

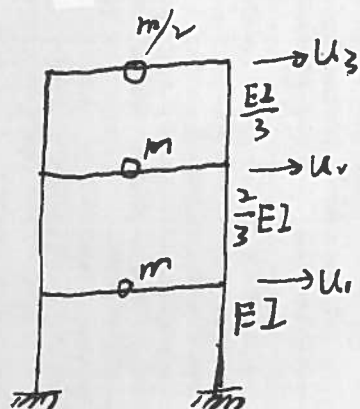
CIVE 603

Structural Dynamics

Hexiao Zhang

266784352.

Problem 1:



We can easily get

$$[K] = \begin{bmatrix} \frac{5}{3} & -\frac{2}{3} & 0 \\ -\frac{2}{3} & 1 & -\frac{1}{3} \\ 0 & -\frac{1}{3} & \frac{1}{3} \end{bmatrix} \cdot \frac{24EI}{h^3}$$

$$[M] = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0.5 \end{bmatrix} \cdot m$$

1.

$$[K - \omega_n^2 M] = \begin{bmatrix} \frac{5}{3} \frac{EI}{h^3} - \omega_n^2 m & -\frac{2}{3} \frac{EI}{h^3} & 0 \\ -\frac{2}{3} \frac{EI}{h^3} & \frac{EI}{h^3} - \omega_n^2 m & -\frac{1}{3} \frac{EI}{h^3} \\ 0 & -\frac{1}{3} \frac{EI}{h^3} & \frac{EI}{3h^3} - \frac{\omega_n^2 m}{2} \end{bmatrix} \cdot \frac{24EI}{h^3}$$

$$\det [K - \omega_n^2 M] = 0 \Rightarrow \begin{cases} \omega_{n1}^2 = 5.016 \frac{EI}{mh^3} \\ \omega_{n2}^2 = 24 \frac{EI}{mh^3} \\ \omega_{n3}^2 = 50.976 \frac{EI}{mh^3} \end{cases} \Rightarrow \begin{cases} \omega_{n1} = 2.24 \sqrt{\frac{EI}{mh^3}} \\ \omega_{n2} = 4.90 \sqrt{\frac{EI}{mh^3}} \\ \omega_{n3} = 7.149 \sqrt{\frac{EI}{mh^3}} \end{cases} \Rightarrow \begin{cases} T_1 = 2.80 \sqrt{\frac{mh^3}{EI}} \\ T_2 = 1.28 \sqrt{\frac{mh^3}{EI}} \\ T_3 = 0.88 \sqrt{\frac{mh^3}{EI}} \end{cases}$$

For $W_{n1}^2 = 5.016 \frac{EI}{mh^3}$

$$\frac{24EI}{h^3} \begin{bmatrix} 43/3/2000 & -\frac{2}{3} & 0 \\ -\frac{2}{3} & 791/1000 & -\frac{1}{3} \\ 0 & -\frac{1}{3} & 3/3/2000 \end{bmatrix} \cdot \begin{bmatrix} \phi_{11} \\ \phi_{21} \\ \phi_{31} \end{bmatrix} = 0$$

Assume $\phi_{31} = 1 \Rightarrow \phi_1 = \begin{bmatrix} 0.314 \\ 0.686 \\ 1 \end{bmatrix}$

For $W_{n2}^2 = 24 \frac{EI}{mh^3}$

$$\frac{24EI}{h^3} \begin{bmatrix} \frac{2}{3} & -\frac{1}{3} & 0 \\ -\frac{2}{3} & 0 & -\frac{1}{3} \\ 0 & -\frac{2}{3} & -\frac{2}{3} \end{bmatrix} \cdot \begin{bmatrix} \phi_{12} \\ \phi_{22} \\ \phi_{32} \end{bmatrix} = 0$$

Assume $\phi_{32} = 1 \Rightarrow \phi_2 = \begin{bmatrix} -0.5 \\ -0.5 \\ 1 \end{bmatrix}$

For $W_{n3}^2 = 50.976 \frac{EI}{mh^3}$

Repeat the same process we get

$$\frac{24EI}{h^3} \begin{bmatrix} -0.4573 & -\frac{2}{3} & 0 \\ -\frac{2}{3} & -1.1240 & -\frac{1}{3} \\ 0 & -\frac{1}{3} & -0.7287 \end{bmatrix} \cdot \begin{bmatrix} \phi_{13} \\ \phi_{23} \\ \phi_{33} \end{bmatrix} = 0$$

