

S 与 t 的符号意义

$$s: \text{时域微分} \quad sF(s) \rightarrow \frac{d}{dt}f(t)$$

$$\frac{1}{s}: \text{时域积分} \quad \frac{1}{s}F(s) \rightarrow \int_0^t f(x)dx$$

$$t: \text{频域微分} \quad t f(t) \rightarrow -\frac{d}{ds}F(s) \quad t^n f(t) \rightarrow (-1)^n \frac{d^n}{ds^n}F(s)$$

$$\frac{1}{t}: \text{频域积分} \quad \frac{1}{t}f(t) \rightarrow \int_s^{+\infty} F(s)ds$$

(i) For linear factor $as + b$ of $Q(s)$, exists a partial fraction of the form

$$\frac{A}{as + b}, \quad A \text{ constant}$$

(ii) For repeated linear factor $(as + b)^n$ of $Q(s)$, exists a partial fraction of the form

$$\frac{A_1}{as + b} + \frac{A_2}{(as + b)^2} + \cdots + \frac{A_n}{(as + b)^n}, \quad A_1, A_2, \dots, A_n \text{ constants}$$

(iii) For quadratic factor $as^2 + bs + c$ of $Q(s)$, exists a partial fraction of the form

$$\frac{As + B}{as^2 + bs + c}, \quad A, B \text{ constants}$$

(iv) For repeated quadratic factor $(as^2 + bs + c)^n$ of $Q(s)$, exists a partial fraction of the form

$$\frac{A_1s + B_1}{as^2 + bs + c} + \frac{A_2s + B_2}{(as^2 + bs + c)^2} + \cdots + \frac{A_ns + B_n}{(as^2 + bs + c)^n}, \quad A_1, \dots, A_n, B_1, \dots, B_n \text{ constants}$$

关于 S 的分式多项式进行 Laplace 反变换

求系数的通用方法:

- ① 系数所在分母为该项的最高次项, 则同乘该项, 令 S 取值使其余项为 0.
 ↓
 ② 不为 则乘最高次项, 并求导 ↑

Example:

$$\mathcal{L}^{-1}\left(\frac{s+1}{s^2(s-1)}\right) \xrightarrow{\text{Partial Fraction}} F(s) = \frac{s+1}{s^2(s-1)} = \frac{A}{s} + \frac{B}{s^2} + \frac{C}{s-1}$$

求系数的方程:
~~和分子消去其余项~~
 $C = (s-1)F(s)|_{s=1} = 2, \quad B = s^2 F(s)|_{s=0} = -1, \quad A = \left[\frac{d}{ds}\right](s^2 F(s))|_{s=0} = -2$



存在比该项分母更高阶的分母项时用微分

Case: 对微分方程进行拉普拉斯变换后仍为微分方程 ($aF(s) + bF'(s) + c = 0$)

$$y'' + ty' - 2y = 4 \quad y(0) = -1 \quad y'(0) = 0$$

$$\begin{aligned} L(ty'(t)) &= -\frac{d}{ds}(sY(s)) = -(Y(s) + sY'(s)) \\ L(y(t)) &= sY(s) \end{aligned}$$

$$[s^2 Y(s) - sY(0) - y'(0)] - [Y(s) + sY'(s)] - 2Y(s) = \frac{4}{s}$$

$$s^2 Y(s) + s - 3Y(s) - sY'(s) = \frac{4}{s} \quad (s^2 - 3)Y(s) - sY'(s) + s = \frac{4}{s} \quad (s - \frac{3}{s})Y(s) - Y(s) = \frac{4}{s} - 1$$

$$Y'(s) + (\frac{3}{s} - s)Y(s) = 1 - \frac{4}{s^2}$$

↓ 一般求解微分方程方法

$$\text{Integrating Factor } M(s) = e^{\int (\frac{3}{s} - s) ds} = s^3 e^{-s^2/2}$$

微分方程两边同乘积分因子 $M(s)$, 使得左边变为某项的导数形式

$$M'(s) = 3s^2 e^{-s^2/2} + s^3 \cdot e^{-s^2/2} \cdot (-s) = 3s^2 e^{-s^2/2} - s^4 e^{-s^2/2} = (\frac{3}{s} - s) \cdot s^3 e^{-s^2/2} = (\frac{3}{s} - s)M(s)$$

左边:

$$M(s) \cdot Y'(s) + M(s) \cdot (\frac{3}{s} - s)Y(s) = M(s)Y'(s) + M(s)Y(s) = (M(s)Y(s))'$$

右边:

$$(1 - \frac{4}{s^2}) \cdot M(s) = (1 - \frac{4}{s^2}) \cdot (s^3 e^{-s^2/2})$$

方程:

$$(Y(s) \cdot s^3 e^{-s^2/2})' = s^3 e^{-s^2/2} - 4s^2 e^{-s^2/2}$$

$$\text{两边积分: } Y(s) \cdot s^3 e^{-s^2/2} = \int s^3 e^{-s^2/2} ds - \int 4s^2 e^{-s^2/2} ds$$

