

A Gazebo Simulator for Continuum Parallel Robots

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22/02/2021

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- ➋ Modelling of Continuum
- ➌ Methods
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Serial and parallel robots

- Serial robots
 - Simpler and more used
 - Limited by weight and inertia
- Parallel robots
 - Less inertia, high velocities
 - More joints involved

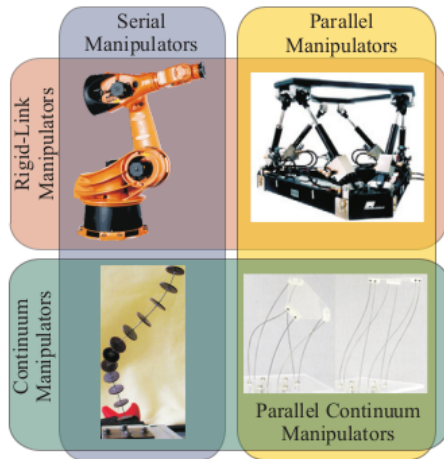


Figure: Different robot architectures [2].

Continuum parallel robots

- Continuum parallel robots
 - May enhance safety
 - Cheaper components
 - Possible to miniaturize
- Model and stability problems
 - More unstable configurations
 - Lower payload
 - Not analytical solution
- Definition of a general simulator
 - Gazebo plugins

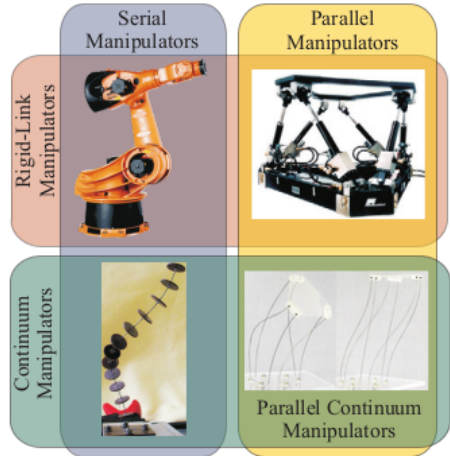


Figure: Different robot architectures [2].

Geometric modelling: Cosserat rod theory

- Rod as 1D body
- Function of the arc-length s
 - Centerline position $p_{(s)} \in \mathbb{R}^3$
 - Cross-section orientation $R_{(s)} \in se(3)$
- Define transformation

$$T_{(s)} = \begin{bmatrix} R_{(s)} & p_{(s)} \\ 0 & 1 \end{bmatrix} \in SE(3) \quad (1)$$

- Derivative wrt arc-length

$$x' = \frac{dx}{ds}$$

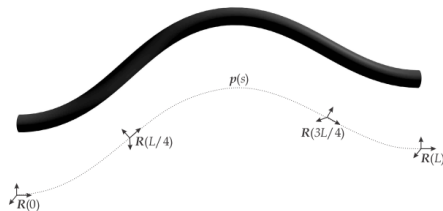


Figure: Rod geometric modelling [4].

Equilibrium Equations

- Equilibrium consideration
 - Distributed forces/moments
 - Internal forces/moments

$$n'_{(s)} = -f_{(s)} \quad (2)$$

$$m'_{(s)} = -p'_{(s)} n_{(s)} - l_{(s)} \quad (3)$$

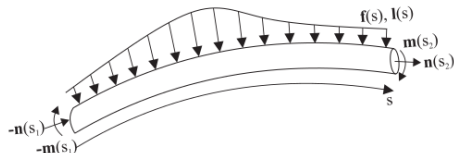


Figure: Sections of the beam considered for the static equilibrium [1].

