



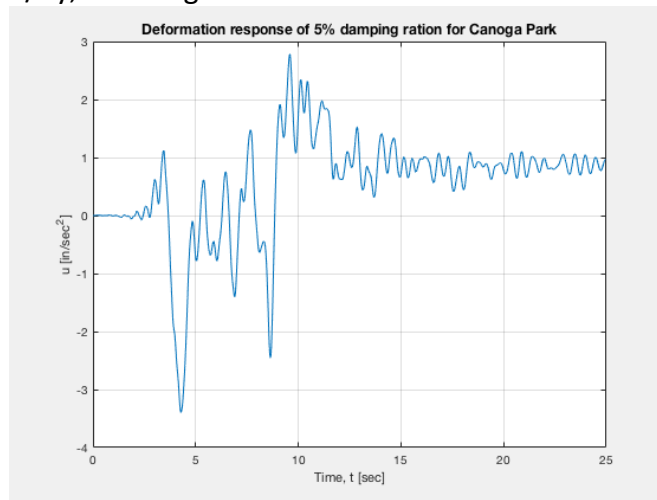
**McGill University**  
**Department of Civil Engineering and**  
**Applied Mechanics**  
**CIVE 603 – Structural Dynamics**  
**HM#4**  
**Group assignment by**

**Hao Shi      260782588**

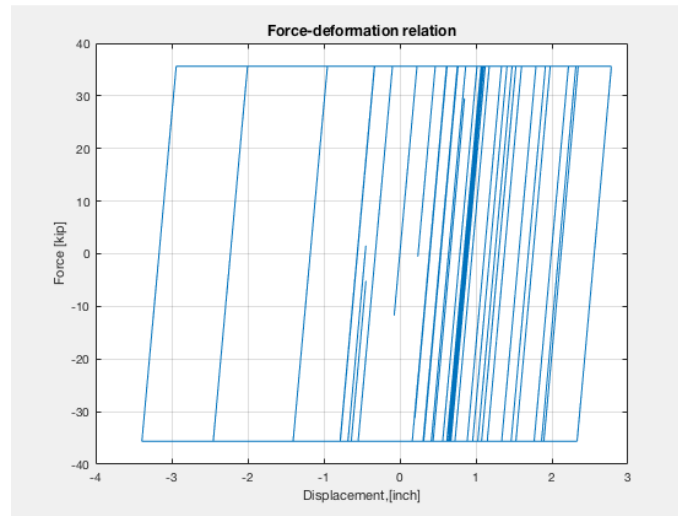
**Hexiao Zhang    266784352**

Problem1:

1. By setting  $R_y=1$ , we first get the elastic response and get the  $u_0 = 1.8084$  in, then set the  $R_y = 8$ , and  $u_y = u_0/R_y$ , we can get



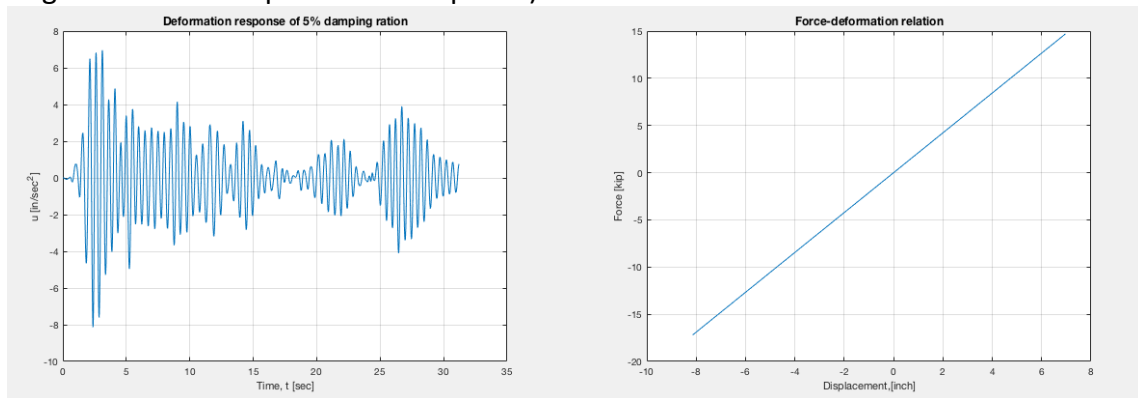
2. The Force-deformation relation is shown as below:



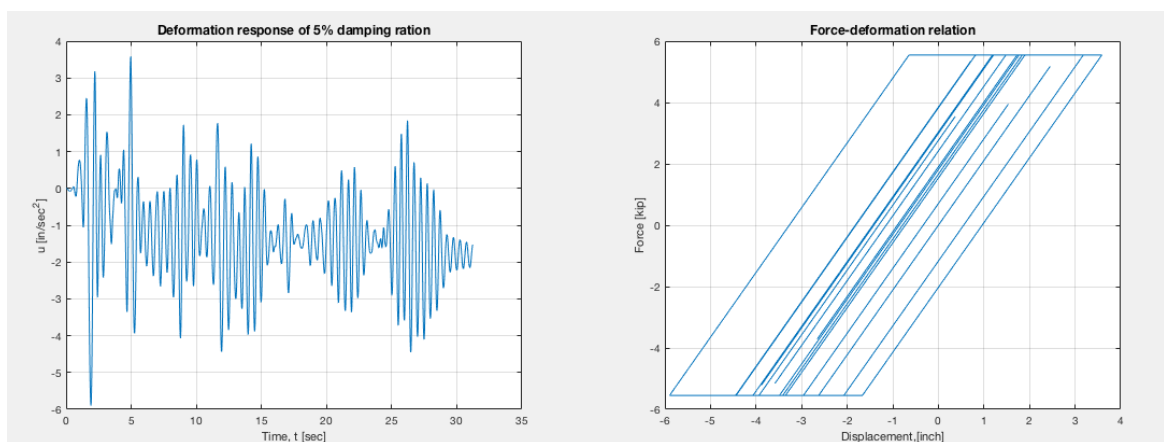
3. By the Command  $\langle \max(\text{abs}(u)) \rangle$ , we get the maximum deformation  $u_{\max} = 3.38$   
 $\mu = u_{\max}/u_y = u_{\max}/(u_0/R_y) = 14.96$

## Problem2:

- $T_n = 2\pi \cdot (w/(k \cdot g))^{0.5} = 0.502s$   
 $\xi = 2\%$   
 $u_y = f_y/k = 2.628 \text{ in}$
- No, when the system vibrates at larger amplitude, it means the system is no longer elastic, and the force-deformation relationship is not linear, and the  $k$  is changed and  $T_n = 2\pi \cdot (w/(k \cdot g))^{0.5}$  is also changed. But the  $\xi$  keeps the same.
- In corresponding system, the  $u_0 = 8.187$  in (By assuming an elastic response in the code to get maximum displacement response).