↓

$$Y(s) = \frac{2!}{s^3} - \frac{1}{s} + \frac{C}{s^3} e^{s^2/2}$$

$$Y(t) = L(Y(s)) = t^2 - 1 + 0 \quad ?$$

Free Undamped Vibration

$$m\ddot{x} + kx = 0 \Rightarrow \ddot{x} + \omega^2 x = 0, \quad \omega = \sqrt{\frac{k}{m}}$$

↓ Laplace Transform

design

Free undamped vibration (continue):

无阻尼自由振动

$$s^2 \mathcal{L}(x) - sx(0) - \dot{x}(0) + \omega^2 \mathcal{L}(x) = 0$$



$$\mathcal{L}(x) = x(0) \frac{s}{s^2 + \omega^2} + \frac{\dot{x}(0)}{\omega} \frac{\omega}{s^2 + \omega^2}$$

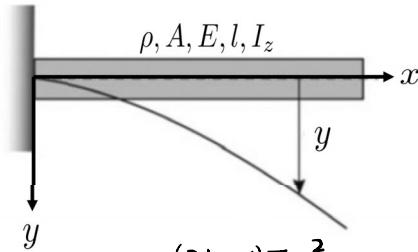
↓ Inverse Laplace transform

$$x(t) = A \cos \omega t + B \sin \omega t, \quad A = x(0), B = \frac{\dot{x}(0)}{\omega}$$

$$= X \sin(\omega t + \phi), \quad X = \sqrt{A^2 + B^2}, \quad \phi = \tan^{-1} \left(\frac{A}{B} \right) \quad \omega = \sqrt{\frac{k}{m}}$$

X is called the amplitude, ϕ is called the phase angle, ω is called the natural frequency.

Example 3: equivalent bending vibration (cantilever beam)



ρ : density
 A : cross-section area
 E : Young's modulus
 l : length
 I_z : area moment

静态加载时: $y(x) = \frac{(3l-x)Fx^2}{6EIz}$

amplitude at free end

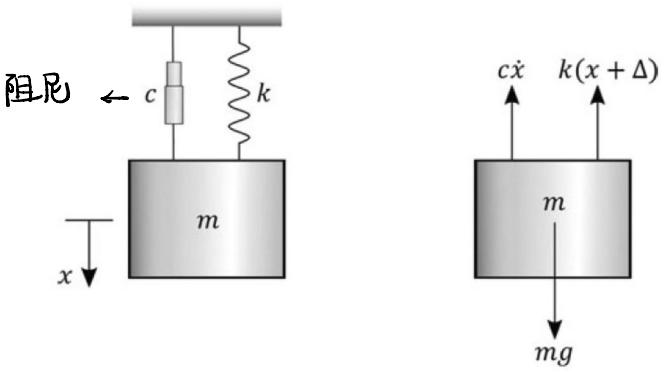
假设动态与静态加载变化一致: $y(x,t) = \phi(x) \cdot q(t)$

↓
shape function

System	Shape Function	m_e	k_e
 Longitudinal vibration	$\phi(x) = \frac{x}{l}$	$m + \frac{\rho Al}{3}$	$\frac{EA}{l}$
 Torsional vibration	$\phi(x) = \frac{x}{l}$	$I + \frac{\rho J l}{3}$	$\frac{GJ}{l}$

System	Shape Function	m_e	k_e
 Bending of a cantilever beam	$\phi(x) = \frac{3x^2l - x^3}{2l^3}$	$m + \frac{33\rho Al}{140}$	$\frac{3EIz}{l^3}$
 Bending of a simply supported beam	$\phi(x) = \sin\left(\frac{\pi x}{l}\right)$	$m + \frac{\rho Al}{2}$	$\frac{\pi^4 EIz}{2l^3}$

Free Damped Vibration



$$m\ddot{x} = mg - c\dot{x} - k(x + \Delta)$$

$$mg = k\Delta x$$

↓

$$m\ddot{x} + c\dot{x} + kx = 0$$

↓ Laplace Transform

$$m \cdot (s^2 L(x) - s x(0) - \dot{x}(0)) + c(s L(x) - x(0)) + k L(x) = 0$$

$$m s^2 L(x) - m s x_0 - m \dot{x}_0 + c s L(x) - c x_0 + k L(x) = 0$$

$$(m s^2 + c s + k) L(x) - (m s + c) x_0 - m \dot{x}_0 = 0$$

$$L(x) = \frac{(m s + c) x_0 + m \dot{x}_0}{m s^2 + c s + k} = \frac{(s + \frac{c}{m}) x_0 + \dot{x}_0}{s^2 + \frac{c}{m} s + \frac{k}{m}} = \frac{x_0 s + \frac{c}{m} x_0 + \dot{x}_0}{(s + \frac{c}{2m})^2 + \frac{k}{m} - \frac{c^2}{4m^2}} = \frac{x_0 s + 2\zeta \omega_n x_0 + \dot{x}_0}{(s + \zeta \omega_n)^2 + (1 - \zeta^2) \omega_n^2}$$