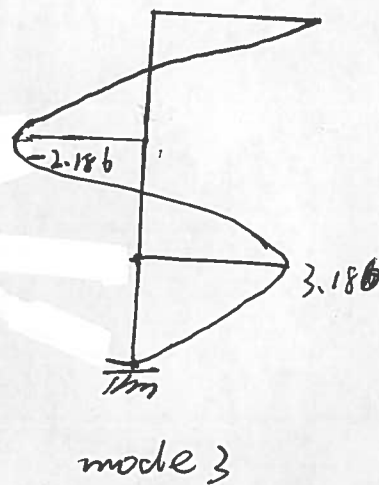
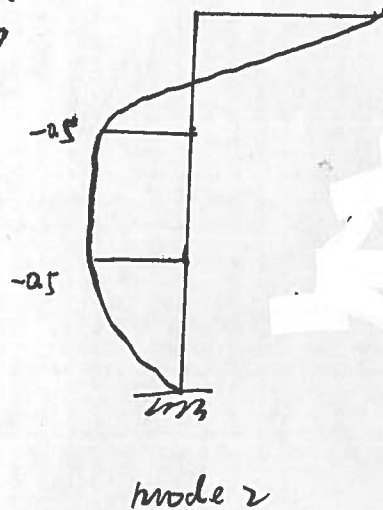
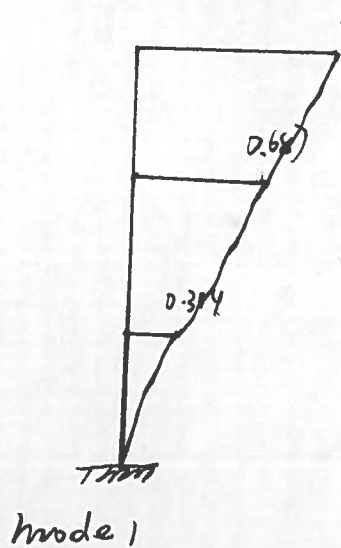
Assume $\phi_{33} = 1 \Rightarrow \phi_3 = \begin{bmatrix} 3.186 \\ -2.186 \\ 1 \end{bmatrix}$

So the results are:

$$W_1 = 2.24 \sqrt{\frac{EI}{mh^3}}$$

$$W_2 = 4.90 \sqrt{\frac{EI}{mh^3}}$$

$$W_3 = 7.14 \sqrt{\frac{EI}{mh^3}}$$



2. Verify the orthogonality

The detail of calculation is shown in matlab.

$$\phi_1^T \cdot K \phi_2 = 0$$

$$\phi_2^T \cdot m \phi_1 = 0$$

$$\phi_2^T \cdot K \phi_3 = 0$$

$$\phi_3^T \cdot m \phi_2 = 0$$

$$\phi_3^T \cdot K \phi_1 = 0$$

$$\phi_1^T \cdot m \phi_3 = 0$$

So we can verify

$$\begin{cases} \phi_n^T \cdot K \phi_r = 0 \\ \phi_n^T \cdot m \phi_r = 0 \end{cases}$$

$$(\forall n \neq r)$$

$$(r \neq n)$$

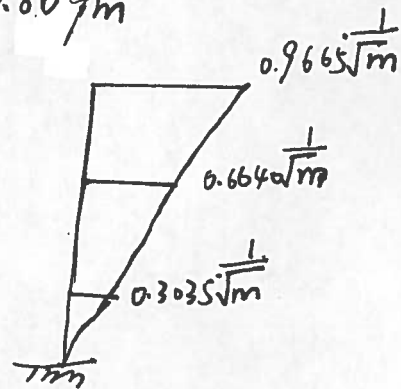
3. For mode 1 :

$$M_1 = \phi_1^T \cdot m \cdot \phi_1 = (0.314, 0.686, 1) \cdot \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0.5 \end{bmatrix} \cdot m \cdot \begin{pmatrix} 0.314 \\ 0.686 \\ 1 \end{pmatrix}$$

$$= 1.069 \cdot m$$

To make $M_1 = 1 \Rightarrow$ divide ϕ_1 by $\sqrt{1.069} \cdot m$

$$\phi_1 = \begin{pmatrix} 0.3035 \\ 0.6640 \\ 0.9665 \end{pmatrix} \cdot \frac{1}{\sqrt{m}}$$

