

18220 Exam 2 Review

We got the POWER

Def. Power is defined as

$$P = \underset{\substack{\uparrow \\ \text{current}}}{I} \underset{\substack{\uparrow \\ \text{voltage}}}{V}$$

Cor: w/ $V=IR$ we can write:

$$P = IV = I^2 R = \frac{V^2}{R}$$

Def: we define the capacitor equation as

$$i_c(t) = C \frac{dV_c(t)}{dt}$$

Cor: Using power, we have

$$P_c(t) = i_c(t) \cdot V_c(t)$$

Since energy = power · time,

$$\begin{aligned} E_c &= \int P_c(t) dt = \int i_c(t) V_c(t) dt \\ &= \int \frac{dV_c(t)}{dt} V_c(t) dt \\ &= C \int V_c(t) dV_c(t) \\ &= \frac{1}{2} C V_c^2 \end{aligned}$$

Def: The inductor equation is

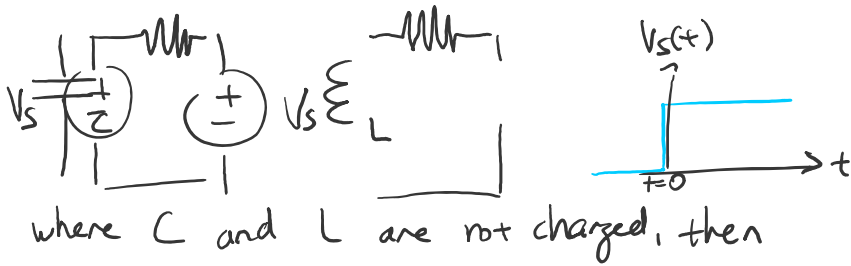
$$V_L(t) = L \frac{di_L(t)}{dt}$$

Cor: Similar to the deriv. for the cap, we can get

$$E_L = \frac{1}{2} L I_L^2$$

Long Time / Frequency Analysis of L/C

Consider



where C and L are not charged, then

Cap: $\frac{t=0}{\text{short}} \quad \frac{t \rightarrow \infty}{\text{open}}$

Ind: $\text{open} \quad \text{short}$

Def: The complex impedance for a capacitor is

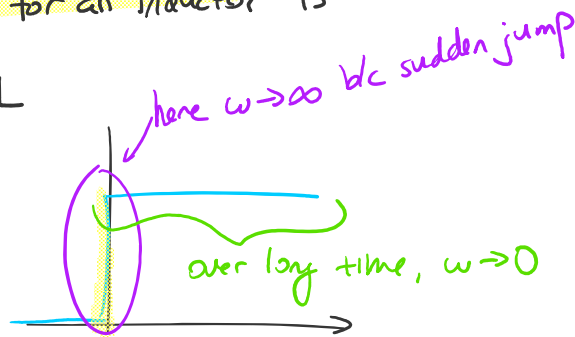
$$Z_C = \frac{1}{j\omega C}$$

Def: The complex impedance for an inductor is

$$Z_L = j\omega L$$

Cap: $\frac{\omega \rightarrow \infty}{\text{short}} \quad \frac{\omega = 0}{\text{open}}$

Ind: $\text{open} \quad \text{short}$



Just an interesting coincidence...

Transforming the POWER

Def: We define M to be the mutual inductance. $M = k\sqrt{L_1 L_2}$ (Henries)

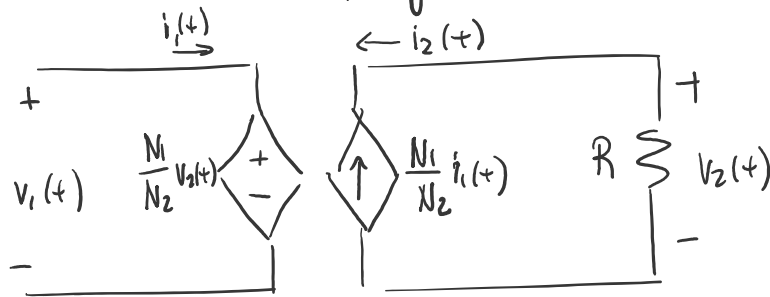
Def: k is the coupling coefficient. (unitless)

