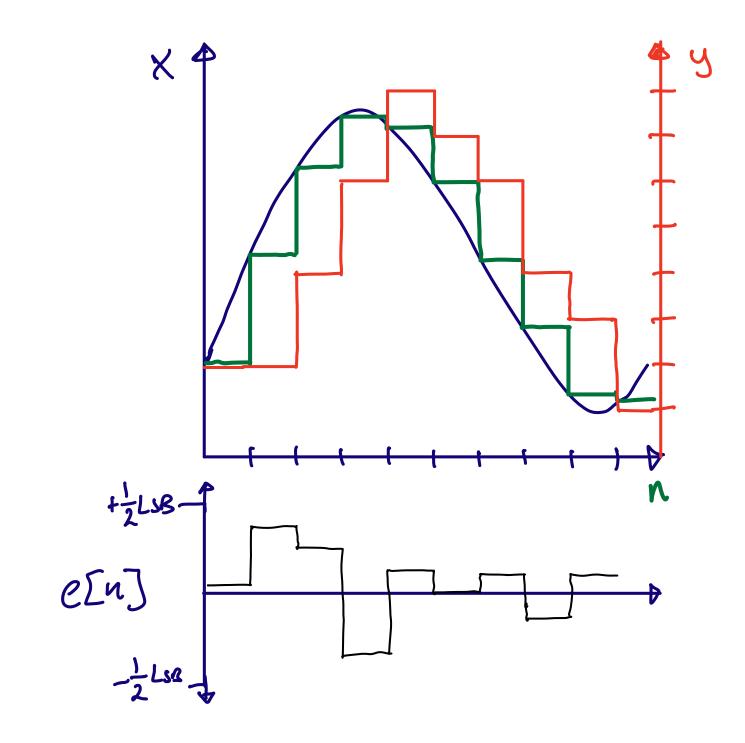
Above 180 dB is extreme



Quantization







$$e_n(t) = \sum_{p=1}^{\infty} A_p \sin p \omega t$$

where p is the harmonic index, and

$$A_p = egin{cases} \delta_{p1} A + \sum_{m=1}^\infty rac{2}{m\pi} J_p(2m\pi A) &, p = ext{ odd} \ 0 &, p = ext{ even} \end{cases}$$

$$\delta_{p1} egin{cases} 1 &, p=1 \ 0 &, p
eq 1 \end{cases}$$

and $J_p(x)$ is a Bessel function of the first kind, A is the amplitude of the input signal.

If we approximate the amplitude of the input signal as

$$A=rac{2^n-1}{2}pprox 2^{n-1}$$

where n is the number of bits, we can rewrite as

See The intermodulation and distortion due to quantization of sinusoids

$$e_n(t) = \sum_{p=1}^{\infty} A_p \sin p \omega t$$

$$A_p = \delta_{p1} 2^{n-1} + \sum_{m=1}^{\infty} rac{2}{m\pi} J_p(2m\pi 2^{n-1}), p = odd$$

$$\overline{e_n(t)}=0$$

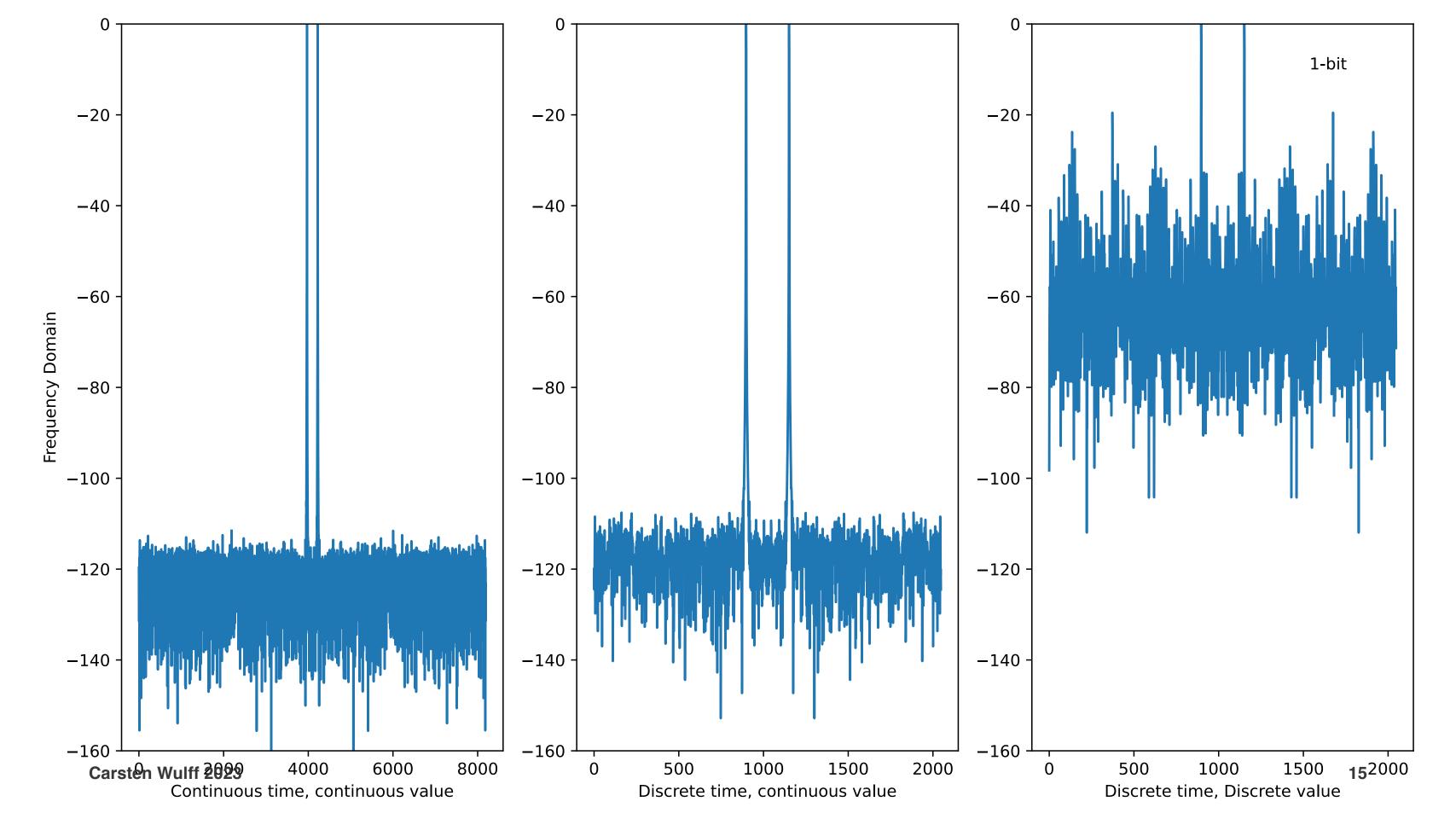
$$\overline{e_n(t)^2} = rac{\Delta^2}{12}$$

