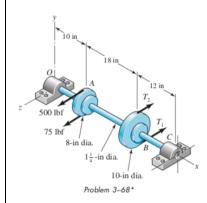
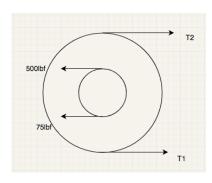
3-68 A countershaft carrying two V-belt pulleys is shown in the figure. Pulley A receives power from a motor through a belt with the belt tensions shown. The power is transmitted through the shaft and delivered to the belt on pulley B. Assume the belt tension on the loose side at B is 15 per- cent of the tension on the tight side.

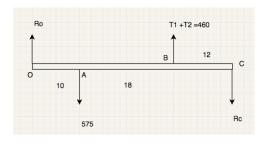


1. (a) Determine the tensions in the belt on pulley B, assuming the shaft is running at a constant speed.



#Sum of Torques $solve(\{(500-75)\cdot(4)-(T[2]-T[1])\cdot(5)=0,1700-(T[2]-0.15T[2])\cdot(5)=0\},$ $\{T[1], T[2]\})$

(b) Find the magnitudes of the bearing reaction forces, assuming the bearings act as simple



#Sum of moments at 'O'

$$R[C] := evalf \left(\frac{\left(-575 \cdot 10 + \left(10 + 18\right) \cdot \left(460\right)\right)}{\left(12 + 18 + 10\right)} \right)$$

$$R_C := 178.2500000$$

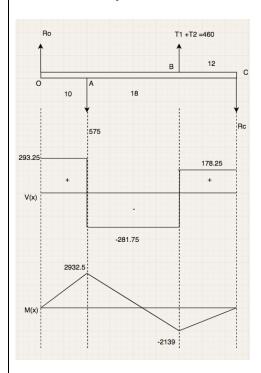
#Sum of moments at 'C'

#Sum of moments at 'C'
$$R[O] := evalf\left(\frac{(-460 \cdot 12 + (18 + 12) \cdot 575)}{10 + 18 + 12}\right)$$

$$R_O := 293.2500000$$

Homework Set 3 HW#3 - 3-68, 3-122, 3-138 Christopher Allred A02233404

3. (c) Draw shear-force and bending-moment diagrams for the shaft. If needed, make one set for the horizontal plane and another set for the vertical plane.



(d) At the point of maximum bending moment, determine the bending stress and the torsional shear

#max bending moment

$$sigma = \frac{Mc}{Iota}$$

$$\sigma = \frac{Mc}{I}$$

$$sigma := \frac{32 \cdot M}{Pi \cdot d^3}$$

$$\sigma := \frac{32 M}{\pi d^3} \qquad \text{# find torshinal Shear}$$

$$\tan = \frac{T \cdot r}{J}$$

$$tau = \frac{T \cdot r}{I}$$

$$d := 1.25$$

$$d := 1.25$$

$$\tau = \frac{Tr}{T}$$

$$M := 2932.5$$

$$M := 2932.5$$

$$M := 2932.5$$
 $T := (500 - 75) \cdot 4$ $T := 1700$

$$T := 1700$$

$$sigma := \frac{32 \cdot M}{Pi \cdot d^3}$$

$$tau := \frac{16 \cdot T}{\text{Pi} \cdot d^3}$$

$$\sigma := 15293.54225$$

$$\tau := 4432.910798$$

5. (e) At the point of maximum bending moment, determine the principal stresses and the maximum

#Princeible stresses

$$\operatorname{sigma}[1] := \frac{\operatorname{sigma}[x]}{2} + \operatorname{sqrt}\left(\left(\frac{\operatorname{(sigma}[x])}{2}\right)^{2} + \tan[xy]^{2}\right)$$
$$\sigma_{1} := 16485.53839$$

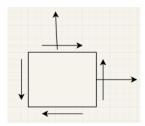
$$\operatorname{sigma}[3] := \frac{\operatorname{sigma}[x]}{2} - \operatorname{sqrt}\left(\left(\frac{(\operatorname{sigma}[x])}{2}\right)^{2} + \tan[xy]^{2}\right)$$
$$\sigma_{3} := -1191.996141$$

$$sigma[\,2\,] \coloneqq 0$$

$$\sigma_2 := 0$$

$$tau[max] := \frac{sigma[1] - sigma[2]}{2}$$

$$\tau_{\text{max}} := 8242.769195$$



3-122 The steel eyebolt shown in the figure is loaded with a force F 5 300 N. The bolt is formed from wire of diameter d 5 6 mm to a radius R_i 5 10 mm in the eye and at the shank. Estimate the stresses at the inner and outer surfaces at section A–A.

