

# 具有精确电流监控器和快速过压保护功能的 TPS2596 2.7V 至 19V、 0.125A 至 2A、89mΩ 电子保险丝

## 1 特性

- 宽输入电压范围: 2.7V 至 19V
  - 绝对最大值为 21V
- 低导通电阻:  $R_{on} = 89\text{m}\Omega$  (典型值)
- 带有可调节欠压锁定 (UVLO) 的高电平有效使能输入
- 可用过压保护选项:
  - 快速过压钳位 (3.8V、5.7V 和 13.8V 引脚可选 阈值), 响应时间为  $5\mu\text{s}$  (典型值)
  - 可调节过压锁定 (OVLO), 响应时间为  $1.3\mu\text{s}$  (典型值)
- 配备负载电流监控器输出 (ILM) 的可调节电流限制
  - 电流范围: 0.125A 至 2A
  - 电流限制准确度:
    - 整个电流范围内为  $\pm 10.4\%$  (最大值)
    - 在 1A 电流限制下为  $\pm 5.5\%$  (最大值)
- 不受电气快速瞬变干扰 (IEC 61000-4-4)
- 可调节的输出压摆率控制 ( $dVdt$ )
- 提供过热保护 (OTP)
- 故障指示引脚 (FLT)
- UL2367 认证正在处理中
- IEC 62368 CB 认证 (正在申请中)
- 小尺寸: 4.91mm × 3.9mm SOIC 封装

## 2 应用

- 能量计
- UL 60335-1 15W LPC 在电器中的应用
  - 冰箱
  - 洗碗机
  - 洗衣机和烘干机
- 机顶盒
- IP 网络摄像头

## 3 说明

TPS2596xx 系列 **电子保险丝** (集成式 FET 热插拔器件) 是采用小型封装且高度集成的电路保护和电源管理解决方案。这些设备只需很少的外部组件即可提供多种保护模式, 能够非常有效地抵御过载、短路、电压浪涌和过多浪涌电流。输出电流限制级别可通过单个外部电阻设定。还可能通过测量整个电流限制电阻的压降实现对输出负载电流的准确感应。对浪涌电流有特别要求的应用可以通过单个外部电容器设定输出转换率。对于 TPS25962x 型号, 发生输入过压情况时, 内部钳位电路会将输出限制在一个安全的固定最大电压 (引脚可选), 而无需外部组件。TPS25963x 型号使用户可以设置指定的过压截止阈值。

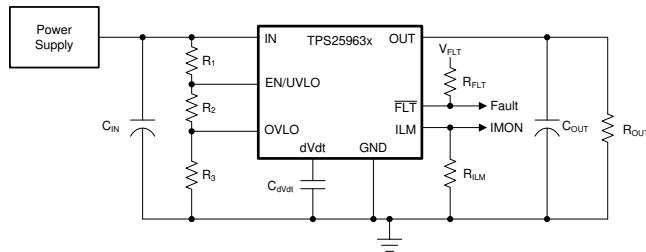
这些器件的额定工作结温范围为  $-40^\circ\text{C}$  至  $+125^\circ\text{C}$ 。

### 器件信息<sup>(1)</sup>

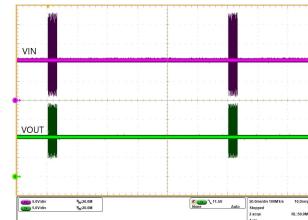
器件型号	封装	封装尺寸 (标称值)
TPS259620DDA	SOIC (8)	4.91mm x 3.9mm
TPS259621DDA	SOIC (8)	4.91mm x 3.9mm
TPS259630DDA	SOIC (8)	4.91mm x 3.9mm
TPS259631DDA	SOIC (8)	4.91mm x 3.9mm

(1) 如需了解所有可用封装, 请参阅数据表末尾的可订购产品附录。

### 简化原理图



### TPS25963x 1KV EFT 响应



本文档旨在为方便起见, 提供有关 TI 产品中文版本的信息, 以确认产品的概要。有关适用的官方英文版本的最新信息, 请访问 [www.ti.com](http://www.ti.com), 其内容始终优先。TI 不保证翻译的准确性和有效性。在实际设计之前, 请务必参考最新版本的英文版本。

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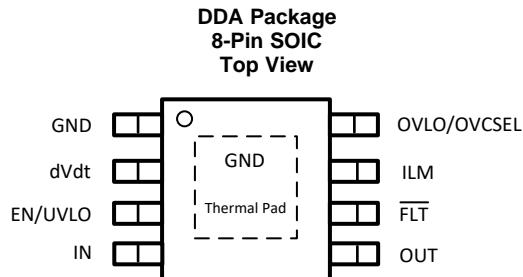
## 4 修订历史记录

Changes from Original (May 2019) to Revision A	Page
• 将“预告信息”更改为“生产数据” .....	1

## 5 器件比较表

部件号	过压响应	热关断 (TSD) 响应
TPS259620	OVC - 3.8V、5.7V、13.8V (引脚可选)	闭锁
TPS259621	OVC - 3.8V、5.7V、13.8V (引脚可选)	自动重试
TPS259630	可调 OVLO	闭锁
TPS259631	可调 OVLO	自动重试

## 6 Pin Configuration and Functions



**Pin Functions**

PIN		I/O	DESCRIPTION
NAME	NO.		
GND	1	Ground	Ground
dVdt	2	Analog Output	A capacitor from this pin to GND sets the output turn on slew rate. Leave this pin floating for the fastest turn on slew rate.
EN/UVLO	3	Analog Input	Active High Enable for the Device. A resistor divider can be used to adjust the Undervoltage Lockout threshold. <b>Do not leave floating.</b>
IN	4	Power	Power Input
OUT	5	Power	Power Output
FLT	6	Digital Output	Active Low indicator which will be pulled low when a fault is detected. It is an open-drain output that requires an external pull-up resistance.
ILM	7	Analog Output	This is a dual function pin used to limit and monitor the output current. An external resistor from this pin to GND sets the output current limit. The pin voltage can also be used to monitor the output load current.
OVLO	8	Analog Input	<b>TPS25963x:</b> A resistor divider can be used to adjust the Overvoltage Lockout threshold. <b>Do not leave floating.</b>
OVCSEL			<b>TPS25962x:</b> Overvoltage Clamp level select pin. Refer to <a href="#">Overvoltage Clamp</a> for more details.
Thermal pad		Ground	The Exposed Pad is used primarily for heat dissipation and must be connected to system ground plane for best thermal performance.

## 7 Specifications

### 7.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

PARAMETER	PIN	MIN	MAX	UNITS
$V_{IN}$	IN	-0.3	21	V
			22	V
$V_{OUT}$	OUT	-0.3	min (21, $V_{IN} + 0.3$ )	V
$V_{EN/UVLO}$	EN/UVLO	-0.3	7	V
$V_{OV}$	OVCSEL/OVLO	-0.3	7	V
$V_{dVdT}$	DVDT		2.5	V
$V_{FLT_B}$	FLT	-0.3	7	V
$I_{FLT_B}$	FLT		10	mA
$I_{MAX}$	IN to OUT	Internally Limited		A
$T_J$		Internally Limited		°C
$T_{LEAD}$			300	°C
$T_{stg}$		-65	150	°C

- (1) Stresses beyond those listed under *Absolute Maximum Rating* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Condition*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

### 7.2 ESD Ratings

		VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001, all pins <sup>(1)</sup>	$\pm 2000$
		Charged device model (CDM), per JEDEC specification JESD22-C101, all pins <sup>(2)</sup>	$\pm 500$

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

PARAMETER	PIN	MIN	MAX	UNITS
$V_{IN}$	IN	2.7	19 <sup>(1)</sup>	V
$V_{OUT}$	OUT		$V_{IN} + 0.3$	V
$V_{EN/UVLO}$	EN/UVLO		6 <sup>(2)</sup>	V
$V_{OV}$	OVLO	0.5	2	V
$V_{dVdT}$	DVDT	4		V
$V_{FLT_B}$	FLT		6	V
$R_{ILM}$	ILM	453	7869	Ω
$I_{MAX}$	IN to OUT		2	A
$T_J$		-40	125	°C

- (1) For TPS25962x, the input voltage should be limited to the selected Output Voltage Clamp Option as listed in the Electrical Characteristics section
- (2) For supply voltages below 6V, it is okay to pull up the EN pin to IN through a resistor of 100 KΩ or higher. For supply voltages greater than 6V, it is recommended to use an appropriate resistor divider between IN, EN and GND to ensure the voltage at the EN pin is within the specified limits.

## 7.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		TPS2596X	UNIT
		DDA (SOIC-EP)	
		8 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	52.7 <sup>(2)</sup>	°C/W
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	119.8 <sup>(3)</sup>	°C/W
Ψ <sub>JT</sub>	Junction-to-top characterization parameter	8.9 <sup>(2)</sup>	°C/W
Ψ <sub>JT</sub>	Junction-to-top characterization parameter	17.5 <sup>(3)</sup>	°C/W
Ψ <sub>JB</sub>	Junction-to-board characterization parameter	27.1 <sup>(2)</sup>	°C/W
Ψ <sub>JB</sub>	Junction-to-board characterization parameter	68.1 <sup>(3)</sup>	°C/W

(1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application report.

(2) With exposed pad soldered to PCB

(3) Without exposed pad soldered to PCB

## 7.5 Electrical Characteristics

(Test conditions unless otherwise noted)  $-40^{\circ}\text{C} \leq T_{\text{J}} \leq 125^{\circ}\text{C}$ ,  $V_{\text{IN}} = 12\text{ V}$ ,  $R_{\text{ILM}} = 453\text{ }\Omega$ ,  $C_{\text{dVdT}} = \text{Open}$ ,  $\text{OUT} = \text{Open}$ . All voltages referenced to GND.

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS
<b>INPUT SUPPLY (IN)</b>					
I <sub>Q</sub>	IN quiescent current	TPS25963x	193	259	µA
		TPS25962x	206	266	µA
I <sub>SD</sub>	IN Shutdown Current	$V_{\text{IN}} < 4\text{ V}$ , $V_{\text{EN/UVLO}} < V_{\text{SD}}$	0.1	0.1	µA
		$V_{\text{IN}} \geq 4\text{ V}$ , $V_{\text{EN/UVLO}} < V_{\text{SD}}$	0.4	1.132	µA
V <sub>UVP(R)</sub>	IN Undervoltage Protection threshold	$V_{\text{IN}}$ Rising	2.46	2.53	2.58
V <sub>UVP(F)</sub>		$V_{\text{IN}}$ Falling	2.36	2.42	2.46
	IN Undervoltage Protection Hysteresis		110		mV
<b>OUTPUT VOLTAGE CLAMP (OUT) - TPS25962X</b>					
V <sub>OVC</sub>	Overvoltage Clamp Threshold	R <sub>OVCSEL</sub> = Short to GND, R <sub>OUT</sub> = 10 KΩ	3.75	3.83	3.92
		R <sub>OVCSEL</sub> = 400 KΩ to GND, R <sub>OUT</sub> = 10 KΩ	5.54	5.69	5.83
		R <sub>OVCSEL</sub> = OPEN, R <sub>OUT</sub> = 10 KΩ	12.97	13.77	14.52
V <sub>CLAMP</sub>	Output Voltage During Clamping	R <sub>OVCSEL</sub> = Short to GND, I <sub>OUT</sub> = 10 mA	3.47	3.59	3.7
		R <sub>OVCSEL</sub> = 400 KΩ to GND, I <sub>OUT</sub> = 10 mA	5.28	5.45	5.61
		R <sub>OVCSEL</sub> = OPEN, I <sub>OUT</sub> = 10 mA	13.13	13.58	13.97
<b>OUTPUT CURRENT LIMIT AND MONITOR (ILM)</b>					
G <sub>IMON</sub>	Current monitor gain as measured on ILM pin (I <sub>ILM</sub> / I <sub>OUT</sub> )	I <sub>OUT</sub> = 0.13 A	531.22	653.21	800.00
		I <sub>OUT</sub> = 2 A	635.77	657.15	684.05
I <sub>ILM</sub>	I <sub>OUT</sub> Current Limit	R <sub>ILM</sub> = 7.87 KΩ, V <sub>DS</sub> = 0.5 V, $-40^{\circ}\text{C} \leq T_{\text{A}} \leq 80^{\circ}\text{C}$	0.113	0.125	0.139
		R <sub>ILM</sub> = 3.83 KΩ, V <sub>DS</sub> = 0.5 V	0.224	0.247	0.269
		R <sub>ILM</sub> = 909 Ω, V <sub>DS</sub> = 0.5 V	0.949	1.005	1.051
		R <sub>ILM</sub> = 453 Ω, V <sub>DS</sub> = 0.5 V	1.83	2.004	2.147
		R <sub>ILM</sub> = OPEN	0		A
I <sub>CB</sub>	I <sub>OUT</sub> Circuit Breaker Threshold during R <sub>ILM</sub> Short condition	R <sub>ILM</sub> = Short to GND (Single Point Failure Test IEC 62368-1)		1.5	A

## Electrical Characteristics (continued)

(Test conditions unless otherwise noted)  $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$ ,  $V_{IN} = 12\text{ V}$ ,  $R_{ILM} = 453\text{ }\Omega$ ,  $C_{dVdT} = \text{Open}$ , OUT = Open. All voltages referenced to GND.

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNITS
<b>ON-RESISTANCE (IN TO OUT)</b>						
$R_{ON}$	ON State Resistance	$V_{IN} < 4\text{ V}$ , $I_{OUT} = 0.2\text{ A}$ , $T_J = 25^\circ\text{C}$		97	99.8	$\text{m}\Omega$
		$V_{IN} < 4\text{ V}$ , $I_{OUT} = 0.2\text{ A}$ , $T_J = -40$ to $85^\circ\text{C}$			125.4	$\text{m}\Omega$
		$V_{IN} < 4\text{ V}$ , $I_{OUT} = 0.2\text{ A}$ , $T_J = -40$ to $125^\circ\text{C}$			143.4	$\text{m}\Omega$
		$V_{IN} > 4\text{ V}$ , $I_{OUT} = 0.2\text{ A}$ , $T_J = 25^\circ\text{C}$		89	92.6	$\text{m}\Omega$
		$V_{IN} > 4\text{ V}$ , $I_{OUT} = 0.2\text{ A}$ , $T_J = -40$ to $85^\circ\text{C}$			115.3	$\text{m}\Omega$
		$V_{IN} > 4\text{ V}$ , $I_{OUT} = 0.2\text{ A}$ , $T_J = -40$ to $125^\circ\text{C}$			131	$\text{m}\Omega$
<b>ENABLE/UNDERVOLTAGE LOCK OUT (EN/UVLO)</b>						
$V_{UVLO(R)}$	UVLO Threshold	$V_{EN}$ Rising	1.18	1.2	1.22	V
$V_{UVLO(F)}$		$V_{EN}$ Falling	1.08	1.1	1.13	V
	UVLO Hysteresis			95		$\text{mV}$
$V_{SD}$	$V_{EN}$ threshold for lowest shutdown current	$V_{EN}$ Falling	0.53		1.05	V
$I_{ENLKG}$	EN leakage current		-0.1		0.1	$\mu\text{A}$
<b>OVERVOLTAGE LOCKOUT (OVLO) - TPS25963X</b>						
$V_{OVLO(R)}$	OVLO Threshold	$V_{OVLO}$ Rising	1.17	1.2	1.22	V
$V_{OVLO(F)}$		$V_{OVLO}$ Falling	1.08	1.1	1.13	V
	OVLO Hysteresis			95		$\text{mV}$
$I_{OVLKKG}$	OVLO pin leakage current	$0.5 \leq V_{OVLO} \leq 1.5\text{V}$	-0.1		0.1	$\mu\text{A}$
<b>FAULT INDICATION (FLT)</b>						
$R_{FLTB}$	FLT Internal Pull-down resistance	FLT asserted		11.52		$\Omega$
$I_{FLTLKG}$	FLT pin leakage current	FLT de-asserted, pull-up voltage 6 V	-1		1	$\mu\text{A}$
<b>OVERTEMPERATURE PROTECTION (OTP)</b>						
TSD	Thermal Shutdown Rising Threshold	$T_J$ Rising		157		$^\circ\text{C}$
TSD <sub>HYS</sub>	Thermal Shutdown Hysteresis	$T_J$ Falling		11.5		$^\circ\text{C}$
<b>DVDT</b>						
$I_{DVDT}$	dVdt Pin Charging Current		1.89	2.11	2.33	$\mu\text{A}$
$G_{DVDT}$	DVDT gain		20.31	20.93	21.5	V

## 7.6 Timing Requirements

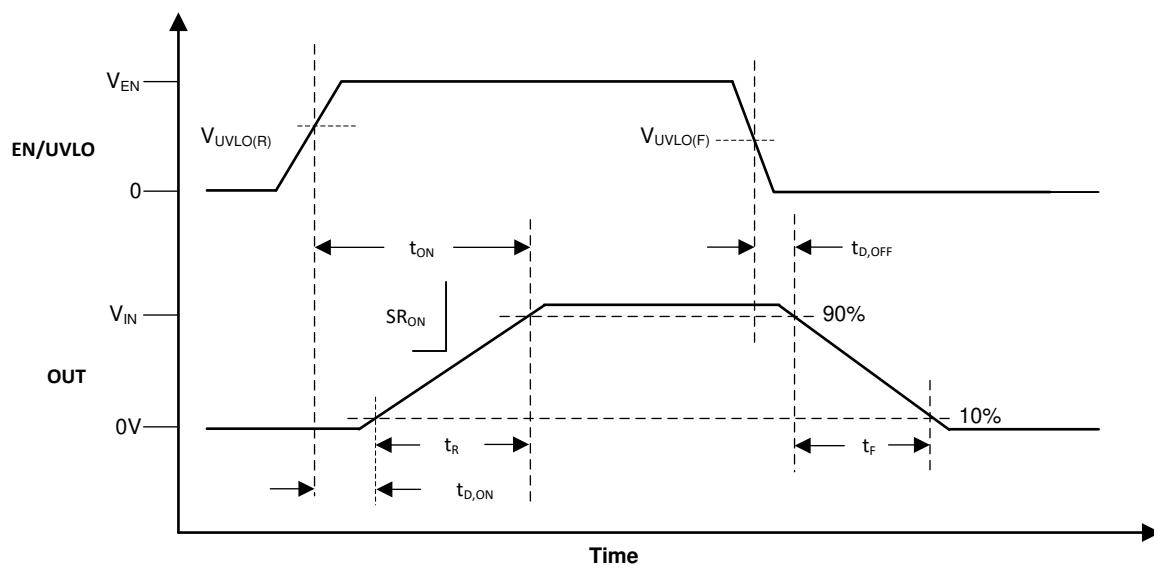
Typical Values are taken at  $T_J = 25^\circ\text{C}$  unless specifically noted otherwise.