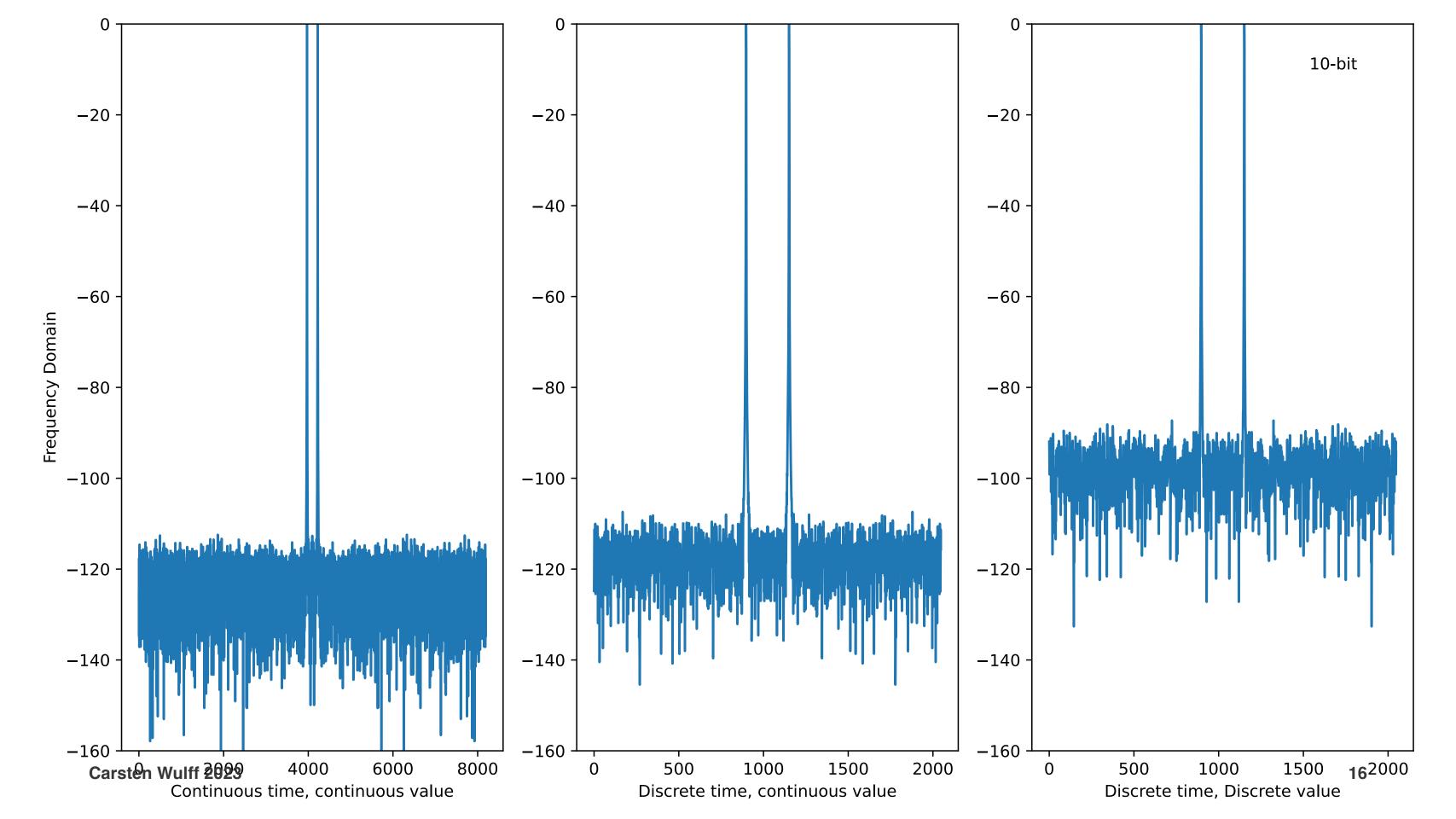
$$SQNR = 10\logigg(rac{A^2/2}{\Delta^2/12}igg) = 10\logigg(rac{6A^2}{\Delta^2}igg)$$