- $k=0$ if no coupling
- $k=1$ is a perfect transformer

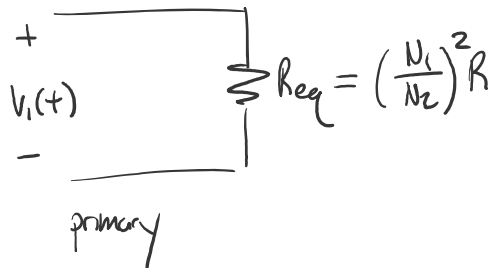
Def: An ideal transformer is defined to be:

- $L, M \rightarrow \infty$ so little current flows through inductors and therefore the transformer stores no energy

$k=1$ perf. coupling



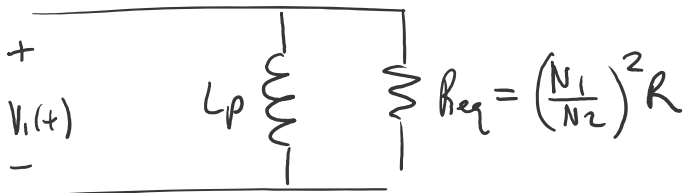
Ex: Using transformer properties, we can derive



Def: A perfect transformer is a transformer w/ $k=1$ but

M, L not nec. $\rightarrow \infty$.

This means we have a leakage inductance, so when we derive the equivalent resistance, we instead have:



where L_p is the leakage inductance, can be defined in several ways. One such way is:

$$L_p = k \cdot L_1$$

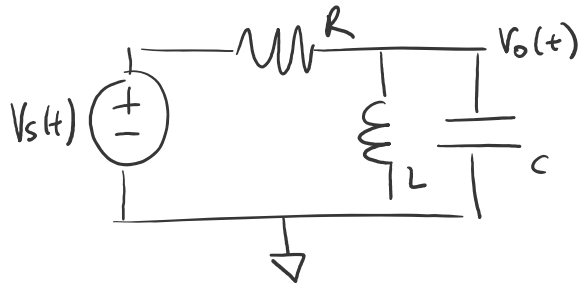
Def: A non-ideal transformer in general does not have any ideal assumptions. You have to write out the coupled differential equations to solve these problems.

Oscillating w/the POWER

Def: A RLC circuit has a resistor (usually in series)

Def: A **RLC circuit** has a resistor (usually in series) w/ a L, C either in parallel or series.

For our example, we'll do the one in parallel:



If we write the diff. eq for this circuit, we get

$$\frac{d^2 V_o(t)}{dt^2} + \frac{1}{RC} \frac{dV_o(t)}{dt} + \frac{1}{LC} V_o(t) = \frac{1}{RC} \frac{dV_s(t)}{dt}$$

To solve the homogeneous solution, we first make an ansatz of

$$V_o(t) = A e^{st}$$

Plugging in gives us $s = -\frac{1}{2RC} \pm \sqrt{\left(\frac{1}{2RC}\right)^2 - \frac{1}{LC}}$

we like to define

$$\cdot \alpha = \frac{1}{2RC}$$

$$\cdot \tau = \sqrt{LC}$$

$$\cdot \omega_0 = \frac{1}{\sqrt{LC}} = \frac{1}{\tau}$$

$$s = -\alpha \pm \sqrt{\alpha^2 - \omega_0^2}$$

Now, before we write our general solutions, we need to consider 3 cases

• det. is < 0 , then we have a complex root, i.e.

$$s = a \pm jb$$

so

$$A_1 e^{t(a+jb)} + A_2 e^{t(a-jb)}$$

$$\Rightarrow A_1 e^{at} \cos(bt) + A_2 e^{at} \sin(bt) \text{ (spans same sol. space)}$$

This is called underdamping

- $\det = 0$ Then we only have one sol. It turns out we need to make our general solution

$$A_1 e^{at} + A_2 t e^{at}$$

in this case.