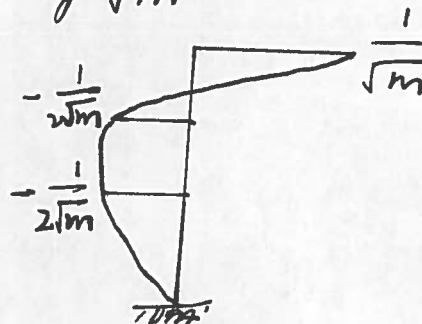


For mode 2 :

$$M_2 = \phi_2^T \cdot m \cdot \phi_2 = (-0.5, -0.5, 1) \cdot \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0.5 \end{bmatrix} \cdot m \cdot \begin{pmatrix} -0.5 \\ -0.5 \\ 1 \end{pmatrix} = m$$

To make $M_2 = 1$ divide ϕ_2 by \sqrt{m}

$$\phi_2 = \begin{pmatrix} -0.5 \\ -0.5 \\ 1 \end{pmatrix} \cdot \frac{1}{\sqrt{m}}$$

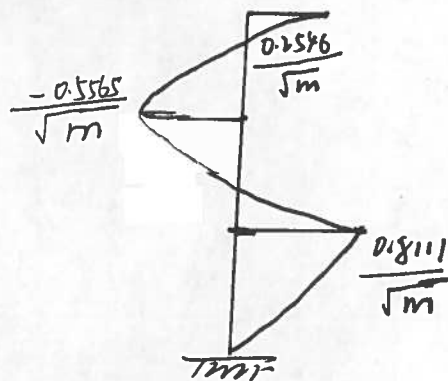


For mode 3:

$$M_3 = \phi_3^T \cdot m \phi_3 = (-3.186, -2.186, 1) \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0.5 \end{pmatrix} m \begin{pmatrix} -3.186 \\ -2.186 \\ 1 \end{pmatrix} = 15.4292 m$$

To make $M_3 = 1$ divide by $\sqrt{15.4292 m}$

$$\phi_3 = \begin{pmatrix} 0.8111 \\ -0.5565 \\ 0.2546 \end{pmatrix} \frac{1}{\sqrt{m}}$$



Compare. The ~~prop~~ ratio of u_1, u_2, u_3 (displacement at mass point) is same in the modes and normalized modes, but the values may be changed ~~by~~ by the normalization, but the mode is multiples of the mode in the first question

problem 2:

Condition a: $u_1 = \begin{pmatrix} -1 \\ 2 \\ 3 \end{pmatrix}$:

$$q_1 = \frac{\phi_1^T m u_1}{\phi_1^T m \phi_1} = \frac{(0.314, 0.687, 1) \cdot \begin{pmatrix} 1, 0, 0 \\ 0, 1, 0 \\ 0, 0, 0.5 \end{pmatrix} \cdot \begin{pmatrix} 3 \\ 2 \\ 1 \end{pmatrix}}{(0.314, 0.687, 1) \cdot \begin{pmatrix} 1, 0, 0 \\ 0, 1, 0 \\ 0, 0, 0.5 \end{pmatrix} \cdot \begin{pmatrix} 0.314 \\ 0.687 \\ 1 \end{pmatrix}} = 2.9779$$

$$q_2 = \frac{\phi_2^T m u_1}{\phi_2^T m \phi_2} = 0$$

$$q_3 = \frac{\phi_3^T m u_1}{\phi_3^T m \phi_3} = 0.0204 \quad \text{and} \quad \dot{q}_1(0) = 0 \quad \dot{q}_2(0) = 0 \quad \dot{q}_3(0) = 0$$

$$u(t) = \sum_{n=1}^N \phi_n \left[q_n(0) \cos \omega_n t + \frac{\dot{q}_n(0)}{\omega_n} \sin \omega_n t \right]$$

$$= \begin{pmatrix} 0.314 \\ 0.687 \\ 1 \end{pmatrix} \cdot [2.9779 \cdot \cos(2.24 \sqrt{\frac{EI}{mh^3}} t)] + \begin{pmatrix} 2.186 \\ -2.186 \\ 1 \end{pmatrix} [0.0204 \cdot \cos(7.140 \sqrt{\frac{EI}{mh^3}} t)]$$

$$= \begin{pmatrix} 0.935 \cdot \cos(2.24 \sqrt{\frac{EI}{mh^3}} t) + 0.065 \cdot \cos(7.140 \sqrt{\frac{EI}{mh^3}} t) \\ 2.046 \cdot \cos(2.24 \sqrt{\frac{EI}{mh^3}} t) - 0.044 \cos(7.140 \sqrt{\frac{EI}{mh^3}} t) \\ 2.978 \cdot \cos(2.24 \sqrt{\frac{EI}{mh^3}} t) + 0.020 \cos(7.140 \sqrt{\frac{EI}{mh^3}} t) \end{pmatrix}$$

