

ECE264A Lect 10 Stability

1. ECE486 UIUC Lect 18

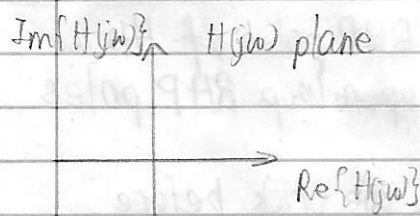
Nyquist Criterion

mapping

$$1.1. H(s) = \frac{(s-z_1)\dots(s-z_m)}{(s-p_1)\dots(s-p_n)} \quad m < n$$

(strictly proper)

$$H(j\omega) = \frac{(j\omega-z_1)\dots(j\omega-z_m)}{(j\omega-p_1)\dots(j\omega-p_n)}$$



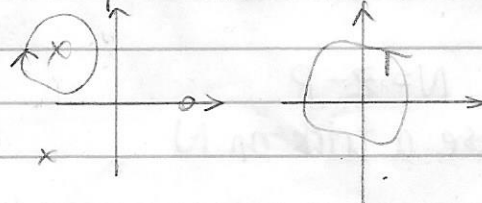
$$\psi_1 - 360^\circ$$

other ψ and ϕ no change

$$\Rightarrow \angle H(s) - 360^\circ$$

$\Rightarrow H(s)$ encircle origin once in $H(s)$ -plane, \curvearrowright (cw)

1.2.2. pole encirclement



$$\psi_1 - 360^\circ$$

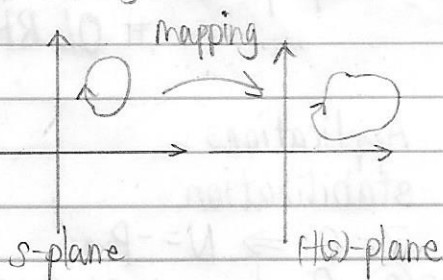
other no change

$$\Rightarrow \angle H(s) + 360^\circ$$

$\Rightarrow \curvearrowleft$ (ccw) encirclement of origin

which is like the Γ -plane in RF

But, in general



1.2.3. nothing encirclement

$H(s)$ no encirclement of origin

1.2.4. Argument Principle

$$N = Z - P$$

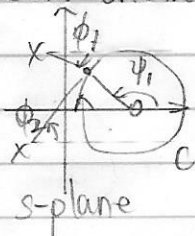
$$H(s) \curvearrowright \text{ (cw)} = (\# \text{ of } z - \# \text{ of } p) \text{ in } C$$

$$1.2. \angle H(s) = \sum_{i=1}^m \angle(s-z_i) - \sum_{j=1}^n \angle(s-p_j)$$

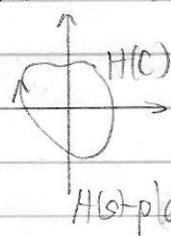
$$= \sum_{i=1}^m \psi_i - \sum_{j=1}^n \phi_j$$

phase change
contour
traversal

1.2.1. zero encirclement



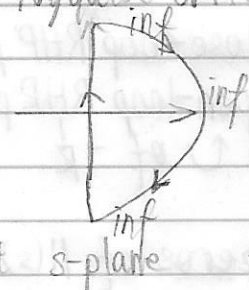
and zero
pole
encirclement



1.3. Nyquist Criterion

1.3.1.

Nyquist
Contour
and
Nyquist
Plot



$H(s)$ is the
"Nyquist" plot

for strictly proper $H(s)$,
 $H(\infty) = 0$

1.3.2

In ECE 486, the fb sys 1.3.3.2 $P = \# \text{ RHP poles of } H(s)$ $= ?$

This is not immediately obvious.

Need to link it to open-loop quantities.

$$Q(s) = \frac{q(s)}{p(s)}$$

$$H(s) = 1 + KQ(s) = \frac{p(s) + Kq(s)}{p(s)}$$

$$\frac{KG(s)}{1+KG(s)}$$

$$\text{Let } H(s) = KG(s) + 1$$

Thus,

$$P = \# \text{ RHP poles of } H(s)$$

$$= \# \text{ open-loop RHP poles}$$

$$N = Z - P$$

use a trick on N

1.3.3.3 N is the trick before

$$N = H(s) \curvearrowright \text{ of } 0$$

$$= 1 + KG(s) \curvearrowright \text{ of } 0$$

$$= KG(s) \curvearrowright \text{ of } -1$$

$$= G(s) \curvearrowright \text{ of } -\frac{1}{K}$$

1.3.4. Nyquist Theorem

$$Z = N + P$$

$$\# \text{ CL RHP poles} = G(s) \curvearrowright -\frac{1}{K} + \# \text{ OL RHP poles}$$

1.4. Applications

1.4.1. stabilization

$$Z = 0 \Rightarrow N = -P$$

$$G(s) \curvearrowright -\frac{1}{K} = \# \text{ OL RHP poles}$$

1.3.3. Convert the problem to ...

$$Z = N + P$$

will show

$$Z = \# \text{ close-loop RHP poles}$$

$$P = \# \text{ open-loop RHP poles}$$

$$N = G(s) \curvearrowright \text{ of } -\frac{1}{K}$$

1.3.3.1 Z: # RHP zeros of $H(s)$

$$= \# \text{ closed-loop RHP poles of } \frac{KG(s)}{1+KG(s)}$$

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4. Examples

4.3. $A(s) = A_0 \frac{a(s)}{1 + f_0 a(s)}$

$$T(s) = f_0 a(s)$$

If $a(s) = \frac{a_0}{1 - \frac{s}{\omega_{pa}}}$

$$T(s) = \frac{f_0 a_0}{1 - \frac{s}{\omega_{pa}}}$$

$$A(s) = K \frac{1 - \frac{s}{\omega_{pa}}}{1 + \frac{f_0 a_0}{1 - \frac{s}{\omega_{pa}}}}$$

$$= K \frac{a_0}{1 + a_0 f_0 - \frac{s}{\omega_{pa}}}$$

$$= A_0 \frac{1}{1 - \frac{s}{\omega_{pA}}}$$

$$\omega_{pA} = (1 + a_0 f_0) \omega_{pa}$$

4.4. If $a(s) = \frac{a_0}{(1 - \frac{s}{\omega_{pa1}})(1 - \frac{s}{\omega_{pa2}})}$

$$T(s) = \frac{a_0 f_0}{(1 - \frac{s}{\omega_{pa1}})(1 - \frac{s}{\omega_{pa2}})}$$

$$A(s) = K \frac{\frac{a_0}{(1 - \frac{s}{\omega_{pa1}})(1 - \frac{s}{\omega_{pa2}})}}{1 + \frac{a_0 f_0}{(1 - \frac{s}{\omega_{pa1}})(1 - \frac{s}{\omega_{pa2}})}}$$

$$= K \frac{a_0}{(1 - \frac{s}{\omega_{pa1}})(1 - \frac{s}{\omega_{pa2}}) + a_0 f_0}$$