

## Supplementary material

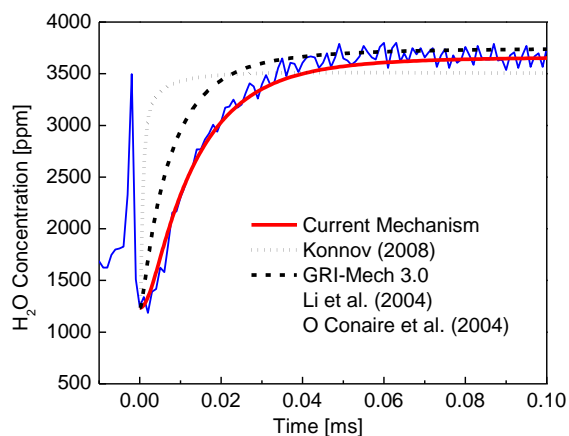


Figure S1.  $\text{H}_2\text{O}$  time-history during the thermal decomposition of  $\text{H}_2\text{O}_2$  at 1.91 atm, 1398 K. Test mixture: 2540 ppm  $\text{H}_2\text{O}_2$ /1234 ppm  $\text{H}_2\text{O}$ /617 ppm  $\text{O}_2$ /Ar. Experimental data (in blue) from Hong et al. [16].

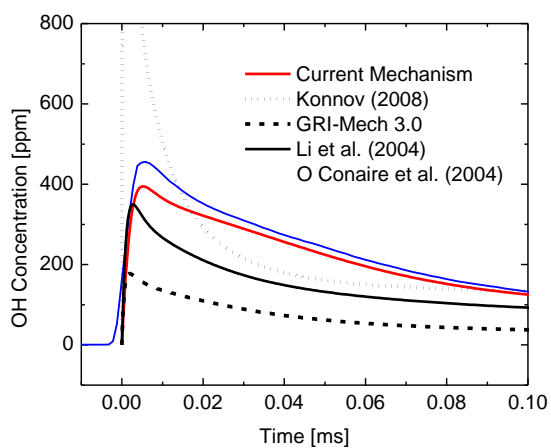


Figure S2.  $\text{OH}$  time-history during the thermal decomposition of  $\text{H}_2\text{O}_2$  at conditions of those of Figure S1. Experimental data (in blue) are from Hong et al. [16].

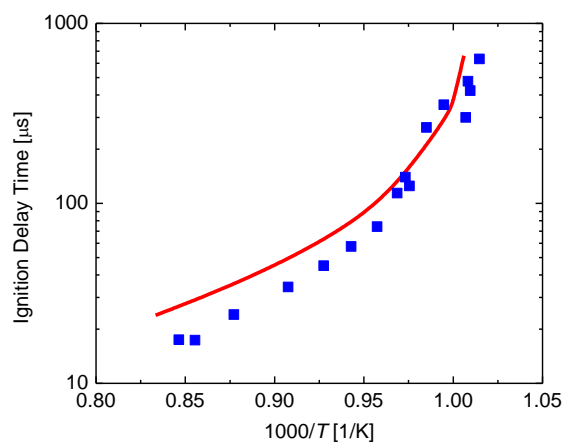


Figure S3. Comparison between experimental data (in blue) (Slack [82]) and the prediction of the current mechanism in a stoichiometric  $\text{H}_2/\text{air}$  mixture at 2 atm.

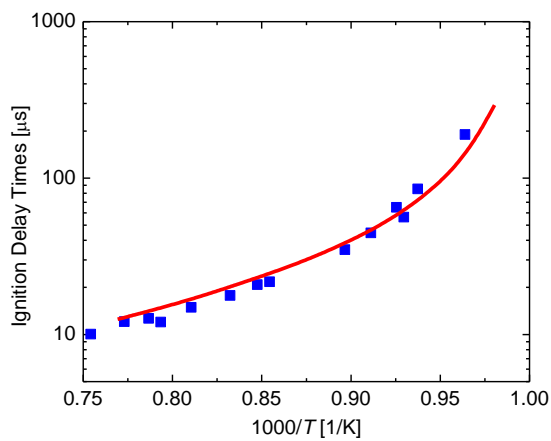


Figure S4. Comparison between experimental data (in blue) (Bhaskaran et al. [83]) and the prediction of the current mechanism in a mixture consisting of 22.59%  $\text{H}_2$ , 14.79%  $\text{O}_2$ , balance  $\text{N}_2$  at 2.5 atm.