damping ratio

$$\zeta = \frac{c}{2\sqrt{km}} \quad \omega_n = \sqrt{\frac{k}{m}}$$

natural frequency

Case under-damped $\zeta < 1$ 欠阻尼, 系统仍会过振

$$L(x) = \frac{x_0 s + 2\zeta \omega_n x_0 + \dot{x}_0}{(s + \zeta \omega_n)^2 + (1 - \zeta^2) \omega_n^2}$$

$$= x_0 \frac{(s + \zeta \omega_n)}{(s + \zeta \omega_n)^2 + (\sqrt{1 - \zeta^2} \omega_n)^2} - \frac{x_0 \zeta \omega_n + \dot{x}_0 \zeta \omega_n}{(s + \zeta \omega_n)^2 + (\sqrt{1 - \zeta^2} \omega_n)^2}$$

$$L^{-1} \downarrow$$

$$= x_0 \frac{(s + \zeta \omega_n)}{(s + \zeta \omega_n)^2 + (\sqrt{1 - \zeta^2} \omega_n)^2} - \frac{3x_0 \zeta \omega_n + \dot{x}_0}{(\sqrt{1 - \zeta^2} \omega_n)^2} \cdot \frac{(\sqrt{1 - \zeta^2} \omega_n)^2}{(s + \zeta \omega_n)^2 + (\sqrt{1 - \zeta^2} \omega_n)^2}$$

$$x(t) = x_0 \cdot e^{-\zeta \omega_n t} \cos(\sqrt{1 - \zeta^2} \omega_n t) - \frac{3x_0 \zeta \omega_n + \dot{x}_0}{(\sqrt{1 - \zeta^2} \omega_n)^2} e^{-\zeta \omega_n t} \sin(\sqrt{1 - \zeta^2} \omega_n t)$$

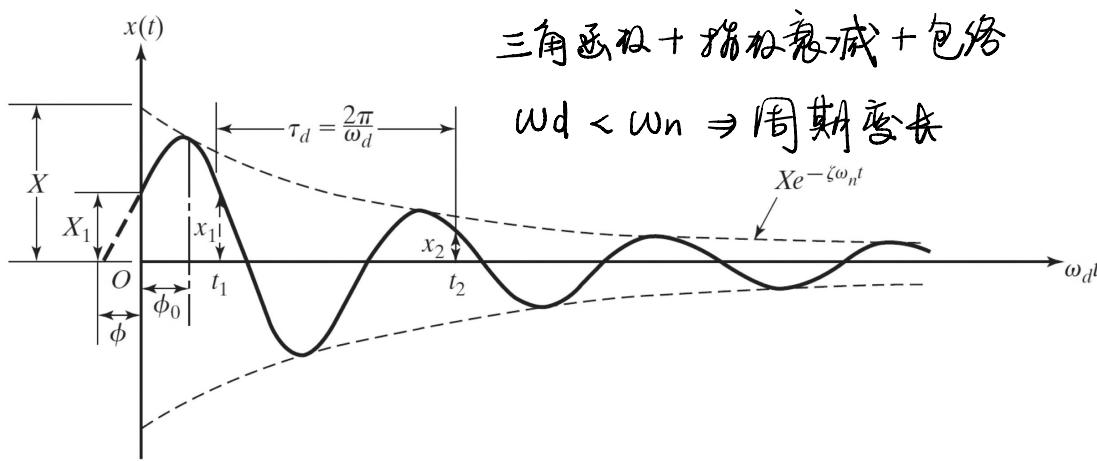
$$= e^{-\zeta \omega_n t} \cdot \sqrt{\frac{x_0^2 + (3x_0 \zeta \omega_n + \dot{x}_0)^2}{(\sqrt{1 - \zeta^2} \omega_n)^4}} \cdot \cos(\sqrt{1 - \zeta^2} \omega_n t + \phi)$$

其中

$$\tan \phi = \frac{3x_0 \zeta \omega_n + \dot{x}_0}{x_0 \cdot (\sqrt{1 - \zeta^2} \omega_n)^2}$$

$$\omega_d = \sqrt{1 - \zeta^2} \omega_n$$

damped frequency



Case $\zeta = 1$ critical damped 系统不会过振 阶跃+斜坡+阶跃衰减

$$L(X) = \frac{\chi_0 s + 2\zeta \omega_n \chi_0 + \dot{\chi}_0}{(s + \zeta \omega_n)^2 + (1 - \zeta^2) \omega_n^2} = \frac{\chi_0 s + 2\omega_n \chi_0 + \dot{\chi}_0}{(s + \omega_n)^2} = \frac{\chi_0(s + \omega_n) - \chi_0 \omega_n}{(s + \omega_n)^2} + \frac{2\omega_n \chi_0 + \dot{\chi}_0}{(s + \omega_n)^2}$$