6

Condition b: $u_r = \begin{pmatrix} -1 \\ 0.25 \\ 1 \end{pmatrix}$

$$q_1 = \frac{\phi_1^T m u_r}{\phi_1^T m \phi_1} = 0.3342$$

$$q_2 = \frac{\phi_2^T m u_r}{\phi_2^T m \phi_2} = 0.8750$$

$$q_3 = \frac{\phi_3^T m u_r}{\phi_3^T m \phi_3} = -0.2095 \quad \dot{q}_1(0) = 0 \quad \dot{q}_2(0) = 0 \quad \dot{q}_3(0) = 0$$

$$u(t) = \sum_{n=1}^3 \phi_n \left[q_n(0) \cdot \cos \omega_n t + \frac{\dot{q}_n(0)}{\omega_n} \sin \omega_n t \right]$$

$$= \begin{pmatrix} 0.319 \\ 0.687 \\ 1 \end{pmatrix} \left(0.3342 \cos(2.24 \sqrt{\frac{EI}{mh^3}} t) \right) + \begin{pmatrix} -0.5 \\ -0.5 \\ 1 \end{pmatrix} \left(0.8750 \cos(4.90 \sqrt{\frac{EI}{mh^3}} t) \right)$$

$$+ \begin{pmatrix} 3.186 \\ -2.186 \\ 1 \end{pmatrix} \left(-0.2095 \cos(7.140 \sqrt{\frac{EI}{mh^3}} t) \right)$$

$$= \begin{pmatrix} 0.165 \cos(2.24 \sqrt{\frac{EI}{mh^3}} t) - 0.438 \cos(4.90 \sqrt{\frac{EI}{mh^3}} t) - 0.667 \cos(7.140 \sqrt{\frac{EI}{mh^3}} t) \\ 0.230 \cos(2.24 \sqrt{\frac{EI}{mh^3}} t) - 0.438 \cos(4.90 \sqrt{\frac{EI}{mh^3}} t) + 0.458 \cos(7.140 \sqrt{\frac{EI}{mh^3}} t) \\ 0.334 \cos(2.24 \sqrt{\frac{EI}{mh^3}} t) + 0.875 \cos(4.90 \sqrt{\frac{EI}{mh^3}} t) - 0.209 \cos(7.140 \sqrt{\frac{EI}{mh^3}} t) \end{pmatrix}$$