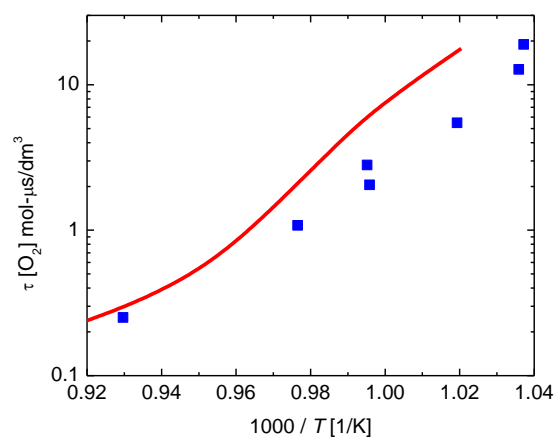


Figure S5. Comparison between experimental data (in blue) (Skinner & Ringrose [84]) and the prediction of the current mechanism in a mixture consisting of 8% H<sub>2</sub>, 2% O<sub>2</sub>, balance Ar at 5 atm.

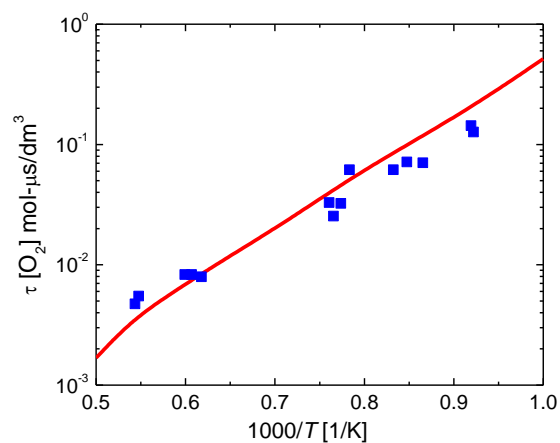


Figure S6. Comparison between experimental data (in blue) (Schott & Kinsey [85]) and the prediction of the current mechanism in a mixture consisting of 1% H<sub>2</sub>, 2% O<sub>2</sub>, balance Ar at 1 atm.

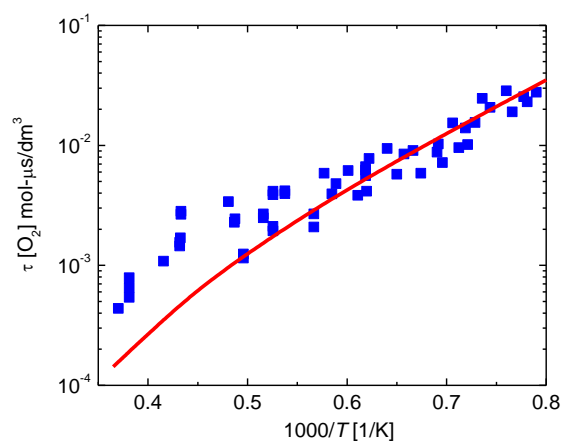


Figure S7. Comparison between experimental data (in blue) (Schott & Kinsey [85]) and the prediction of the current mechanism in a mixture consisting of 4% H<sub>2</sub>, 2% O<sub>2</sub>, balance Ar at 1 atm.