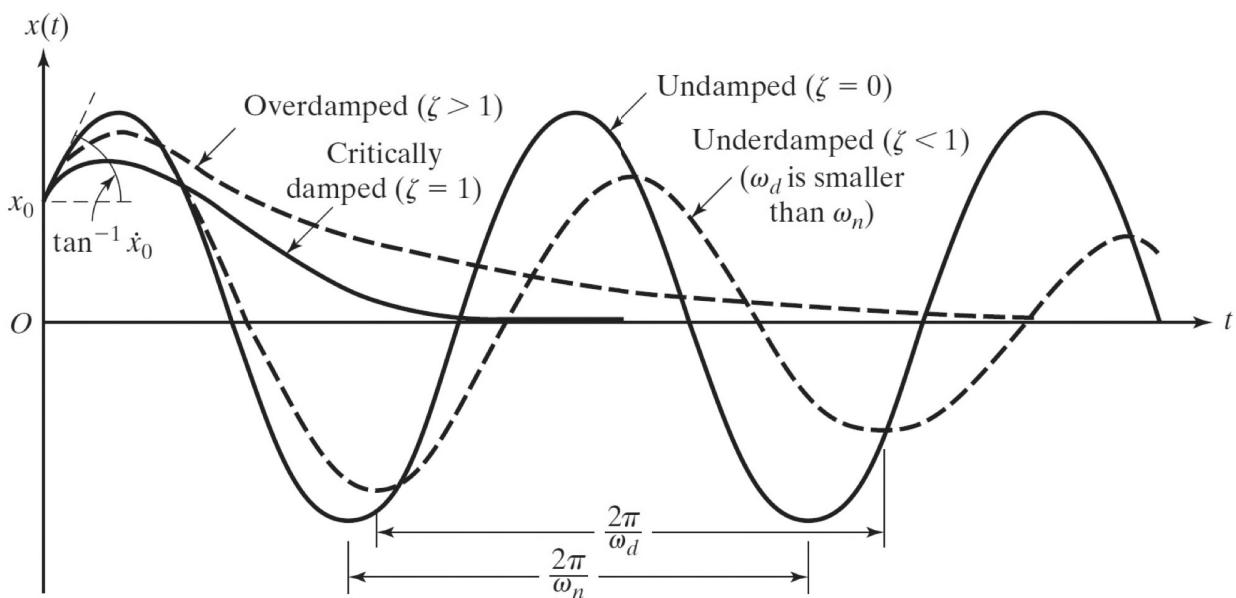
$$= \chi_0 \frac{(s + \omega_n)}{(s + \omega_n)^2} + (\omega_n \chi_0 + \dot{\chi}_0) \cdot \frac{1}{(s + \omega_n)^2}$$

$$X(t) = \chi_0 \cdot e^{-\omega_n t} \cdot u(t) + (\omega_n \chi_0 + \dot{\chi}_0) \cdot e^{-\omega_n t} \cdot t = [\chi_0 + (\omega_n \chi_0 + \dot{\chi}_0) t] e^{-\omega_n t}$$

Case $\zeta > 1$ over damped

$$L(X) = \frac{\chi_0 s + 2\zeta \omega_n \chi_0 + \dot{\chi}_0}{(s + \zeta \omega_n)^2 - (\zeta^2 - 1) \omega_n^2} = \chi_0 \frac{s + \zeta \omega_n}{(s + \zeta \omega_n)^2 - (\sqrt{\zeta^2 - 1} \omega_n)^2} + \frac{-\zeta \omega_n \chi_0 + 2\zeta \omega_n \chi_0 + \dot{\chi}_0}{(s + \zeta \omega_n)^2 - (\sqrt{\zeta^2 - 1} \omega_n)^2}$$

$$X(t) = \chi_0 \cdot e^{-\zeta \omega_n t} \cdot \cosh(\sqrt{\zeta^2 - 1} \omega_n t) + \frac{\zeta \omega_n \chi_0 + \dot{\chi}_0}{\sqrt{\zeta^2 - 1} \omega_n} \sinh(\sqrt{\zeta^2 - 1} \omega_n t) \cdot e^{-\zeta \omega_n t}$$



$$L(x) = \frac{(m\ddot{x} + c\dot{x})x_0 + m\dot{x}_0}{m\ddot{s}^2 + cs + k} = \frac{x_0 s + 2\zeta \omega_n x_0 + \dot{x}_0}{(s + \zeta \omega_n)^2 + (1 - \zeta^2) \omega_n^2} = \frac{x_0 s + 2\zeta \omega_n x_0 + \dot{x}_0}{s^2 + 2\zeta \omega_n s + \zeta^2 \omega_n^2}$$

特征根 (根轨迹法)

$$\text{求 } m\ddot{s}^2 + cs + k = 0 \quad / \quad s^2 + 2\zeta \omega_n s + \zeta^2 \omega_n^2 = 0 \quad \text{根轨迹}$$

Case i) $\zeta = 0$ (harmonic oscillation)

$$s_1 = i\omega_n, \quad s_2 = -i\omega_n$$

Case ii) $\zeta < 1$ (underdamped)

