

4 Electromagnetic waves in material

Let's let everything move!

4.1 Displacement current

Conservation of charge

$$\nabla \cdot \mathbf{J}_s = -\frac{\partial \rho_f}{\partial t}$$

However, this is incompatible with

$$\nabla \times \mathbf{H} = \mathbf{J}_f$$

Lets take the divergence for both sides, we get

$$\nabla \cdot (\nabla \times \mathbf{H}) = 0 = \nabla \cdot \mathbf{J} + \underbrace{\frac{\partial}{\partial t} \nabla \cdot \mathbf{D}}_{\rho_f}$$

\Rightarrow add an additional term to the current density $\mathbf{J}_f = \nabla \times \mathbf{H}$

$$\Rightarrow \nabla \times \mathbf{H} = \mathbf{J}_f + \underbrace{\frac{\partial \mathbf{D}}{\partial t}}_{\text{displacement current}}$$

$$\text{LHS: } \nabla \times \left(\frac{\mathbf{B}}{\mu_0} - \mathbf{M} \right) = \frac{1}{\mu_0} \nabla \times \mathbf{B} - \underbrace{\nabla \times \mathbf{M}}_{\mathbf{J}_b}$$

Where \mathbf{J}_b is the bound current density.

$$\text{RHS} = \mathbf{J}_s + \frac{\partial \mathbf{D}}{\partial t} = \mathbf{J}_s + \frac{\partial \mathbf{P}}{\partial t} + \epsilon_0 \frac{\partial \mathbf{E}}{\partial t}$$

$$\Rightarrow \text{we could write } \nabla \times \mathbf{B} = \mu_0 (\mathbf{J}_f + \mathbf{J}_b + \mathbf{J}_p) + \mu_0 \epsilon_0 \frac{\partial \mathbf{E}}{\partial t}$$

where \mathbf{J}_p is the polarization current density. which equals $\frac{\partial \mathbf{P}}{\partial t}$

Note that $\nabla \cdot \mathbf{J}_p = -\frac{\partial \rho_p}{\partial t}$ from conservation of charge.

Thus the polarization current responds to changes to bound charge, and hence in \mathbf{P}

4.2 Maxwell's equations in insulating linear dielectrics

Since it is insulating linear dielectrics, we have $\mathbf{J}_f = 0$ and $\mathbf{J}_b = 0$

Hence, we could get Maxwell's equation

$$\nabla \cdot \mathbf{D} = 0 \quad \nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$

$$\nabla \cdot \mathbf{B} = 0 \quad \nabla \times \mathbf{H} = \frac{\partial \mathbf{D}}{\partial t}$$

remember, $\mathbf{D} = \epsilon_0 \epsilon_r \mathbf{E} + \mathbf{P}$ and $\mathbf{B} = \mu_0 \mu_r \mathbf{H}$

which gives

$$\nabla \cdot \mathbf{E} = 0 \quad \nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$

$$\nabla \cdot \mathbf{B} = 0 \quad \nabla \times \mathbf{B} = \mu_0 \mu_r \epsilon_0 \epsilon_r \frac{\partial \mathbf{E}}{\partial t}$$

Consider

$$\begin{aligned} \nabla \times (\nabla \times \mathbf{E}) &= \nabla(\nabla \cdot \mathbf{E}) - \nabla^2 \mathbf{E} = -\frac{\partial}{\partial t} \nabla \times \mathbf{B} \\ \Rightarrow \nabla^2 \mathbf{E} &= \underbrace{\mu_0 \mu_r \epsilon_0 \epsilon_r}_{\frac{1}{v^2}} \frac{\partial^2 \mathbf{E}}{\partial t^2} \end{aligned}$$

which is wave equation.

$$\Rightarrow v = \frac{c}{n} \text{ where } c = \frac{1}{\sqrt{\epsilon_0 \mu_0}} \text{ and } n = \sqrt{\epsilon_r \mu_r} \text{ where } n \text{ is also called } \textit{refractive index}$$

Plane waves solutions

Lets choose propagation parallel to z, and hence

$$\frac{\partial \Psi}{\partial x} = \frac{\partial \Psi}{\partial y} = 0$$

$$\text{remember that } \nabla \cdot \mathbf{E} = 0 \Rightarrow \frac{\partial E_z}{\partial z} = 0$$

$$\text{similarly, } \nabla \cdot \mathbf{B} = 0 \Rightarrow \frac{\partial B_z}{\partial z} = 0$$

$$\text{we also have } \nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t} \Rightarrow \frac{\partial B_z}{\partial t} = 0$$

$$\text{And } \nabla \times \mathbf{B} = \mu_0 \mu_r \epsilon_0 \epsilon_r \frac{\partial \mathbf{E}}{\partial t} \Rightarrow \frac{\partial E_z}{\partial t} = 0$$

Hence, E_z and B_z are constant in z and t, they are not part of wave motion

now analyze the x,y components of curl:

$$-\frac{\partial E_y}{\partial z} = -\frac{\partial B_x}{\partial t}, -\frac{\partial B_y}{\partial z} = \frac{1}{v^2} \frac{\partial E_x}{\partial t}$$

$$\Rightarrow E_x, B_y \text{ are solutions}$$

Lets then take

$$\begin{aligned} \frac{\partial^2 E_x}{\partial t^2} &= \frac{1}{v^2} \frac{\partial^2 E_x}{\partial t^2} \\ \Rightarrow E_x(z, t) &= E_{x0} e^{i(\pm kz - \omega t)} \hat{\mathbf{x}} \end{aligned}$$

Then, we could have

$$\Rightarrow B(z, t) = B_0 e^{i(\pm kz - \omega t)} \hat{\mathbf{y}}$$

And then we could get the wave travelling in $\pm \mathbf{z}$ direction

$$\begin{aligned}\Rightarrow \mp k E_0 &= -\omega B_0 \\ \text{and } \pm k B_0 &= \frac{\omega}{v^2} E_0 \\ \Rightarrow \frac{E_0}{B_0} &= \pm \frac{\omega}{k} = \pm v\end{aligned}$$

Define Impedance Z as

$$Z = \left| \frac{E_0}{H_0} \right| = \sqrt{\frac{\mu_0 \mu_r}{\epsilon_0 \epsilon_r}}$$

remember that $H_0 = \frac{B_0}{\mu_0 \mu_r}$

The motivation of doing so is that $v = -\int \mathbf{E} \cdot d\mathbf{l}$ and $I = \oint \mathbf{H} \cdot d\mathbf{l}$