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNITS
$t_{LIM}$	Current limit response time	$I_{OUT} > 20\%$ over $I_{LIM}$ to $I_{OUT} \leq I_{LIM}$		87		$\mu\text{s}$
$t_{SC}$	Short circuit response time	$V_{OUT} \downarrow$ to $I_{OUT} \leq I_{LIM}$		5		$\mu\text{s}$
$t_{OVLO}$	Overvoltage lockout response time	TPS25963x Only		1.3		$\mu\text{s}$
$t_{OVC}$	Output clamp response time	TPS25962x Only, $I_{OUT} = 2\text{ A}$		5		$\mu\text{s}$
$t_{TSD,RST}$	Thermal Shutdown Auto-Retry Interval	TPS2596x1 Only		95		ms

## 7.7 Switching Characteristics

The output rising slew rate is internally controlled and constant across the entire operating voltage range to ensure the turn-on timing is not affected by the load conditions. The rising slew rate can be adjusted by adding capacitance from the  $dVdt$  pin to ground. As  $C_{dVdt}$  is increased, it will slow the rising slew rate (SR). See Slew Rate and Inrush Current Control ( $dVdt$ ) section for more details. The fall time, however, is dependent on the RC time constant of the load capacitance ( $C_{OUT}$ ) and Load Resistance ( $R_L$ ). The Switching Characteristics are only valid for the power-up sequence where the supply is available in steady state condition and the load voltage is completely discharged before the device is enabled. Typical Values are taken at  $T_J = 25^\circ\text{C}$  unless specifically noted otherwise.  $R_{OUT} = 100\ \Omega$ ,  $C_{OUT} = 1\ \mu\text{F}$ .

PARAMETER		$V_{IN}$	$C_{dVdt} = \text{Open}$	$C_{dVdt} = 3300\text{pF}$	UNIT
$SR_{ON}$	Output Rising slew rate	2.7 V	28.9	12.1	V/ms
		5 V	42.7	13.1	
		12 V	75.1	13.6	
$t_{D,ON}$	Turn on delay	2.7 V	77.5	216.5	$\mu\text{s}$
		5 V	78.9	247.3	
		12 V	82.9	314.9	
$t_R$	Rise time	2.7 V	74.7	182.4	$\mu\text{s}$
		5 V	94.1	311.0	
		12 V	128.4	707.8	
$t_{ON}$	Turn on time	2.7 V	152.2	398.9	$\mu\text{s}$
		5 V	173	558.4	
		12 V	211.3	1022.7	
$t_{D,OFF}$	Turn off delay	2.7 V	12.2	12.3	$\mu\text{s}$
		5 V	11.6	11.9	
		12 V	10.3	10.4	



**图 1. TPS2596xx Switching Times**

## 7.8 Typical Characteristics

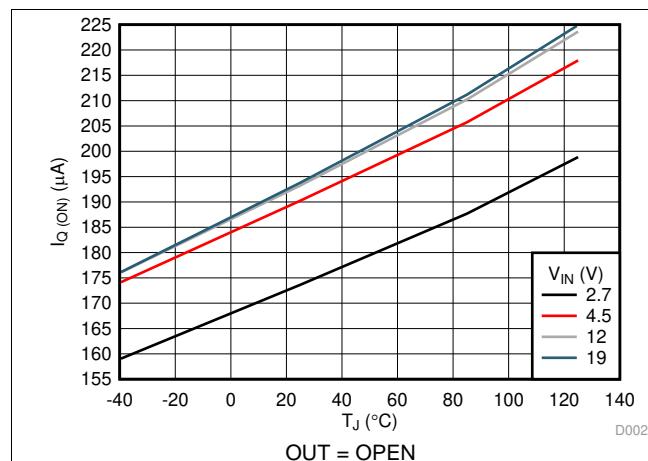


图 2. TPS25963x Quiescent Current

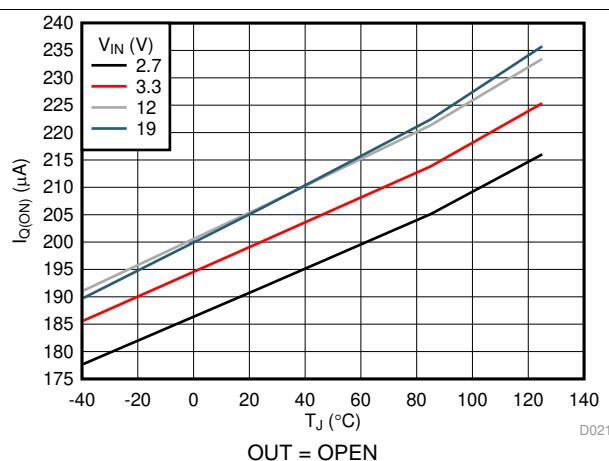


图 3. TPS25962x Quiescent Current

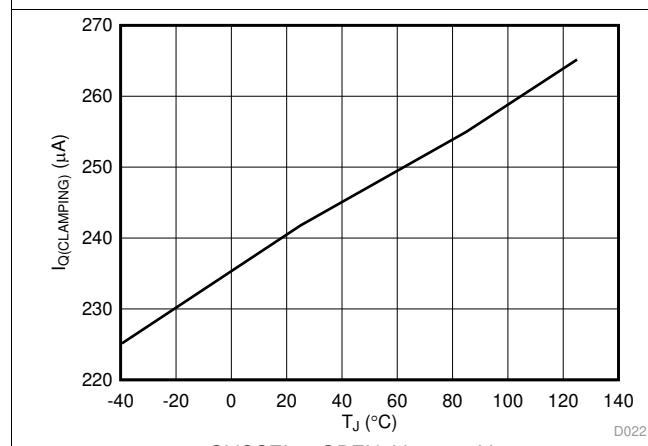


图 4. TPS25962x Quiescent Current During Overvoltage Clamping

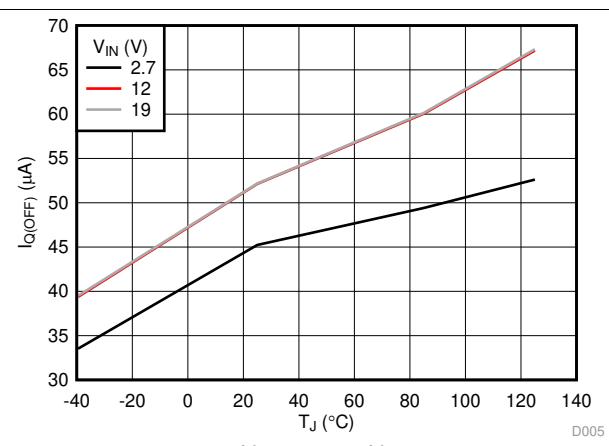


图 5. Disabled State Current

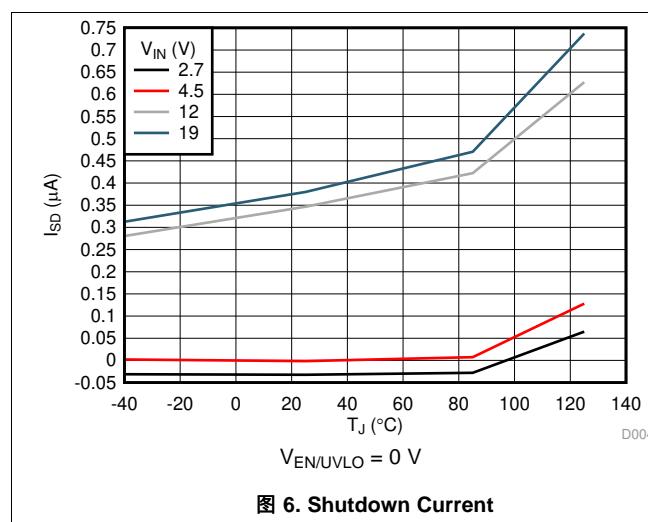


图 6. Shutdown Current

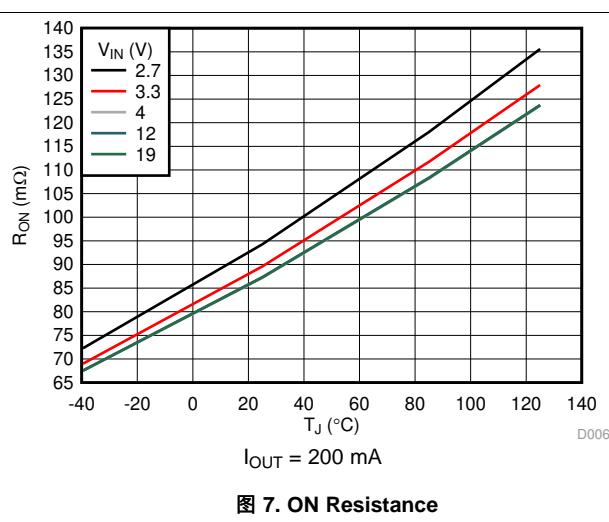
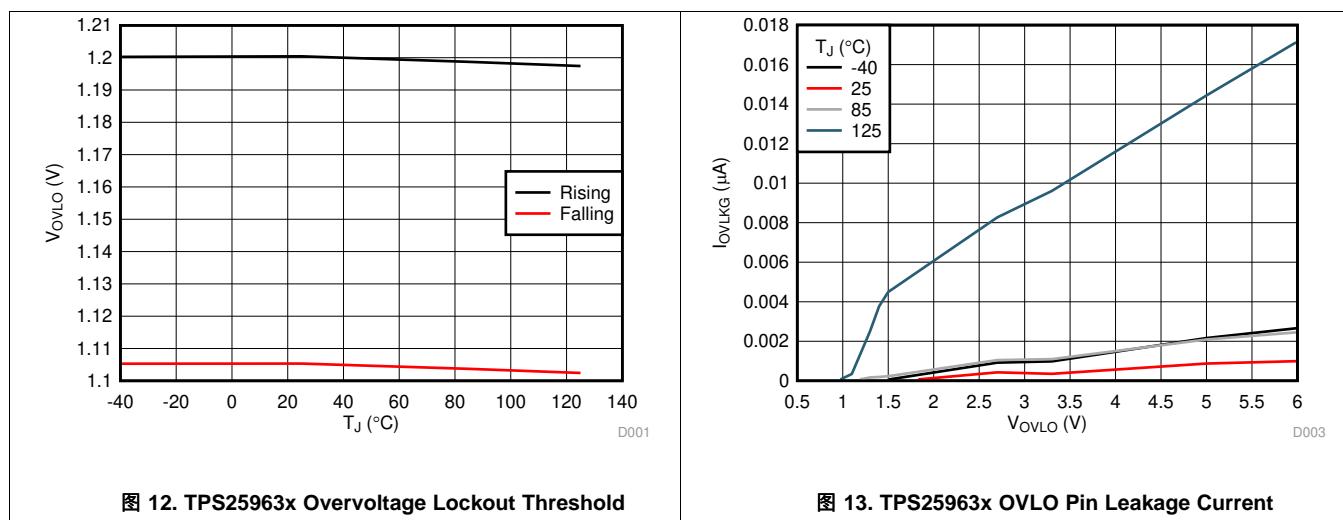
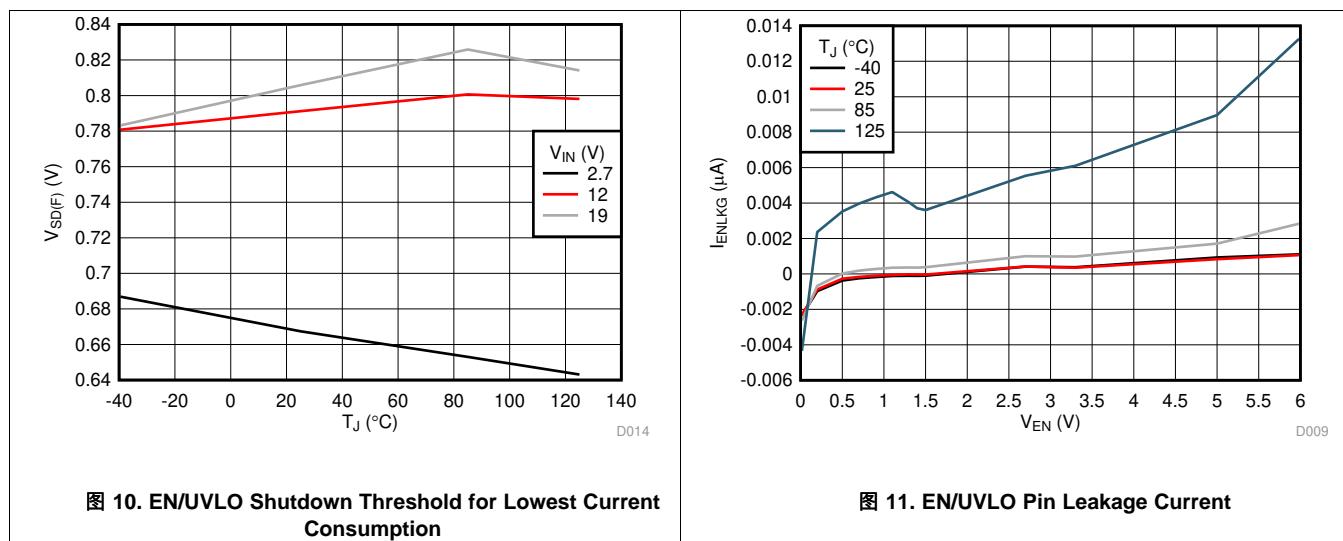
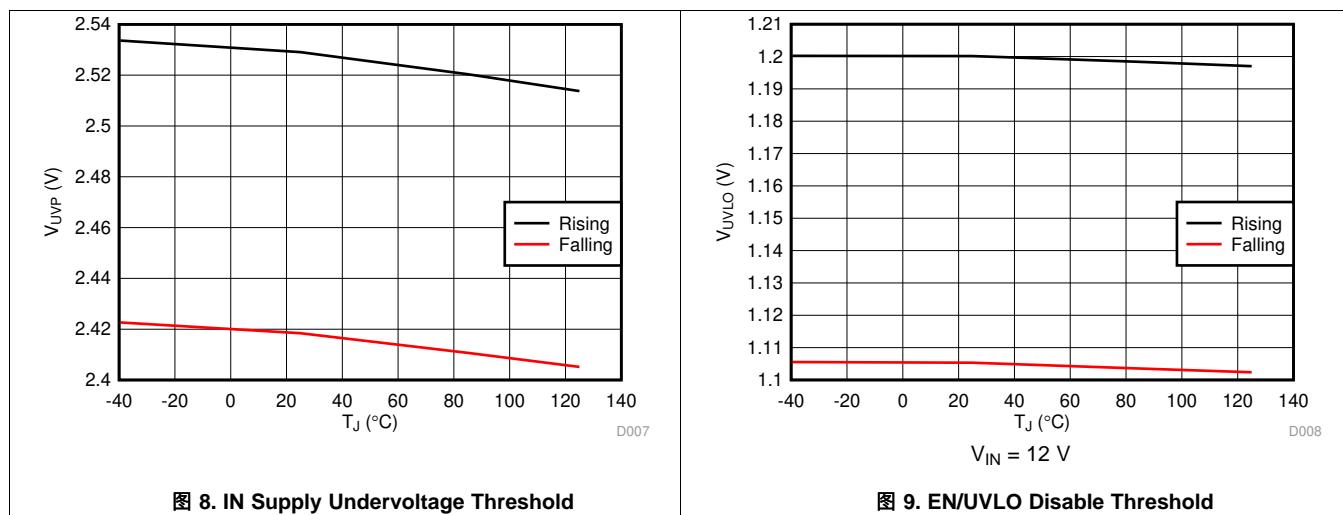
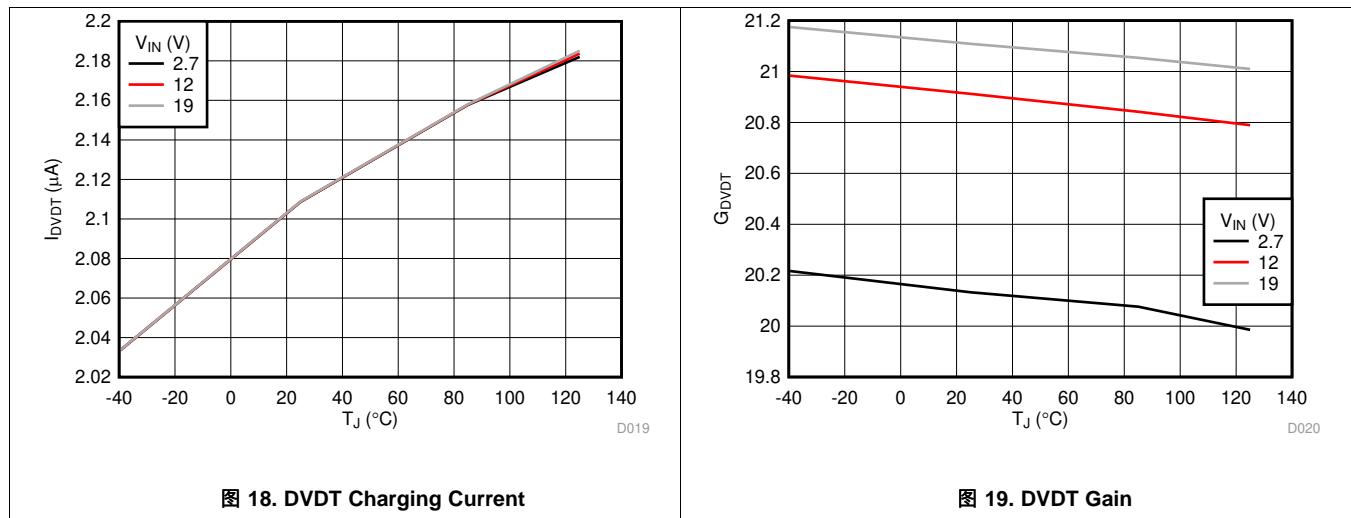
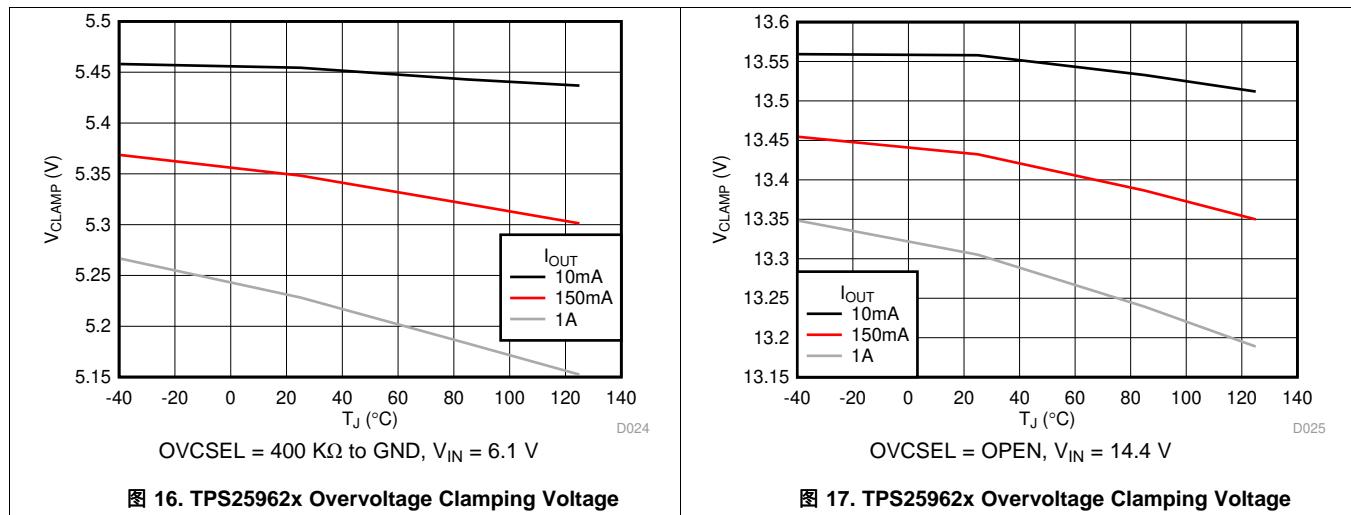
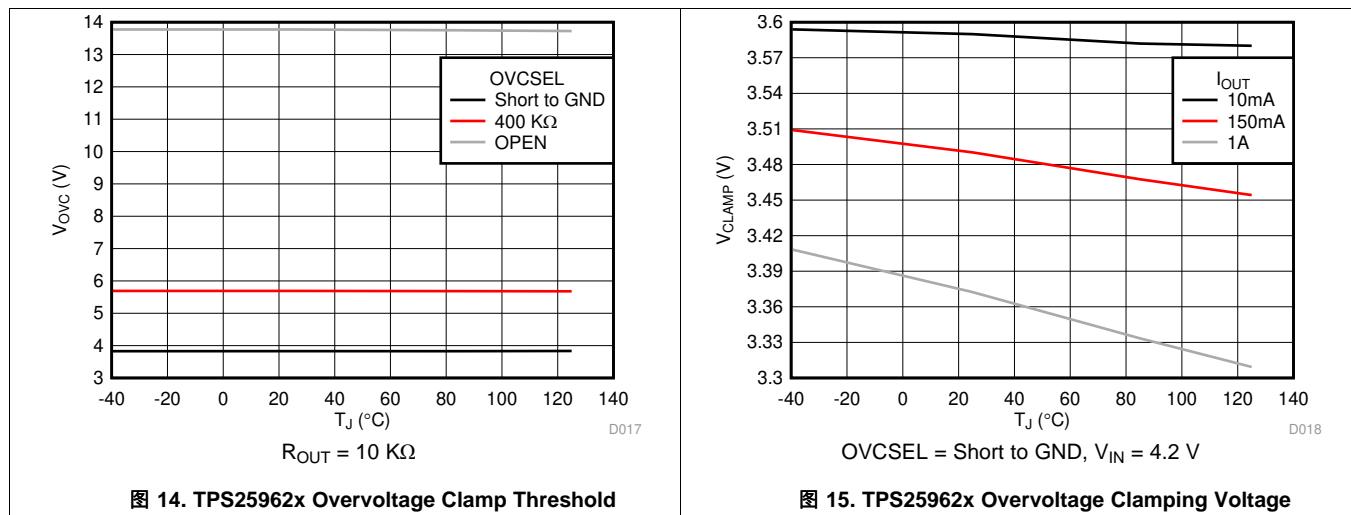