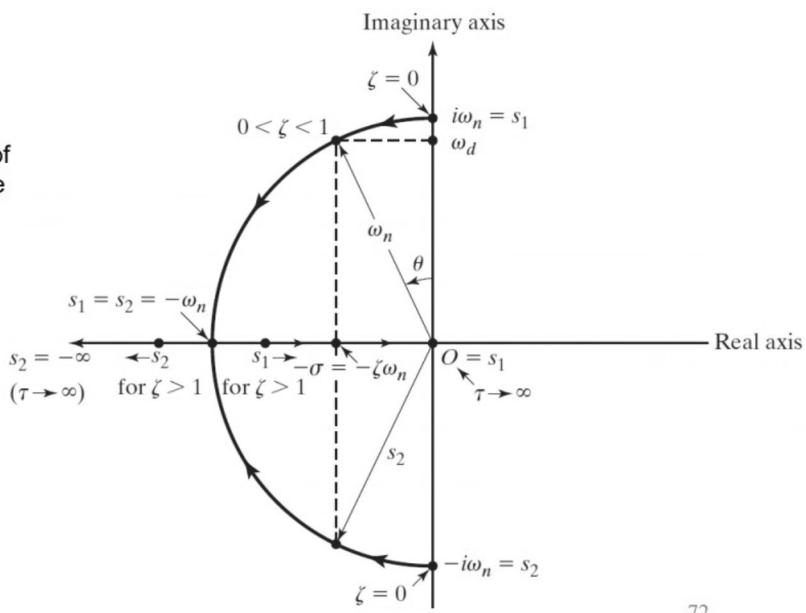
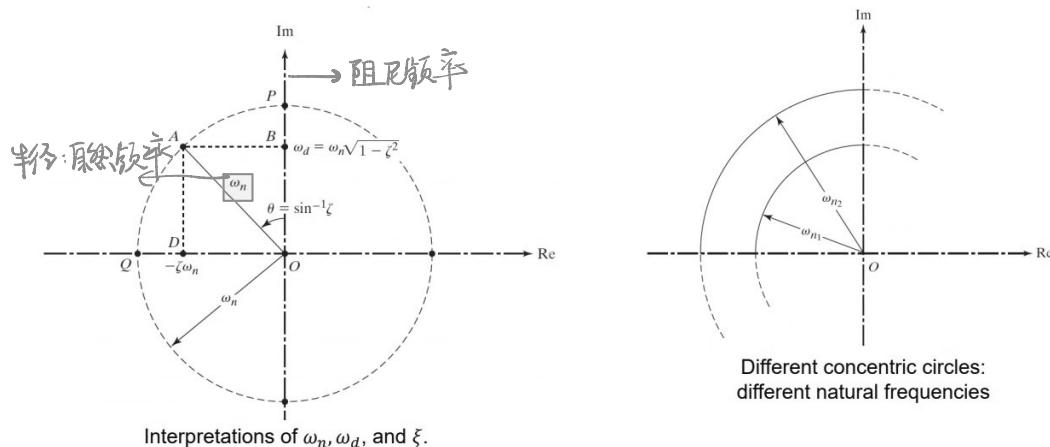
$$s_1 = (-\zeta + i\sqrt{1 - \zeta^2})\omega_n, \quad s_2 = (-\zeta - i\sqrt{1 - \zeta^2})\omega_n$$

Case iii) $\zeta = 1$ (critically damped)

$$s_1 = s_2 = -\zeta\omega_n$$

Case iv) $\zeta > 1$ (overdamped)

$$s_1 = (-\zeta + \sqrt{\zeta^2 - 1})\omega_n, \quad s_2 = (-\zeta - \sqrt{\zeta^2 - 1})\omega_n$$



有关 Hyperbolic Function

双曲函数 (hyperbolic function) 可借助指数函数定义 [1]

$$\text{双曲正弦: } \sinh x = \frac{e^x - e^{-x}}{2}$$

$$\text{双曲余弦: } \cosh x = \frac{e^x + e^{-x}}{2}$$

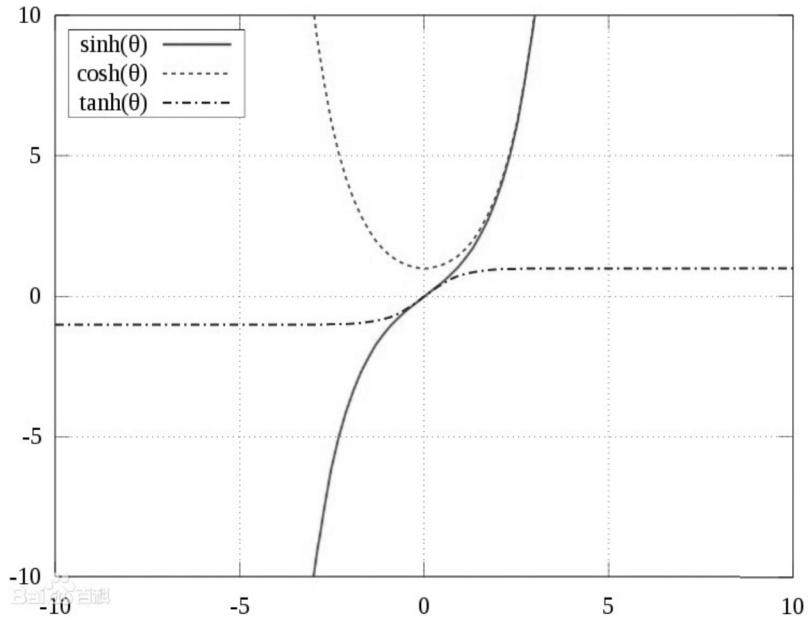
$$\text{双曲正切: } \tanh x = \frac{\sinh x}{\cosh x} = \frac{e^x - e^{-x}}{e^x + e^{-x}}$$