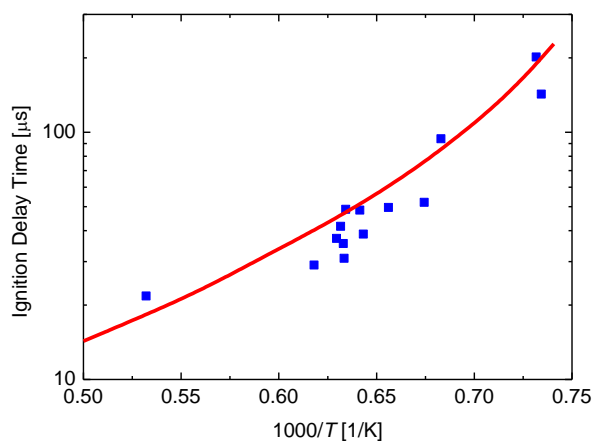


Figure S8. Experimental data (in blue) are from Petersen et al. [86]. Test mixture consisted of 0.1% H<sub>2</sub>, 0.05% O<sub>2</sub>, and balance Ar at 64 atm. Ignition time defined as the point where d(OH)/dt is maximum.

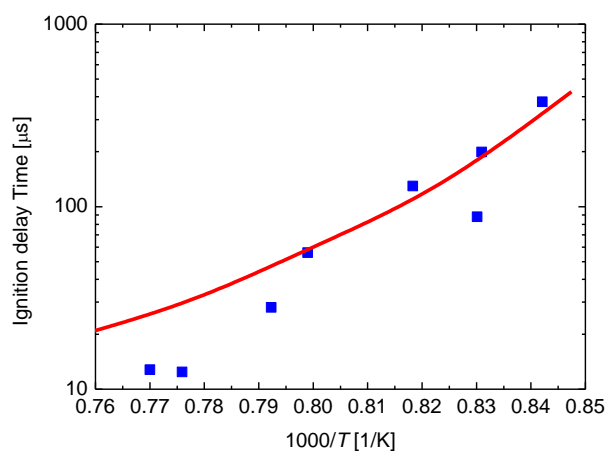


Figure S9. Experimental data (in blue) are from Petersen et al. [86]. Test mixture consisted of 2% H<sub>2</sub>, 1% O<sub>2</sub>, and balance Ar at 33 atm. Ignition time defined as the point where  $d(\text{OH})/dt$  is maximum.

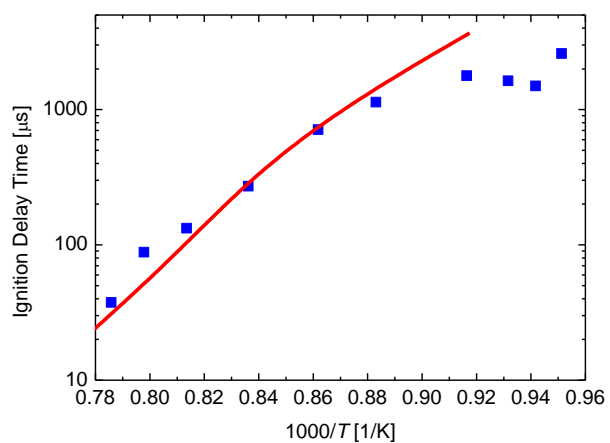


Figure S10. Experimental data (in blue) are from Wang et al. [87]. Test mixture consisted of 11.25% H<sub>2</sub>, 63.75% air, 25% H<sub>2</sub>O, at 4-5 atm. Ignition time defined as the onset of OH emission.

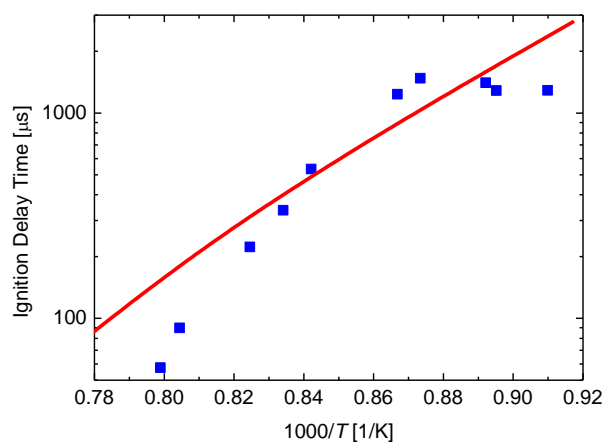


Figure S11. Experimental data (in blue) are from Wang et al. [87]. Test mixture consisted of 11.25% H<sub>2</sub>, 63.75% air, 25% H<sub>2</sub>O, at 9-10 atm. Ignition time defined as the onset of OH emission.