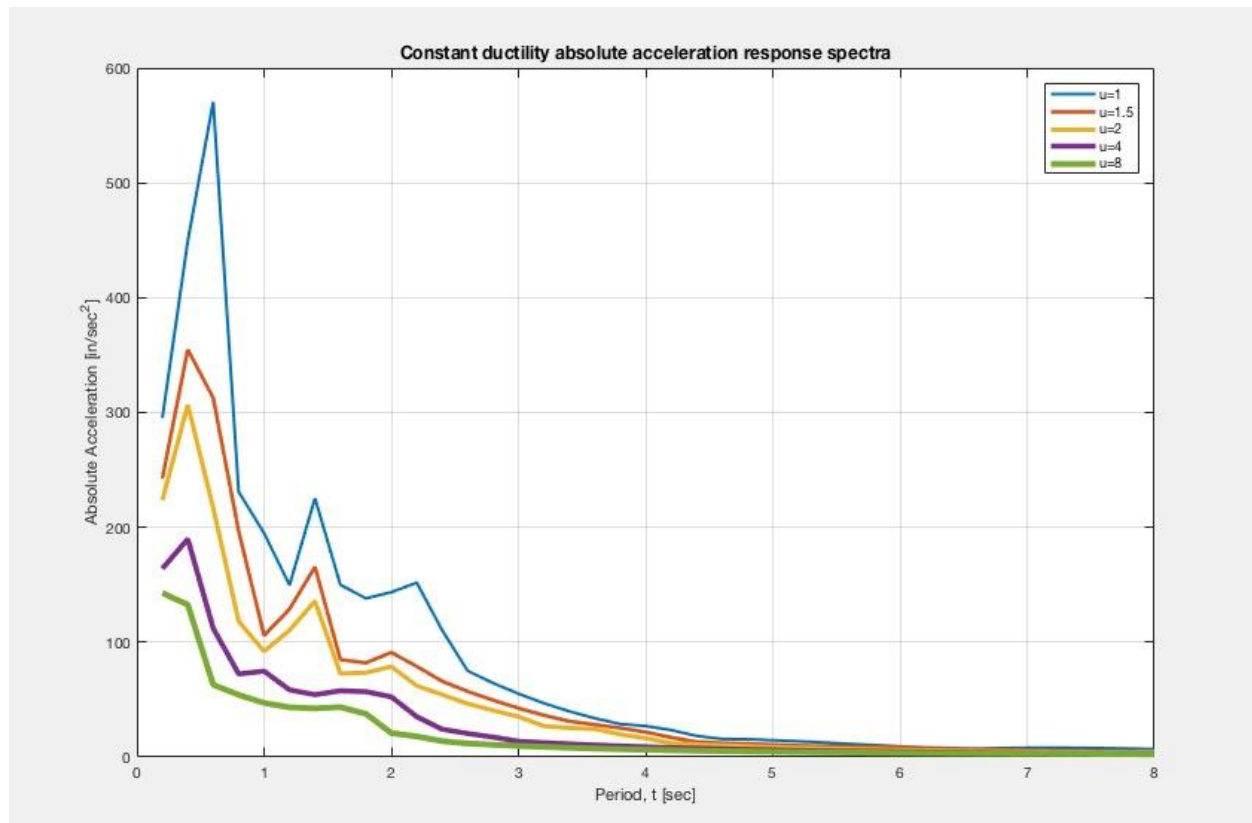
by setting the  $u_y = f_y/k = 2.628$  in, we can get:



$$R_y = u_0/u_y = 8.187/2.628 = 3.115;$$

$$f_y = 1/R_y = 0.321;$$

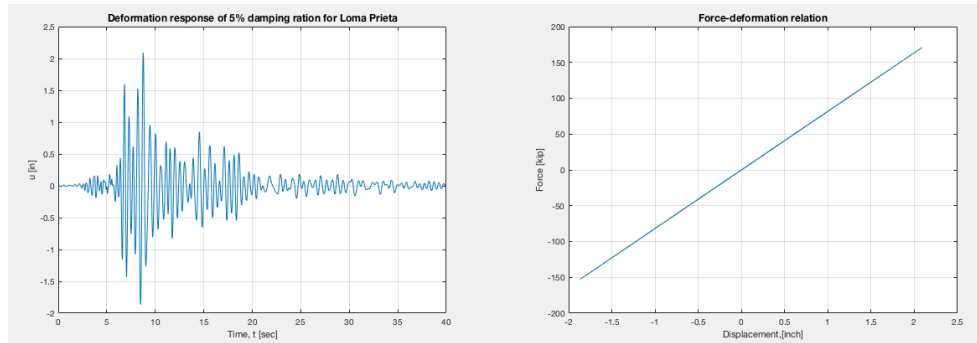
### Problem3:



## Problem5:

### PartA

For  $T_n = 0.5\text{sec}$ , the corresponding liner response is shown below:

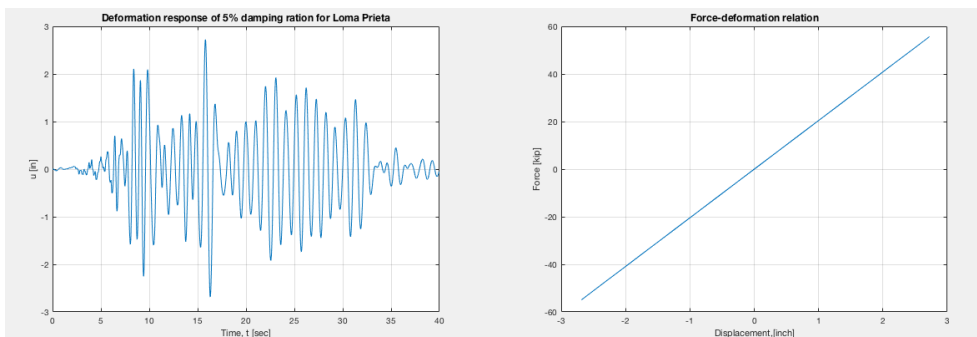


$$k = m \cdot \omega_n^2$$

The maximum displacement  $u_0 = 2.0923$  in

The force demand  $f_0 = k \cdot u_0 = m \cdot \omega_n^2 \cdot u_0 = 171.08$  kips