So dimension would work

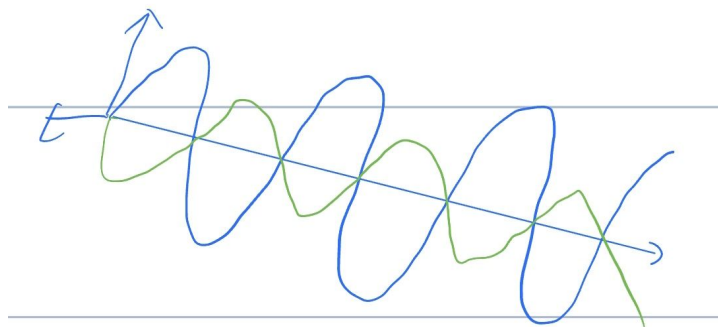
For free space, then, $\epsilon_r = \mu_r = 1$ and $Z = \sqrt{\frac{\mu_0}{\epsilon_0}} = 377\Omega$

Remember that $\nabla \times \mathbf{E} = -\dot{\mathbf{B}}$, and use $E, B \propto e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)}$, we could get

$$\begin{aligned}i\mathbf{k} \times \mathbf{E} &= -(-i\omega)\mathbf{B} \\ &= i\omega\mu_0\mu_r\mathbf{H} \\ \Rightarrow z &= \left| \frac{\mathbf{E}}{\mathbf{H}} \right| = \sqrt{\frac{\mu_0\mu_r\omega}{k}}\end{aligned}$$

Which gives the same answer because $v = \frac{c}{n} = \frac{\omega}{k} = \frac{1}{\sqrt{\epsilon_0\epsilon_r\mu_0\mu_r}}$

which is this wave



4.3 conductors

Remember that

$$\nabla \cdot \mathbf{J}_f = -\frac{\partial \rho_f}{\partial t}$$

$$\nabla \cdot \mathbf{J}_p = -\frac{\partial \rho_p}{\partial t}$$

$$\nabla \cdot \mathbf{J}_b = 0$$

The last one is 0 because $\nabla \cdot (\nabla \times \mathbf{M}) = 0$

For conductors, we have

$\rho_f = 0$ since there are no free charges in equilibrium
 $\mathbf{J}_f = \sigma \mathbf{E}$ from Ohm's law where σ is the conductivity
 $\mathbf{D} = \epsilon_0 \epsilon_r \mathbf{E}$ and $\mathbf{B} = \mu_0 \mu_r \mathbf{H}$ from linearity

Then we could get Maxwell's equation in conductors

$$\begin{aligned}\nabla \cdot \mathbf{E} &= 0 & \nabla \times \mathbf{E} &= -\frac{\partial \mathbf{B}}{\partial t} \\ \nabla \cdot \mathbf{B} &= 0 & \nabla \times \mathbf{B} &= \underbrace{\mu_0 \mu_r \sigma \mathbf{E}}_{\text{conduction } \mathbf{J}} + \underbrace{\mu_0 \mu_r \sigma_0 \sigma_r \frac{\partial \mathbf{E}}{\partial t}}_{\text{displacement } \mathbf{J}}\end{aligned}$$

Free charge will decay to zero in a short time τ , and it is easy to prove (said Blundell)

$$\nabla \cdot \mathbf{J} = \frac{\partial \rho}{\partial t}$$

Where $\nabla \cdot \mathbf{J}$ is equal to $\sigma \cdot \nabla \cdot \mathbf{E}$ from Ohm's law

and $\nabla \cdot \mathbf{E}$ is equal to $\frac{\rho}{\epsilon_0 \epsilon_r}$ from Gauss's law

$$\Rightarrow \rho(f) = \rho(0) e^{-\frac{t}{\tau}}$$

$$\text{Where } \tau = \frac{\epsilon_0 \epsilon_r}{\sigma}$$

If the metal has great conductivity, then τ is very small, and hence $\rho(f)$ is very small.

Let's consider the electromagnetic wave having frequency ω , so we would like to compare $\frac{1}{\omega}$ with τ :

Condition	Conductor Type	Charge Response	Conductivity
$\omega\tau \ll 1$	Good conductor	Charges respond very quickly	$\sigma \gg \epsilon_0 \epsilon_r \omega$ Conduction current dominates
$\omega\tau \gg 1$	Bad conductor	Charges respond very slowly	$\sigma \ll \epsilon_0 \epsilon_r \omega$ Displacement current dominates

Take real life examples

	$\sigma(\Omega m)$	ϵ_r	$\frac{\sigma}{\epsilon_0 \epsilon_r} (S^{-1})$
metal	10^7	1	10^{19}
Silicon	$4 \cdot 10^{-4}$	11.7	10^7
Glass	10^{-10}	5	10

Note that visible light would have frequency $\sim 5 \cdot 10^{14}$ Hz

Let's now do some electromagnetism

$$\begin{aligned}
\nabla \times (\nabla \times \mathbf{E}) &= \underbrace{\nabla(\nabla \cdot \mathbf{E})}_0 - \nabla^2 \mathbf{E} \\
&= -\frac{\partial}{\partial t} \nabla \times \mathbf{B} \\
\nabla^2 \mathbf{E} &= \mu_0 \mu_r \sigma \frac{\partial \mathbf{E}}{\partial t} + \mu_0 \mu_r \epsilon_0 \sigma_r \frac{\partial^2 \mathbf{E}}{\partial t^2}
\end{aligned}$$

Again, this would yield transverse plane waves with $\mathbf{E}, \mathbf{B} \perp$ to each others

$$\Rightarrow \mathbf{E} = \mathbf{E}_0 \hat{\mathbf{x}} e^{i(\tilde{\mathbf{k}} \cdot \mathbf{z} - \omega t)}$$

$$\text{with } \tilde{\mathbf{k}} = \mathbf{k} + i\kappa$$

$$\Rightarrow \tilde{k}^2 = \underbrace{i\mu_0 \mu_r \sigma \omega}_{\mu} + \underbrace{\mu_0 \mu_r \epsilon_0 \epsilon_r \omega^2}_{\mu \epsilon}$$

$$(k + i\kappa)^2 = k^2 - \kappa^2 + 2ik\kappa$$

$$k^2 - \kappa^2 = \mu_0 \epsilon_0 \omega^2$$

$$2k\kappa = \mu\sigma\omega \Rightarrow k = \frac{\mu\sigma\omega}{2\kappa}$$

$$0 = \left(\frac{\mu\sigma\omega}{2}\right)^2 \frac{1}{k^2} - k^2 - \mu\epsilon_0\omega^2$$

$$0 = (k^2)^2 + \mu\epsilon\omega^2(k^2) - \left(\frac{\mu\sigma\omega}{2}\right)^2$$

$$\kappa^2 = -\frac{\mu\epsilon\omega^2}{2} \pm \sqrt{\left(\frac{\mu\epsilon\omega^2}{2}\right)^2 + \left(\frac{\mu\sigma\omega}{2}\right)^2}$$

$$\kappa^2 = \frac{\mu\epsilon\omega^2}{2} \left[\pm \sqrt{1 + \left(\frac{\sigma}{\epsilon\omega}\right)^2} - 1 \right]$$