$$d := 6$$

$$d := 6$$

$$F := 300$$

$$F := 300$$

$$R := 10$$

$$R := 10$$

$$r[In] := 10$$

$$r_{In} := 10$$

$$r[out] := 16$$

$$r_{out} := 16$$

$$r[centr] := r[In] + \frac{d}{2}$$

$$r_{centr} := 13$$

$$r[nut] := evalf \left(\left(\frac{d}{2} \right)^2 \middle/ \left(2 \cdot \left(r[centr] \right) - \operatorname{sqrt} \left(\left(r[centr] \right)^2 - \left(\frac{d}{2} \right)^2 \right) \right) \right) \right)$$

$$r_{nut} := 12.82455529$$

$$A := evalf\left(\frac{\text{Pi}}{4}d^2\right)$$
$$A := 28.27433389$$

$$e := r[centr] - r[nut]$$

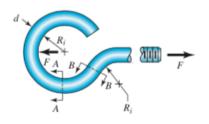
$$e := 0.17544471$$

$$C[o] := r[out] - r[nut]$$

$$C_o := 3.17544471$$

$$C[i] := r[nut] - r[In]$$

$$C_i := 2.82455529$$



 $M := 300 \cdot 13$

$$M := 3900$$

$$\sigma_o := 260.2631645$$

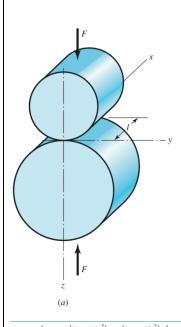
$$sigma[i] := \frac{F}{A} + \frac{M \cdot C[i]}{A \cdot e \cdot r[In]}$$

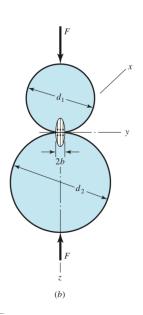
$$\sigma_i := 232.6763077$$

$$\operatorname{sigma}[o] := \frac{F}{A} - \frac{M \cdot C[o]}{A \cdot e \cdot r[out]}$$

$$\sigma_o := -145.4226924$$

3-138 An aluminum alloy cylindrical roller with diameter 1.25 in and length 2 in rolls on the inside of a cast-iron ring having an inside radius of 6 in, which is 2 in thick. Find the maximum contact force F that can be used if the shear stress is not to exceed 4000 psi.





$$d[1] \quad d[2]$$

$$b := \sqrt{2} \qquad F\left(\frac{-v_1^2 + 1}{E_1} + \frac{-v_2^2 + 1}{E_2}\right)$$

$$F := 4000$$

$$L := 2 \# in$$

$$L := 2$$

$$nu[1] := .333 \# AI$$

$$v_1 := 0.333$$

$$nu[2] := .211 \# cast iron$$

$$E[1] := 10.4 \cdot 10^6$$

$$E_1 := 1.04000000 10^7$$

$$E[2] := 14.5 \cdot 10^6$$

$$E_2 := 1.45000000 10^7$$

$$d[1] := 1.25$$

$$d[2] := 6 \cdot 2$$

$$d_2 := 12$$

$$evaly(b)$$

$$0.0002593045282 \sqrt{F}$$

$$solve\left(P = \frac{2 F}{Pi \cdot b \cdot L}, F\right)$$

$$\frac{112.7404749}{3}$$

$$\frac{375.8015830}{375.8015830}$$

$$\frac{112.7404749}{322}$$

$$\frac{350.1256984}{322} \left(\frac{4000}{.322}\right)^2$$

$$1.543150342 10^8$$

$$b = \sqrt{\frac{2F}{\pi l} \frac{(1 - \nu_1^2)/E_1 + (1 - \nu_2^2)/E_2}{1/d_1 + 1/d_2}}$$

The maximum pressure is

$$p_{\max} = \frac{2F}{\pi bl}$$

$$\sigma_x = -2\nu p_{\text{max}} \left(\sqrt{1 + \frac{z^2}{b^2}} - \left| \frac{z}{b} \right| \right)$$
 (3-75)

$$\sigma_{y} = -p_{\text{max}} \left(\frac{1 + 2\frac{z^{2}}{b^{2}}}{\sqrt{1 + \frac{z^{2}}{b^{2}}}} - 2\left| \frac{z}{b} \right| \right)$$
 (3-76)

$$\sigma_3 = \sigma_z = \frac{-p_{\text{max}}}{\sqrt{1 + z^2/b^2}}$$
 (3–77)