图 7. ON Resistance

## Typical Characteristics (接下页)



## Typical Characteristics (接下页)



## Typical Characteristics (接下页)

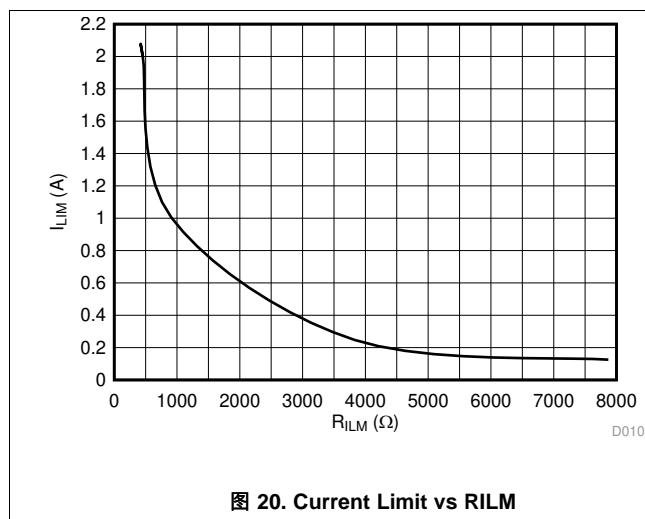


图 20. Current Limit vs RILM

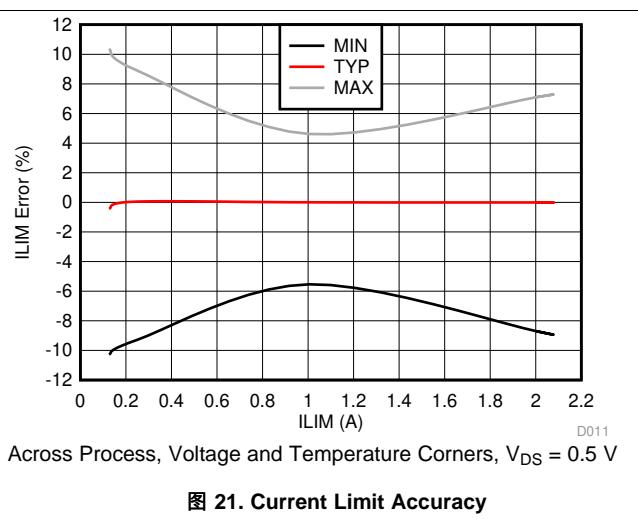


图 21. Current Limit Accuracy

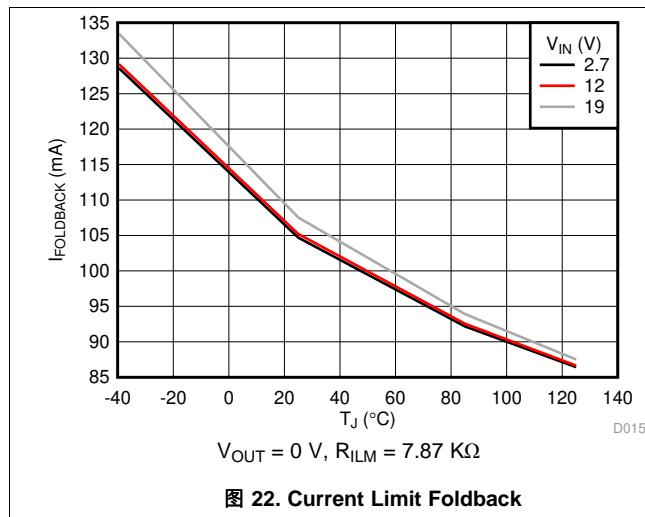


图 22. Current Limit Foldback

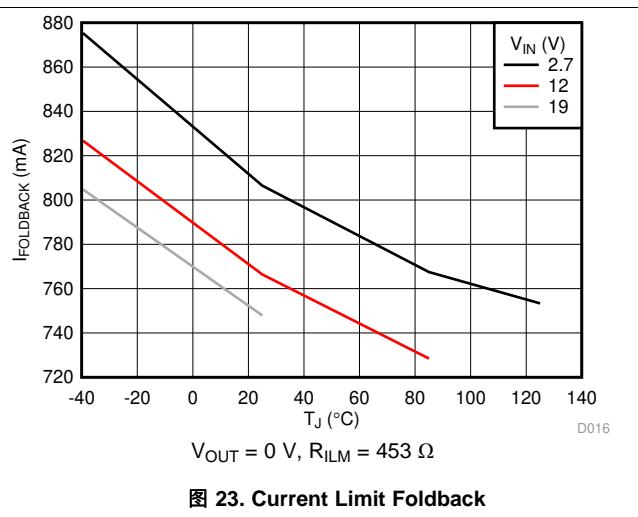


图 23. Current Limit Foldback

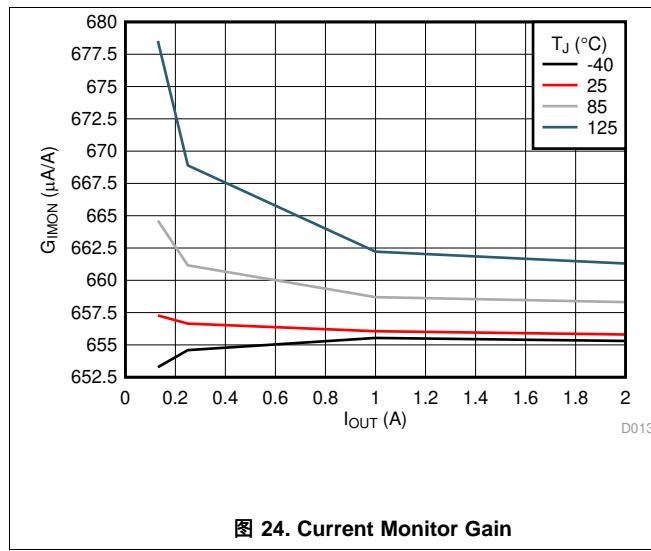


图 24. Current Monitor Gain

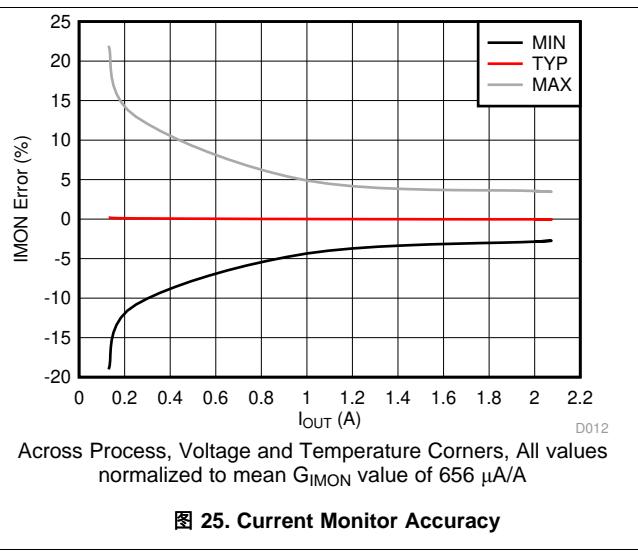
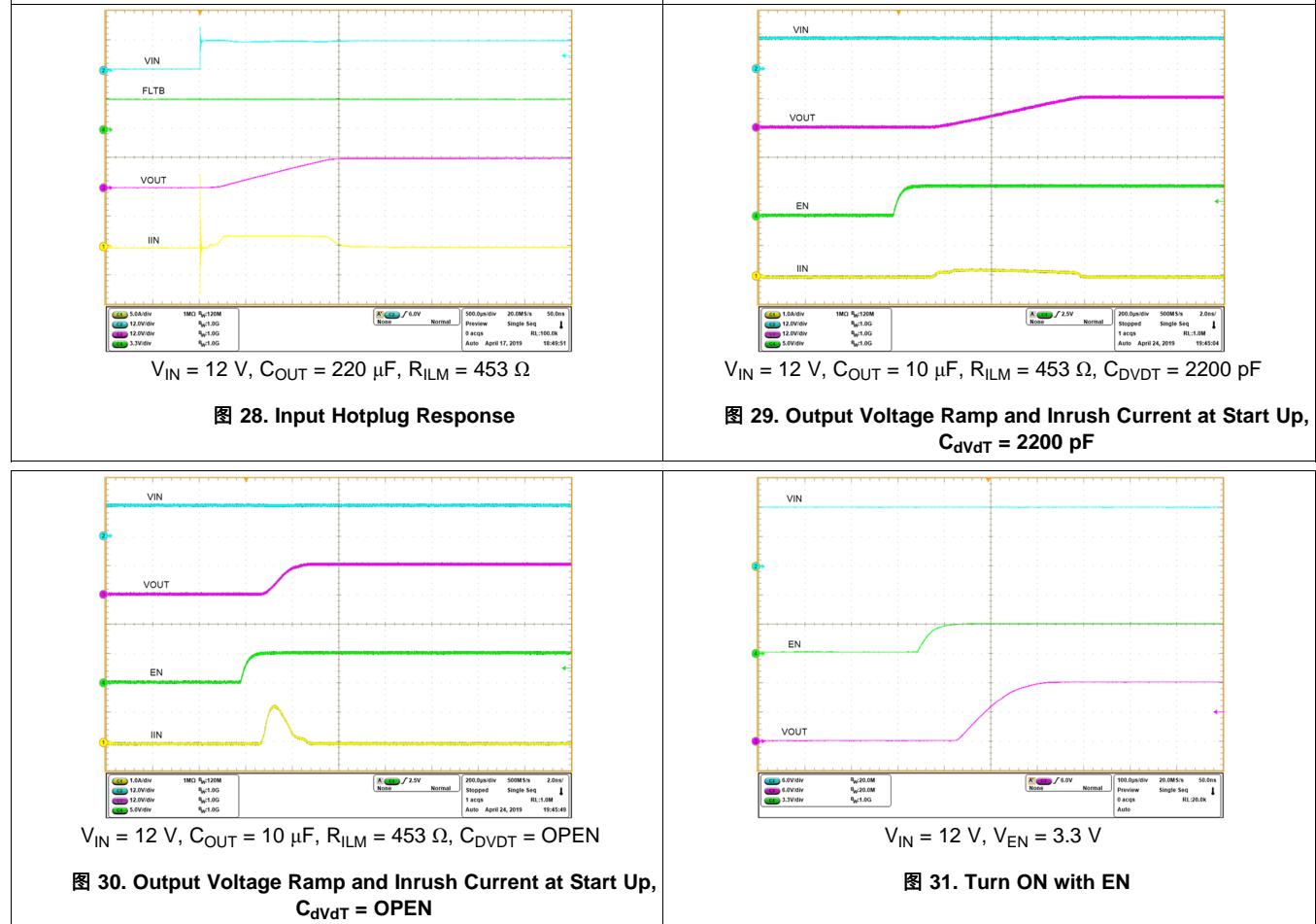
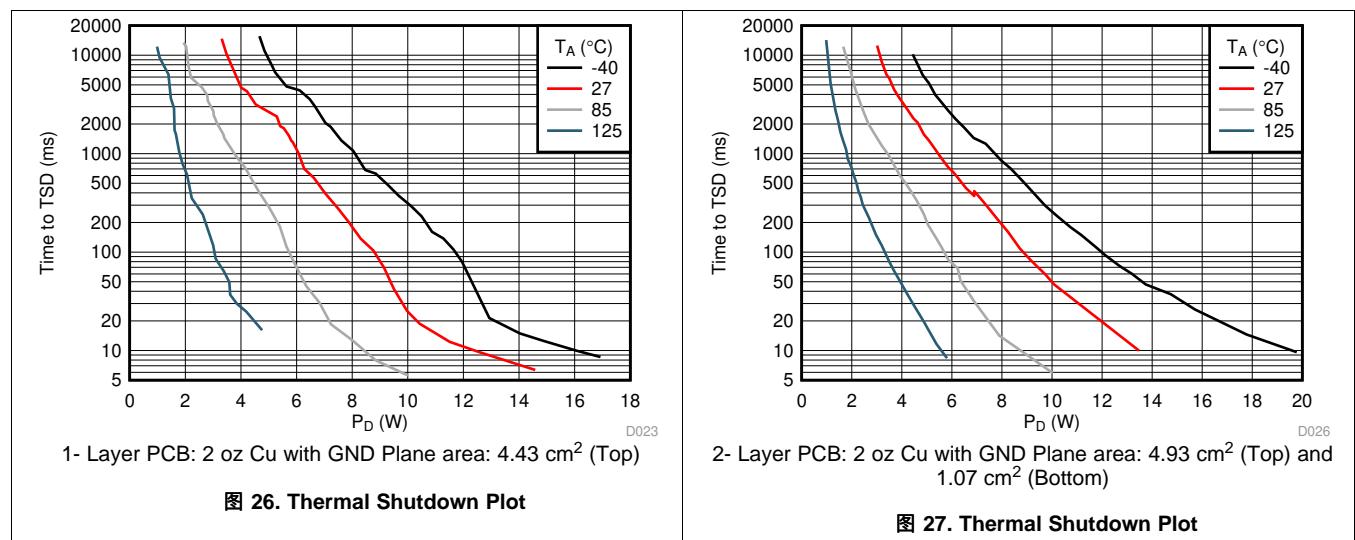
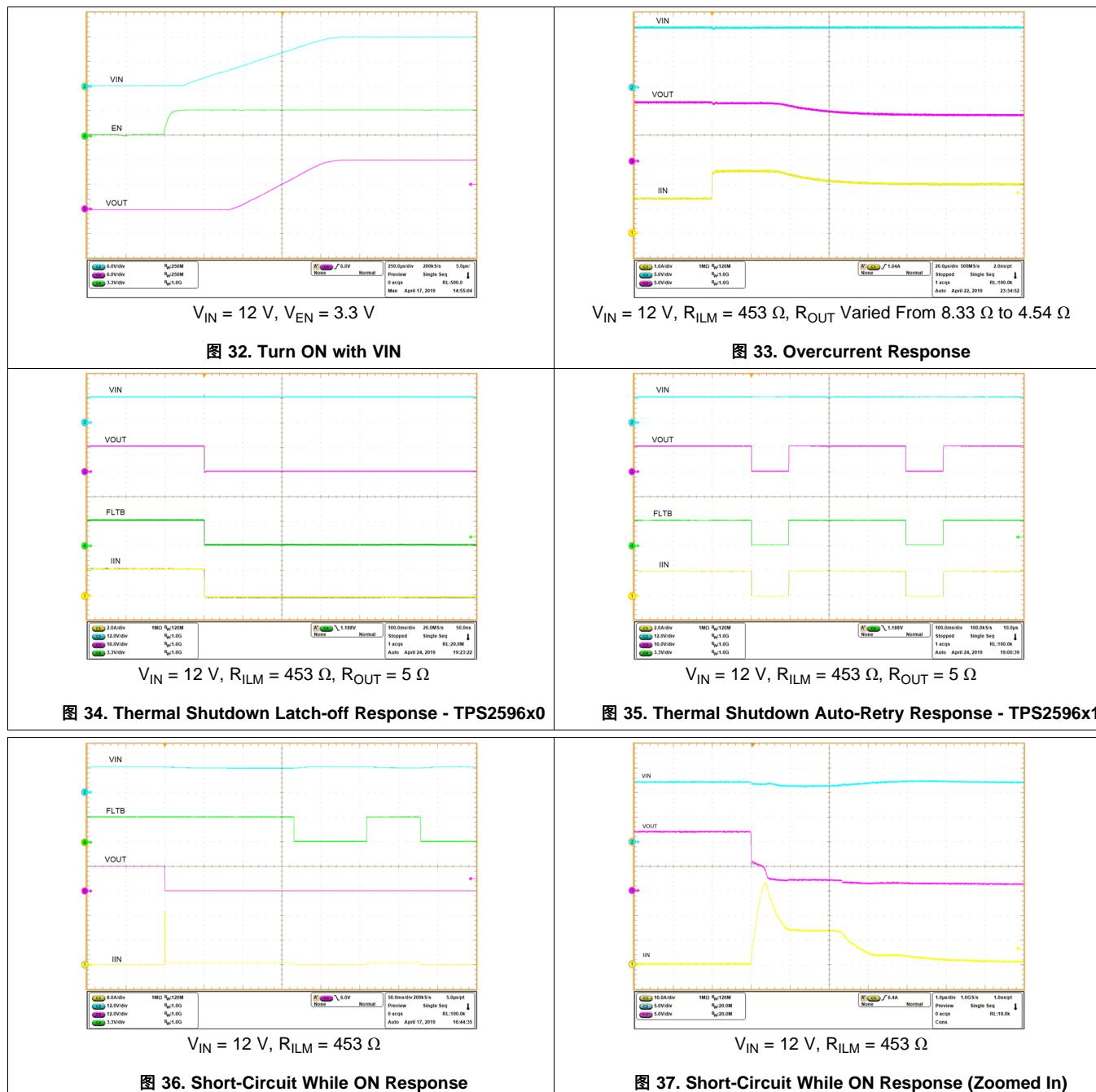