For  $T_n = 1.0\text{sec}$ , the corresponding liner response is shown below:

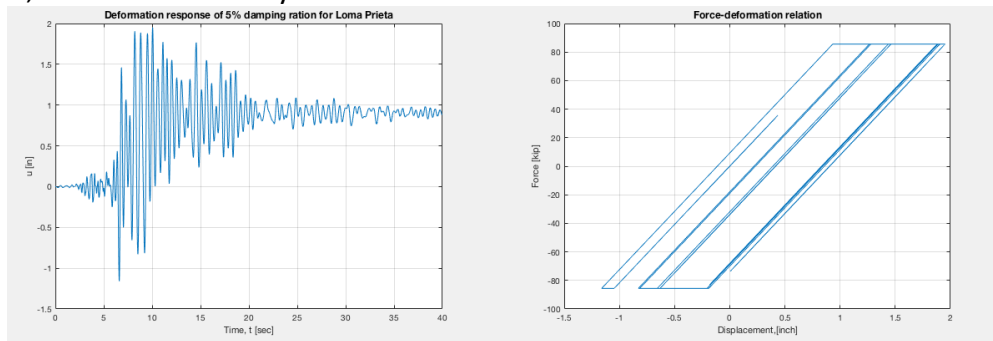


The maximum displacement  $u_0 = 2.723$  in

The force demand  $f_0 = k \cdot u_0 = m \cdot \omega_n^2 \cdot u_0 = 55.66$  kips

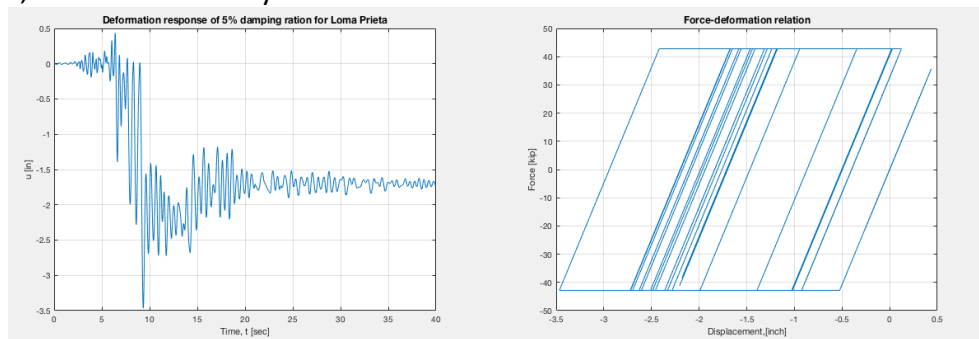
## PartB

$T_n = 0.5$  sec, reduction factor  $R_y = 2$



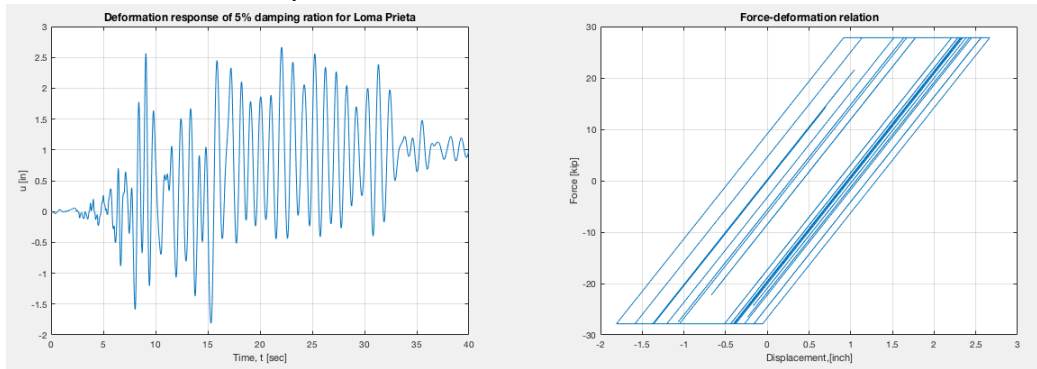
The maximum displacement  $u_{max} = 1.95$  in  
 $u_y = 1.0465$  in  
 $f_y = 85.55$  kips  
 $\mu = 1.86$