$$\Delta = rac{2A}{2^B}$$

$$SQNR = 10 \log \left(rac{6A^2}{4A^2/2^B}
ight) = 20B \log 2 + 10 \log 6/4$$

$$SQNR \approx 6.02B + 1.76$$





Oversampling

In-band quantization noise at an oversampling ratio (OSR)

$$\overline{e_n(t)^2} = rac{\Delta^2}{12 OSR}$$

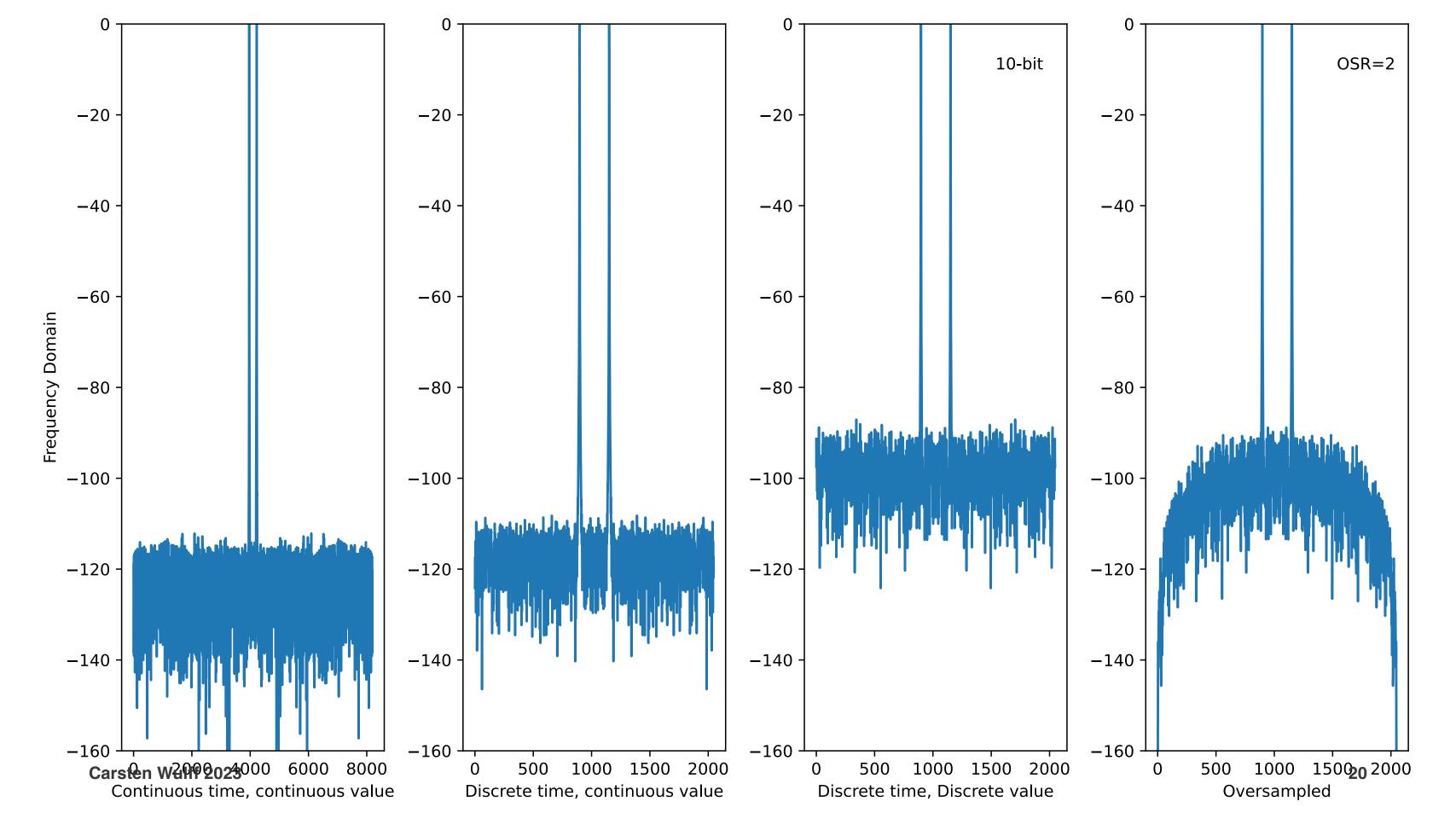
$$SQNR = 10\logigg(rac{6A^2}{\Delta^2/OSR}igg) = 10\logigg(rac{6A^2}{\Delta^2}igg) + 10\log(OSR)$$