Taking the positive root

$$\Rightarrow \kappa = \sqrt{\frac{\mu\epsilon}{2}} \omega \sqrt{\sqrt{1 + \left(\frac{\sigma}{\epsilon\omega}\right)^2} - 1}$$

Sub into original equation

$$k = \frac{\mu\sigma\omega}{2\kappa} = \sqrt{\frac{\mu\epsilon}{2}} \omega \sqrt{\sqrt{1 + \left(\frac{\sigma}{\epsilon\omega}\right)^2} + 1}$$

$$\Rightarrow \mathbf{E} = \mathbf{E}_0 \hat{\mathbf{x}} \underbrace{e^{-\kappa z}}_{e^{-\frac{z}{\delta}}} e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)}$$

Where $\delta = \frac{1}{\kappa}$ is the *skin depth*

Reminder: Good conductors have $\sigma \gg \epsilon\omega$

$$k = \kappa = \sqrt{\frac{\mu\epsilon}{2}} \omega \sqrt{\frac{\sigma}{\epsilon\omega}} = \sqrt{\frac{\mu\omega\sigma}{2}}$$

We could therefore have

$$\nabla^2 \mathbf{E} = \mu\sigma \frac{\partial \mathbf{E}}{\partial t} + \mu\epsilon \frac{\partial^2 \mathbf{E}}{\partial t^2}$$

We could also neglect the last term, since $\frac{\partial^2 \mathbf{E}}{\partial t^2} \ll \frac{\partial \mathbf{E}}{\partial t}$

$$\begin{aligned}\Rightarrow \tilde{k}^2 &= i\mu\sigma\omega \\ \Rightarrow \tilde{k} &= \frac{1+i}{\sqrt{2}} \sqrt{\mu\sigma\omega} \\ \Rightarrow \tilde{k} &= \kappa = \sqrt{\frac{\mu\sigma\omega}{2}}\end{aligned}$$

Hence, we could have

$$\delta = \frac{1}{k} = \sqrt{\frac{2}{\mu\sigma\omega}}$$

For a typical metal, δ is

$$\begin{cases} \text{few nm - visible light} \\ \text{few } \mu\text{m} - \text{microwave} \\ \text{few mm - radio waves} \end{cases}$$

Lets go to poor conductors

Poor conductors has $\sigma \ll \epsilon\omega$, hence

$$\begin{aligned}k &\approx \sqrt{\frac{\mu\epsilon}{2}}\omega\sqrt{2} = \sqrt{\mu\epsilon}\omega \\ \kappa &= \sqrt{\frac{\mu\epsilon}{2}}\omega \left(1 + \frac{1}{2}\left(\frac{\sigma}{\epsilon\omega}\right)^2 + \dots - 1\right)^{\frac{1}{2}}\end{aligned}$$

which equals to $\frac{\sigma}{2}\sqrt{\frac{\mu}{\epsilon}}$ which is independent to ω

In an insulating dielectric, $\sigma = 0$, hence $\kappa = 0$, and hence $k = \frac{\omega}{v}$ as expected.

Lets return to previous equation

Lets consider the curl equation in the conductor

$$\begin{aligned}\frac{\partial \mathbf{E}_x}{\partial z} &= \frac{\partial B_y}{\partial t} \\ i(k + \kappa)\mathbf{E}_0 &= i\omega\mathbf{B}_0 \\ z = \frac{\mu E_0}{B_0} &= \frac{\mu\omega}{k + i\kappa} \\ \tilde{k} &= \frac{\mu\omega}{\sqrt{k^2 + \kappa^2}} e^{i\phi}\end{aligned}$$

If we expand, ϕ would be

$$\phi = \tan^{-1} \left(\frac{\sqrt{1+(Q/\epsilon\omega)^2}-1}{\sqrt{1+(Q/\epsilon\omega)^2}+1} \right)^{\frac{1}{2}}$$

For a good conductor, $\sigma \gg \epsilon\omega$, hence $\phi \rightarrow \tan^{-1} 1 = \frac{\pi}{4}$

So this means that B lags behind E in a metal

Poyting vectors

Work done on charge

$$\begin{aligned}\delta q &= \rho \delta\tau \\ \delta F &= \delta q(\mathbf{E} + \mathbf{V} \times \mathbf{B}) \\ \delta \mathbf{F} \cdot d\mathbf{l} &= \delta q(\mathbf{E} + \mathbf{V} \times \mathbf{B}) \cdot \mathbf{v} \delta t \\ &= \mathbf{E} \cdot \mathbf{J}_f \delta\tau \delta t\end{aligned}$$

where \mathbf{J}_f equals to $\rho\mathbf{v}$

Rate of work on charges

$$\begin{aligned}\mathbf{F} &= \frac{dw}{dt} \\ &= \mathbf{E} \cdot \mathbf{J}_f d\tau \\ &= \frac{d}{dt} \int \underbrace{u_{mech}}_{\text{Energy density}} d\tau\end{aligned}$$

From Maxwell's equation:

$$\mathbf{J}_f = \nabla \times \mathbf{H} - \frac{\partial \mathbf{D}}{\partial t}$$

We have

$$\mathbf{E} \cdot \mathbf{J}_f = \mathbf{E} \cdot \nabla \times \mathbf{H} - \mathbf{E} \cdot \frac{\partial \mathbf{D}}{\partial t}$$