图 25. Current Monitor Accuracy

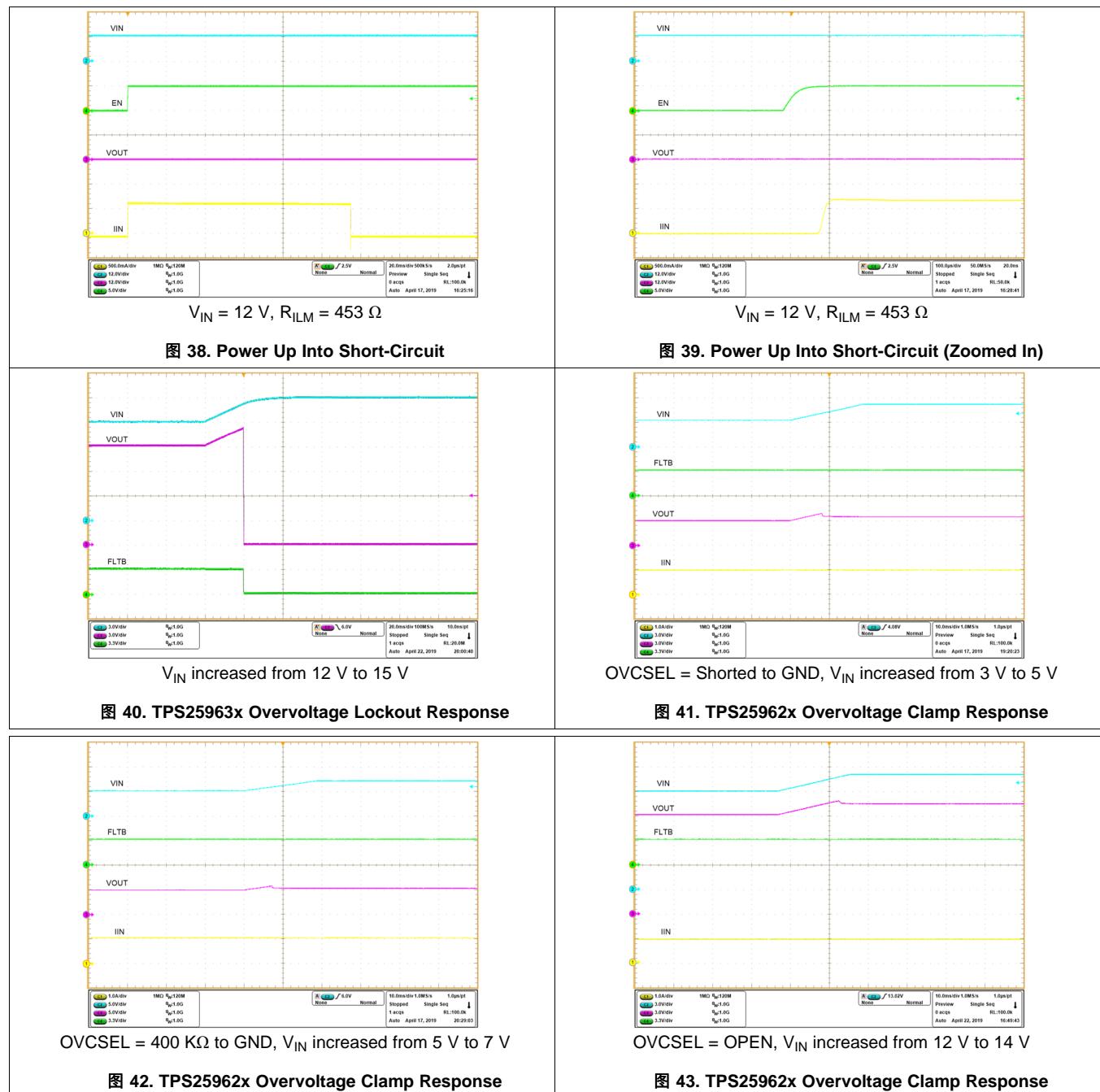
## Typical Characteristics (接下页)



## Typical Characteristics (接下页)



## Typical Characteristics (接下页)

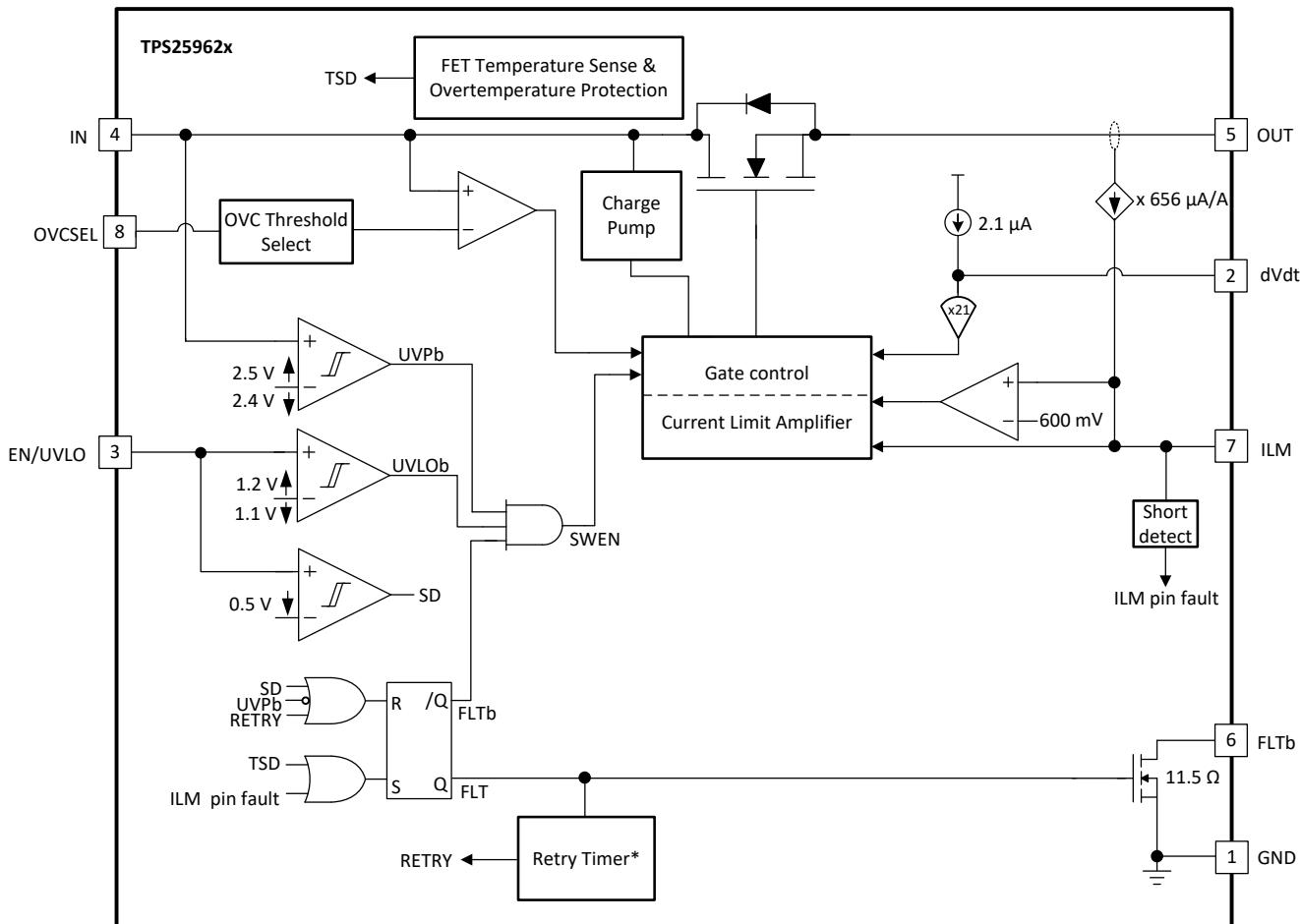


## 8 Detailed Description

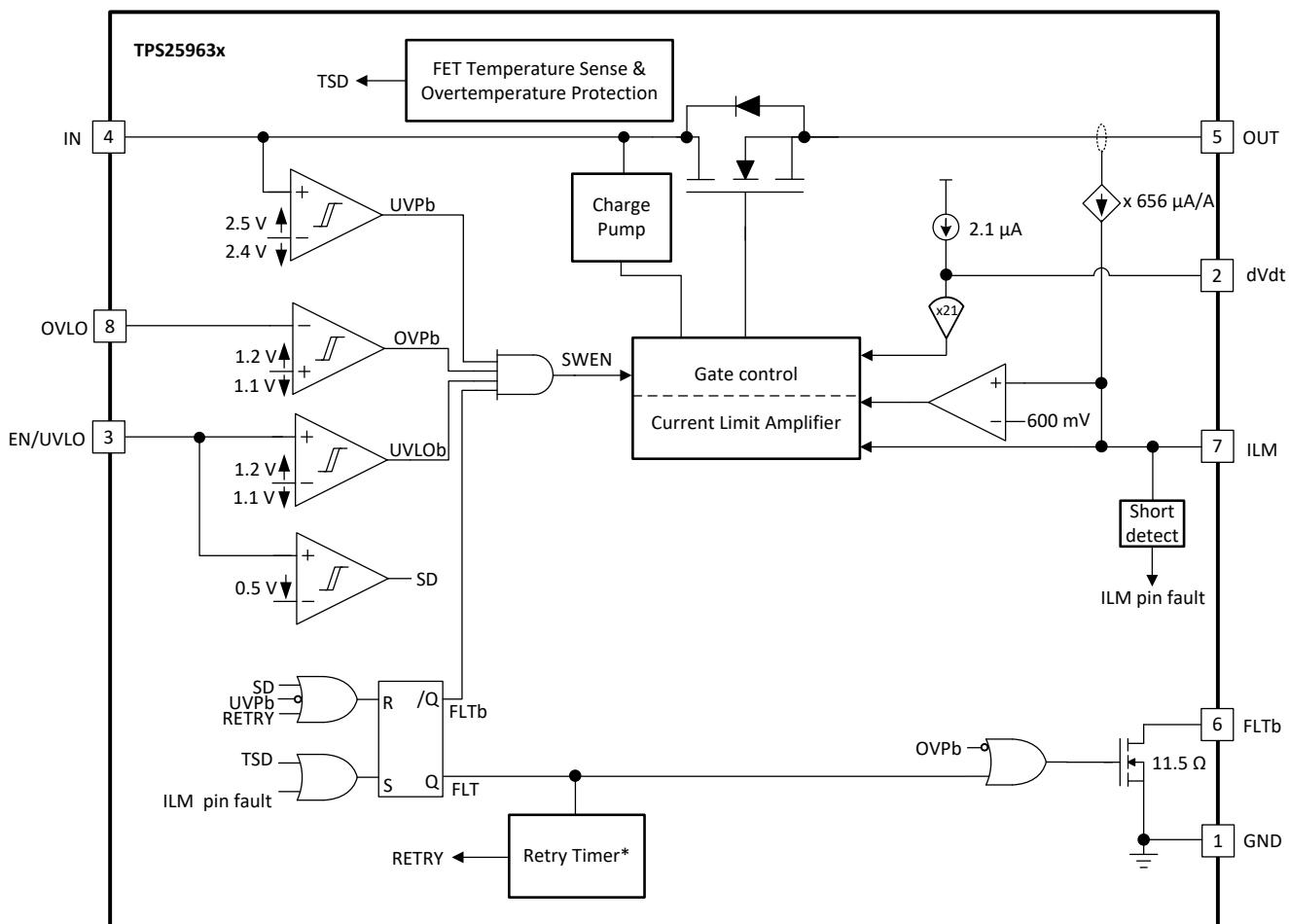
### 8.1 Overview

The TPS2596xx is an integrated eFuse device that is used to manage load voltage and load current. The device provides various factory programmed settings and user manageable settings, which allow device configuration for handling different transient and steady state supply and load fault conditions, thereby protecting the input supply and the downstream circuits connected to the device. The device also uses an in-built thermal shutdown mechanism to protect itself during these fault events.

### 8.2 Functional Block Diagram



## Functional Block Diagram (接下页)



\* Only for Auto-Retry Variant (TPS259631)

## 8.3 Feature Description

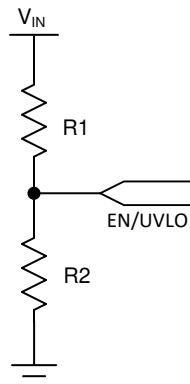
### 8.3.1 Undervoltage Protection (UVP) and Undervoltage Lockout (UVLO)

TPS2596xx constantly monitors the input supply to ensure that the load is powered up only when the voltage is at a sufficient level. During the start-up condition, the device waits for the input supply to rise above an internal fixed threshold  $V_{UVP(R)}$  before it proceeds to turn ON the FET. Similarly, during the ON condition, if the input supply falls below the UVP threshold  $V_{UVP(F)}$ , the FET is turned OFF. The UVP rising and falling thresholds are slightly different, thereby providing some hysteresis and ensuring stable operation around the threshold voltage.

The TPS2596xx devices also provide an user adjustable UVLO mechanism to ensure that the load is powered up only when the voltage is at a sufficient level. This can be achieved by dividing the input supply and feeding it to the EN/UVLO pin. Whenever the voltage at the EN/UVLO pin falls below a threshold  $V_{UVLO(F)}$ , the device turns OFF the FET. The FET is turned ON again when the voltage rises above the threshold  $V_{UVLO(R)}$ . The rising and falling thresholds on this pin are slightly different, thereby providing some hysteresis and ensuring stable operation around the threshold voltage.

The user must choose the resistor divider values appropriately to map the desired input undervoltage level to the UVLO threshold of the part.

## Feature Description (接下页)



**图 44. Adjustable Undervoltage Lockout**

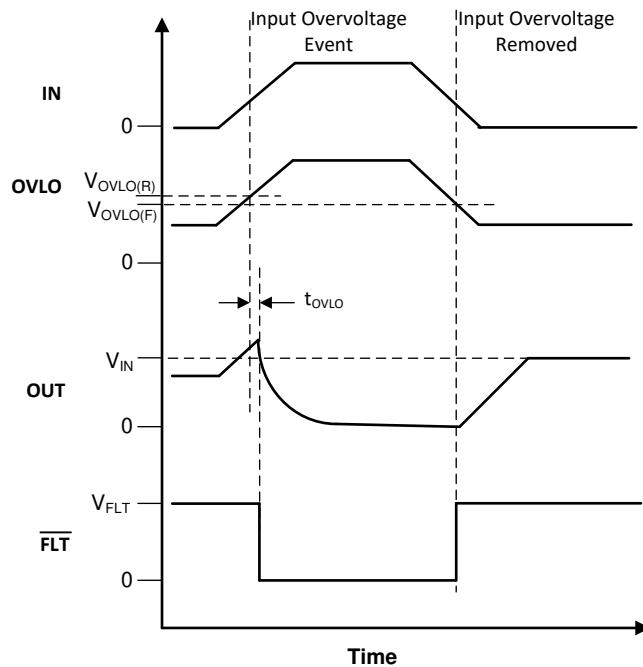
$$V_{IN(UV)} = V_{UVLO(F)} \times \frac{(R_1 + R_2)}{R_2} \quad (1)$$

### 8.3.2 Overvoltage Protection

The TPS2596xx devices provide 2 ways to handle an input overvoltage condition.

#### 8.3.2.1 Overvoltage Lockout

The TPS25963x variants provide an user adjustable OVLO mechanism to ensure that the supply to the load is cut off if the input supply voltage exceeds a certain level. This can be achieved by dividing the input supply and feeding it to the OVLO pin. Whenever the voltage at the OVLO pin rises above a threshold  $V_{OVLO(R)}$ , the device turns OFF the FET. When the voltage at the OVLO pin falls below the threshold  $V_{OVLO(F)}$ , the FET is turned ON again. The rising and falling thresholds on this pin are slightly different, thereby providing some hysteresis and ensuring stable operation around the threshold voltage.



**图 45. TPS25963x Overvoltage Lockout Response**

## Feature Description (接下页)

The user should choose the resistor divider values appropriately to map the desired input overvoltage level to the OVLO threshold of the part.

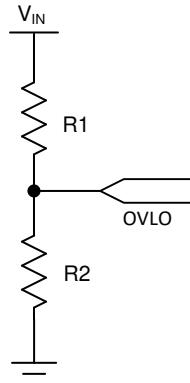


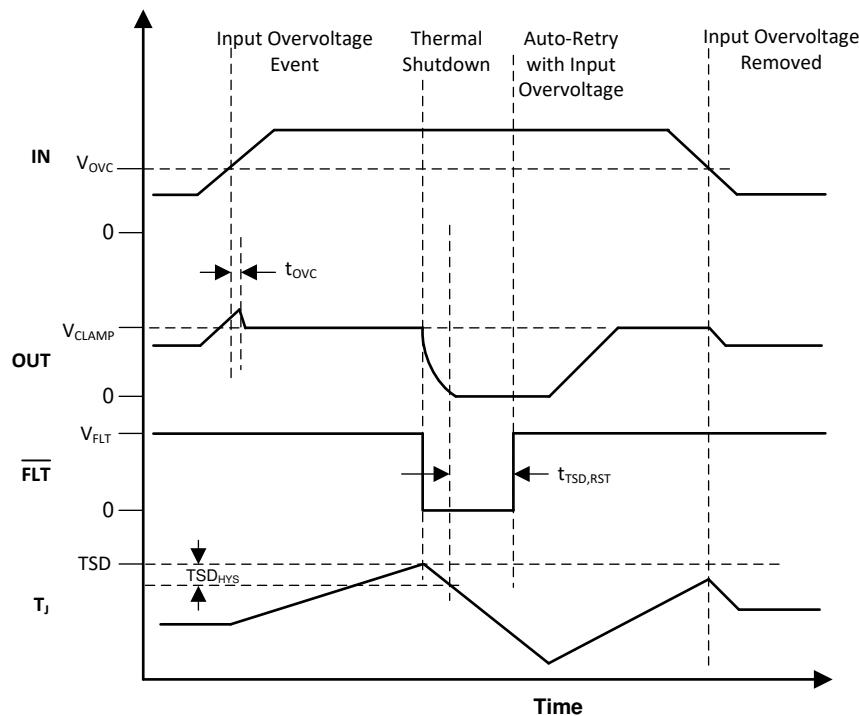
图 46. TPS25963x Adjustable Overvoltage Lockout

$$V_{IN(OV)} = V_{OVLO(R)} \times \frac{(R_1 + R_2)}{R_2} \quad (2)$$

### 8.3.2.2 Overvoltage Clamp

The TPS25962x variants provide a mechanism to clamp the output voltage to a user-selectable level quickly if the input voltage crosses a certain threshold. This ensures the load is not exposed to high voltages during any input overvoltage events and lowers the dependence on external protection devices (such as TVS/Zener diodes) in this condition. Once the input supply voltage rises above the OVC threshold voltage  $V_{OVC}$ , the device responds by clamping the voltage to  $V_{CLAMP}$  within a very short response time  $t_{OVC}$ . As long as an overvoltage condition is present on the input, the output voltage will be clamped to  $V_{CLAMP}$ . When the input drops below the output clamp threshold  $V_{OVC}$ , the clamp releases the output voltage as shown in [图 47](#).