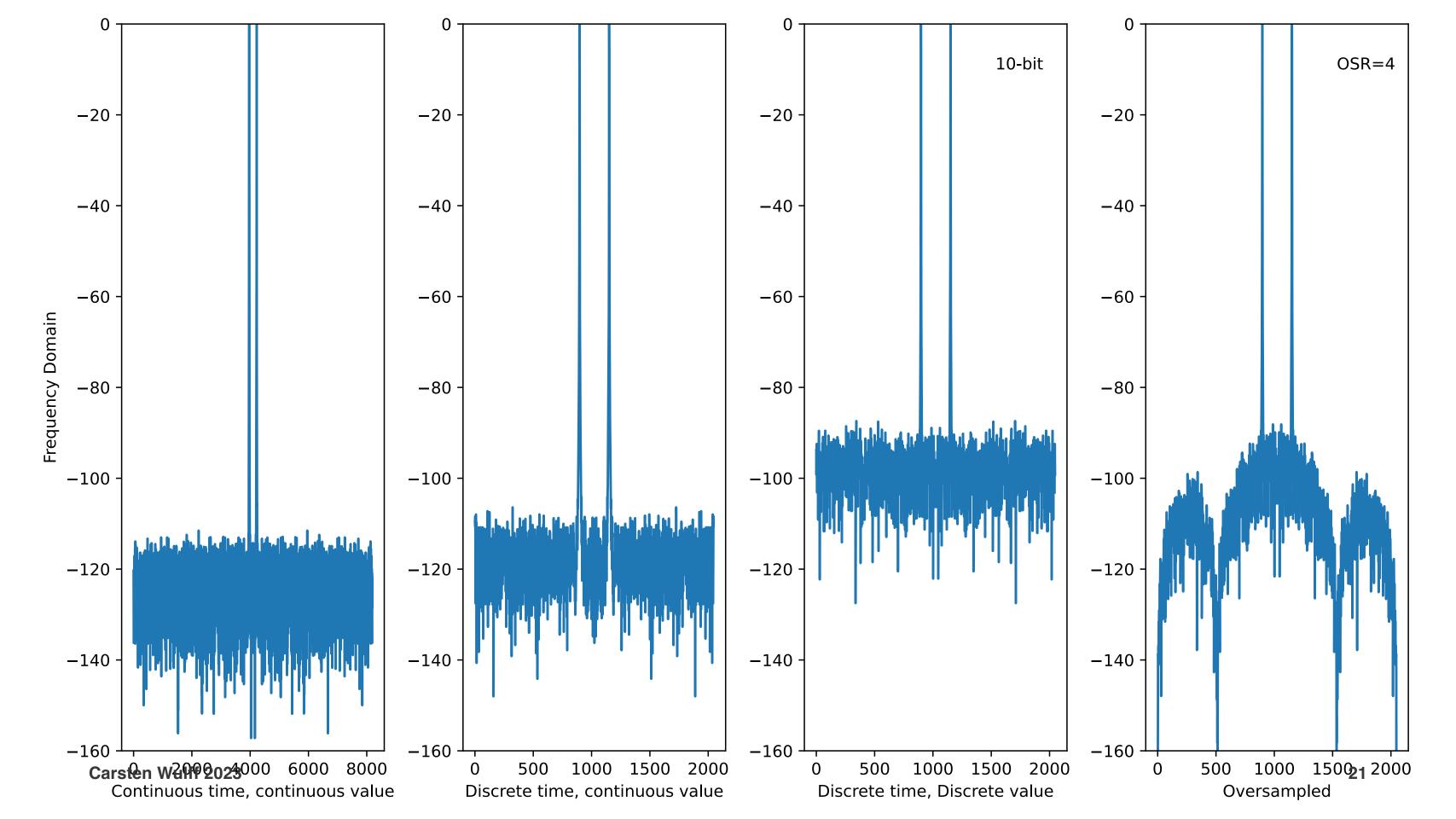
$$SQNR pprox 6.02B + 1.76 + 10\log(OSR)$$