By dotting everything, and then

$$\begin{aligned}\nabla \cdot (\mathbf{E} \times \mathbf{H}) &= \mathbf{H} \cdot \nabla \times \mathbf{E} - \mathbf{E} \cdot \nabla \times \mathbf{H} \\ \mathbf{E} \cdot \mathbf{J}_f &= \mathbf{H} \cdot \underbrace{\nabla \times \mathbf{E}}_{-\frac{\partial \mathbf{B}}{\partial t}} - \mathbf{E} \cdot \frac{\partial \mathbf{D}}{\partial t} - \nabla \cdot (\mathbf{E} \times \mathbf{H})\end{aligned}$$

Where we call $\mathbf{H} \cdot \underbrace{\nabla \times \mathbf{E}}_{-\frac{\partial \mathbf{B}}{\partial t}} - \mathbf{E} \cdot \frac{\partial \mathbf{D}}{\partial t}$ " $\frac{\partial}{\partial t} u_{EM}$ " (remember that

$u_{EM} = \frac{1}{2}(\mathbf{B} \cdot \mathbf{H} + \mathbf{E} \cdot \mathbf{D})$ which equals to Energy stored in EM field per unit volume) and $\nabla \cdot (\mathbf{E} \times \mathbf{H})$ as " $\mathbf{S} = \mathbf{E} \times \mathbf{H}$ " or Poynting vector.

How is this working?

Assume that we are using a linear media:

$$\begin{aligned}\mathbf{E} \cdot \frac{\partial \mathbf{D}}{\partial t} &= \frac{1}{2} \mathbf{E} \cdot \frac{\partial (\mathbf{E} \cdot \mathbf{D})}{\partial t} \\ \mathbf{H} \cdot \frac{\partial \mathbf{B}}{\partial t} &= \frac{1}{2} \mathbf{H} \cdot \frac{\partial (\mathbf{B} \cdot \mathbf{H})}{\partial t}\end{aligned}$$

Remember that

$$\left. \begin{aligned}\frac{1}{2} \epsilon_0 E^2 &= \frac{1}{2} \mathbf{E} \cdot \mathbf{D} \\ \frac{B^2}{2\mu_0} &= \frac{1}{2} \mathbf{B} \cdot \mathbf{H}\end{aligned} \right\} \text{In free space}$$

Bringing everything together, we could get

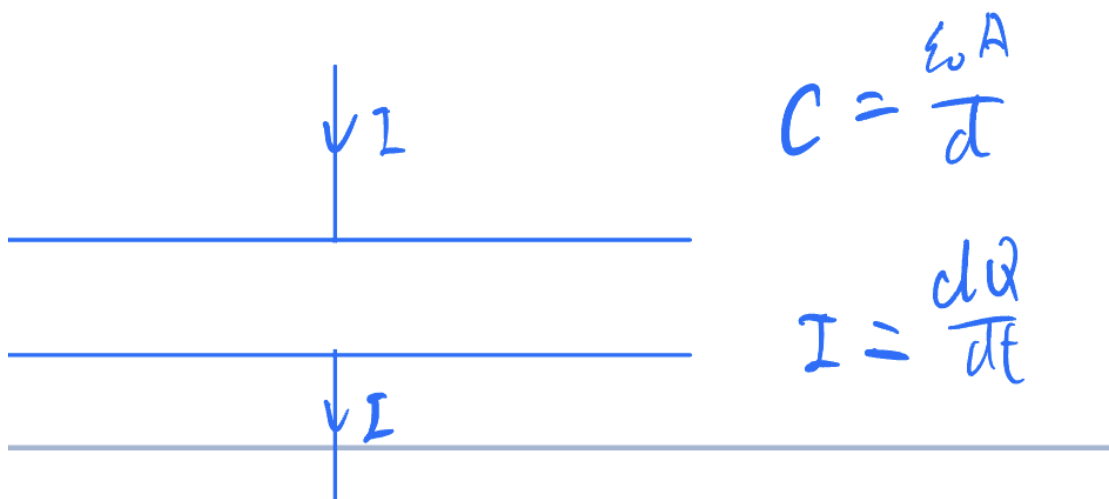
$$\Rightarrow \frac{d}{dt} (u_{mech} + u_{EM}) + \nabla \cdot \mathbf{S} = 0$$

Where \mathbf{S} is the Poynting vector, or equivalently,

$$\frac{d}{dt} \int (u_{mech} + u_{EM}) d\tau + \oint \mathbf{S} \cdot d\mathbf{a} = 0$$

We could say that, therefore \mathbf{S} is the energy flux density, or the rate of flow of energy per unit area in the direction of \mathbf{S} .

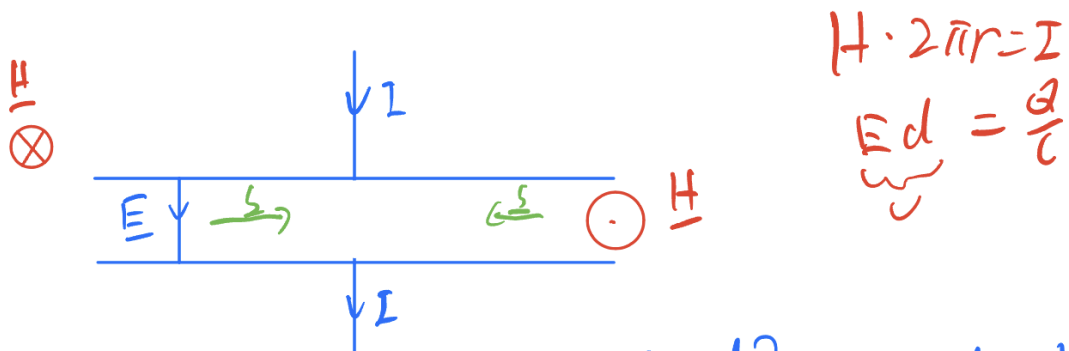
Example: a capacitor



The stored energy increase at rate

$$\dot{U} = \frac{Q}{C} \frac{dQ}{dt} \quad U = \frac{Q^2}{2C}$$

also:

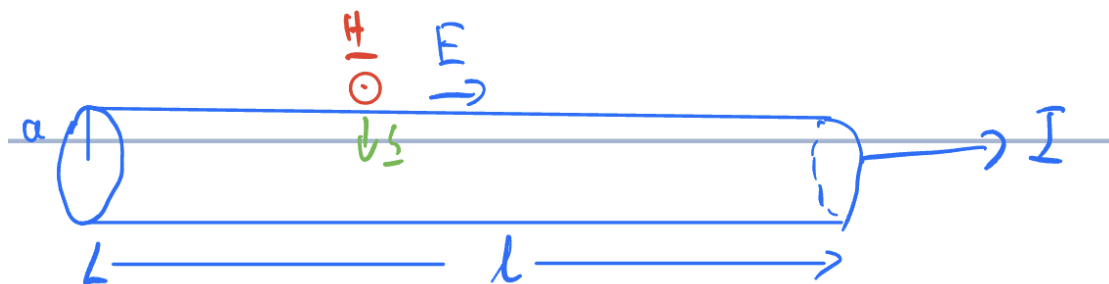


Hence, we have

$$\dot{U} = S \cdot 2\pi r d = \frac{Q}{c} \frac{dQ}{dt}$$

$$\text{where } S = EH = \frac{Q}{dc} \frac{dQ}{dt} \frac{1}{2\pi r}$$

There is another example



$$H \cdot S\pi a = I$$

$$E = \frac{V}{l}$$

$$\Rightarrow S = \frac{V}{l} \frac{I}{2\pi a}$$

$$\int \mathbf{S} \cdot d\mathbf{a} = -IV = -I^2 R$$

4.5 Radiation pressure

EM waves are made up of photons, and hence they have momentum

$$E = pc$$

\Rightarrow Transport of energy is appointed by transport of momentum

$$P_{rad} = \frac{\langle S \rangle}{c}$$

For a perfect absorber, where P_{rad} is the radiation pressure

Example For a plane EM wave in free space, we have

$$U = \frac{1}{2}\epsilon_0 E^2 + \frac{1}{2}\frac{B^2}{\mu_0}$$

$$\text{but } E = cB$$

$$\Rightarrow U = \epsilon_0 E^2$$

$$\mathbf{E} = \frac{1}{2}E_0 \cos(kz - \omega t)\hat{\mathbf{x}}$$

$$= E_0 \cos^2(kz - \omega t)$$

$$\langle E^2 \rangle = \frac{1}{2}E_0^2$$

$$\Rightarrow \langle u \rangle = \frac{1}{2}\epsilon_0 E_0^2$$

$$\langle S \rangle = \frac{1}{2}\epsilon_0 E_0^2 c = I$$

Where I is the intensity of wave

$$\Rightarrow P_{rad} = \begin{cases} \frac{1}{2}\epsilon_0 E_0^2 & \text{perfect absorber} \\ \epsilon_0 E_0^2 & \text{perfect reflector} \end{cases}$$

Sunlight: $I \sim 1 \text{ kW m}^{-2}$

$$\Rightarrow P_{rad} = 10^{-5} \text{ Pa}$$

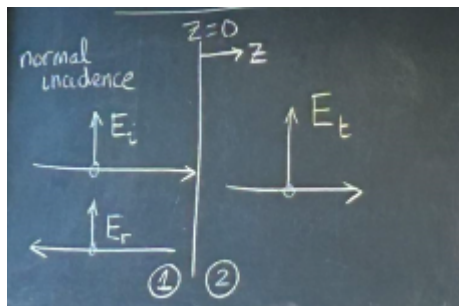
$$\text{FYI, } P_{atm} = 10^5 \text{ Pa}$$

Example Consider a star which is growing by accretion

i.e. matter is falling onto it uniformly in all directions

The star has luminosity L

4.6 EM waves - reflection and refraction



Left:

$$E_i e^{i(k_1 x - \omega t)} + E_r e^{i(-k_1 x - \omega t)}$$

Right:

$$E_t e^{i(k_2 x - \omega t)}$$

Using electrom boundary conditions, we could get

E_{\parallel} is continuous

$$E_i^{\parallel} + E_r^{\parallel} = E_t^{\parallel}$$

H^{\parallel} is continuous

$$\frac{E_i}{Z_1} - \frac{E_r}{Z_1} = \frac{E_t}{Z_2}$$

Putting two equations together

$$\frac{E_r}{E_i} = \frac{Z_2 - Z_1}{Z_2 + Z_1} \quad \frac{E_t}{E_i} = \frac{2Z_2}{Z_2 + Z_1}$$

Where $Z = \sqrt{\frac{\mu}{\epsilon}}$

$$|\text{Poyting vector}| = S = |\mathbf{E} \times \mathbf{H}| = \frac{E^2}{Z}$$

$$\text{We expect } S_{\text{incident}} = S_{\text{reflected}} + S_{\text{transmitted}}$$

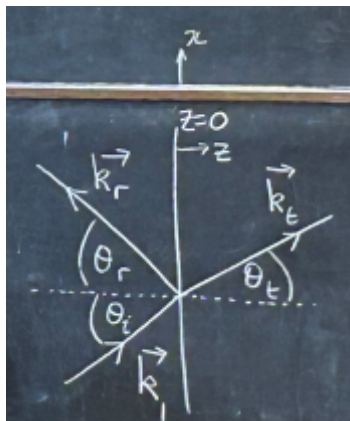
Where they equal to

$$\frac{E_i^2}{Z_1} + \frac{E_r^2}{Z_1} = \frac{E_t^2}{Z_2}$$

separately

Lets now have angles

$$E_r e^{i(\mathbf{k}_r \cdot \mathbf{r} - \omega t)}$$



$$\mathbf{E}_i e^{i(\mathbf{k}_i \cdot \mathbf{r} - \omega t)}$$

$$E_t e^{i(\mathbf{k}_t \cdot \mathbf{r} - \omega t)}$$

Choose \mathbf{k}_i in x-z plane

At $z = 0$, E_{\parallel} is continuous and this holds for all x y and t

$\Rightarrow \omega$ must be the same

$$\Rightarrow \mathbf{k}_i \cdot \mathbf{r} = \mathbf{k}_r \cdot \mathbf{r} = \mathbf{k}_t \cdot \mathbf{r} \text{ for all x, y at } z=0$$

Take $\mathbf{r} = (0, y, 0)$

$$\Rightarrow \mathbf{k}_i, \mathbf{k}_r \text{ and } \mathbf{k}_t \text{ all lie in the xz plane}$$

(the plane of incidence)

Take $\mathbf{r} = (x, 0, 0)$ so $\mathbf{k}_i \cdot \mathbf{r} = k \sin \theta_x$

$$\begin{aligned}
 |\mathbf{k}_i| &= |\mathbf{k}_r| = k_1 \\
 |\mathbf{k}_t| &= k_2 \\
 \Rightarrow \underbrace{k_1 \sin \theta_i = k_1 \sin \theta_r = k_2 \sin \theta_t}_{\theta_i = \theta_r, \text{ law of reflection}}
 \end{aligned}$$