$$\text{双曲余切: } \coth x = \frac{1}{\tanh x} = \frac{e^x + e^{-x}}{e^x - e^{-x}}$$

$$\text{双曲正割: } \operatorname{sech} x = \frac{1}{\cosh x} = \frac{2}{e^x + e^{-x}}$$

$$\text{双曲余割: } \operatorname{csch} x = \frac{1}{\sinh x} = \frac{2}{e^x - e^{-x}}$$

$$\cosh^2 x - \sinh^2 x = 1$$



与三角函数关系

双曲函数与三角函数有如下的关系:

$$\sinh x = -i \sin ix$$

$$\cosh x = \cos ix$$

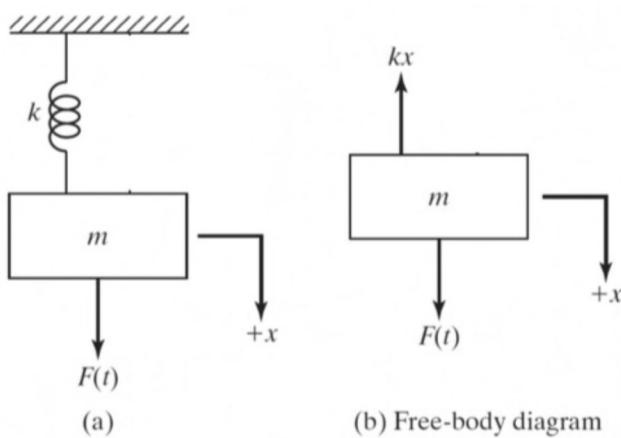
$$\tanh x = -i \tan ix$$

$$\coth x = i \cot ix$$

$$\operatorname{sech} x = \sec ix$$

$$\operatorname{csch} x = i \csc ix$$

Forced Vibration 单自由度受迫振动



$$\text{equation of motion : } F(t) + mg - k(x+\delta) = m\ddot{x}$$

习惯上定义物体平衡点为X原点。

Laplace Transform :

$$\mathcal{L}(x) = \frac{F_0}{m} \frac{s}{(s^2 + \omega^2)(s^2 + \omega_n^2)} + \frac{x_0 s + \dot{x}_0}{s^2 + \omega_n^2}, \quad \omega_n = \sqrt{\frac{k}{m}}$$

$$\mathcal{L}(x) = \frac{F_0}{m(\omega_n^2 - \omega^2)} \left(\frac{s}{s^2 + \omega^2} - \frac{s}{s^2 + \omega_n^2} \right) + x_0 \frac{s}{s^2 + \omega_n^2} + \frac{\dot{x}_0}{\omega_n} \frac{\omega_n}{s^2 + \omega_n^2}$$

Define static deflection $\delta_{st} = F_0/k$

$$x(t) = \left(x_0 - \frac{\delta_{st}}{m(\omega_n^2 - \omega^2)/k} \right) \cos \omega_n t + \frac{\dot{x}_0}{\omega_n} \sin \omega_n t + \frac{\delta_{st}}{m(\omega_n^2 - \omega^2)/k} \cos \omega t$$

$$= \underbrace{\left(x_0 - \frac{\delta_{st}}{1 - \left(\frac{\omega}{\omega_n} \right)^2} \right) \cos \omega_n t + \frac{\dot{x}_0}{\omega_n} \sin \omega_n t}_{\text{Homogeneous solution } x_h \text{ (transient)}} + \underbrace{\frac{\delta_{st}}{1 - \left(\frac{\omega}{\omega_n} \right)^2} \cos \omega t}_{X}$$

Particular solution x_p
(steady-state)

$$\text{Amplitude ratio } X/\delta_{st} \text{ and frequency ratio } r = \omega/\omega_n$$

X	1
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受迫振动中，
 频率 ω 为自然频率 ω_n 部分为 脉冲态 transient
 (振动物体)
 频率 ω 为施加力的频率 ω 部分为 稳态 steady state

频率 ω 为施加力的频率 ω 部分为 稳态 steady

振动图像为脉冲态与稳态的叠加。

(见 Matlab Session)