>

Condition C: $u_3 = \begin{pmatrix} 1 \\ -1 \\ 1 \end{pmatrix}$

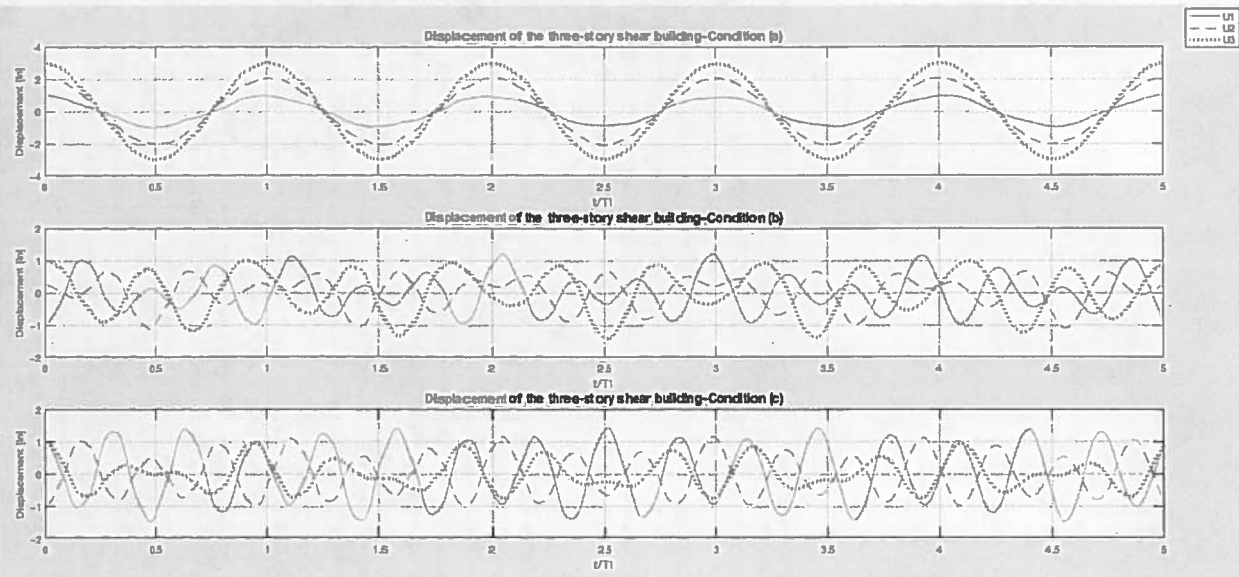
$$q_1 = \frac{\phi_1^T m u_3}{\phi_1^T m \phi_1} = 0.1186 \quad q_2 = \frac{\phi_2^T m u_3}{\phi_2^T m \phi_2} = 0.5 \quad q_3 = \frac{\phi_3^T m u_3}{\phi_3^T m \phi_3} = 0.3806$$

$\dot{q}_1(0) = 0 \quad \dot{q}_2(0) = 0 \quad \dot{q}_3(0) = 0$

$$u(t) = \sum_{n=1}^3 \phi_n \left[\dot{q}_n(0) \cdot \cos \omega_n t + \frac{q_n(0)}{\omega_n} \sin \omega_n t \right]$$

$$= \begin{pmatrix} 0.314 \\ 0.687 \\ 1 \end{pmatrix} (0.1186 \cos \omega_1 t) + \begin{pmatrix} -0.5 \\ -0.5 \\ 1 \end{pmatrix} (0.5 \cos \omega_2 t) + \begin{pmatrix} 2.186 \\ -2.186 \\ 1 \end{pmatrix} (0.3806 \cos \omega_3 t)$$

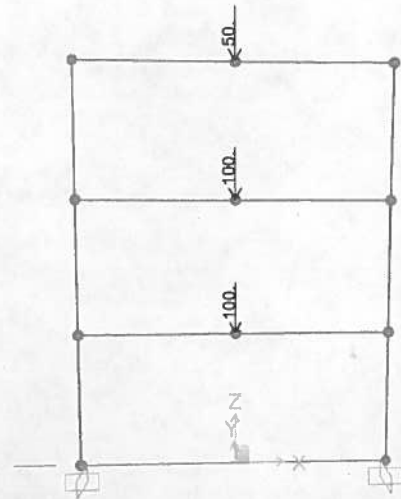
$$= \begin{pmatrix} 0.03 \cdot \cos(2.24 \sqrt{\frac{EI}{mh^3}} t) - 0.25 \cdot \cos(4.90 \sqrt{\frac{EI}{mh^3}} t) + 1.213 \cdot \cos(7.140 \sqrt{\frac{EI}{mh^3}} t) \\ 0.081 \cdot \cos(2.24 \sqrt{\frac{EI}{mh^3}} t) - 0.25 \cdot \cos(4.90 \sqrt{\frac{EI}{mh^3}} t) - 0.832 \cdot \cos(7.140 \sqrt{\frac{EI}{mh^3}} t) \\ 0.119 \cdot \cos(2.24 \sqrt{\frac{EI}{mh^3}} t) + 0.5 \cos(4.90 \sqrt{\frac{EI}{mh^3}} t) + 0.381 \cos(7.140 \sqrt{\frac{EI}{mh^3}} t) \end{pmatrix}$$



Problem 3:

The model and information are as shown.