Remember that $\frac{\omega}{k} = \frac{c}{n}$, And the last two would lead to

$$\frac{\sin \theta_t}{\sin \theta_i} = \frac{k_1}{k_2} = \frac{n_2}{n_1} \text{ -law of refraction, or snell's law}$$

$$\text{Where } n = \sqrt{\epsilon_r \mu_r}$$

Fresnel equations

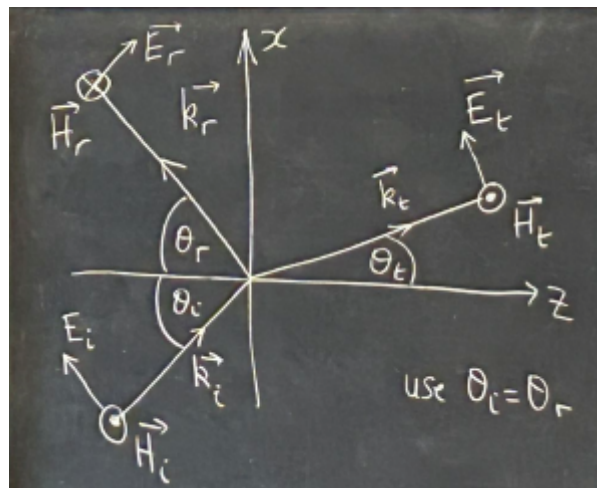
Worrying about polarization directions

We work in those steps

1. \mathbf{E} in the plane of incidence

"parallel-like" = parallel

Remind that \mathbf{E} , \mathbf{H} and \mathbf{k} form a right-handed system



	incident	reflected	transmitted
E_x	$E_i \cos \theta_i$	$E_r \cos \theta_r$	$E_t \cos \theta_t$
E_z	$-E_i \sin \theta_i$	$E_r \cos \theta_r$	$-E_t \sin \theta_t$
H_y	$\frac{E_i}{Z_1}$	$-\frac{E_r}{Z_1}$	$\frac{E_t}{Z_2}$

$$E_{\parallel} \text{ continuous} \Rightarrow E_x \text{ continuous} \Rightarrow E_i \cos \theta_i + E_r \cos \theta_i = E_t \cos \theta_t$$

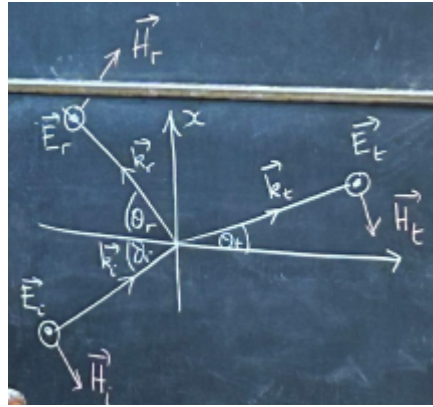
$$\frac{E_r}{E_i} = \frac{Z_2 \cos \theta_t - Z_1 \cos \theta_i}{Z_2 \cos \theta_i + Z_1 \cos \theta_t}$$

$$\frac{E_t}{E_i} = \frac{2Z_2 \cos \theta_i}{Z_2 \cos \theta_i + Z_1 \cos \theta_t}$$

Now look for Fresnel equations for p-polarizations

2. \mathbf{E} perpendicular to the plane of incidence

"s-like" s = senkrecht = perpendicular



	incident	reflected	transmitted
E_y	E_i	E_r	E_t
H_x	$-\frac{E_i}{Z_1} \cos \theta_i$	$\frac{E_r}{Z_1} \cos \theta_r$	$-\frac{E_t}{Z_2} \cos \theta_t$
H_z	$\frac{E_i}{Z_1} \sin \theta_i$	$\frac{E_r}{Z_1} \sin \theta_r$	$\frac{E_t}{Z_2} \sin \theta_t$

E_{\parallel} continuous

$$\Rightarrow E_y \text{ continuous} \quad E_i + E_r = E_t$$

H_{\parallel} continuous

$$\Rightarrow H_x \text{ continuous} \quad -\frac{E_i}{Z_1} \cos \theta_i + \frac{E_r}{Z_1} \cos \theta_r = -\frac{E_t}{Z_2} \cos \theta_t$$

Remember that

$$Z = \sqrt{\frac{\mu_r \mu_0}{\epsilon_r \epsilon_0}} = \frac{Z_0}{n} \quad n = \sqrt{\epsilon_r} \text{ while } \mu_r = 1$$

Let's set $\mu_r = 1$

$$\text{Then, } Z = \sqrt{\frac{\mu_r \mu_0}{\epsilon_r \epsilon_0}} = \frac{Z_0}{n} \quad n = \sqrt{\epsilon_r}$$

So we can replace Z_i with $\frac{1}{n_i}$ in expressions involving ratios of Z's.

e.g. Fresnel equations for p-polarization

$$r = \frac{E_r}{E_i} = \frac{\frac{1}{n_2} \cos \theta_t - \frac{1}{n_1} \cos \theta_i}{\frac{1}{n_2} \cos \theta_t + \frac{1}{n_1} \cos \theta_i}$$

$$= \frac{n_1 \cos \theta_t - n_2 \cos \theta_i}{n_1 \cos \theta_t + n_2 \cos \theta_i}$$

Use Snell's law

$$n_1 \sin \theta_i = n_2 \sin \theta_t$$

$$\Rightarrow r = \frac{\sin 2\theta_t - \sin 2\theta_i}{\sin 2\theta_t + \sin 2\theta_i}$$

$$t = \frac{4 \sin \theta_t \cos \theta_i}{\sin 2\theta_t + \sin 2\theta_i}$$

For s-polarization, we have

$$r = \frac{\sin(\theta_t - \theta_i)}{\sin(\theta_t + \theta_i)}$$

$$t = \frac{2 \sin \theta_t \cos \theta_i}{\sin(\theta_t + \theta_i)}$$

We also have

$$n_1 \sin \theta_i = n_2 \sin \theta_t$$

$$\sin \theta_t = \frac{n_1}{n_2} \sin \theta_i$$

$$\cos \theta_t = \sqrt{1 - \sin^2 \theta_t} = \sqrt{1 - \frac{n_1^2}{n_2^2} \sin^2 \theta_i}$$

Fresnel equations:

/ $n_1 \cos \theta_i$ on top and bottom

$$\alpha = \frac{\cos \theta_t}{\cos \theta_i} = \frac{1}{\cos \theta_i} \sqrt{1 - \left(\frac{n_1}{n_2} \sin \theta_i\right)^2}$$

$$\beta = \frac{n_2}{n_1}$$

	$E^{\parallel}(\mathbf{p})$	$E^{\perp}(\mathbf{s})$
r	$\frac{\alpha - \beta}{\alpha + \beta}$	$\frac{1 - \alpha\beta}{1 + \alpha\beta}$
t	$\frac{2\alpha}{\alpha + \beta}$	$\frac{2}{1 + \alpha\beta}$

Remember, EM waves have an energy flux given by

$$\mathbf{S} = |\mathbf{E} \times \mathbf{H}| = \frac{E^2}{Z}$$

Intensify coefficients

$$T = \frac{I_r}{I_i} = |r|^2 = \begin{cases} \left(\frac{\alpha - \beta}{\alpha + \beta}\right)^2 & (p) \\ \left(\frac{1 - \alpha\beta}{1 + \alpha\beta}\right)^2 & (s) \end{cases}$$

$$T = \frac{I_t}{I_i} = |t|^2 \frac{n_2}{n_1} \frac{\cos \theta_t}{\cos \theta_i}$$

where $\frac{n_2}{n_1}$ is due to waves at different speeds. And $\frac{\cos \theta_t}{\cos \theta_i}$ is due to the wavefronts at different angles.

$$T = |t|^2 \alpha \beta = \begin{cases} \alpha \beta \left(\frac{2}{\alpha + \beta}\right)^2 & (p) \\ \alpha \beta \left(\frac{2}{1 + \alpha\beta}\right)^2 & (s) \end{cases}$$

Lets check in certain cases

- $\theta_i = 0 \Rightarrow \alpha = 1$

$$r_s = r_p = \frac{1 - \beta}{1 + \beta} = \frac{n_1 - n_2}{n_1 + n_2}$$

$$t_s = t_p = \frac{2}{1 + \beta} = \frac{2n_1}{n_1 + n_2}$$

$$R_s = R_p = \left(\frac{n_1 - n_2}{n_1 + n_2}\right)^2$$

$$T_s = T_p = \frac{n_2}{n_1} \frac{4n_1^2}{(n_1 + n_2)^2} = \frac{4n_1 n_2}{(n_1 + n_2)^2}$$

Example: air/glass interface

$$\begin{aligned}
 n_1 &= 1 & n_2 &= 1.5 \\
 r_s &= r_p = -0.2 \\
 T_s &= T_p = 0.8 \\
 R_s &= R_p = 0.04 \\
 T_s &= T_p = 0.96
 \end{aligned}$$

\Rightarrow 4% of light is reflected, 96% is transmitted

[If n_2 , for example, = 1.75, $R_s = R_p = 0.074$, which is a problem]

Lets take another go at different angle

- $\theta_i = 90^\circ$, and set $\beta > 1$

$$\begin{aligned}
 \sin \theta_i &= 1 & \cos \theta_i &= 0 \\
 \Rightarrow \alpha &\rightarrow \infty \\
 r_p &= 1 & r_s &= -1 \\
 t_p &= 0 & t_s &= 0
 \end{aligned}$$

- now consider $\beta < 1$, we can have total internal reflection for $\theta_i > \theta_c$ where θ_c is the critical angle = $\beta = \frac{n_2}{n_1}$

$$\text{At } \theta_c = \sin^{-1} \beta, \alpha = \frac{1}{\cos \theta_c} \sqrt{1 - \left(\frac{\sin \theta_c}{\beta}\right)^2} = 0$$

Hence, we have

$$\begin{aligned}
 r_p &= -1 & r_s &= 1 \\
 t_p &= \frac{2}{\beta} & t_s &= 2
 \end{aligned}$$

$$\sin \theta_c = \beta$$

r_p vanishes at the certain angle called "**Brewster's angle**" θ_B

$$r_p = \frac{\alpha - \beta}{\alpha + \beta} = 0 \text{ when } \alpha = \beta = \frac{n_2}{n_1}$$

$$\frac{1}{\cos \theta_B} \sqrt{1 - \left(\frac{\sin \theta_B}{\beta}\right)^2} = \beta$$

square both sides:

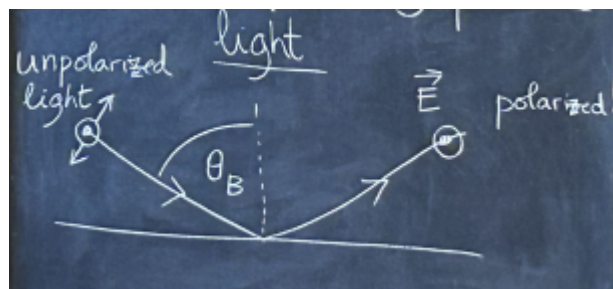
$$\sec^2 \theta_B - \frac{1}{\beta^2} \tan^2 \theta_B = \beta^2$$

$$\left(1 - \frac{1}{\beta^2}\right) \tan^2 \theta_B = \beta^2 - 1$$

$$\frac{(\beta^2 - 1)}{\beta^2} \tan^2 \theta_B = (\beta^2 - 1)$$

$$\Rightarrow \tan \theta_B = \beta$$

Method of producing polarized light



Reflected light polarized with \mathbf{E} perpendicular to the plane of incidence

Polarizing sunglasses with transmission axis vertical reduce glare because reflected light is mainly horizontally polarized.

Total internal reflection

$$n_1 \sin \theta_i = n_2 \sin \theta_t$$

$$\sin \theta_t = \frac{\sin \theta_i}{n_2/n_1}$$

Since $n_2 < n_1$, there will be total internal reflection when $\sin \theta_t > 1$

For transmitted wave, its like

- $e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)}$ in medium
 $= e^{i(k_2[x \sin \theta_t + z \cos \theta_t] - \omega t)}$

$$\text{since } z \cos \theta_t = 1 - \sin^2 \theta_t = \underbrace{e^{i(k_2 x \sin \theta_t - \omega t)}}_{\text{wave}} \underbrace{e^{-(\sin^2 \theta_t - 1)^{\frac{1}{2}} k_2 z}}_{e^{-z/\delta}} \text{ where}$$

$$\delta = \frac{\lambda_2}{2\pi} \frac{1}{(\sin^2 \theta_t - 1)^{\frac{1}{2}}}$$