Boundary Value Problem

- Constraints at the distal plate

- External wrench $\Psi_{ext} = \begin{bmatrix} F \\ M \end{bmatrix}$

- Rod contribution

$$\Psi_i = \begin{bmatrix} n_{i(L_i)} \\ m_{i(L_i)} \end{bmatrix}$$

- Constraints at the base

- Actuations Ψ_{a_i}
- Joints and geometry

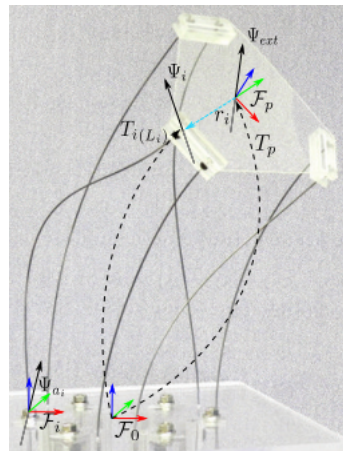


Figure: Geometrical and actuation constraints for a Stewart-Gough CPR.

Shooting Method in statics (Stewart-Gough CPR)

- ODE system in statics
 - Equilibrium equations
 - Material properties
 - Geometrical considerations
- Recursive solution
 - Needs an initial guess
 - Evaluation on a cost function

$$\mathbf{f} = \begin{bmatrix} \sum n_{i(L_i)} - F \\ \sum \left[p_{i(L_i)} n_{i(L_i)} + m_{i(L_i)} \right] - p_d F - M \\ p_d + R_d r_i - p_{i(L_i)} \\ \left[R_{i(L_i)}^T R_d - R_{i(L_i)} R_d^T \right]^v \end{bmatrix} \quad (4)$$

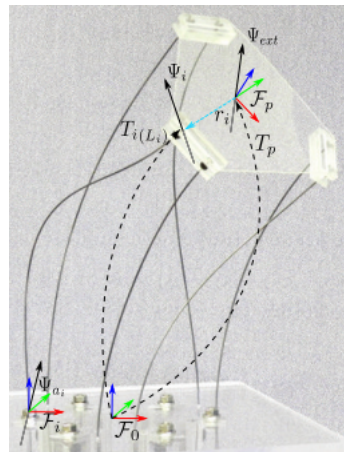


Figure: Geometrical and actuation constraints for a Stewart-Gough CPR.

Shooting Method in dynamics

- PDE system

- Derivative wrt to arc-length $x' = \frac{\partial x}{\partial s}$
- Derivative wrt to time $\dot{x} = \frac{\partial x}{\partial t}$

- From PDE to ODE

- Implicit discretization

$$\frac{\partial x}{\partial t} = c_0 x^{(i)} + \sum_{k=1}^{\infty} \left[c_k x^{(i-k)} + d_k \dot{x}^{(i-k)} \right] \quad (5)$$

$$\frac{\partial x}{\partial t} = c_0 x^{(i)} + c_1^{(i-1)} x^{(i-1)} + c_2^{(i-2)} x^{(i-2)} + d_1^{(i-1)} \frac{\partial x^{(i-1)}}{\partial t} \quad (6)$$

Non linear solver: Levenberg-Marquardt algorithm

- Iterative algorithm
 - From initial conditions
 - Very sensitive
- Evaluates influence of parameter vector u

$$J = \frac{df}{du} \quad (7)$$

- Updates the parameter vector

$$u_{k+1} = u_k + \left(J_k^T J_k + \mu I \right)^{-1} J_k^T f_k \quad (8)$$

Strain approach

- Modelling of a continuum body in space
 - Internally actuated Cosserat beam
 - With its configuration space $C = SE(3) \times S$
- From assumption on rod deformation
 - Allowed ξ_a , prohibited ξ_c twists
 - Strain generalized coordinates $q_{[n \times 1]}$
 - Basis functions $\Phi_{[n_a \times n]}$