## Feature Description (接下页)



**图 47. TPS25962x Overvoltage Clamp Response**

The OVC threshold can be configured to one of 3 pre-defined levels by connecting the OVCSEL pin as shown in 表 1.

**表 1. TPS25962x Overvoltage Clamp Threshold Selection**

OVCSEL Pin Connection	OVC Threshold (typ)
Shorted to GND	3.8 V
Connected to GND through 400 KΩ resistor	5.7 V
Open	13.7 V

During the overvoltage clamp condition, there could be significant heat dissipation in the internal FET depending on the  $V_{IN} - V_{OUT}$  voltage drop and the current ( $I_{OUT}$ ) through the FET leading to thermal shutdown if the condition persists for an extended period of time. In this case, the device would either stay latched-off or start an auto-retry cycle as explained in the *Overtemperature Protection (OTP)* section.

### 8.3.3 Inrush Current, Overcurrent and Short Circuit Protection

The TPS2596xx devices incorporate three levels of protection against overcurrent:

- Adjustable slew rate for inrush current control ( $dVdt$ )
- Active current limiting with adjustable limit ( $I_{LIM}$ ) for overcurrent protection
- Fast short-circuit response to protect against hard short-circuits

#### 8.3.3.1 Slew Rate and Inrush Current Control ( $dVdt$ )

The inrush current during turn on is directly proportional to the load capacitance and rising slew rate. 公式 3 can be used to find the slew rate  $SR_{ON}$  required to limit the inrush current  $I_{INRUSH}$  for a given load capacitance  $C_{OUT}$ .

$$SR(\text{mV / } \mu\text{s}) = \frac{I_{INRUSH}(\text{mA})}{C_L(\mu\text{F})} \quad (3)$$

For loads requiring a slower rising slew rate, a capacitor can be connected to the dVdt pin to adjust the rising slew rate and lower the inrush current during turn on. The required  $C_{dVdt}$  capacitance value to produce a given slew rate can be calculated using [公式 4](#).

$$C_{dVdt}(\mu F) = \frac{42000}{SR(mV / \mu s)} \quad (4)$$

### 8.3.3.2 Active Current Limiting

The load current is monitored during start-up and normal operation. When the load current exceeds the current limit  $I_{LIM}$  programmed by  $R_{ILM}$  resistor, the device regulates the current to the set limit  $I_{LIM}$  within  $t_{LIM}$ . The device exits current limiting when the load current falls below  $I_{LIM}$ . [公式 5](#) can be used to find the  $R_{ILM}$  value for a desired current limit.

$$R_{ILM}(\Omega) = \frac{903}{I_{LIM}(A) - 0.0112} \quad (5)$$

In the current limiting state, the output voltage drops resulting in increased power dissipation in the internal FET leading to thermal shutdown if the condition persists for an extended period of time. In this case, the device either stays latched-off or starts an auto-retry cycle as explained in the [Overtemperature Protection \(OTP\)](#) section.

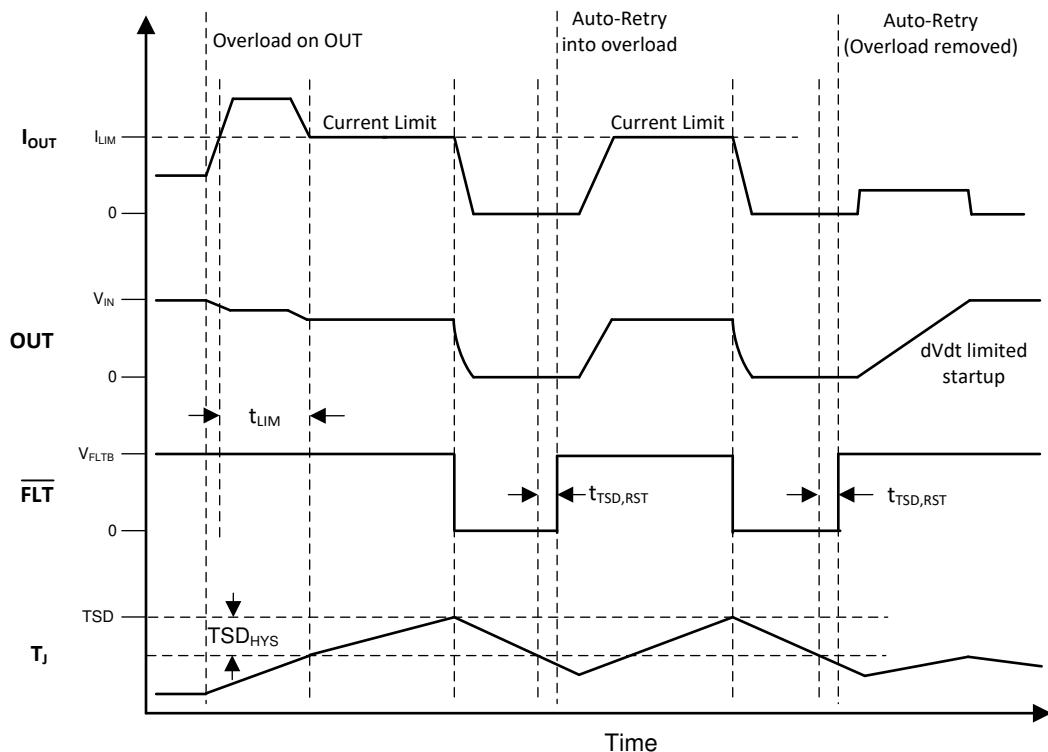
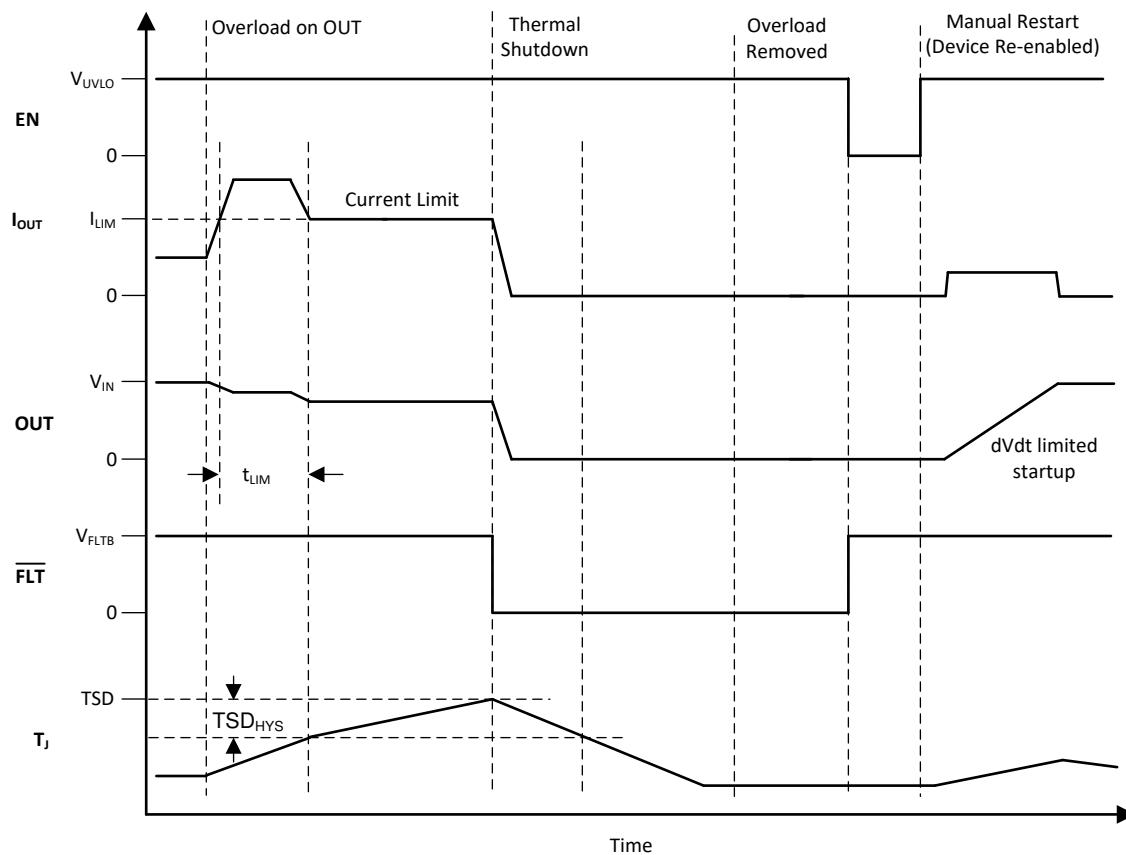


图 48. TPS2596x1 Overcurrent Response (Auto-retry)



**图 49. TPS2596x0 Overcurrent Response (Latch-off)**

### 8.3.3.3 Short-Circuit Protection

The current through the device increases very rapidly during a short-circuit event. If the current exceeds  $1.5 \times I_{LIM}$ , the device engages a fast current clamping circuit to regulate down the current faster than the nominal overcurrent response time ( $t_{LIM}$ ). The device does not completely turn off the power FET to ensure uninterrupted power in the event of transient overcurrents or supply transients. The device stops limiting the current once the load current falls below the programmed  $I_{LIM}$  threshold.

The output voltage drops in the current limiting state, resulting in increased power dissipation in the internal FET and might lead to thermal shutdown if the condition persists for an extended period of time. In this case, the device either stays latched-off or starts an auto retry cycle as explained in the [Overtemperature Protection \(OTP\)](#) section.

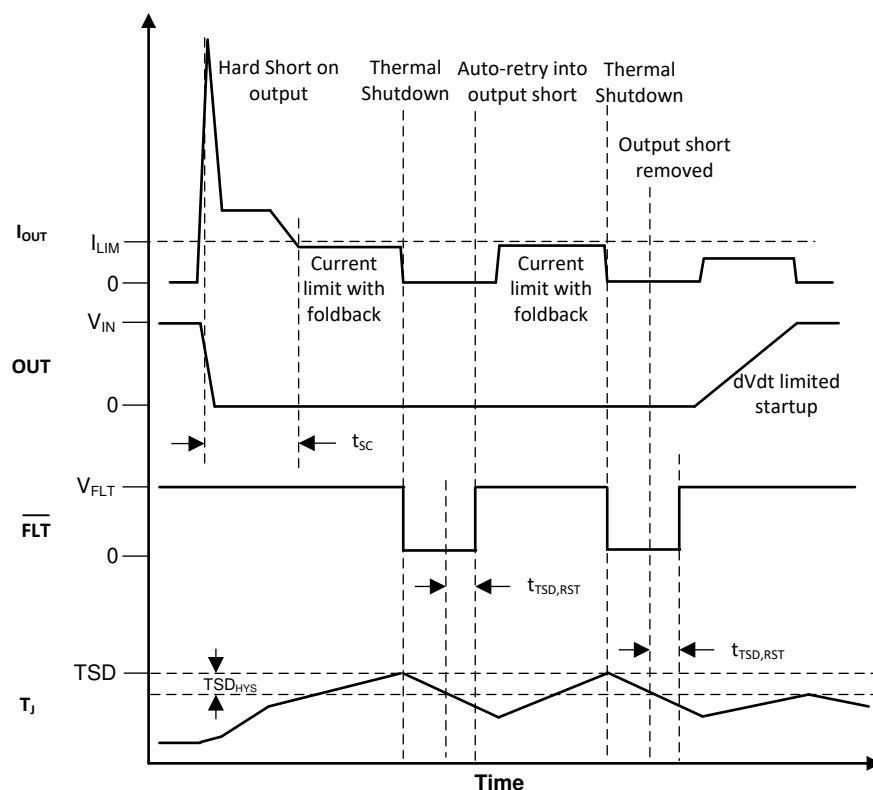


图 50. TPS2596xx Short Circuit Response

### 8.3.4 Analog Load Current Monitor (IMON)

The device allows the system to monitor the output load current accurately by providing an analog current on the ILM pin which is proportional to the current ( $I_{OUT}$ ) through the FET. The user can sense the voltage ( $V_{ILM}$ ) across the  $R_{ILM}$  to get a measure of the output load current.

$$I_{OUT}(A) = \frac{V_{ILM}(V)}{G_{IMON}(\mu A / A) \times R_{ILM}(\Omega)} \quad (6)$$

### 8.3.5 Overtemperature Protection (OTP)

Thermal Shutdown will occur when the junction temperature ( $T_J$ ) exceeds the thermal shutdown threshold ( $T_{SD}$ ). When the TPS2596x0 variant detects thermal overload, it will be shut down and remain latched off until the device is power cycled or re-enabled by toggling the EN/UVLO pin. When the TPS2596x1 variant detects thermal overload, it will remain off until it has cooled down sufficiently. Once the TPS2596x1 junction has cooled down below  $T_{SD} - T_{SD_{HYS}}$ , it will remain off for an additional delay of  $t_{TSD,RST}$  after which it will automatically retry to turn on if it is still enabled.

表 2. TPS2596x Thermal Shutdown

Device	Enter TSD	Exit TSD
TPS2596x0 (Latch-Off)	$T_J \geq T_{SD}$	$T_J < T_{SD} - T_{SD_{HYS}}$ and Power Cycle ( $V_{IN} < V_{UVP(F)}$ ) / Enable Cycle ( $V_{EN} < V_{SD}$ )
TPS2596x1 (Auto-Retry)	$T_J \geq T_{SD}$	$T_J < T_{SD} - T_{SD_{HYS}}$ and $t_{TSD,RST}$ timer expired

### 8.3.6 Fault Indication

表 3 summarizes the protection response to various fault conditions.

**表 3. Fault Response**

Event / Fault	Protection Response	FLT Asserted	FLT Delay
Overtemperature	Shutdown	Yes	
Undervoltage	Cut-off	No	
Overvoltage	Clamp (OVC - TPS25962x only)	No	
	Cut-off (OVLO - TPS25963x only)	Yes	$t_{OVLO}$
Overcurrent	Current Limit	No	
Short-Circuit	Current Limit	No	
ILM Pin Short to GND	Shut down	Yes	
ILM Pin Open	Shut down	No	

When the device turns off due to one of these fault conditions, the  $\overline{FLT}$  pin is pulled low.

Power cycling the part or pulling the EN/UVLO pin voltage below  $V_{SD}$  clears the fault and the  $\overline{FLT}$  pin is de-asserted. It also clears the  $t_{TSD,RST}$  timer (Auto-retry variants only). Pulling the EN/UVLO just below the UVLO threshold ( $V_{UVLO(F)}$ ) has no impact on the device in this condition. This is true for both Latch-off (TPS2596x0) and Auto-retry (TPS2596x1) variants.

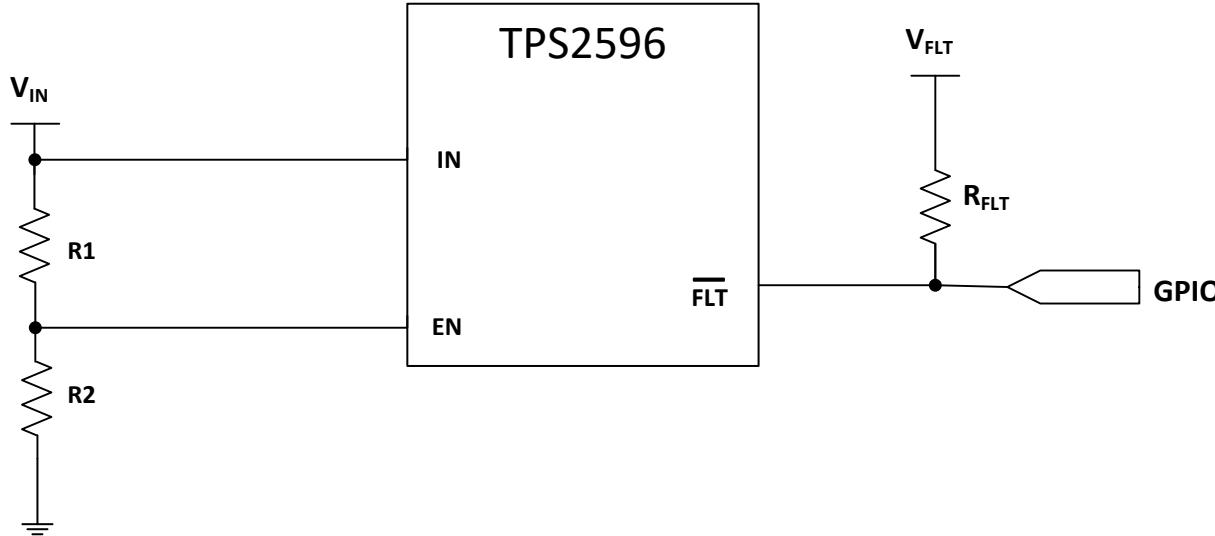
For Auto-retry (TPS2596x1) variants, at the end of the  $t_{TSD,RST}$  timer after a fault, the device restarts automatically and the  $\overline{FLT}$  pin is de-asserted.

## 8.4 Device Functional Modes

The features of the device depend on the operating mode.

### 8.4.1 Enable and Fault Pin Functional Mode 1: Single Device, Self-Controlled

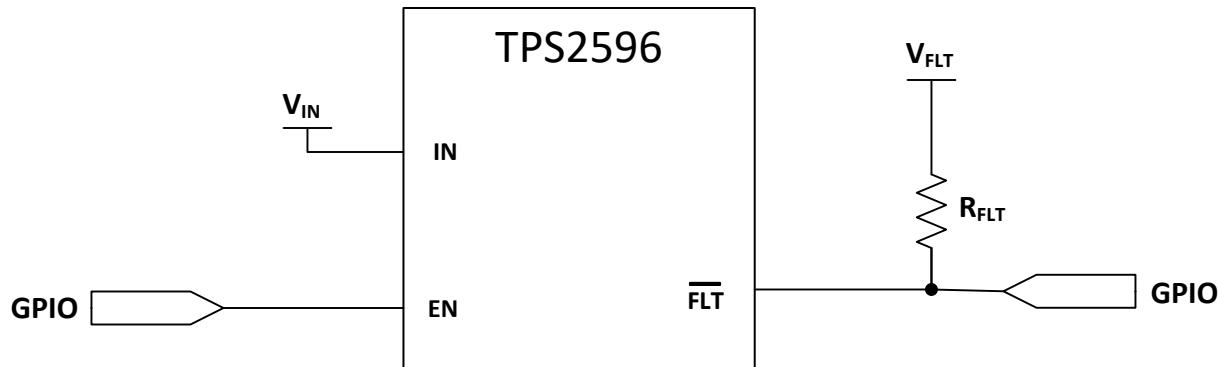
In this mode of operation, the device is enabled by the VIN voltage without the need of an external processor to drive the ENABLE pin. The FLT pin is optionally monitored by an external host as shown in 图 51.