This is called an *evanescent wave*

Lets now consider the **Plane travelling wave**

$$E_x = E_0 e^{i(kz - \omega t)}$$

$$\nabla \times \mathbf{E} = -\dot{\mathbf{B}} = i\omega \mathbf{B}$$

$$\begin{aligned} \mathbf{B} &= \frac{1}{i\omega} \begin{vmatrix} \hat{\mathbf{i}} & \hat{\mathbf{j}} & \hat{\mathbf{k}} \\ \partial_x & \partial_y & \partial_z \\ E_x & 0 & 0 \end{vmatrix} \\ &= \frac{1}{i\omega} \begin{pmatrix} 0 \\ \partial_z E_x \\ -\partial_y E_x \end{pmatrix} \\ &= \frac{1}{i\omega} \begin{pmatrix} 0 \\ ikE_x \\ 0 \end{pmatrix} \\ &= \frac{E_x}{\omega/k} \hat{\mathbf{y}} \\ &= \frac{E_x}{c} \hat{\mathbf{y}} \end{aligned}$$

For s-polarization, $\theta_i > \theta_c$, we have

$$\sin \theta_t = \frac{\sin \theta_i}{n_2/n_1} > 1$$

$$\cos \theta_t = i\sqrt{\sin^2 \theta_t - 1}$$

$$\begin{aligned} r_s &= \frac{n_1 \cos \theta_i - n_2 \cos \theta_t}{n_1 \cos \theta_i + n_2 \cos \theta_t} \\ &= \frac{A - iB}{A + iB} \end{aligned}$$

$$\Rightarrow R_s = |r_s|^2 = \frac{A^2 + B^2}{A^2 + B^2} = 1$$

$$t_s = \frac{2n_1 \cos \theta_i}{n_1 \cos \theta_i + n_2 \cos \theta_t} = \frac{2A}{A + iB}$$

So is complex

$$\Rightarrow \mathbf{E}_t = \hat{\mathbf{y}} t_s E_i e^{i(k_2[x \sin \theta_t - \omega t])} e^{-z/\delta}$$

$$\text{where } \delta = \frac{\lambda_2}{2\pi} \frac{1}{(\sin^2 \theta_t - 1)^{\frac{1}{2}}}$$

$$\nabla \times \mathbf{E} = -\dot{\mathbf{B}} = i\omega \mathbf{B}$$

$$\begin{aligned} \mathbf{B} &= \frac{1}{i\omega} \begin{vmatrix} \hat{\mathbf{i}} & \hat{\mathbf{j}} & \hat{\mathbf{k}} \\ \partial_x & \partial_y & \partial_z \\ 0 & E_t & 0 \end{vmatrix} \\ &= \frac{1}{i\omega} \begin{pmatrix} -\partial_z E_t \\ 0 \\ \partial_x E_t \end{pmatrix} \\ &= \begin{pmatrix} \frac{iE_t}{\omega\delta} \\ 0 \\ k_2 \sin \theta_t E_t / \omega \end{pmatrix} \end{aligned}$$

$\Rightarrow B_z$ is in phase with E_y

\Rightarrow transport of energy along x

B_x is out of phase with E_y

\Rightarrow no transport of energy along z

$$\langle \mathbf{S} \rangle = \langle \mathbf{E} \times \mathbf{H}^* \rangle$$

\mathbf{H}^* is the complex conjugate of H

Reminder on conductors

$$\nabla \times (\nabla \times \mathbf{E}) = \nabla(\nabla \cdot \mathbf{E}) - \nabla^2 \mathbf{E} - \frac{\partial}{\partial t} \nabla \times \mathbf{B}$$

$$\mu_0 \mu_r \sigma \mathbf{E} + \mu_0 \mu_r \sigma_0 \sigma_r \frac{\partial \mathbf{E}}{\partial t} = 0 \quad \text{if good conductor}$$

$$\nabla^2 \mathbf{E} = \mu_0 \sigma \frac{\partial \mathbf{E}}{\partial t}$$

$$-\tilde{k}^2 = i\omega \mu_0 \sigma$$

$$\Rightarrow \tilde{k} = k + i\kappa \quad k = \kappa = \sqrt{\frac{\mu_0 \sigma \omega}{2}}$$

$$\nabla \times \mathbf{E} = -\dot{\mathbf{B}}$$

$$-\frac{\partial B_y}{\partial t} = (\nabla \times \mathbf{E})_y = \frac{\partial E_x}{\partial z}$$

$$i\omega B_0 = i(k + i\kappa) E_0$$

$$Z = \frac{E_0}{H_0} = \frac{E_0}{B_0/\mu_0} = \frac{\mu_0 \omega}{k + i\kappa}$$

$$= \sqrt{\frac{2\mu_0 \omega}{\sigma}} \frac{1}{1 + i}$$

$$\Rightarrow Z = \sqrt{\frac{\mu_0 \omega}{2\sigma}} (1 - i)$$

Reflection from a metal surface

air	metal
$Z_1 = \sqrt{\frac{\mu_0}{\epsilon_0}}$	$Z_2 = \sqrt{\frac{\mu_0 \omega}{2\sigma}}(1 - i)$

$|z_2| \ll |Z_1|$ for a good conductor because $\sigma \gg \epsilon_0 \epsilon_r \omega$

write $\alpha = \frac{\sqrt{\frac{\mu_0 \omega}{2\sigma}}}{\sqrt{\frac{\mu_0}{\epsilon_0}}} = \sqrt{\frac{\omega \epsilon_0}{2\sigma}} \ll 1$

$$\begin{aligned}
 r &= \frac{E_r}{E_i} \quad \text{normal incidence} \\
 &= \frac{Z_2 - Z_1}{Z_2 + Z_1} \\
 &= \frac{Z_2/Z_1 - 1}{Z_2/Z_1 + 1} \\
 &= \frac{\alpha(1 - i) - 1}{\alpha(1 - i) + 1} \\
 &\approx \frac{1 - 2\alpha + \dots}{1 + 2\alpha + \dots} \\
 &= 1 - 4\alpha + O(\alpha^2) \\
 &= 1 - \frac{2\omega\delta}{c} + O(\alpha^2) \\
 &= 1 - \frac{4\pi\delta}{\lambda} + O(\alpha^2)
 \end{aligned}$$

where $\delta = \sqrt{\frac{2}{\omega \mu_0 \sigma}}$ is the skin depth

\Rightarrow most of the EM wave intensity is reflected

\Rightarrow metals are shiny!