$$10\log(2)pprox 3dB \ 10\log(4)pprox 6dB$$

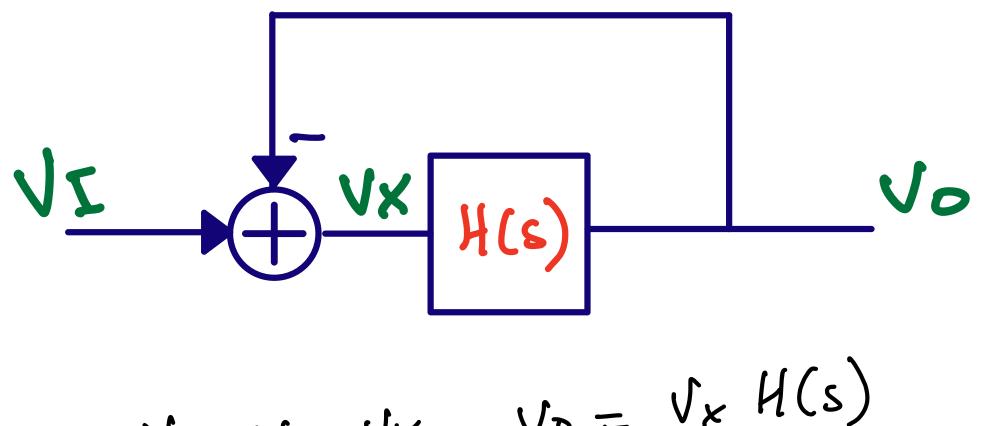
0.5-bit per doubling of OSR

```
def oversample(x, OSR):
    N = len(x)
    y = np.zeros(N)
    for n in range(0,N):
        for k in range(0,0SR):
            m = n+k
            if (m < N):
                y[n] += x[m]
    return y
```





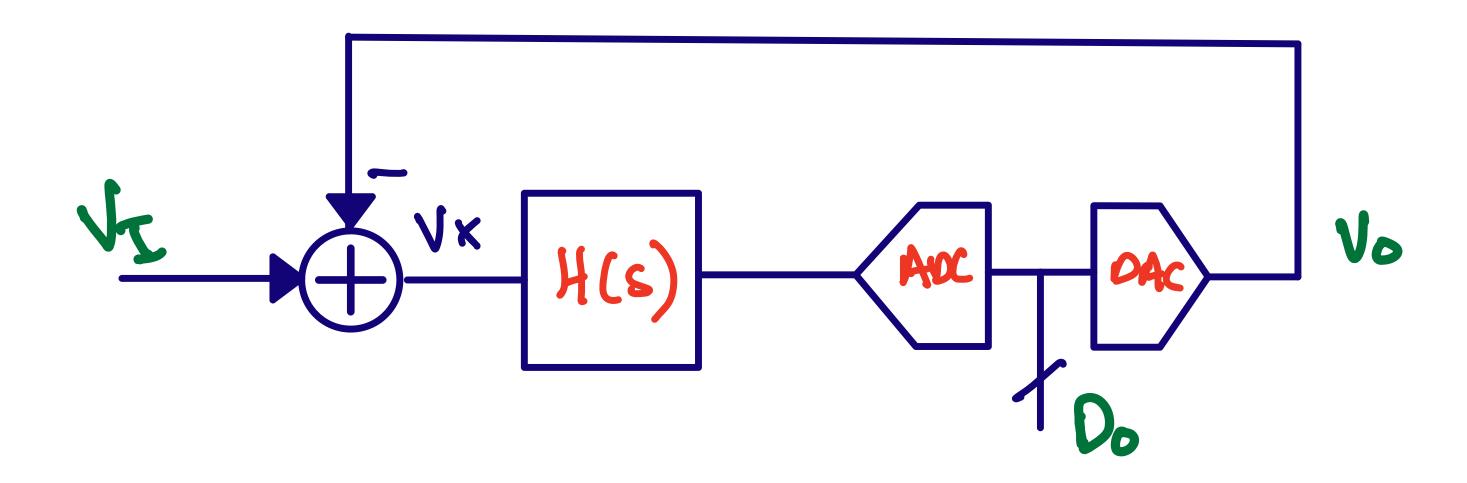
Noise Shaping



$$V_{\overline{L}} - V_{0} = V_{x}$$
 $V_{0} = V_{x}$ $H(s)$

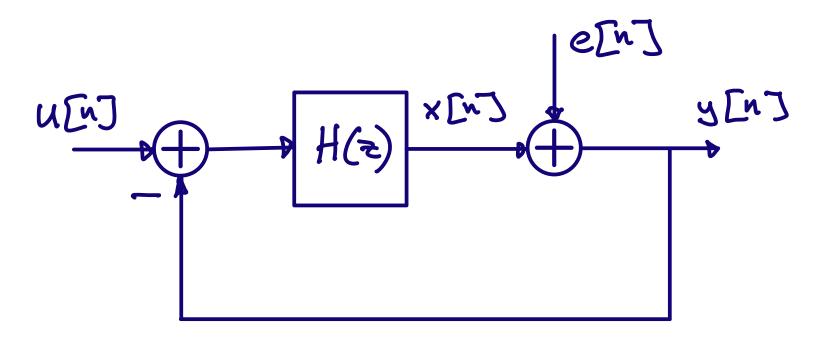
$$V_{\overline{L}} = V_{0} + \frac{V_{0}}{H(s)} = 0$$