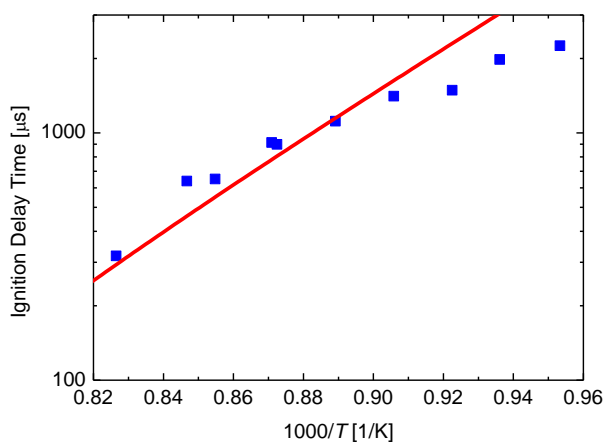


Figure S12. Experimental data (in blue) are from Wang et al. [87]. Test mixture consisted of 11.25% H<sub>2</sub>, 63.75% air, 25% H<sub>2</sub>O, at 15-17 atm. Ignition time defined as the onset of OH emission.

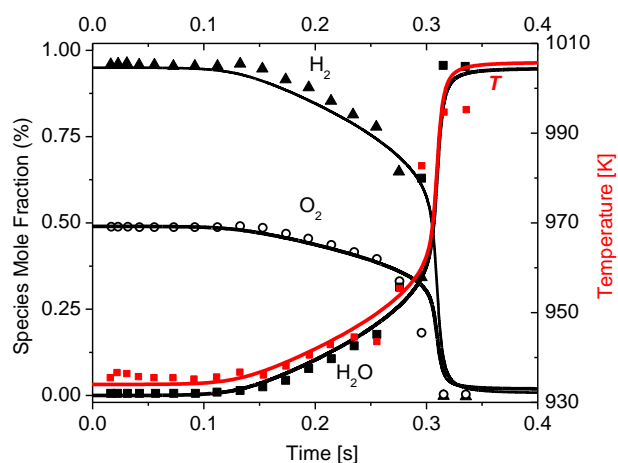


Figure S13. Species profiles from a flow reactor experiment [2]. Unburnt mixture was at 934 K, 3.02 atm and consisting of 0.95%  $\text{H}_2$ , 0.49%  $\text{O}_2$ , and  $\text{N}_2$  balance gas. The curves are calculated with the presented mechanism by using adiabatic approximation and are shifted simultaneously by 0.22 s in time. The calculated adiabatic temperature profile is also compared with experimental values.

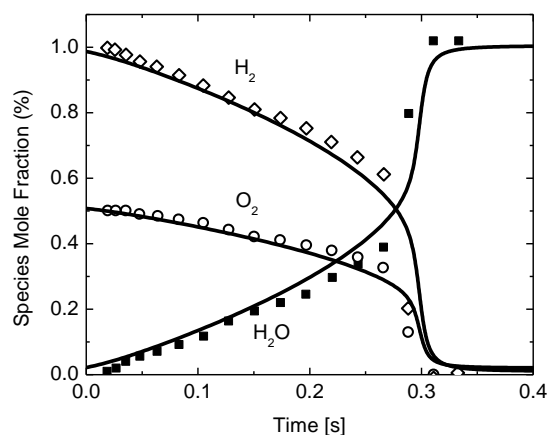


Figure S14. Species profiles from a flow reactor experiment [2]. Unburnt mixture was at 933 K, 3.4 atm and consisting of 1.01%  $\text{H}_2$ , 0.52%  $\text{O}_2$ , and  $\text{N}_2$  balance gas. The curves are calculated with the presented mechanism by using adiabatic approximation and are shifted simultaneously by 0.35 s in time.