(1)



Section Name Beam

Section Notes Modify/Show Notes

Dimensions

Outside height (t3) 12

Top flange width (t2) 5

Top flange thickness (tf) 0.38

Web thickness (tw) 0.25

Bottom flange width (t2b) 5

Bottom flange thickness (tfb) 0.38

Material A992Fy50

Property Modifiers Set Modifiers

Frame Property/Stiffness Modification Factors

Property/Stiffness Modifiers for Analysis

Cross-section (axial) Area 1

Shear Area in 2 direction 10000

Shear Area in 3 direction 10000

Torsional Constant 1

Moment of Inertia about 2 axis 10000

Moment of Inertia about 3 axis 10000

Mass 0.01

Weight 0

OK Cancel

Section Name story1

Section Notes Modify/Show Notes

Dimensions

Outside height (t3) 12

Top flange width (t2) 5

Top flange thickness (tf) 0.38

Web thickness (tw) 0.25

Bottom flange width (t2b) 5

Bottom flange thickness (tfb) 0.38

Material A992Fy50

Property Modifiers Set Modifiers

Property Data

Section Name story1

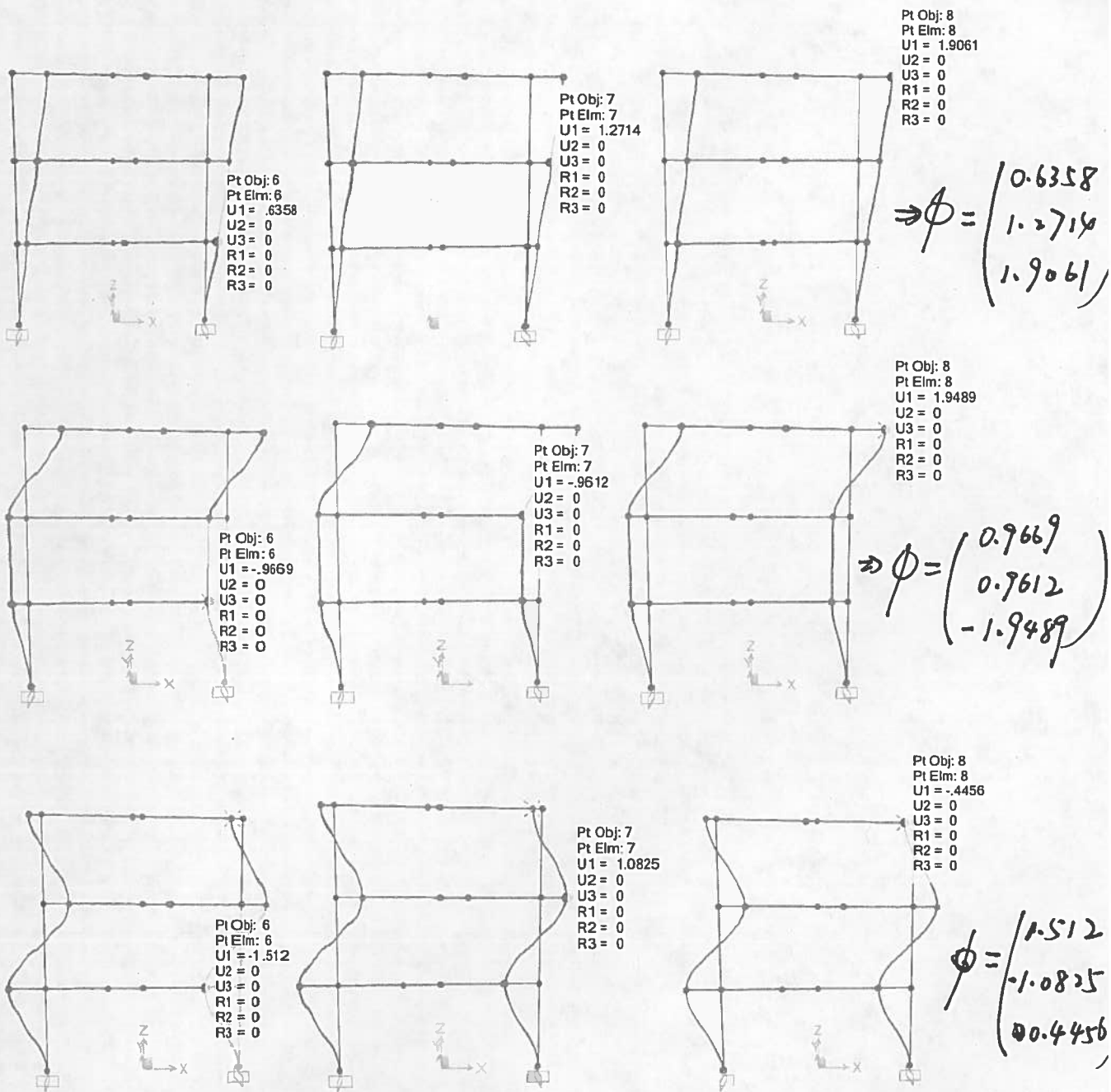
Properties

Cross-section (axial) area	6.99	Section modulus about 3 axis	26.9223
Moment of Inertia about 3 axis	170.0375	Section modulus about 2 axis	3.6043
Moment of Inertia about 2 axis	10.613	Plastic modulus about 3 axis	32.0375
Product of Inertia about 2-3	0	Plastic modulus about 2 axis	5.9706
Shear area in 2 direction	3	Radius of Gyration about 3 axis	4.9321
Shear area in 3 direction	3.4833	Radius of Gyration about 2 axis	1.2438
Torsional constant	0.2502	Shear Center Eccentricity (x3)	0

OK

	OutputCase	StepType Text	StepNum Unitless	Period Sec	Frequency Cyc/sec	CircFreq rad/sec	Eigenvalue rad2/sec2
▶	MODAL	Mode	1	0.522942	1.9122568...	<u>12.015063...</u>	144.36176...
	MODAL	Mode	2	0.24631	4.0599163...	<u>25.509206...</u>	650.71964...