$$V_{0} = V_{x}$$



Sample domain

$$y[n] = e[n] + h*(u[n] - y[n])$$



Z-Domain

$$Y(z)=E(z)+H(z)\left[U(z)-Y(z)
ight]$$

Signal transfer function

Assume U and E are uncorrelated, and E is zero

$$Y = HU - HY$$

$$STF=rac{Y}{U}=rac{H}{1+H}=rac{1}{1+rac{1}{H}}$$

Noise transfer function

Assume U is zero

$$Y=E+HY o NTF=rac{1}{1+H}$$

Combined transfer function

$$Y(z) = STF(z)U(z) + NTF(z)E(z)$$

First-Order Noise-Shaping

$$H(z) = \frac{1}{z-1}$$

$$STF = rac{1/(z-1)}{1+1/(z-1)} = rac{1}{z} = z^{-1}$$

$$NFT = rac{1}{1+1/(z-1)} = rac{z-1}{z} = 1-z^{-1}$$

$$NFT = 1 - z^{-1}$$

$$z=e^{sT}\stackrel{s=j\omega}{
ightarrow}e^{j\omega T}=e^{j2\pi f/f_s}$$

$$NTF(f)=1-e^{-j2\pi f/f_s}$$

$$=rac{e^{j\pi f/f_s}-e^{-j\pi f/f_s}}{2j} imes 2j imes e^{-j\pi f/f_s}$$

$$=\sinrac{\pi f}{f_s} imes 2j imes e^{-j\pi f/f_s}$$

$$|NFT(f)| = \left| 2 \sin \left(rac{\pi f}{f_s}
ight)
ight|$$

$$P_s = A^2/2 \ P_n = \int_{-f_0}^{f_0} rac{\Delta^2}{12} rac{1}{f_s} [2\sin\pi f/f_s]^2 dt$$