$T_n = 0.5$  sec, reduction factor  $R_y = 4$



The maximum displacement  $u_{max} = 3.47$  in  
 $u_y = 0.523$  in  
 $f_y = 42.77$  kips  
 $\mu = 6.64$

$T_n = 1.0$  sec, reduction factor  $R_y = 2$



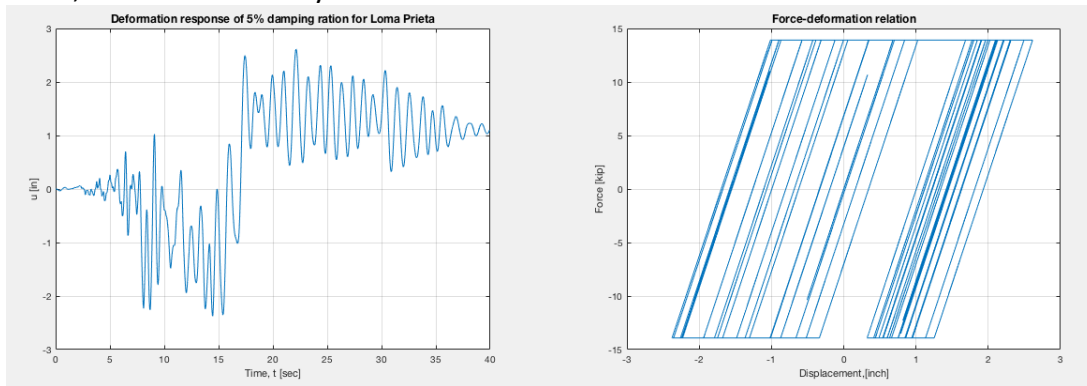
The maximum displacement  $u_{max} = 2.67$

$u_y = 1.362$  in

$f_y = 27.83$  kips

$\mu = 1.96$

$T_n = 1.0$  sec, reduction factor  $R_y = 4$



The maximum displacement  $u_{max} = 2.61$

$u_y = 0.681$  in

$f_y = 13.92$  kips

$\mu = 3.84$

Conclusion:

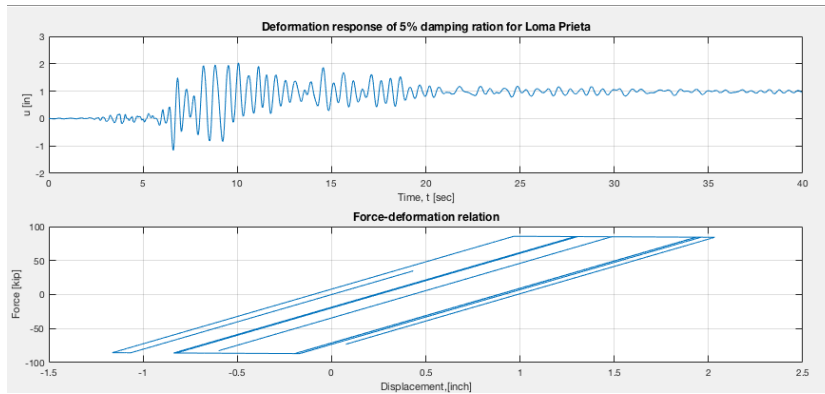
As structural engineers, we should design structures looking for lower ductility demand because the ductility capacity should exceed the ductility demand.

When  $R_y$  equals to 4, the ductility demand is too high thus we eliminate these two cases first. For  $R_y = 2$ , the properties and responses are similar, but when  $T_n = 1$  sec, the yield force  $f_y$  is much smaller than the case when  $T_n = 0.5$  sec, which means the cost of construction will be much lesser when  $T_n = 1$  sec.