**图 51. Single Device, Self-Controlled**

### 8.4.2 Enable and Fault Pin Functional Mode 2: Single Device, Host-Controlled

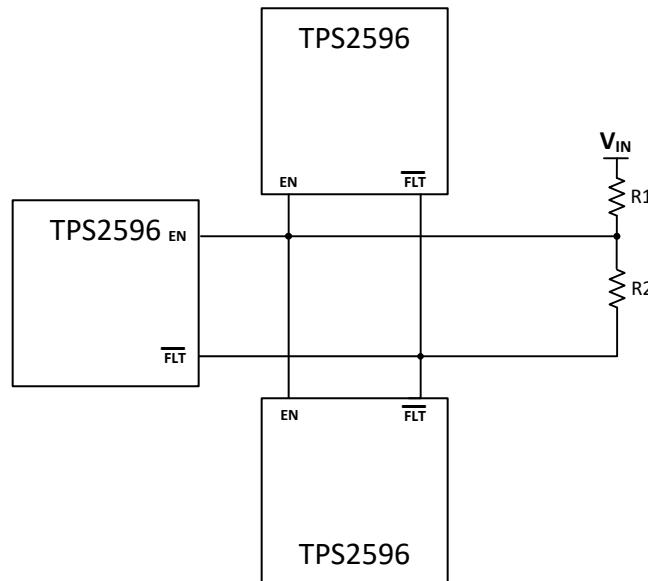
In this mode of operation, the device is enabled by the VIN voltage without the need of an external processor to drive the ENABLE pin. The FLT pin is optionally monitored by an external host as shown in 图 53.

**Device Functional Modes (接下页)**


**图 52. Single Device, Self-Controlled**

#### 8.4.3 Enable and Fault Pin Functional Mode 3: Multiple Devices, Self-Controlled

In this mode of operation, the devices are self-controlled (no host present). The EN and  $\overline{\text{FLT}}$  pins of multiple devices are shorted together as shown in [图 52](#). In this configuration, when any one of the TPS2596xx devices detects a fault, it automatically disables the other TPS2596xx devices in the system.



**图 53. Multiple Devices, Self-Controlled**

## 9 Application and Implementation

注

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

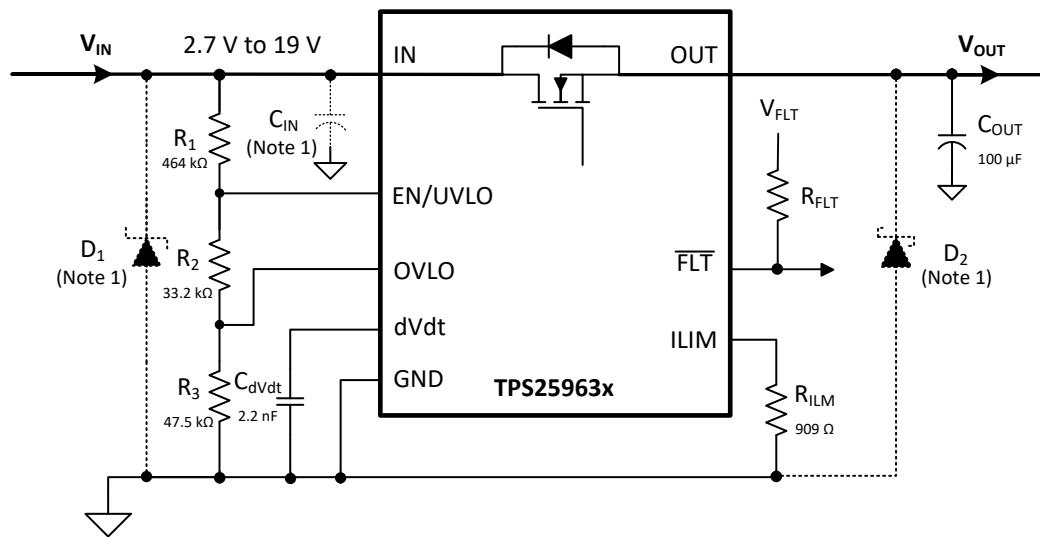
### 9.1 Application Information

The TPS2596xx device is an integrated eFuse that is typically used for hot-swap and power rail protection applications. The device operates from 2.7 V to 19 V with adjustable current limit and undervoltage protection. The device aids in controlling the in-rush current and provides precise current limiting during overload conditions for systems such as energy meters, white goods, building automation and adapter input protection. The device also provides robust protection for multiple faults on the sub-system rail.

The following design procedure can be used to select the supporting component values based on the application requirement.

### 9.2 Typical Application

#### 9.2.1 Precision Current Limiting and Protection for White Goods



- (1)  $C_{IN}$  is optional and 0.1  $\mu$ F is recommended to suppress transients due to the inductance of PCB routing or from input wiring. If system needs to pass IEC 61000-4-4 EFT test, minimum  $C_{IN}$  of 1  $\mu$ F should be used to prevent eFuse from turning off during EFT bursts.

**图 54. Typical Application Schematic: Simple eFuse for White Goods**

#### 9.2.2 Design Requirements

**表 4. Design Parameters**

DESIGN PARAMETER	EXAMPLE VALUE
Input voltage , $V_{IN}$	12 V
Undervoltage lockout set point, $V_{UV}$	8 V
Oversupply protection set point , $V_{OV}$	13.7 V
Oversupply protection type	Lock-out
Load at start-up, $R_{L(SU)}$	24 $\Omega$

## Typical Application (接下页)

表 4. Design Parameters (接下页)

DESIGN PARAMETER	EXAMPLE VALUE
Current limit, $I_{LIM}$	1 A
Load capacitance, $C_{OUT}$	100 $\mu$ F
Maximum ambient temperatures, $T_A$	85°C

### 9.2.3 Detailed Design Procedure

The designer must know the following:

- Normal input operation voltage
- Maximum output capacitance
- Maximum current limit
- Load during start-up
- Maximum ambient temperature of operation

This design procedure seeks to control the junction temperature of device under both static and transient conditions by proper selection of output ramp-up time and associated support components. The designer can adjust this procedure to fit the application and design criteria. A spreadsheet design tool [TPS2596 Design Calculator](#) is also available for simplified calculations.

#### 9.2.3.1 Programming the Current-Limit Threshold: $R_{ILM}$ Selection

The  $R_{ILM}$  resistor at the ILM pin sets the over load current limit, this can be set using [公式 7](#).

$$R_{ILM}(\Omega) = \frac{903}{I_{LIM}(A) - 0.0112} = \frac{903}{1 - 0.0112} = 913.2 \Omega \quad (7)$$

Choose closest standard value resistor: 909  $\Omega$  with 1% tolerance.

#### 9.2.3.2 Undervoltage and Overvoltage Lockout Set Point

The undervoltage lockout (UVLO) and overvoltage lockout (OVLO) trip point is adjusted using the external voltage divider network of  $R_1$ ,  $R_2$  and  $R_3$  as connected between IN, EN/UVLO, OVLO and GND pins of the device. The values required for setting the undervoltage and overvoltage are calculated solving [公式 8](#) and [公式 9](#).

$$V_{UVLO} = \frac{R_2 + R_3}{(R_1 + R_2 + R_3)} \times V_{IN(UV)} \quad (8)$$

$$V_{OVLO} = \frac{R_3}{(R_1 + R_2 + R_3)} \times V_{IN(OV)} \quad (9)$$

Where  $V_{UVLO(R)}$  is UVLO rising threshold (1.2 V). Because  $R_1$ ,  $R_2$  and  $R_3$  leak the current from input supply  $V_{IN}$ , these resistors must be selected based on the acceptable leakage current from input power supply  $V_{IN}$ .

The current drawn by  $R_1$ ,  $R_2$  and  $R_3$  from the power supply is  $I_{R123} = V_{IN} / (R_1 + R_2 + R_3)$ .

However, leakage currents due to external active components connected to the resistor string can add error to these calculations. So, the resistor string current,  $I_{R123}$  must be chosen to be 20 times greater than the leakage current expected.

From the device electrical specifications,  $V_{OVLO} = 1.2$  V and  $V_{UVLO} = 1.2$  V. For design requirements,  $V_{OV} = 13.7$  V and  $V_{UV} = 8$  V. To solve the equation, first choose the value of  $R_3 = 47$  k $\Omega$  and use [公式 9](#) to solve for  $(R_1 + R_2) = 489.58$  k $\Omega$ . Use Equation 8 and value of  $(R_1 + R_2)$  to solve for  $R_2 = 33.48$  k $\Omega$  and finally  $R_1 = 456.1$  k $\Omega$ . Using the closest standard 1% resistor values gives  $R_1 = 464$  k $\Omega$ ,  $R_2 = 33.2$  k $\Omega$ , and  $R_3 = 47.5$  k $\Omega$ .

### 9.2.3.3 Setting Output Voltage Ramp Time ( $T_{dVdT}$ )

For a successful design, the junction temperature of device must be kept below the absolute maximum rating during both dynamic (start-up) and steady state conditions. Dynamic power stresses often are an order of magnitude greater than the static stresses, so it is important to determine the right start-up time and in-rush current limit required with system capacitance to avoid thermal shutdown during start-up with and without load.

The required ramp-up capacitor  $C_{dVdT}$  is calculated considering the two possible cases (see [Case 1: Start-Up Without Load. Only Output Capacitance  \$C\_{OUT}\$  Draws Current](#) and [Case 2: Start-Up With Load. Output Capacitance  \$C\_{OUT}\$  and Load Draw Current](#)).

#### 9.2.3.3.1 Case 1: Start-Up Without Load. Only Output Capacitance $C_{OUT}$ Draws Current

During start-up, as the output capacitor charges, the voltage drop as well as the power dissipated across the internal FET decreases. The average power dissipated in the device during start-up is calculated using [公式 11](#).

For TPS2596xx device, the inrush current is determined as shown in [公式 10](#).

$$I_{INRUSH} = C_{OUT} \times \frac{V_{IN}}{T_{dVdT}} \quad (10)$$

Power dissipation during start-up is shown in [公式 11](#).

$$P_{D(INRUSH)} = 0.5 \times V_{IN} \times I_{INRUSH} \quad (11)$$

[公式 11](#) assumes that load does not draw any current until the output voltage has reached its final value.

#### 9.2.3.3.2 Case 2: Start-Up With Load. Output Capacitance $C_{OUT}$ and Load Draw Current

When the load draws current during the turnon sequence, there is additional power dissipated. Considering a resistive load during start-up  $R_{L(SU)}$ , load current ramps up proportionally with increase in output voltage during  $T_{dVdT}$  time. Equations 12 to 15 show the average power dissipation in the internal FET during charging time due to resistive load.

$$P_{D(LOAD)} = \left(\frac{1}{6}\right) \times \frac{V_{IN}^2}{R_{L(SU)}} \quad (12)$$

Total power dissipated in the device during start-up is [公式 13](#).

$$P_{D(STARTUP)} = P_{D(INRUSH)} + P_{D(LOAD)} \quad (13)$$

Total current during start-up is given by [公式 14](#).

$$I_{STARTUP} = I_{INRUSH} + I_L(t) \quad (14)$$

If  $I_{STARTUP} > I_{LIMIT}$ , the device limits the current to  $I_{LIMIT}$  and the current-limited charging time is determined by [公式 15](#).

$$T_{dvdT(Current-Limited)} = C_{OUT} \times R_{L(SU)} \times \left[ \frac{I_{LIMIT}}{I_{INRUSH}} - 1 + \ln \left( \frac{I_{INRUSH}}{I_{LIMIT} - \frac{V_{IN}}{R_{L(SU)}}} \right) \right] \quad (15)$$

The power dissipation, with and without load, for selected start-up time must not exceed the shutdown limits as shown in [图 55](#).

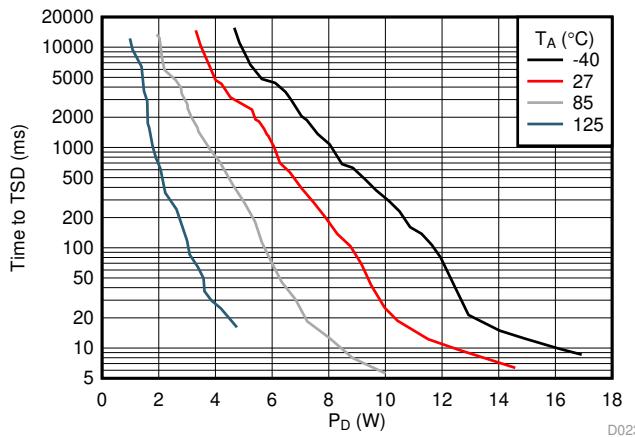


图 55. Thermal Shutdown Limit Plot

For the design example under discussion, select ramp-up capacitor  $C_{dvdt} = 22000 \text{ pF}$ . The default slew rate for  $C_{dvdt} = 22000 \text{ pF}$  is  $1.9 \text{ mV}/\mu\text{s}$ . With slew rate of  $1.9 \text{ mV}/\mu\text{s}$ , the ramp-up time  $T_{dvdt}$  for  $12 \text{ V}$  input is  $6.3 \text{ ms}$ .

The inrush current drawn by the load capacitance  $C_{OUT}$  during ramp-up using 公式 16.

$$I_{INRUSH} = \frac{100 \mu\text{F} \times 1.9 \text{ mV}}{\mu\text{s}} = 190 \text{ mA} \quad (16)$$

The inrush power dissipation is calculated using 公式 17.

$$P_{D(INRUSH)} = 0.5 \times 12 \times 190 \text{ m} = 1.14 \text{ W} \quad (17)$$

For  $1.14 \text{ W}$  of power loss, the thermal shutdown time of the device must not be less than the ramp-up time  $T_{dvdt}$  to avoid the false trip at the maximum operating temperature. 图 55 shows the thermal shutdown limit at  $T_A = 85^\circ\text{C}$ , for  $1.14 \text{ W}$  of power, the shutdown time is infinite. Therefore, it is safe to use  $6.3 \text{ ms}$  as the start-up time without any load on the output.

The additional power dissipation when a  $10\text{-}\Omega$  load is present during start-up is calculated using 公式 18.

$$P_{D(LOAD)} = \left(\frac{1}{6}\right) \times \frac{12 \times 12}{24} = 1\text{W} \quad (18)$$

The total device power dissipation during start-up is given in 公式 19.

$$P_{D(STARTUP)} = 1 + 1.14 = 2.24 \text{ W} \quad (19)$$

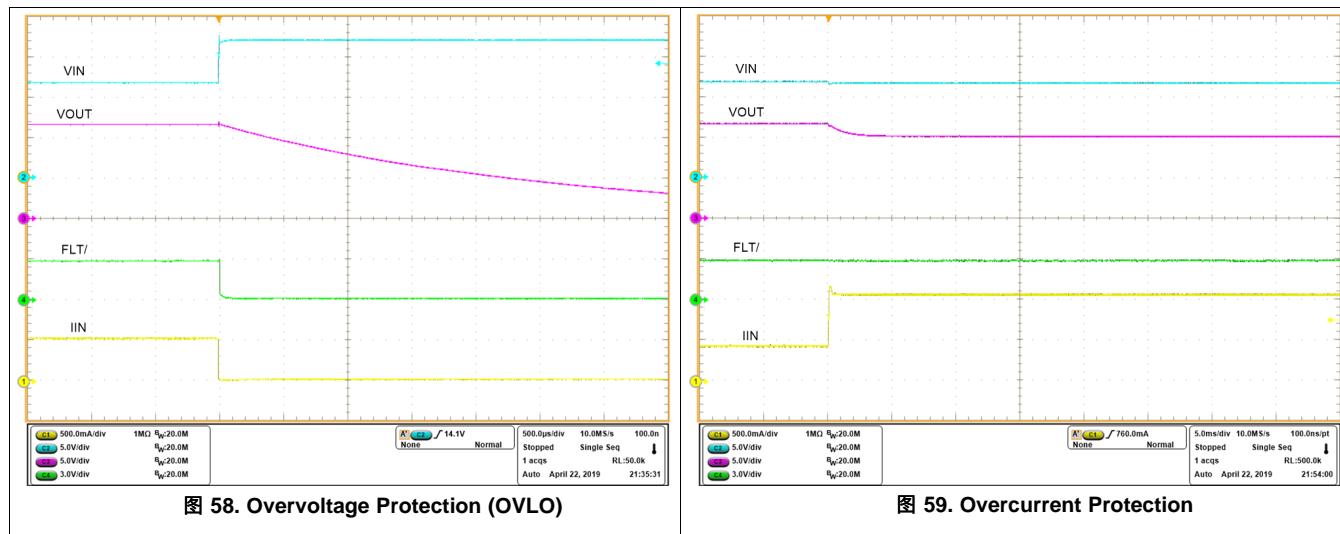
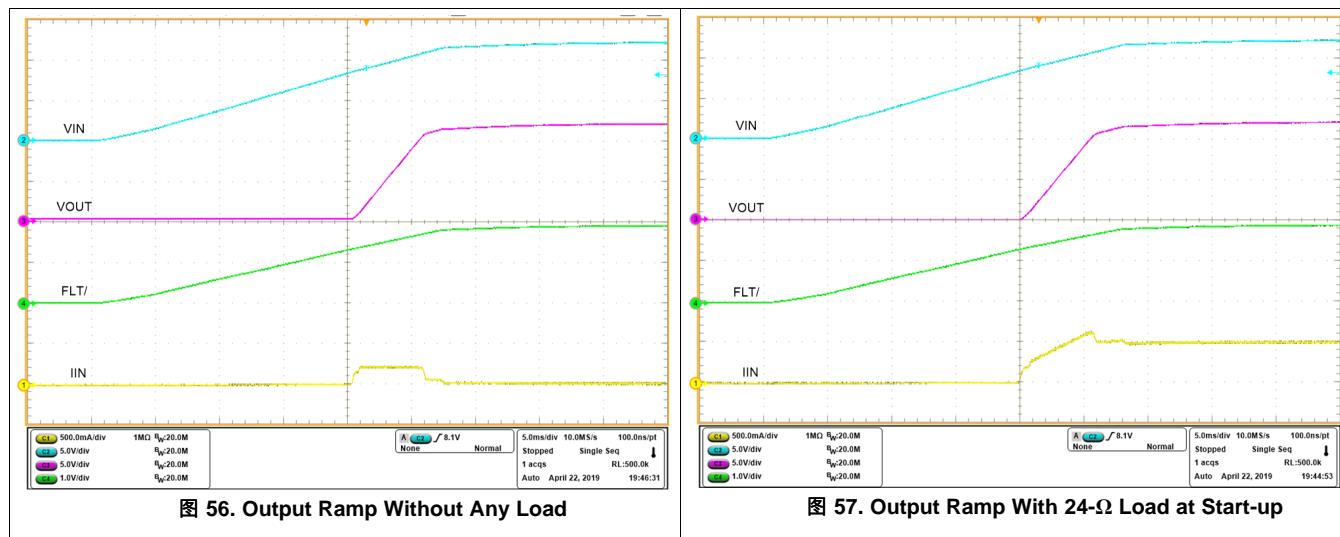
图 55 shows  $T_A = 85^\circ\text{C}$  and the thermal shutdown time for  $2.24 \text{ W}$  is approximately  $2000 \text{ ms}$ , which increases the margins further for shutdown time and ensures successful operation during start up and steady state conditions.