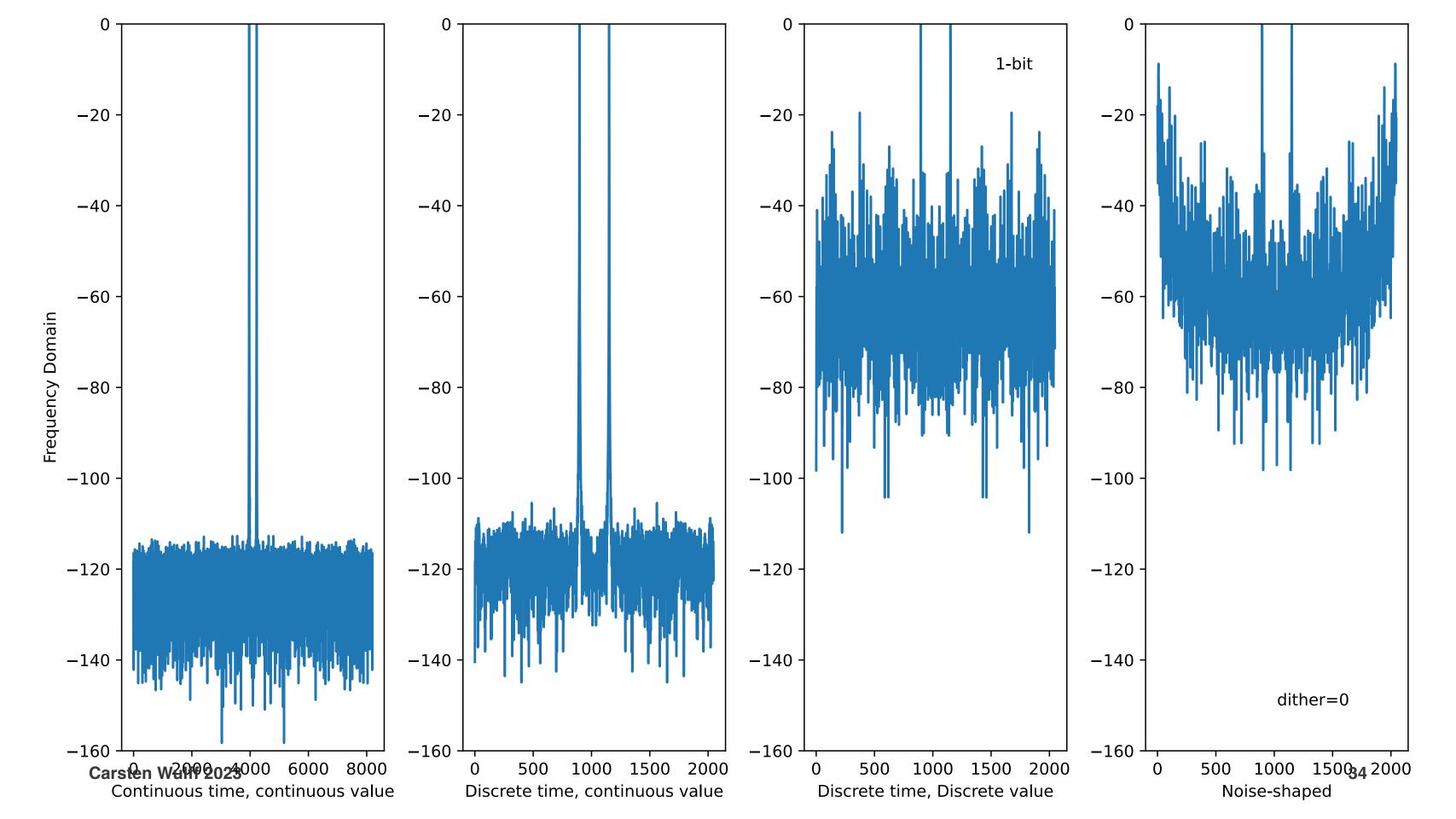
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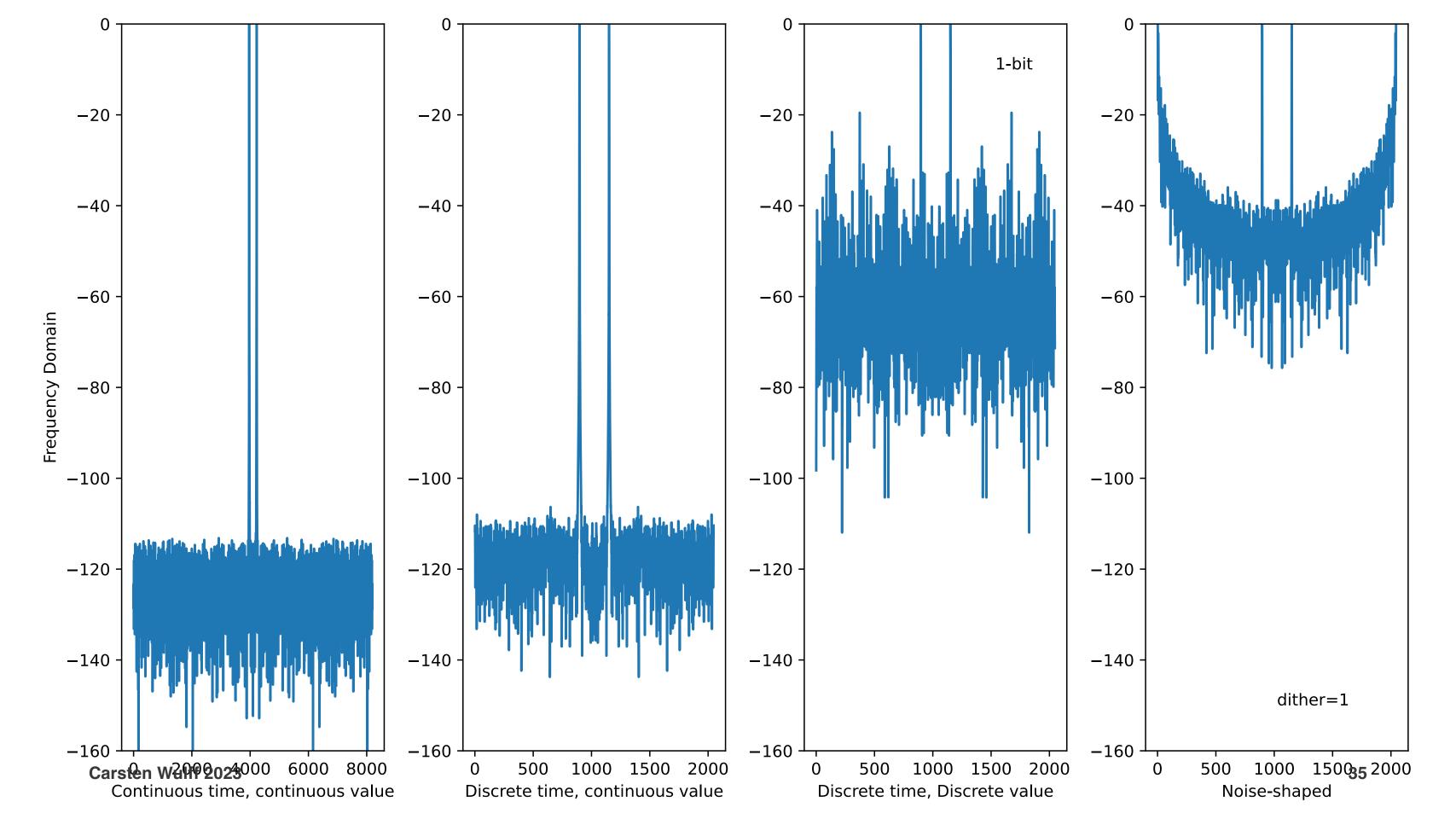
$$SQNR = 6.02B + 1.76 - 5.17 + 30\log(OSR)$$

Assume 1-bit quantizer, what would be the maximum ENOB?

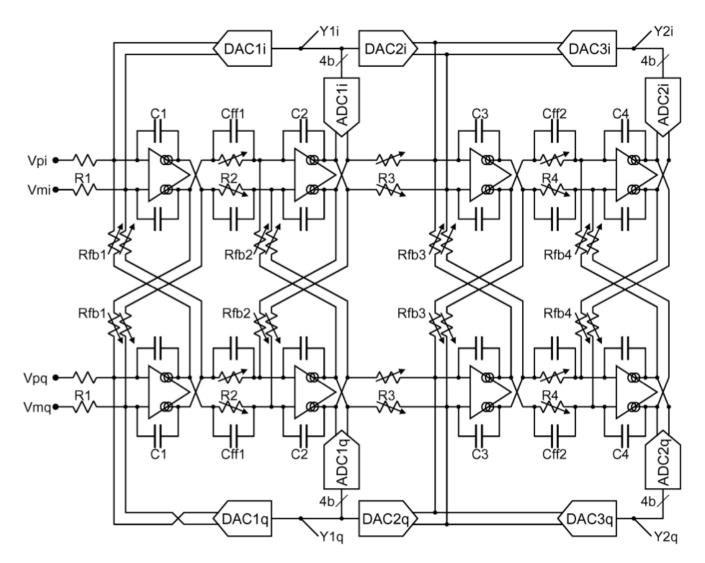
OSR	Oversampling	First-Order	Second Order
4	2	3.1	3.9
64	4	9.1	13.9
1024	6	15.1	23.9

```
# x sn is discrete time, continuous value input
dither = 0
M = len(x sn)
y sd = np.zeros(M)
x = np.zeros(M)
for n in range(1, M):
    x[n] = x sn[n-1] + (x sn[n]-y sd[n-1])
    y sd[n] = np.round(x[n]*2**bits
        + dither*np.random.randn()/4)/2**bits
```





