

$$C = \frac{1 \text{ nC}}{78.9 \text{ V}} = 12.67 \text{ pF}$$

$$E = \frac{1}{2} (12.67 \text{ pF}) (78.9 \text{ V})^2 = 39.4 \text{ nJ}$$

f.) Voltage is  $-\int_a^b \vec{E} \cdot d\vec{l}$

In dielectric, going from  $z=0$  in bottom plate to  $z$  somewhere in the dielectric,

$$V = -\int_0^z (-2.25 \text{ kV/m}) dz = z (2.25 \times 10^3) \text{ V}$$

$$\nabla^2 V = \frac{\partial^2}{\partial z^2} (z (2.25 \times 10^3)) = 0$$

In the air gap, going from  $z=0$  at the point between the air and the dielectric to  $z$  somewhere in the air gap

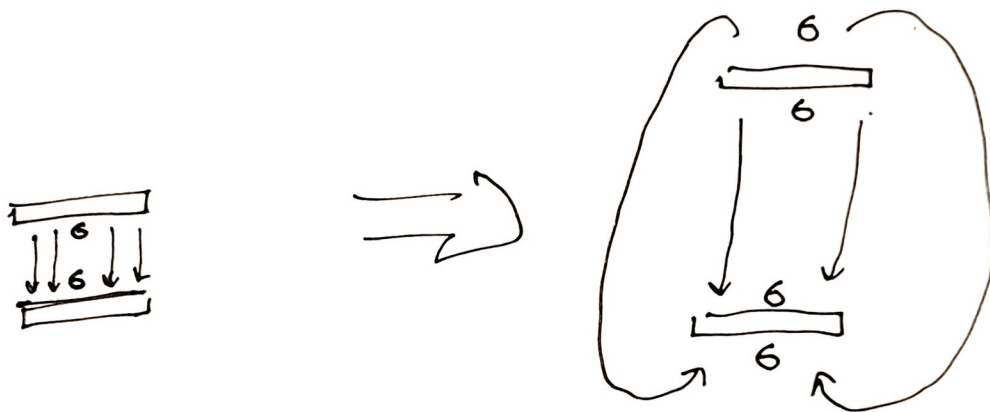
$$V = -\int_0^z (-11.29 \text{ kV/m}) dz + (\text{voltage across dielectric})$$

$$= (11.29 \times 10^3) z + (0.01)(2.25 \times 10^3)$$

$$= 22.5 + z (11290)$$

$$\nabla^2 V = \frac{\partial^2}{\partial z^2} (22.5 + z (11290)) = 0$$

g.) The  $e$ -field and capacitance expressions will be different, as fringing fields will now begin to dominate. The plate surface charge will no longer be confined to the region between plates.



$$a.) \quad \vec{E}_{2+} = \vec{E}_{1+} = 20\hat{x}$$

$$\vec{D}_{1n} - \vec{D}_{2n} = \rho_s = 0$$

$$\vec{D}_{2n} = \vec{D}_{1n}$$

$$\epsilon_2 \vec{E}_{2n} = \epsilon_1 \vec{E}_{1n}$$

$$\epsilon_0 40\hat{y} = 6\epsilon_0 \vec{E}_{1n}$$

$$\vec{E}_{1n} = \frac{1}{6} 40\hat{y} = 6.67\hat{y}$$

$$\vec{E}_1 = 20\hat{x} + 6.67\hat{y}$$

(E on top)

$$b.) \quad \vec{E}_{1t} = \vec{E}_{2t} = 100 \hat{x}$$

$$\vec{D}_{1n} - \vec{D}_{2n} = \rho_s$$

$$\epsilon_0 \vec{E}_{1n} - 2\epsilon_0 (100 \hat{y}) = (10^{-9} \text{ C/m}^2)$$

$$\vec{E}_{1n} = \frac{(10^{-9} \text{ C/m}^2)}{\epsilon_0} + 200 \hat{y} = 312 \hat{y}$$

$$\vec{E}_1 = 100 \hat{x} + 312 \hat{y}$$

4.

Initial guess:  $V_1 = V_2 = V_3 = V_4 = 0$ 

a.) 1st iteration:

$$V_1 = (80V + 20V + 0V + 0V)/4 = 25V$$

$$V_2 = (80V + 25V + 0V + 0V)/4 = 26.25V$$

$$V_3 = (25V + 20V + 50V + 0V)/4 = 23.75V$$

$$V_4 = (26.25V + 23.75V + 50V + 0V)/4 = 25V$$

2nd iteration:

$$V_1 = (80V + 20V + 23.75V + 26.25V)/4 = 37.5V$$

$$V_2 = (80V + 37.625V + 25V + 0V)/4 = 35.66V$$

$$V_3 = (37.625V + 20V + 50V + 25V)/4 = 33.16V$$

$$V_4 = (35.66V + 33.16V + 50V + 0V)/4 = 29.7V$$

$$b.) \quad E_y \approx \frac{-\Delta V}{\Delta x} = - \frac{(80 - 37.625)}{0.1m} = -423.7 \frac{V}{m} \text{ in } \hat{y}$$

c.) 1. Smaller size of calculation elements.

2. More iterations.

## 5. Capacitance part 2

$$a.) \quad J = \frac{I}{Area} = \frac{1 \text{ mA}}{\pi (0.5 \text{ mm})^2} = 1270 \text{ A/m}^2$$

$$J = \sigma E$$

$$1270 \text{ A/m}^2 = (5.9 \times 10^7) E$$

$$|E| = 21.53 \times 10^{-6} \text{ V/m}$$

b.) Electric field magnitude expression:

$$\oint \vec{D} \cdot d\vec{S} = Q_{enc}$$

$$2\pi r l \cdot D = Q_{enc}, \quad l = 5 \text{ mm}$$

$$\vec{D} = \frac{Q_{enc}}{2\pi r l} \hat{r}$$

$\vec{D} = \epsilon \vec{E}$  and  $Q$  on the outer conductor will equal  $Q_{enc}$  on the inner conductor.

The dielectric will fail first at its smallest radius,  $r=1\text{mm}$ . So we calculate the charge that will cause the capacitor to fail in the following manner:

$$E_{\text{breakdown}} = \frac{Q_{\text{outer}}}{2\pi\epsilon r l} = \frac{Q_{\text{outer}}}{2\pi(3\epsilon_0)(1\text{mm})(5\text{mm})} = 300\text{kV/cm}$$

$$Q_{\text{outer}} = (300\text{kV/cm}) \cdot 2\pi \cdot 3\epsilon_0 \cdot 1\text{mm} \cdot 5\text{mm} = 25.03\text{ nC}$$

$$1\text{ mA} = 1 \times 10^{-3}\text{ C/s}$$

$$(1 \times 10^{-3}\text{ C/s}) \cdot (x\text{ s}) = (25.03 \times 10^{-9}\text{ C})$$

$$x = 25.03\text{ }\mu\text{s}.$$

## 6. Conducting Plane

- ⑥ The  $-2nC$  charge causes positive charge to accumulate on the plane's surface in such a way that the  $-2nC$  charge sees a  $+2nC$  "image charge"  $1cm$  below the surface.

$$\vec{F} = \frac{\overset{-2nC}{\downarrow} Q_1 \overset{+2nC}{\downarrow} Q_2}{4\pi\epsilon_0 \underset{\uparrow 1cm}{R^2}} = 3.59 \times 10^{-4} N \text{ pointing down.}$$