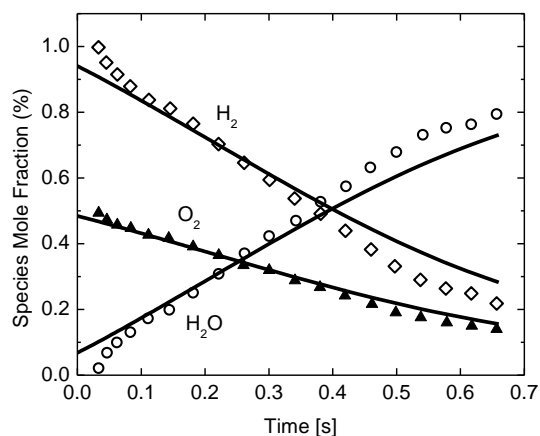


Figure S15. Species profiles from a flow reactor experiment [2]. Unburnt mixture was at 934 K, 6.0 atm and consisting of 1.01%  $\text{H}_2$ , 0.52%  $\text{O}_2$ , and  $\text{N}_2$  balance gas. The curves are calculated with the presented mechanism by using adiabatic approximation and are shifted simultaneously by 0.34 s in time.

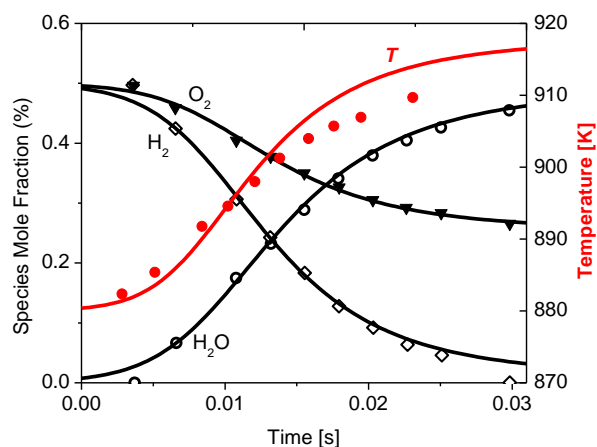


Figure S16. Species profiles from a flow reactor experiment [2]. Unburnt mixture was at 880 K, 0.32 atm and consisting of 0.5%  $\text{H}_2$ , 0.5%  $\text{O}_2$ , and  $\text{N}_2$  balance gas. The curves are calculated with the presented mechanism by using adiabatic approximation and are shifted simultaneously by 0.069 s in time. The calculated adiabatic temperature profile is also compared with experimental values.



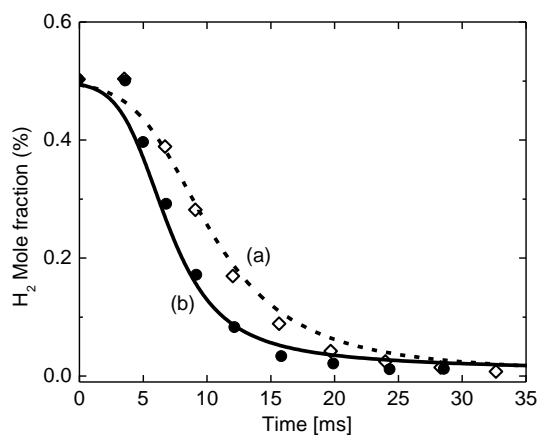


Figure S17. H<sub>2</sub> mole fraction profiles from a flow reactor experiment [2]. (a): 897 K, 0.60 atm, 0.50% H<sub>2</sub>/0.34% O<sub>2</sub>/N<sub>2</sub>,  $\phi = 0.75$ , time shift = 75 ms; (b) 896 K, 0.60 atm, 0.50% H<sub>2</sub>/0.76% O<sub>2</sub>/N<sub>2</sub>,  $\phi = 0.33$ , time shift = 48 ms.