若有阻尼时，脉冲态部分会逐渐衰减，最终只剩下稳态部分

frequency ratio: $r = \omega/\omega_n$

amplitude ratio: $X_{\text{st}} = \frac{1 - (\frac{\omega}{\omega_n})^2}{F_0/k}$

↓
Static deflection

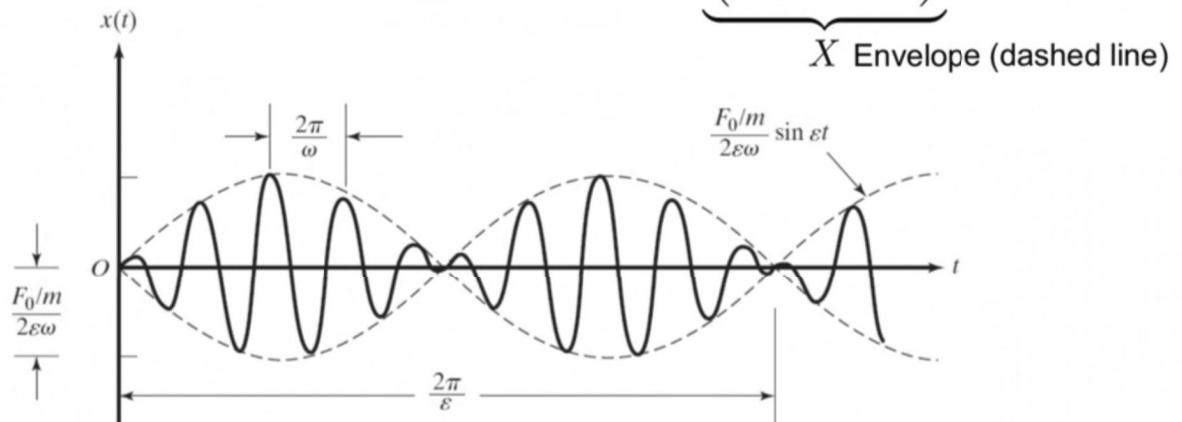
Beating $\omega = \omega_n$

Beating phenomenon (let $x_0 = \dot{x}_0 = 0$):

$$x(t) = \frac{\delta_{\text{st}}}{1 - r^2} \left[2 \sin \frac{\omega + \omega_n}{2} t \sin \frac{\omega_n - \omega}{2} t \right]$$

If $\omega_n - \omega = 2\varepsilon$ is a small positive quantity, then $\omega_n \approx \omega$ and

$$\omega + \omega_n \approx 2\omega, \quad \omega_n^2 - \omega^2 \approx 4\varepsilon\omega \quad \rightarrow \quad x(t) = \underbrace{\left(\frac{F_0/m}{2\varepsilon\omega} \sin \varepsilon t \right)}_{X \text{ Envelope (dashed line)}} \sin \omega t$$

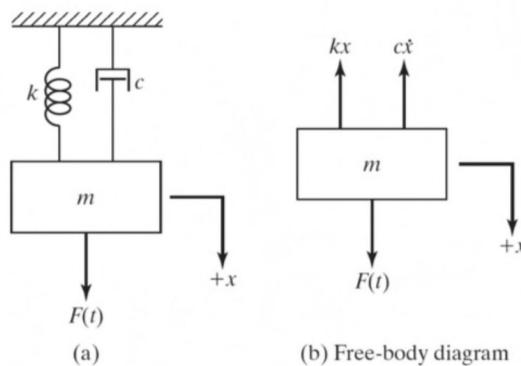


CDM 7.02 Mechanical Eng Design

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单自由度阻尼受迫振动

Response of a damped system under harmonic force



$$m\ddot{x} + c\dot{x} + kx = F_0 \cos \omega t$$

↓ Laplace transform

$$\mathcal{L}(x) = \frac{F_0}{m} \frac{s}{(s^2 + \omega^2)(s^2 + 2\zeta\omega_n s + \omega_n^2)} + \frac{x_0(s + 2\zeta\omega_n) + \dot{x}_0}{s^2 + 2\zeta\omega_n s + \omega_n^2}, \quad \omega_n = \sqrt{\frac{k}{m}}, \zeta = \frac{c}{2\sqrt{mk}}$$

Partial fraction of steady-state part: $F(s) = \mathcal{L}(x_p(t))$

求解太困难了

$$F(s) = \frac{F_0}{m} \left(\frac{a_1 s + a_2}{s^2 + \omega^2} + \frac{a_3 s + a_4}{s^2 + 2\zeta\omega_n s + \omega_n^2} \right)$$

$$a_1 = \frac{\omega_n^2 - \omega^2}{(2\zeta\omega_n)^2\omega^2 + (\omega_n^2 - \omega^2)^2} \quad a_3 = -\frac{\omega_n^2 - \omega^2}{(2\zeta\omega_n)^2\omega^2 + (\omega_n^2 - \omega^2)^2}$$

$$a_2 = \frac{2\zeta\omega_n\omega^2}{(2\zeta\omega_n)^2\omega^2 + (\omega_n^2 - \omega^2)^2} \quad a_4 = -\frac{2\zeta\omega_n^3}{(2\zeta\omega_n)^2\omega^2 + (\omega_n^2 - \omega^2)^2}$$