	MODAL	Mode	3	0.163235	6.1261526...	<u>38.491752...</u>	1481.6149...

Almost same as
example in problem



The modes are almost
as same as the results
in the problem.

(2)

$$m = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 9 \\ 0 & 0 & 2 \end{bmatrix} \cdot \frac{100}{386}$$

$$K = \frac{K}{9} \begin{bmatrix} 16 & -7 & 0 \\ -7 & 10 & -3 \\ 0 & -3 & 3 \end{bmatrix} = \frac{168}{9} \begin{bmatrix} 16 & -7 & 0 \\ -7 & 10 & -3 \\ 0 & -3 & 3 \end{bmatrix}$$

$$\frac{1}{2} \begin{bmatrix} 1/w_i & w_i \\ 1/w_j & w_j \end{bmatrix} \begin{bmatrix} a_0 \\ a_1 \end{bmatrix} = \begin{bmatrix} f_i \\ f_j \end{bmatrix}$$

$$\Rightarrow \frac{1}{2} \begin{bmatrix} \frac{1}{12.01} & 12.01 \\ \frac{1}{38.90} & 38.90 \end{bmatrix} \begin{bmatrix} a_0 \\ a_1 \end{bmatrix} = \begin{bmatrix} 0.05 \\ 0.05 \end{bmatrix} \Rightarrow \begin{bmatrix} a_0 \\ a_1 \end{bmatrix} = \begin{bmatrix} 0.9177 \\ 0.001964 \end{bmatrix}$$

$$C = a_0 m + a_1 K = \begin{bmatrix} 0.824 & -0.25 & 0 \\ -0.2575 & 0.604 & -0.100 \\ 0 & -0.100 & 0.229 \end{bmatrix}$$

$$f_z = \frac{a_0}{z} \cdot \frac{1}{w_{nv}} + \frac{a_1}{z} w_{nv}$$

$$\begin{aligned} 1) &= (0.9177 \cdot \frac{1}{25.47} + 0.0020 \times 25.47) \times \frac{1}{2} \\ &= 4.3\% \end{aligned}$$

~~$$M = \Phi^T \cdot m$$~~

$$\Phi = \begin{bmatrix} 0.6375 & 0.9827 & 1.5778 \\ 1.2750 & 0.9829 & -1.1270 \\ 1.9125 & -1.8642 & 0.4568 \end{bmatrix}$$

$$M = \Phi^T \cdot m \cdot \Phi = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \text{ kips} \cdot \text{s}^2 \cdot \text{in}^{-1}$$

$$K = \Phi^T \cdot k \cdot \Phi = \begin{bmatrix} 144.14 & 0 & 0 \\ 0 & 648.62 & 0 \\ 0 & 0 & 1513.59 \end{bmatrix} \cdot \text{kip/in}$$

$$C = \Phi^T \cdot c \cdot \Phi = \begin{bmatrix} 1.20 & 0 & 0 \\ 0 & 2.19 & 0 \\ 0 & 0 & 3.89 \end{bmatrix}$$