$$\begin{array}{rcl}
\overrightarrow{B_{1n}} &= \overrightarrow{B_{2n}} &= 0.1\hat{g} \\
\overrightarrow{H_{2+1}} &- \overrightarrow{H_{1+1}} &= J_s &= 0 \\
\overrightarrow{H_{1+1}} &= \overrightarrow{H_{2+1}} \\
\overrightarrow{B_{1}} &= \overrightarrow{B_{2+1}} \\
\overrightarrow{B_{1000}}_{N_0} &= \overrightarrow{N_0}
\end{array}$$

$$\overline{B_{1+}} = 1000 \cdot (0.191 - 100 \hat{x})$$

$$\vec{B_1} = 100\hat{x} + 0.1\hat{g}$$

$$\overline{B_{1n}} = \overline{B_{2n}} = 0.1\hat{g}$$

$$\overline{H_{2+}} - \overline{H_{1+}} = J_{s}$$

$$\overline{B_{2+}} - \overline{B_{1+}} = -1 \, A/m = \frac{\text{negative sign}}{\text{due to pointing away from us}}$$

$$\overline{B_{1+}} = (\nu_{0}(1 \, A/m) + (-0.2 \over 1000)) \hat{x}$$

$$\overline{B_{1+}} = -0.0002 \hat{x}$$

$$\vec{B}_{1} = -0.0002 \times + 0.1 \hat{g}$$

2a.)

$$R = \frac{1}{6A} = \frac{1000m}{(5.9 \times 10^7 \text{ s/m})(71 (0.01)^2)} = 0.05395 \Omega$$

$$V = IR$$
 (0.1) =  $I(0.05395)$ 

$$1.854 A = J. \%.(0.01)^{2}$$
  
 $\vec{J} = 5901 A/m^{2}$ 

Inside the wire:

$$H \cdot 2\pi r = 1.854 \frac{r^2}{0.012}$$

$$\frac{1}{H} = 2951r A/m$$

Outside the wire:

$$\frac{\Delta}{B} = NoH = \frac{0.371}{r} \mu T \quad (in \phi)$$
direction

C.) 
$$\overrightarrow{B} = \nabla \times \overrightarrow{A}$$
  $\overrightarrow{A}$  goes in the direction of current, so it only has a  $z$  component.

$$\overrightarrow{B} = \begin{pmatrix} \frac{1}{r} & \frac{\partial Az}{\partial r} & -\frac{\partial Az}{\partial r} & \frac{\partial Az}$$

d.) Since there is only one turn, flux is equal to flux linkage.

e.) 
$$L = \frac{\Lambda}{\pm} = \frac{\Lambda}{\pm}$$
 (flux over (urrent)

$$\frac{1}{m} = \int \vec{B} \cdot \vec{ds} = \int dz \int (3.71r) dr$$

$$= (1000) \int (3.71r) dr$$

$$= (1000) (3.71) (0.01)^{2}/2$$

$$= 0.371 Wb/2$$

$$L = \frac{0.371 Wb}{1.854 A} = 200mH/2$$

f.) 
$$0 - 1000 \, \text{m} \quad \text{in} \quad Z_1$$
 $0.01 \, \text{m} \quad -\infty \quad \text{in} \quad 1$ 

g.) mag. energy density = 
$$\frac{B^2}{2N_0}$$
  
=  $\frac{(3.71 \text{ r} \times 10^{-3})^2}{2N_0}$ 

$$= \frac{(3.71 \, \nu \, \times 10^{-3})^2}{2 \, \mu_0}$$

$$= 5.477r^2 J/m^3$$

3a.)

i.) air 
$$gap$$
:  $R = \frac{0.05}{\nu_0 (0.1)^2} = 3.98 \times 10^6$   
metal loop:  $R = \frac{1 - 0.05}{2500 \mu_0 (0.1)^2} = 3 \times 10^4$ 

11. 
$$\gamma = \frac{NT}{R} = \frac{1000}{3.98 \times 10^6} = 2.5 \times 10^{-4} \text{ Wb}$$

iii.) 
$$L = \frac{1000.4}{T} = 0.25 \text{ H}$$

$$2.5 \times 10^{-4} = 13.(0.1)^{2}$$

$$\vec{B} = 2.5 \times 10^{-2} \text{ T}$$

Inside gap energy = 
$$\frac{B^2}{2\mu_0}$$

Inside metal enersy density

$$= \frac{B^2}{2 \cdot 2500 \, \mu_0}$$

$$(248 \text{ J/m}^3) \cdot (0.1 \text{ m})^2 = 2.48 \text{ N}$$

$$\xi = -\frac{7+}{5}$$

$$\gamma' = \int \vec{B} \cdot \vec{J} \vec{S} = (0.1 \sin (200\% +)) \cdot (0.05)^{2}$$

$$= (2.5 \times 10^{-4}) \sin (200\% +) Wb$$

$$\mathcal{E} = -(2.5 \times 10^{-4})(200\%) \cos(200\%+)$$

$$= -0.157 \cos(200\%+) V$$

For 5 turns,  

$$\xi = -5 \frac{d^4}{dt} = -0.785 \cos(2007t)$$

b.) 
$$\vec{F} = \int I \, dI \times B$$
 $\vec{F} = I \, l \, R \, \rho_{o,n} + \mu_{o} \, o_{n} + \mu_{o} + \mu_{o$ 

the force pulls ontward with equal magnitude on each section of the loop. As a result, there is no net force or torque when the loop is in this position.

## **Problem 5**

- a.) Since,  $B = \mu H$ , the initial permeability will be determined by the slope of the dashed line near the origin of the graph.
- b.) As H becomes strong, the material approaches total magnetization that is, the atoms approach total alignment with the field. At this point, additional H field will not produce additional magnetization, so increase in the B field at this point will match that of free space. Hence,  $\mu$  approaches  $\mu_0$  at very high H.
- c.) Hard magnetic materials magnetize more strongly than soft magnetic materials. The advantage of hard magnetic materials is their ability to retain a strong magnetic field when the externally-applied H-field is removed, making them suitable materials for permanent magnets. Soft magnetic materials, on the other hand, have a smaller area within their hysteresis curve, which translates to less hysteresis energy loss when the externally-applied H-field changes. This makes soft magnetic materials more suitable for transformer and inductor cores.