**Thus, we should select the case when  $T_n = 1$  sec and  $R_y = 2$ .**

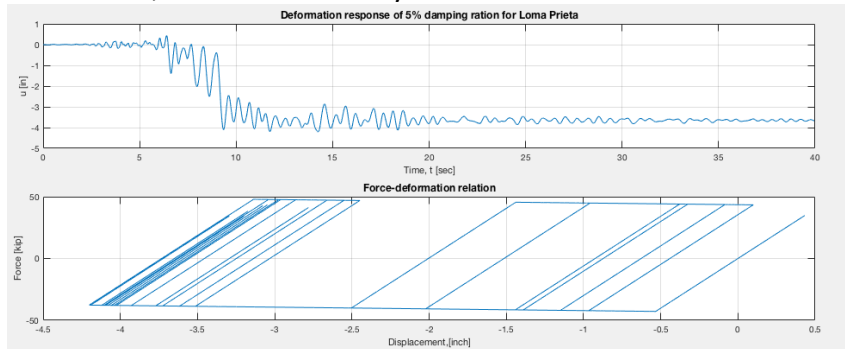
PartC:

$T_n = 0.5$  sec, reduction factor  $R_y = 2$



$u_{max} = 2.03$   
 $u_y = 1.065$  in  
 $f_y = 87.089$  kips  
 $\mu = 1.91$

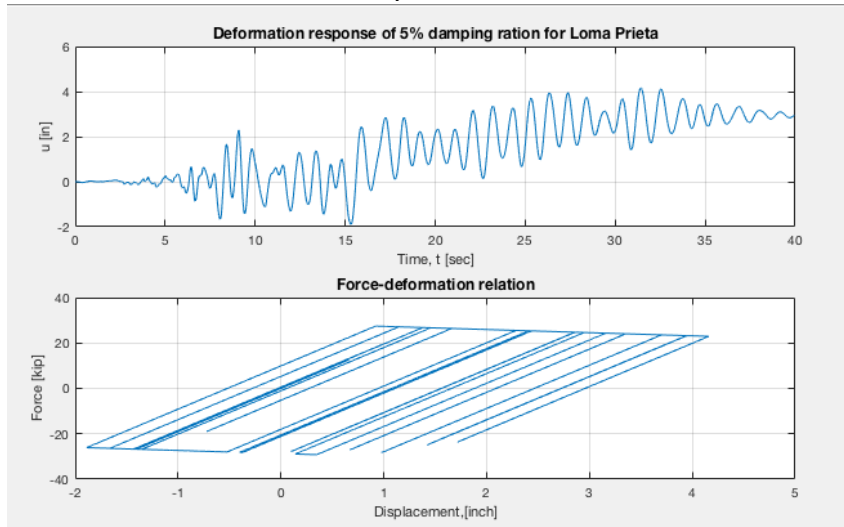
$T_n = 0.5$  sec, reduction factor  $R_y = 4$