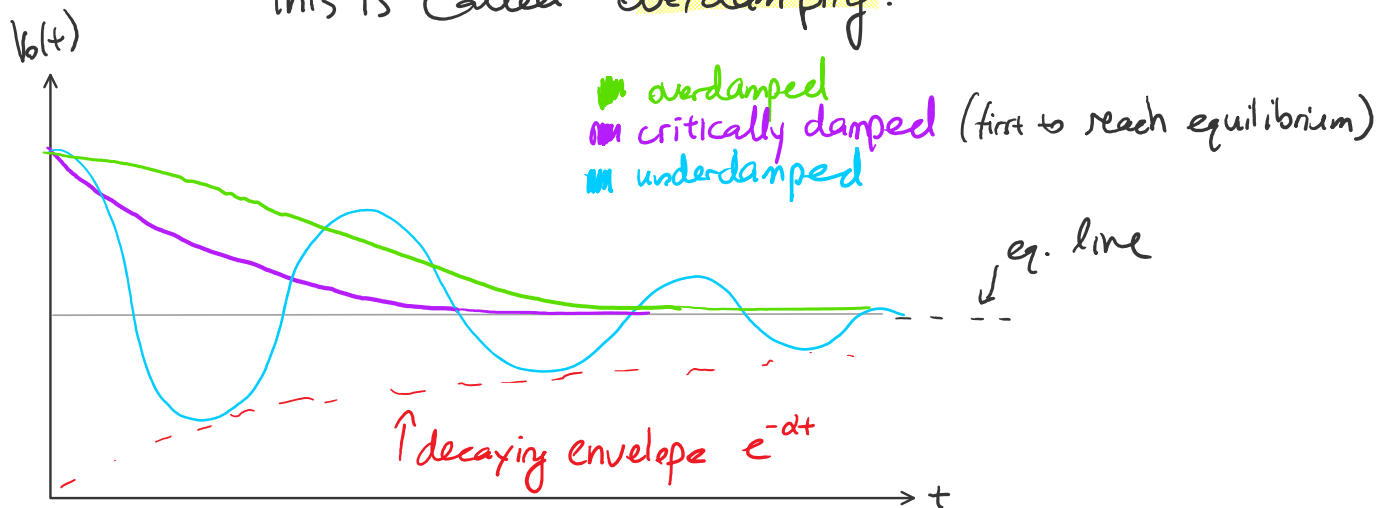
This is called critical damping.

- $\det > 0$ Both characteristic roots are real, so

$$A_1 e^{t(a+b)} + A_2 e^{t(a-b)}$$

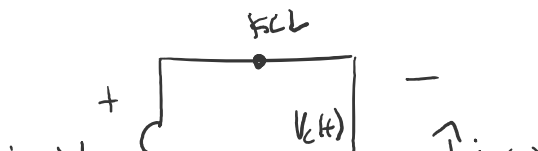
is our general solution

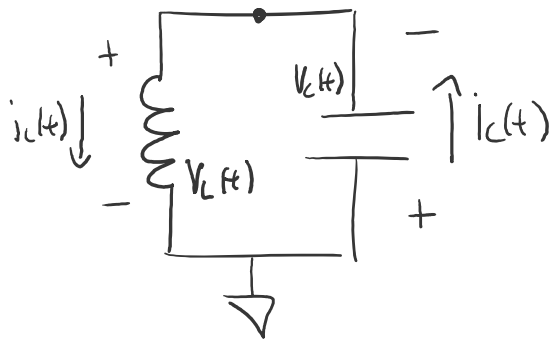
This is called overdamping.