A 56 mW Continuous-Time Quadrature Cascaded Sigma-Delta Modulator With 77 dB DR in a Near Zero-IF 20 MHz Band



igma-delta modulator design.

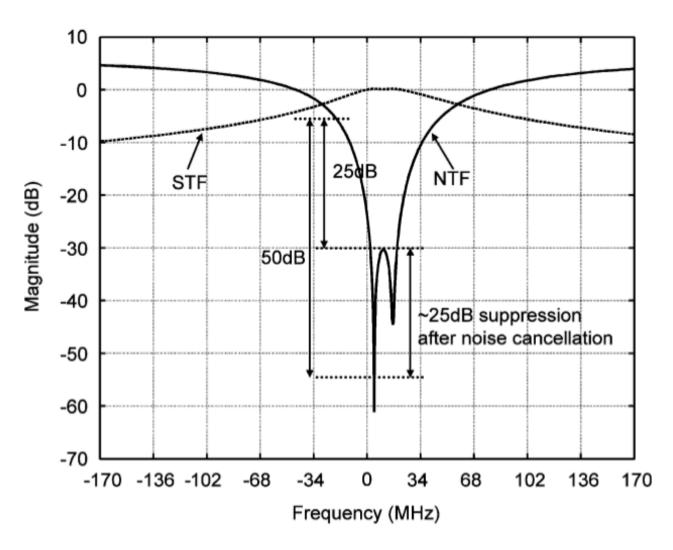
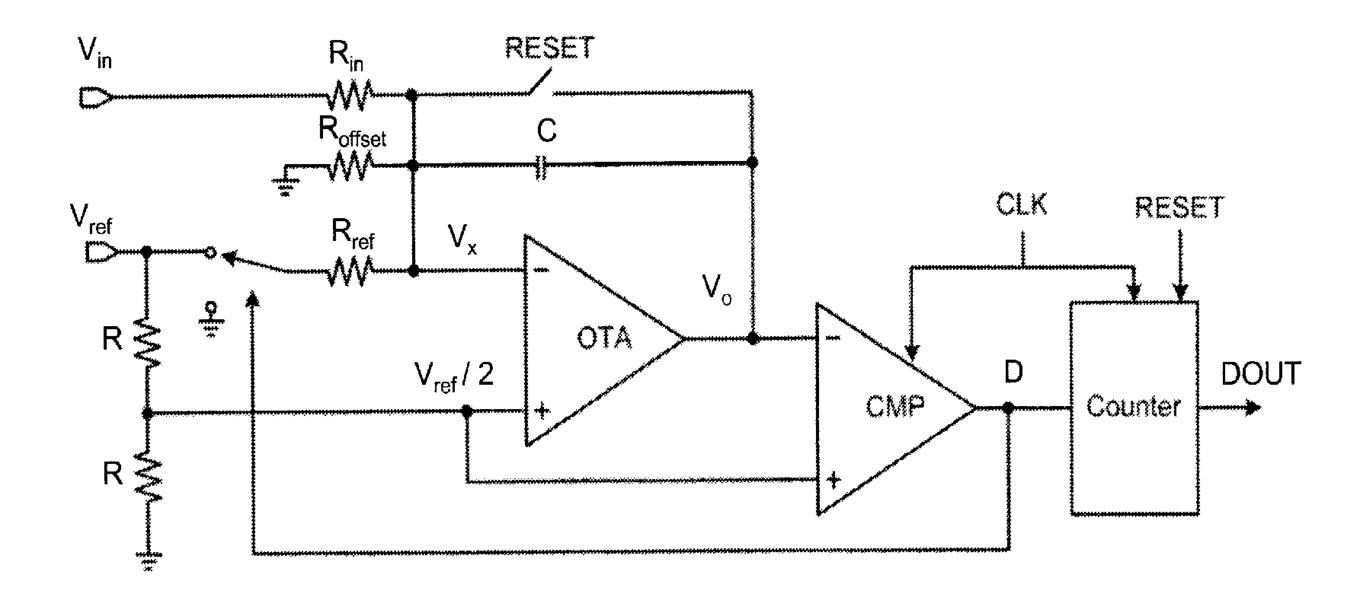


Fig. 9. NTF and STF of first stage.

Analogue-to-digital converter



Thanks!