$$\xi_{a(s,t)} = \xi_{a0(s)} + \Phi_{(s)} q_{(t)} \quad (9)$$

- Configuration space discretization $C = SE(3) \times \mathbb{R}^n$

Strain approach, Lagrangian model of continuum manipulator

- Strain Approach

$$\begin{bmatrix} 0 \\ Q_{ad} \end{bmatrix} = \begin{bmatrix} M_0 & M_{0\epsilon} \\ M_{\epsilon 0} & M_{\epsilon\epsilon} \end{bmatrix} \begin{bmatrix} \dot{\eta}_0 \\ \ddot{q}(t) \end{bmatrix} + \begin{bmatrix} F_v(q, \dot{q}, \eta_0) \\ Q_v(q, \dot{q}, \eta_0) \end{bmatrix} + \begin{bmatrix} F_c(q, g_0) \\ Q_c(q, g_0) \end{bmatrix} + \begin{bmatrix} 0 \\ K_{\epsilon\epsilon} q(t) + D_{\epsilon\epsilon} \dot{q}(t) \end{bmatrix} \quad (10)$$

- Virtual serial mechanism analogy

- Lagrangian model

$$\begin{bmatrix} F_0 \\ Q_a \end{bmatrix} = \begin{bmatrix} M_0 & M_{0\epsilon} \\ M_{\epsilon 0} & M_{\epsilon\epsilon} \end{bmatrix} \begin{bmatrix} \dot{\eta}_0 \\ \ddot{q}(t) \end{bmatrix} + \begin{bmatrix} F_v(q, \dot{q}, \eta_0) \\ Q_v(q, \dot{q}, \eta_0) \end{bmatrix} + \begin{bmatrix} F_c(q, g_0) \\ Q_c(q, g_0) \end{bmatrix} \quad (11)$$

- Recursive reconstruction

Introduction to the Isogeometric Collocation Method

- NURBS curves represent vector field
 - Control point as degree of freedom
 - Basis functions relate influence
- Cost function
 - Equilibrium equation evaluated at collocation points

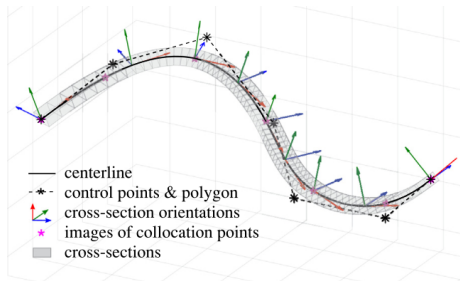


Figure: Rod centerline position and orientation represented with NURBS curves [3].

Properties of the Isogeometric Collocation Method

- Less integrations
 - In statics no integration
 - ODE in dynamics
- Introduces possibility of modelling
 - Contact between rods
 - Changes in shape and or material
 - Rods coupling

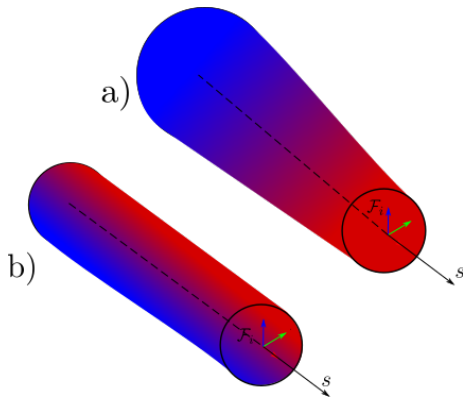


Figure: Rod with properties changing a) axially and b) transversally

Conclusions

- Types of robots
 - Serial robots
 - Parallel robots
 - Continuum parallel robots
- Model of continuum
 - Geometric
 - Equilibrium
- Methods
 - Shooting Method
 - Strain Approach
 - Isogeometric Collocation Method

Expected work

- Method selection
 - Previously presented
 - Combination
- Solve the modelling
 - Rod statics
 - Robot assembly
 - Visual interface
 - Robot dynamics

Thank you for your attention



Black, C. B., J. Till, and D. C. Rucker (Feb. 2018). “Parallel Continuum Robots: Modeling, Analysis, and Actuation-Based Force Sensing”. In: *IEEE Transactions on Robotics* 34.1. Conference Name: IEEE Transactions on Robotics, pp. 29–47.



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