Resonating w/ POWER

Consider the LC circuit





KVL gives us:

$$0 - V_C(t) - V_L(t) = 0$$

$$V_C(t) + V_L(t) = 0 \Rightarrow V_C(t) + L \frac{di_C(t)}{dt} = 0$$

KCL gives us:

$$-i_C(t) + i_L(t) = 0$$

$$\Rightarrow C \frac{dV_C(t)}{dt} = i_C(t)$$

$$V_C(t) + L \frac{d}{dt} \left(C \frac{dV_C(t)}{dt} \right) = 0$$

$$\frac{d^2 V_C(t)}{dt^2} + \frac{1}{LC} V_C(t) = 0$$

solving w/ Aest gives

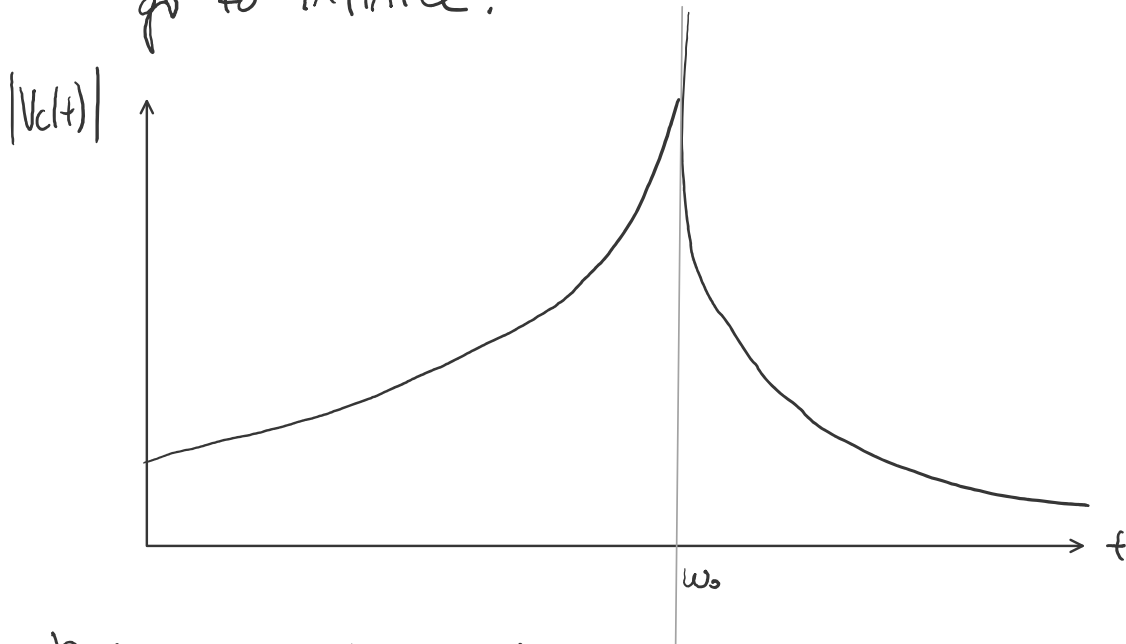
$$s^2 = -\frac{1}{LC} \Rightarrow s = \pm j \left(\frac{1}{\sqrt{LC}} \right)$$

from $\omega = 1/\sqrt{LC}$

our solution is in general

$$\begin{aligned} V_C(t) &= A_1 \cos(\omega_0 t) + A_2 \sin(\omega_0 t) \\ &= K \cos(\omega_0 t + \phi) \end{aligned}$$

for this circuit, resonance occurs at $\omega_0 = \frac{1}{\sqrt{LC}}$, which means if you applied a driving source w/ $f = \omega_0$ then the oscillation would essentially go to infinite.



Def: Since the amplitude at resonance is not ∞ in real life, we define our quality factor as \propto height of resonance, which is

$$Q = \frac{\omega_0}{2\alpha}$$

Notice that since we did not have a resistor in our LC circuit, there was no damping. In general, the damping caused by the resistor depends on the circuit, i.e.

RLC series		RLC parallel
α	$\frac{1}{2} \frac{R}{L}$	$\frac{1}{2RC}$