$u_{max} = 4.20$   
 $u_y = 0.5325$  in  
 $f_y = 43.545$  kips  
 $\mu = 7.89$



Tn =1.0 sec, reduction facor Ry=2



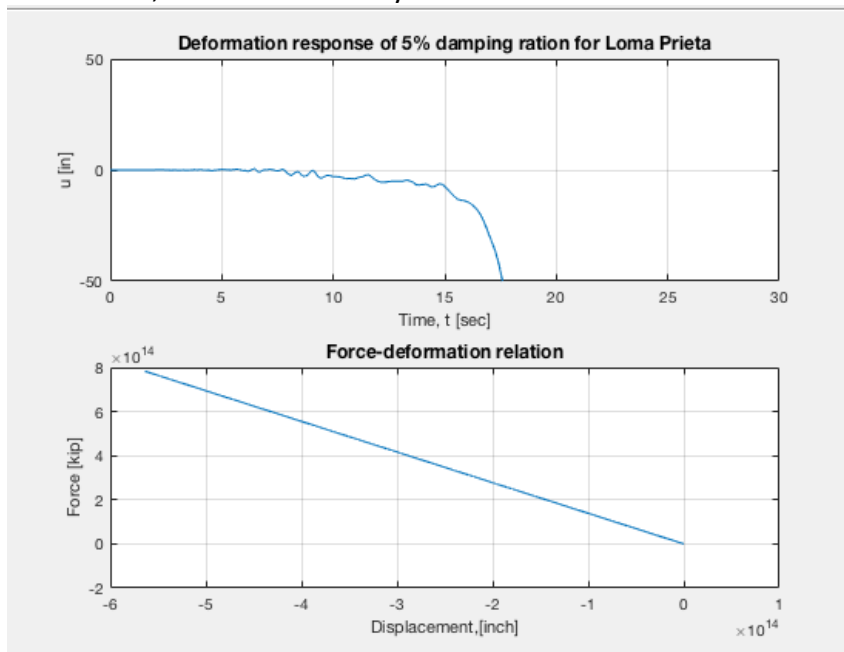
umax= 4.16 in

uy=1.405 in

fy=28.723kips

$\mu = 2.96$

Tn =1.0 sec, reduction facor Ry=4



### Conclusion:

Similarly from the part B, when  $R_y = 4$  and  $T_n = 1.0$  sec, the structure will collapse. When  $R_y = 4$ ,  $T_n = 0.5$  sec, the ductility demand is too high.

When  $R_y = 2$ , although when  $T_n = 0.5$  sec, the yield force is higher than the case when  $T_n = 1$  sec, the  $\mu = 1.91$  is much lower than  $\mu = 2.96$ .

**Thus we should choose  $R_y = 2$  and  $T_n = 0.5$  sec.**

Problem 4:

$$m = \frac{W}{g} = \frac{10 \text{ kips}}{386.22} = 0.02589 \text{ kips} \cdot \text{s}^2/\text{in}$$

$$K = K_1 + K_2 = \frac{3EI}{L_1^3} + \frac{3EI}{L_2^3} = \frac{3 \times 3 \times 10^3 \times \frac{1}{12} \times 10^6}{(10 \times 12)^3} + \frac{3 \times 3 \times 10^3 \times \frac{1}{12} \times 10^6}{(20 \times 12)^3}$$

$$= 4.883 \text{ kip/in}$$

$$T_n = 2\pi \cdot \sqrt{\frac{m}{K}} = 2\pi \cdot \sqrt{\frac{0.02589}{4.883}} = 0.4575 \text{ s}$$

$$A = 271 \times 0.25 \times 386.22 = 261 \text{ in/s}^2$$

$$U_{\max} = \frac{m \cdot A}{K} = 0.5/2 \text{ in}$$

$$\text{Column 1: } M_{\max} = \frac{3EI}{L_1^2} \times U_{\max} = 266.667 \text{ kips} \cdot \text{in}$$

$$\text{Column 2: } M_{\max} = \frac{3EI}{L_2^2} \times U_{\max} = 66.667 \text{ kips} \cdot \text{in}$$

$$b) C_{cr} = 2m \cdot W_n = 2 \times 0.02589 \times \frac{2\pi}{T_n} = 0.7111$$

$$\xi_{sp} = \frac{C}{C_{cr}} = \frac{0.1}{0.7111} = 14.1 \%$$

$$\xi' = \xi_{sp} + \xi = 19.1 \%$$

$$\beta = 1.400 - 0.248 \cdot \ln(19.1) = 0.668$$

$$\therefore S_d(T_n, 19.1) = \beta \cdot S_d(T_n, 5) = \beta \cdot 261 \text{ in/s}^2 = 174.348 \text{ in/s}^2$$

$$U_{\max} = \frac{m \cdot A'}{K} = 0.342 \text{ in}$$

(c)

$$\underline{R_y} = R_y = \mu + (1-\mu) \exp\left(\frac{-2\sigma}{\mu}\right)$$

$$= 4 + (1-4) e^{\frac{-20 \times 0.4575}{4}} = 3.695.$$

$\therefore$  Lateral displacement:

$$= \frac{u_{max}}{R_y} \times \phi = \frac{0.512}{3.695} \times 4 = 0.5543 \text{ in}$$

Lateral force.

$$\frac{M_A}{R_y} = \frac{6.775}{1.829} \text{ kips.}$$