When  $C_{OUT}$  is large, there is a need to decrease the power dissipation during start-up. This can be done by increasing the value of the  $C_{dvdt}$  capacitor.

#### 9.2.4 Support Component Selection: $R_{FLT}$ and $C_{IN}$

Referring to application schematics,  $R_{FLT}$  is required only if  $\overline{FLT}$  is used; The resistor serves as pull-up for the open-drain output driver. The current sunk by this pin should not exceed  $10 \text{ mA}$ .  $C_{IN}$  is a bypass capacitor to help control transient voltages, unit emissions, and local supply noise. Where acceptable, a value in the range from  $0.001 \mu\text{F}$  to  $0.1 \mu\text{F}$  is recommended for  $C_{IN}$ .

### 9.2.5 Application Curves



## 9.3 System Examples

The TPS2596xx provides a simple solution for current limiting, inrush current control and supervision of power rails for wide range of applications operating at 2.7 V to 19 V and delivering up to 2 A.

### 9.3.1 Current Limiting and Overvoltage Protection and for Energy Meter Power Rails

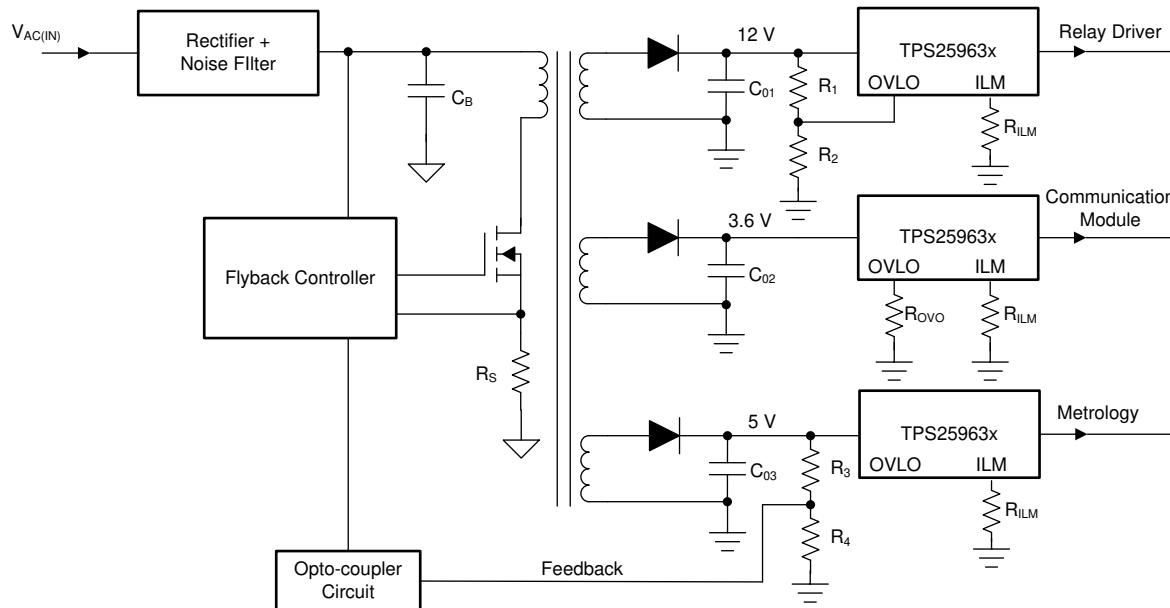
Energy meters generally use a single AC/DC power supply (for example: flyback converter) with multiple DC outputs for powering blocks like Metrology (analog front-end, microcontroller, memory), Real Time Clock (RTC), Relay (for remote load connect/disconnect) and Communications module. Metrology is the most critical subsystem and is required to operate uninterrupted under all conditions, even if a fault occurs in any of the supplementary blocks. One solution would be to oversize the power supply design so that it can handle the excess current demands during a fault condition, which increases the cost of the meter. A more elegant and cost-optimized solution would be to add an eFuse like TPS2596xx on the supplementary power rails, which provides accurate current limiting and fast short-circuit protection, thereby ensuring reliable operation of the metrology block without increasing the size or cost of the power supply. Apart from that, the TPS2596xx provides additional benefits such as:

- Overvoltage Protection (Lock-out and Clamp) to shield down-stream low voltage circuits from harmful overvoltages arising from poor cross-regulation between windings or AC input voltage surges.

## System Examples (接下页)

- Disconnect supply to rarely used loads to minimize power consumption

图 60 显示了使用 TPS2596xx 的典型能源表电源实施例。



**图 60. Energy Meter Power Rail Protection Example**

TIDA-010037 展示了使用 eFuse 保护辅助电源轨的能源表设计。

### 9.3.2 Precision Current Limiting and Protection in Appliances

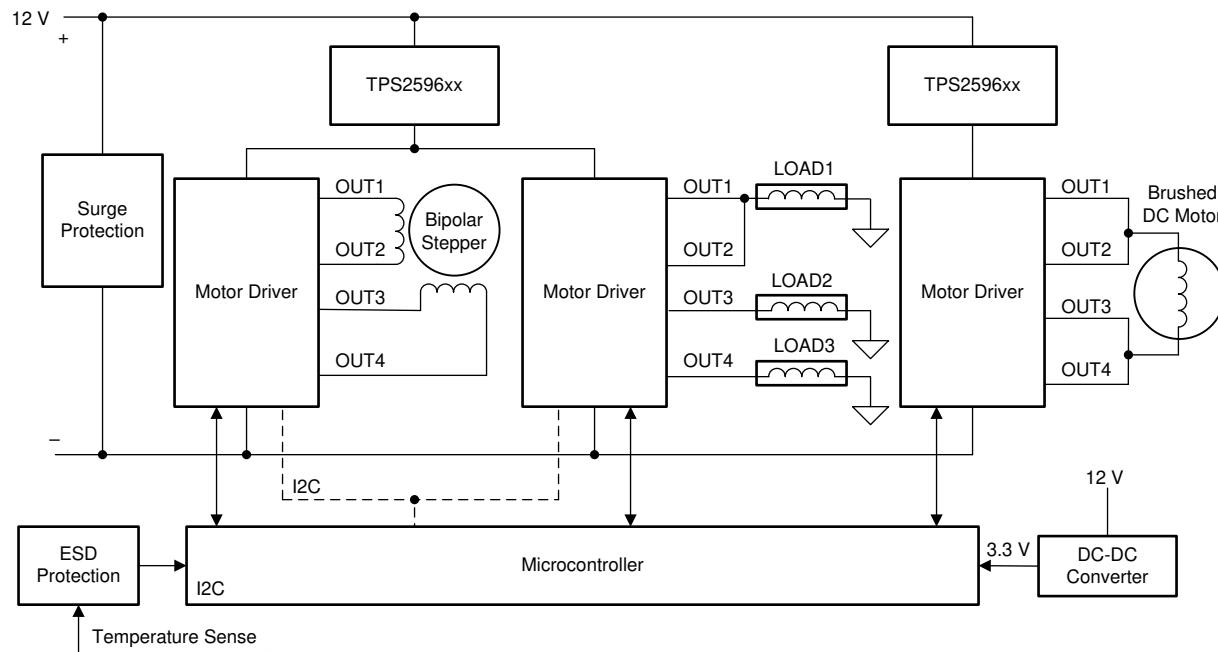
家庭和类似电气设备在进行各种测试时（例如：针火焰、发光丝）作为电气和消防安全合规性的一部分。在设计中需要特别注意，以通过这些测试，这包括使用更高级别的阻燃塑料材料。在标准中有一些规定可以利用，使其更容易、更快地通过认证，同时降低塑料材料的成本。例如，任何节点如果有少于 15 W 的可用功率，则归类为低功耗电路（LPC，根据 IEC 60335-1 定义），并被认为安全。所有从 LPC 节点进一步向下游的电路或子系统都免于上述提及的测试。

eFuses 如 TPS2596xx 是一种简单且成本效益高的方法来限制向下游负载提供的功率。要考虑的关键参数是电流限制容差和精度，这决定了可以设置的额定电流限制，而不会超过 15-W 功率限制的上限。在下限方面，它决定了负载在正常条件下可以正常运行而不触发电流限制的最大功率。TPS2596xx 提供 ±5 % 的电流限制精度（在室温下），这使得负载可以在正常操作条件下使用近 90% 的 15-W 限制。

相比之下，另一种可能的解决方案是具有更宽的电流限制容差，如 ±25 %，这将使负载在正常条件下只能使用约 50% 的 15 W。这给负载电路设计带来了严重的约束条件。

图 61 展示了一个子系统的例子，即冰箱和冷冻系统，其中 TPS2596xx 用于精确的电流限制和 15-W 电源轨的保护，以简化 IEC 60335-1 的合格认证。

## System Examples (接下页)



**图 61. Appliances 15-W LPC Implementation Example**

TIDA-010004 demonstrates a multi-load drive using single driver chip with eFuse for protection and 15-W LPC implementation.

Refer to this [Designing Low-Power Circuits \(LPCs\) using TPS2596 for Household and similar Appliances](#) application note for a detailed insight into implementing power limited circuits using eFuses.

## 10 Power Supply Recommendations

The TPS2596xx devices are designed for a supply voltage range of  $2.7 \text{ V} \leq \text{VIN} \leq 19 \text{ V}$ . An input ceramic bypass capacitor higher than  $0.1 \mu\text{F}$  is recommended if the input supply is located more than a few inches from the device. The power supply must be rated higher than the set current limit to avoid voltage droops during overcurrent and short-circuit conditions.

### 10.1 Transient Protection

In the case of a short circuit and overload current limit when the device interrupts current flow, the input inductance generates a positive voltage spike on the input, and the output inductance generates a negative voltage spike on the output. The peak amplitude of voltage spikes (transients) is dependent on the value of inductance in series to the input or output of the device. Such transients can exceed the absolute maximum ratings of the device if steps are not taken to address the issue. Typical methods for addressing transients include:

- Minimize lead length and inductance into and out of the device.
  - Use a large PCB GND plane.
  - Use a Schottky diode across the output to absorb negative spikes.
  - Use a low-value ceramic capacitor  $C_{IN} = 0.001 \mu\text{F}$  to  $0.1 \mu\text{F}$  to absorb the energy and dampen the transients.
- The approximate value of input capacitance can be estimated with [公式 20](#):

$$V_{SPIKE(Absolute)} = V_{IN} + I_{LOAD} \times \sqrt{\frac{L_{IN}}{C_{IN}}} \quad (20)$$

where

- $V_{IN}$  is the nominal supply voltage
- $I_{LOAD}$  is the load current
- $L_{IN}$  equals the effective inductance seen looking into the source
- $C_{IN}$  is the capacitance present at the input

NOTE: Systems which need to pass IEC 61000-4-4 tests for immunity to Electrical Fast Transients (EFT) should use a minimum  $C_{IN}$  of  $1 \mu\text{F}$  to ensure the TPS2596xx does not turn OFF during the EFT burst.

Some applications may require the addition of a Transient Voltage Suppressor (TVS) to prevent transients from exceeding the absolute maximum ratings of the device. The circuit implementation with optional protection components (a ceramic capacitor, TVS and Schottky diode) is shown in [图 62](#).

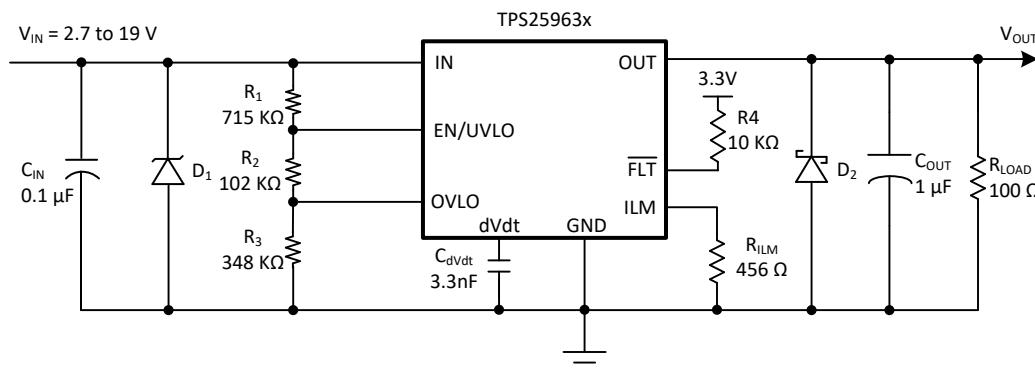


图 62. Circuit Implementation with Optional Protection Components

## 10.2 Output Short-Circuit Measurements

It is difficult to obtain repeatable and similar short-circuit testing results. The following contribute to variation in results:

- Source bypassing
- Input leads
- Circuit layout
- Component selection
- Output shorting method
- Relative location of the short
- Instrumentation

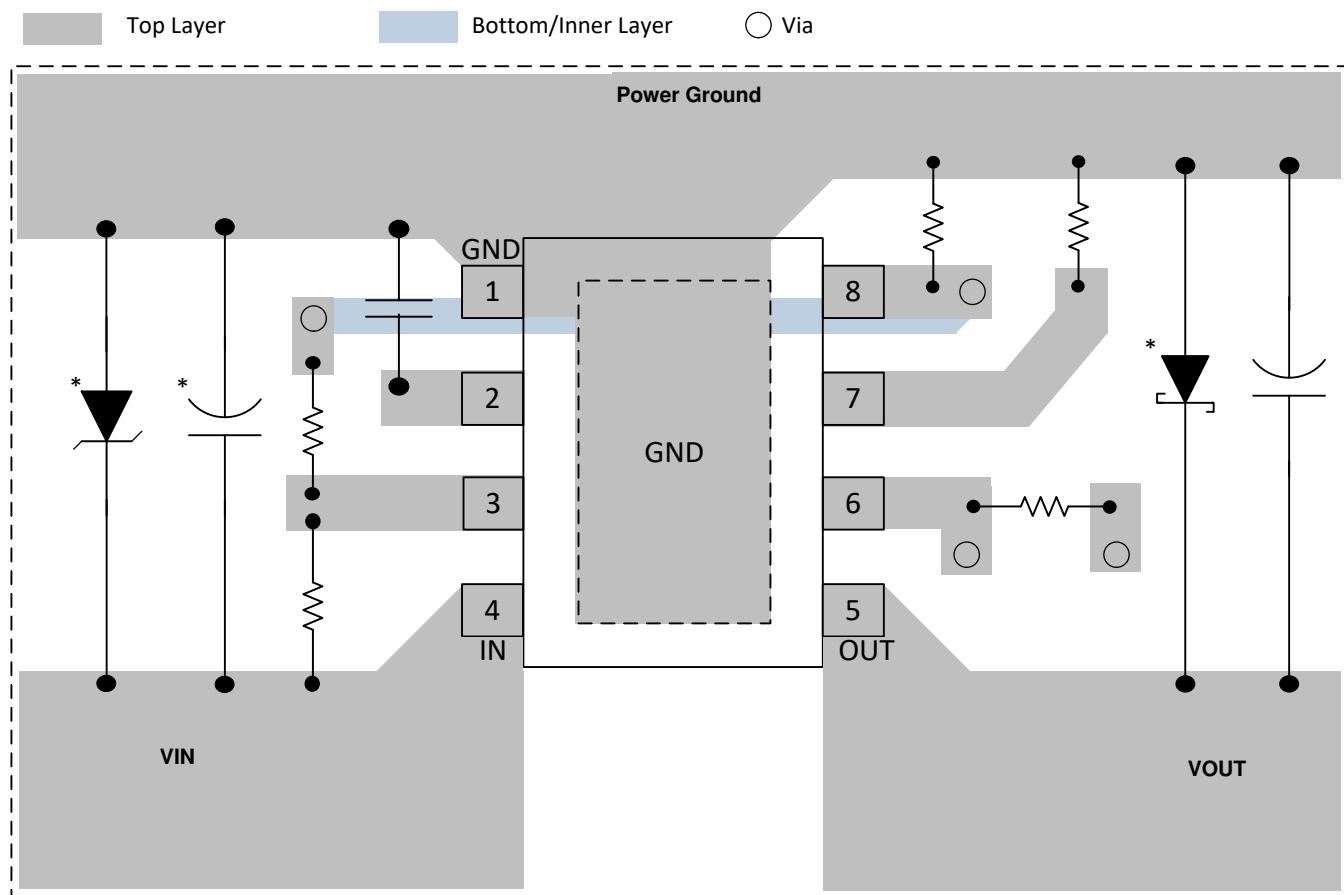
The actual short exhibits a certain degree of randomness because it microscopically bounces and arcs. Ensure that configuration and methods are used to obtain realistic results. Do not expect to see waveforms exactly like those in this data sheet because every setup is different.

## 11 Layout

### 11.1 Layout Guidelines

- For all applications, a ceramic decoupling capacitor of  $0.01 \mu\text{F}$  or greater is recommended between the IN terminal and GND terminal. For hot-plug applications, where input power-path inductance is negligible, this capacitor can be eliminated or minimized.
- The optimal placement of the decoupling capacitor is closest to the IN and GND terminals of the device. Care must be taken to minimize the loop area formed by the bypass-capacitor connection, the IN terminal, and the GND terminal of the IC. See [图 63](#) for a PCB layout example.
- High current-carrying power-path connections must be as short as possible and must be sized to carry at least twice the full-load current.
- The GND terminal must be tied to the PCB ground plane at the terminal of the IC. The PCB ground must be a copper plane or island on the board.
- Locate the following support components close to their connection pins:
  - $R_{ILM}$
  - $C_{dVdT}$
  - Resistor network for the EN/UVLO pin
  - Resistor network for the OVLO pin for TPS25693x variants
  - Pull-down resistor on the OVCSEL pin for TPS25692x variants
 Connect the other end of the component to the GND pin of the device with shortest trace length. The trace routing from the  $R_{ILM}$ ,  $C_{dVdT}$  and  $R_{OVCSEL}$  (for TPS25692x variants) components to the device pins must be as short as possible to reduce parasitic effects on the current limit, soft-start timing and overvoltage clamp response. These traces must not have any coupling to switching signals on the board.
- Protection devices such as TVS, snubbers, capacitors, or diodes must be placed physically close to the device they are intended to protect. These protection devices must be routed with short traces to reduce inductance. For example, a protection Schottky diode is recommended to address negative transients due to switching of inductive loads, and it must be physically close to the OUT pins.
- Obtaining acceptable performance with alternate layout schemes is possible. The Layout Example shown in [图 63](#) has been shown to produce good results and is intended as a guideline.

## 11.2 Layout Example



\* Optional: Needed only to suppress the transients caused by inductive load switching

图 63. TPS2596xx Layout Example

## 12 器件和文档支持

### 12.1 文档支持

#### 12.1.1 相关文档

请参阅如下相关文档：

- [《电子保险丝的基本知识》](#)
- [《TPS2596EVM: TPS2596xx 评估模块》](#)
- [《TPS2596 设计计算器》](#)
- [《使用 TPS2596 为家用或类似用途电器设计低功耗电路 \(LPC\)》](#)
- [《TIDA-010037 高精度分相 CT 电量计》](#)
- [《TIDA-010004 基于单个驱动器且受全面保护的 12V 步进、刷式直流和执行器驱动器》](#)

### 12.2 接收文档更新通知

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 ESD 的损坏小至导致微小的性能降级，大至整个器件故障。精密的集成电路可能更容易受到损坏，这是因为非常细微的参数更改都可能导致器件与其发布的规格不相符。

### 12.6 Glossary

**SLYZ022 — TI Glossary.**

This glossary lists and explains terms, acronyms, and definitions.