Partial fraction of complete solution: $X(s) = \mathcal{L}(x(t))$

力矩不为零 steady

$$X(s) = \frac{F_0}{m} \frac{1}{(2\zeta\omega_n)^2\omega^2 + (\omega_n^2 - \omega^2)^2} \left[\underbrace{(\omega_n^2 - \omega^2) \left(\frac{s}{s^2 + \omega^2} \right) + (2\zeta\omega_n\omega) \left(\frac{\omega}{s^2 + \omega^2} \right)}_{\text{自然频率 transient}} \right. \\ \left. - (\omega_n^2 - \omega^2) \left(\frac{s}{s^2 + 2\zeta\omega_n s + \omega_n^2} \right) - (2\zeta\omega_n) \left(\frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \right) \right]$$

自然频率 transient

Total solution:

$$x(t) = \boxed{\frac{F_0}{m} \frac{1}{(2\zeta\omega_n)^2 + (\omega_n^2 - \omega^2)^2} [(\omega_n^2 - \omega^2) \cos \omega t + 2\zeta\omega_n\omega \sin \omega t] \quad \text{Steady-state } x_p(t)}$$

$$+ \frac{(\omega_n^2 - \omega^2)}{\sqrt{1 - \zeta^2}} e^{-\zeta\omega_n t} \sin(\omega_n \sqrt{1 - \zeta^2} t - \phi) \quad \phi = \tan^{-1} \left(\frac{1 - \zeta^2}{\zeta} \right)$$

$$- \frac{(2\zeta\omega_n^2)}{\sqrt{1 - \zeta^2}} e^{-\zeta\omega_n t} \sin(\omega_n \sqrt{1 - \zeta^2} t) \quad \text{Transient } x_h(t) \text{ (decays to 0 if } \zeta > 0 \text{)}$$

$$x_p(t) = \frac{F_0}{m} \frac{1}{(2\zeta\omega_n)^2 + (\omega_n^2 - \omega^2)^2} [(\omega_n^2 - \omega^2) \cos \omega t + 2\zeta\omega_n\omega \sin \omega t]$$

$$= \underbrace{\frac{F_0}{\sqrt{c^2\omega^2 + (k - m\omega^2)^2}}}_{X} \cos(\omega t - \phi) \quad \phi = \tan^{-1} \left(\frac{2\zeta r}{1 - r^2} \right)$$

对比(有/无)阻尼受迫振动

```

%% Transfer Function 1
clc; close all;
x0=1;x0_dot=1; %Initial condition
L1=TransFunc(0,1);
L2=TransFunc(0.5,1);
L3=TransFunc(1,1);
L4=TransFunc(2,1);
figure
impulse(L1)
xlim([0 20])
hold on
impulse(L2)
impulse(L3)
impulse(L4)
legend("ksi = 0","ksi = 0.5","ksi = 1","ksi = 2")
title("Impulse Response when omega = 1")
hold off

%% Transfer Function 2 无阻尼受迫振动
x0=0.1;x0_dot=0; %Initial condition
F0 = 10;
m = 4;
w = 5; %稳态频率 (力的频率)
wn = 2; %瞬态频率 (物体自然频率)

num_static=[1 0];
den_static=[1 0 w^2];
Ls=F0/(m*(wn^2-w^2))*tf(num_static,den_static)

num_transient1=[1 0];
den_transient1=[1 0 wn^2];
num_transient2=[wn];
den_transient2=[1 0 wn^2];
Lt=(-F0/(m*(wn^2-w^2))+x0)*tf(num_transient1,den_transient1)+x0_dot/wn*tf(num_transient2,den_transient2)

L=Ls+Lt
figure
hold on
impulse(Ls)
impulse(Lt)
impulse(L)
xlim([0 20])
ylim([-0.5 0.5])
legend("Ls","Lt","L")

```



```

%% Transfer Function3 阻尼受迫振动
x0=0.1;x0_dot=0; %Initial condition
F0 = 10;
m = 4;
w = 5; %稳态频率 (力的频率)
wn = 2; %瞬态频率 (物体自然频率)
zeta = 0.1; %阻尼系数

num_s1=[1 0];
den_s1=[1 0 w^2];
num_s2=[w];
den_s2=[1 0 w^2];
Ls=F0/m*((wn^2-w^2)/((2*zeta*wn)^2*w^2+(wn^2-w^2)^2))*tf(num_s1,den_s1)+...
F0/m*((2*zeta*wn*w)/((2*zeta*wn)^2*w^2+(wn^2-w^2)^2))*tf(num_s2,den_s2);

num_t1=[1 0];
den_t1=[1 2*zeta*wn wn^2];
num_t2=[wn^2];
den_t2=[1 2*zeta*wn wn^2];
Lt==F0/m*((wn^2-w^2)/((2*zeta*wn)^2*w^2+(wn^2-w^2)^2))*tf(num_t1,den_t1)-...
F0/m*((2*zeta*wn)/((2*zeta*wn)^2*w^2+(wn^2-w^2)^2))*tf(num_t2,den_t2);

L=Ls+Lt
figure
hold on
impulse(Ls)
impulse(Lt)
impulse(L)
xlim([0 20])
ylim([-0.5 0.5])
legend("Ls","Lt","L")

function [L] = TransFunc(xi,w)
x0=1;x0_dot=1; %Initial condition
num=[x0 x0_dot+2*xi*w*x0];
den=[1 2*xi*w w^2];
L=tf(num,den);
end

```