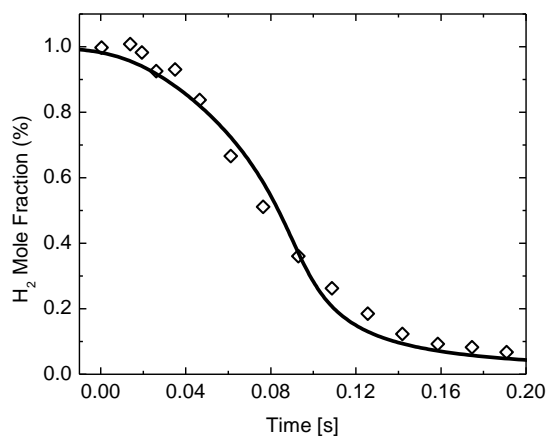


Figure S18. H<sub>2</sub> mole fraction profile from a flow reactor experiment [2]. Unburnt mixture was at 943 K, 2.5 atm and consisting of 1% H<sub>2</sub>, 1.5% O<sub>2</sub>, and N<sub>2</sub> balance gas. The H<sub>2</sub> time-history was shifted forward by 0.23 s in time.

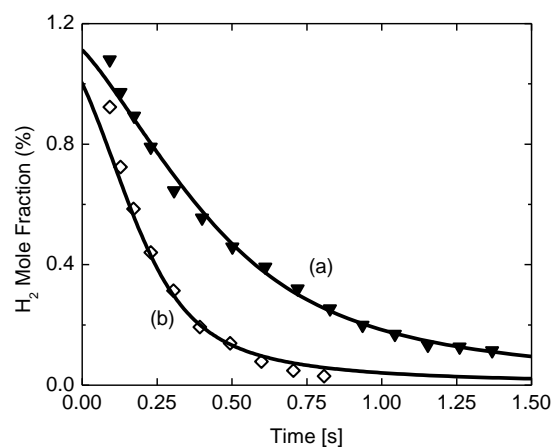


Figure S19.  $\text{H}_2$  mole fraction profiles from a flow reactor experiment [2]. (a): 914 K, 15.7 atm, 1.18%  $\text{H}_2/0.61\% \text{O}_2/\text{N}_2$ ,  $\phi = 1$ , time shift = 0.27 s; (b) 914 K, 15.7 atm, 1.18%  $\text{H}_2/2.21\% \text{O}_2/\text{N}_2$ ,  $\phi = 0.27$ , time shift = 0.31 s.

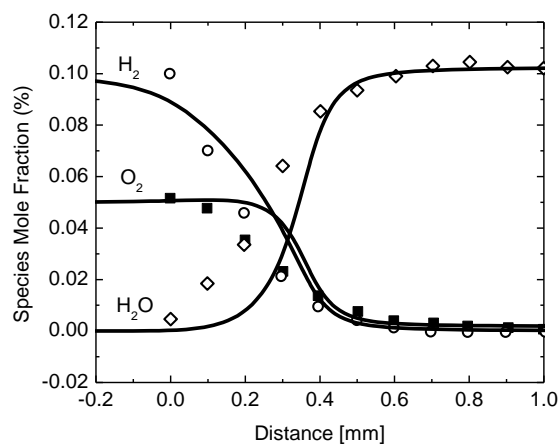


Figure S20. The structure of a burner-stabilized flame studied using a mixture of 10%  $\text{H}_2$ , 5%  $\text{O}_2$  and balance Ar (by mole) at 10 atm and 363 K, mass flow rate:  $0.135 \text{ [g cm}^{-2}\text{s}^{-1}]$ . Experimental data are from the study by Paletskii et al. [100]; and the curves are calculated using the current mechanism.