## 13 机械、封装和可订购信息

以下页面包含机械、封装和可订购信息。这些信息是指定器件的最新可用数据。数据如有变更，恕不另行通知，且不会对此文档进行修订。如需获取此数据表的浏览器版本，请查阅左侧的导航栏。

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**PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
TPS259620DDAR	ACTIVE	SO PowerPAD	DDA	8	2500	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	259620	<span style="background-color: red; color: white;">Samples</span>
TPS259620DDAT	ACTIVE	SO PowerPAD	DDA	8	250	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	259620	<span style="background-color: red; color: white;">Samples</span>
TPS259621DDAR	ACTIVE	SO PowerPAD	DDA	8	2500	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	259621	<span style="background-color: red; color: white;">Samples</span>
TPS259621DDAT	ACTIVE	SO PowerPAD	DDA	8	250	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	259621	<span style="background-color: red; color: white;">Samples</span>
TPS259630DDAR	ACTIVE	SO PowerPAD	DDA	8	2500	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	259630	<span style="background-color: red; color: white;">Samples</span>
TPS259630DDAT	ACTIVE	SO PowerPAD	DDA	8	250	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	259630	<span style="background-color: red; color: white;">Samples</span>
TPS259631DDAR	ACTIVE	SO PowerPAD	DDA	8	2500	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	259631	<span style="background-color: red; color: white;">Samples</span>
TPS259631DDAT	ACTIVE	SO PowerPAD	DDA	8	250	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	259631	<span style="background-color: red; color: white;">Samples</span>

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

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(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

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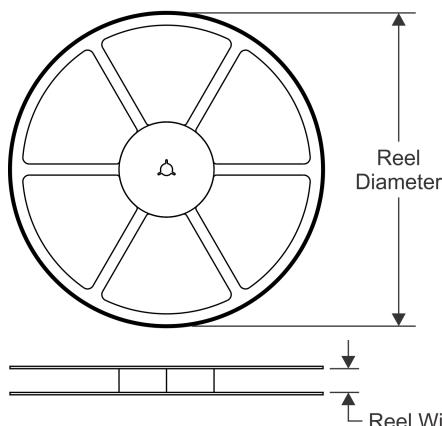
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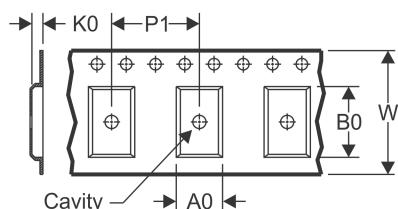
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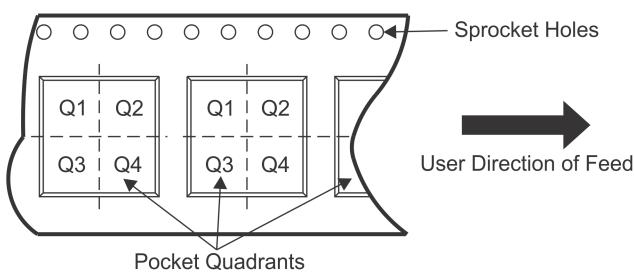


### TAPE DIMENSIONS



A0	Dimension designed to accommodate the component width
B0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

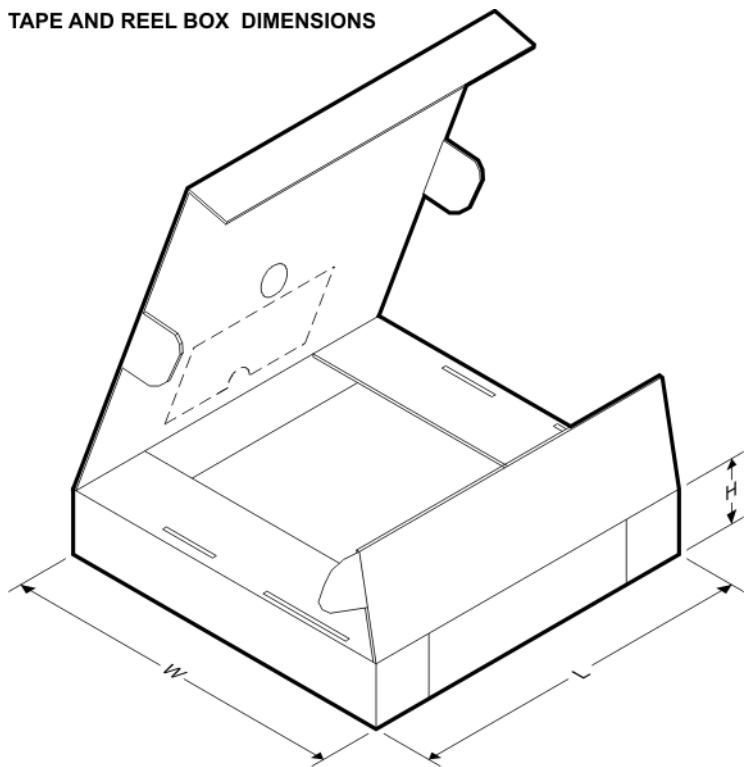
### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS259620DDAR	SO Power PAD	DDA	8	2500	330.0	12.8	6.4	5.2	2.1	8.0	12.0	Q1
TPS259620DDAT	SO Power PAD	DDA	8	250	330.0	12.8	6.4	5.2	2.1	8.0	12.0	Q1
TPS259621DDAR	SO Power PAD	DDA	8	2500	330.0	12.8	6.4	5.2	2.1	8.0	12.0	Q1
TPS259621DDAT	SO Power PAD	DDA	8	250	330.0	12.8	6.4	5.2	2.1	8.0	12.0	Q1
TPS259630DDAR	SO Power PAD	DDA	8	2500	330.0	12.8	6.4	5.2	2.1	8.0	12.0	Q1
TPS259630DDAT	SO Power PAD	DDA	8	250	330.0	12.8	6.4	5.2	2.1	8.0	12.0	Q1
TPS259631DDAR	SO Power PAD	DDA	8	2500	330.0	12.8	6.4	5.2	2.1	8.0	12.0	Q1
TPS259631DDAT	SO	DDA	8	250	330.0	12.8	6.4	5.2	2.1	8.0	12.0	Q1

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
	Power PAD											

**TAPE AND REEL BOX DIMENSIONS**


\*All dimensions are nominal

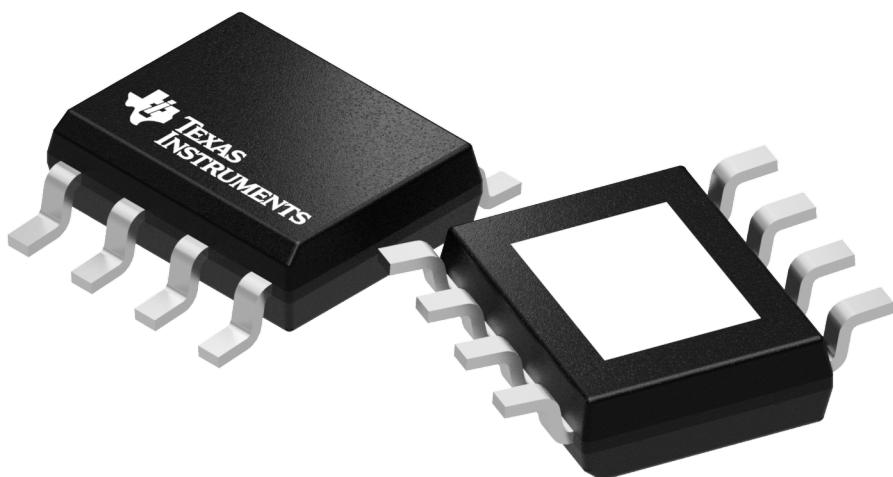
Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS259620DDAR	SO PowerPAD	DDA	8	2500	366.0	364.0	50.0
TPS259620DDAT	SO PowerPAD	DDA	8	250	366.0	364.0	50.0
TPS259621DDAR	SO PowerPAD	DDA	8	2500	366.0	364.0	50.0
TPS259621DDAT	SO PowerPAD	DDA	8	250	366.0	364.0	50.0
TPS259630DDAR	SO PowerPAD	DDA	8	2500	366.0	364.0	50.0
TPS259630DDAT	SO PowerPAD	DDA	8	250	366.0	364.0	50.0
TPS259631DDAR	SO PowerPAD	DDA	8	2500	366.0	364.0	50.0
TPS259631DDAT	SO PowerPAD	DDA	8	250	366.0	364.0	50.0

## GENERIC PACKAGE VIEW

DDA 8

PowerPAD™ SOIC - 1.7 mm max height

PLASTIC SMALL OUTLINE



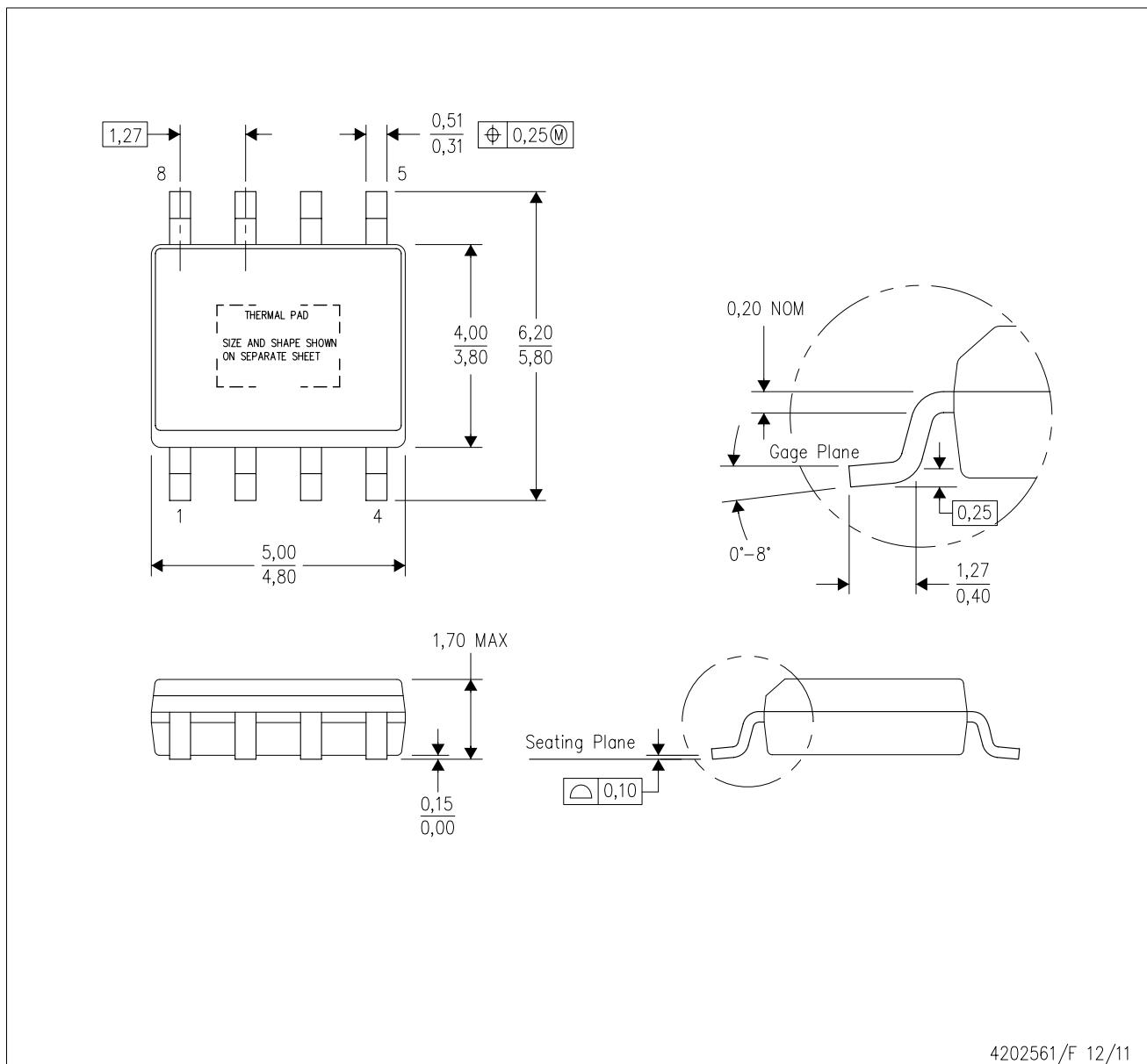
Images above are just a representation of the package family, actual package may vary.  
Refer to the product data sheet for package details.

4202561/G

## MECHANICAL DATA

DDA (R-PDSO-G8)

PowerPAD™ PLASTIC SMALL-OUTLINE



4202561/F 12/11

- NOTES:
- A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5-1994.
  - B. This drawing is subject to change without notice.
  - C. Body dimensions do not include mold flash or protrusion not to exceed 0,15.
  - D. This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 for information regarding recommended board layout. This document is available at [www.ti.com](http://www.ti.com) <<http://www.ti.com>>.
  - E. See the additional figure in the Product Data Sheet for details regarding the exposed thermal pad features and dimensions.
  - F. This package complies to JEDEC MS-012 variation BA

PowerPAD is a trademark of Texas Instruments.

# THERMAL PAD MECHANICAL DATA

DDA (R-PDSO-G8)

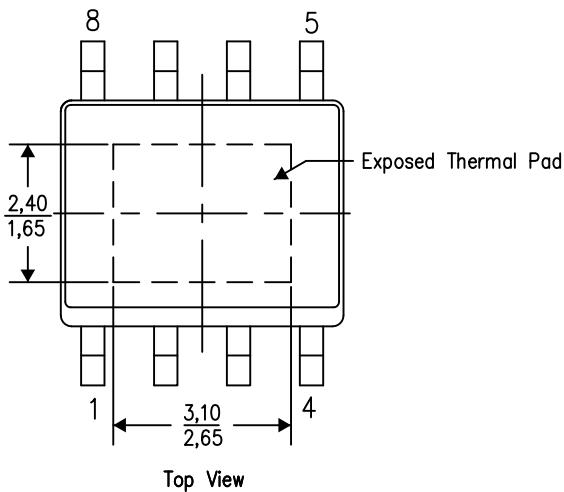
PowerPAD™ PLASTIC SMALL OUTLINE

## THERMAL INFORMATION

This PowerPAD™ package incorporates an exposed thermal pad that is designed to be attached to a printed circuit board (PCB). The thermal pad must be soldered directly to the PCB. After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For additional information on the PowerPAD package and how to take advantage of its heat dissipating abilities, refer to Technical Brief, PowerPAD Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 and Application Brief, PowerPAD Made Easy, Texas Instruments Literature No. SLMA004. Both documents are available at [www.ti.com](http://www.ti.com).

The exposed thermal pad dimensions for this package are shown in the following illustration.



Exposed Thermal Pad Dimensions

4206322-6/L 05/12

NOTE: A. All linear dimensions are in millimeters

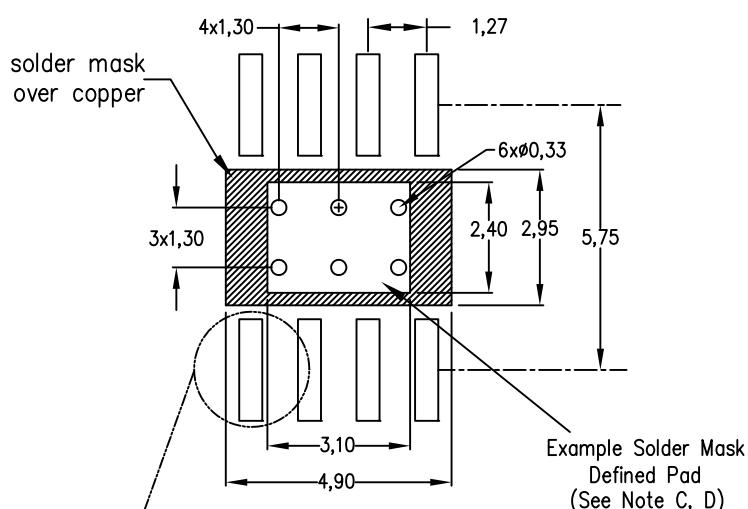
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# LAND PATTERN DATA

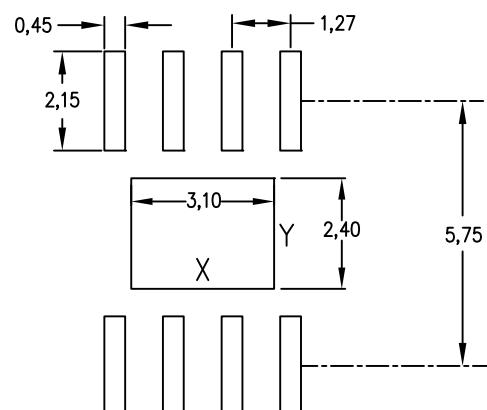
DDA (R-PDSO-G8)

PowerPAD™ PLASTIC SMALL OUTLINE

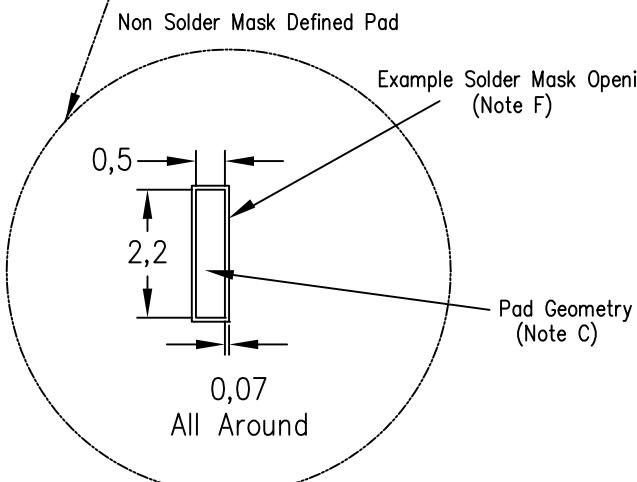
Example Board Layout  
Via pattern and copper pad size  
may vary depending on layout constraints



0,127mm Thick Stencil Design Example  
Reference table below for other  
solder stencil thicknesses  
(Note E)



Example Solder Mask  
Defined Pad  
(See Note C, D)



Example Solder Mask Opening  
(Note F)

Center Power Pad Solder Stencil Opening		
Stencil Thickness	X	Y
0.1mm	3.3	2.6
0.127mm	3.1	2.4
0.152mm	2.9	2.2
0.178mm	2.8	2.1

4208951-6/D 04/12

- NOTES:
- A. All linear dimensions are in millimeters.
  - B. This drawing is subject to change without notice.
  - C. Publication IPC-7351 is recommended for alternate designs.
  - D. This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002, SLMA004, and also the Product Data Sheets for specific thermal information, via requirements, and recommended board layout. These documents are available at [www.ti.com](http://www.ti.com) <<http://www.ti.com>>. Publication IPC-7351 is recommended for alternate designs.
  - E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.
  - F. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.

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