

EXAMPLE 8.1**Calculation of Range, Line of sight, Range-rate, and Elevation****INPUTS:**

| | | | |
|--|-----------------------------------|---|--------------|
| Satellite position (Cartesian ECEF) | $\mathbf{r}_{es}^e(t_{st,a}^s) =$ | 26580000 m 0 m 0 m | |
| Satellite velocity (ECEF) | $\mathbf{v}_{es}^e(t_{st,a}^s) =$ | 0 m s ⁻¹ 1755 m s ⁻¹ 3170 m s ⁻¹ | |
| User latitude | $L_a =$ | 45 deg | 0.785398 rad |
| User longitude | $\lambda_a =$ | 10 deg | 0.174533 rad |
| User height | $h_a =$ | 1000 m | |
| Equatorial radius | $R_0 =$ | 6378137 m | |
| Ellipsoid eccentricity | $e =$ | 0.08181919 | |
| Earth rate | $\omega_{ie} =$ | 7.29E-05 rad s ⁻¹ | |
| Speed of light | $c =$ | 299792458 m s ⁻¹ | |

Convert user position to Cartesian ECEF

Transverse Radius of Curvature

From (2.106),
$$R_E(L_a) = \frac{R_0}{\sqrt{1 - e^2 \sin^2 L_a}}$$

$R_E =$ 6388838.29 m

Cartesian Position (ECEF-frame resolved and referenced)

From (2.112), $x_{ea}^e = (R_E(L_a) + h_a) \cos L_a \cos \lambda_a$

$y_{ea}^e = (R_E(L_a) + h_a) \cos L_a \sin \lambda_a$

$z_{ea}^e = [(1 - e^2)R_E(L_a) + h_a] \sin L_a$

$\mathbf{r}_{ea}^e(t_{sa,a}^s) =$ 4448958.522 m
784471.4236 m
4487348.409 m

Range

From (8.31), $r_{as} = |\mathbf{r}_{es}^e(t_{st,a}^s) - \mathbf{r}_{ea}^e(t_{sa,a}^s)| + \delta\rho_{ie,a}^s$

$\mathbf{r}_{es}^e(t_{st,a}^s) - \mathbf{r}_{ea}^e(t_{sa,a}^s) =$ 22131041 m
-784471.4 m
-4487348 m

Sagnac correction:

From (8.32),
$$\delta\rho_{ie,a}^s \approx \frac{\omega_{ie}}{c} [y_{es}^e(t_{st,a}^s)x_{ea}^e(t_{sa,a}^s) - x_{es}^e(t_{st,a}^s)y_{ea}^e(t_{sa,a}^s)]$$

$\delta\rho_{ie,a}^s \approx$ -5.0718326 m

$r_{as} =$ 22595009.6 m

Line-of-sight unit vector

From (8.41),
$$\mathbf{u}_{as}^e \approx \frac{\mathbf{r}_{es}^e(t_{st,a}^s) - \mathbf{r}_{ea}^e(t_{sa,a}^s)}{|\mathbf{r}_{es}^e(t_{st,a}^s) - \mathbf{r}_{ea}^e(t_{sa,a}^s)|}$$

$$\mathbf{u}_{as}^e \approx \begin{bmatrix} 0.979465683 \\ -0.03471878 \\ -0.19859905 \end{bmatrix}$$

Range rate

From (8.45),
$$\dot{r}_{as} = \mathbf{u}_{as}^{eT} (\mathbf{v}_{es}^e(t_{st,a}^s) - \mathbf{v}_{ea}^e(t_{sa,a}^s)) + \delta\dot{\rho}_{ie,a}^s$$

In this example, $\mathbf{v}_{ea}^e(t_{sa,a}^s) = \mathbf{0}$

Sagnac correction:

From (8.46),
$$\delta\dot{\rho}_{ie,a}^s \approx \frac{\omega_{ie}}{c} \left(v_{es,y}^e(t_{st,a}^s) x_{ea}^e(t_{sa,a}^s) + y_{es}^e(t_{st,a}^s) v_{ea,x}^e(t_{sa,a}^s) - v_{es,x}^e(t_{st,a}^s) y_{ea}^e(t_{sa,a}^s) - x_{es}^e(t_{st,a}^s) v_{ea,y}^e(t_{sa,a}^s) \right)$$

$$\delta\dot{\rho}_{ie,a}^s \approx \begin{bmatrix} 0.001899189 \end{bmatrix} \text{ m s}^{-1}$$

$$\dot{r}_{as} = \begin{bmatrix} -690.488549 \end{bmatrix} \text{ m s}^{-1}$$

Transformation of line of sight to north, east, down

ECEF to NED coordinate transformation matrix

From (2.150),
$$\mathbf{C}_e^n = \begin{pmatrix} -\sin L_b \cos \lambda_b & -\sin L_b \sin \lambda_b & \cos L_b \\ -\sin \lambda_b & \cos \lambda_b & 0 \\ -\cos L_b \cos \lambda_b & -\cos L_b \sin \lambda_b & -\sin L_b \end{pmatrix}$$

$$\mathbf{C}_e^n = \begin{bmatrix} -0.69636424 & -0.122788 & 0.70710678 \\ -0.17364818 & 0.9848078 & 0 \\ -0.69636424 & -0.122788 & -0.70710678 \end{bmatrix}$$

From (8.39),
$$\mathbf{u}_{as}^n = \mathbf{C}_e^n \mathbf{u}_{as}^e$$

$$\mathbf{u}_{as}^n = \begin{bmatrix} -0.81823257 \\ -0.20427376 \\ -0.5373711 \end{bmatrix}$$

Elevation and azimuth

From (8.57),
$$\theta_{nu}^{as} = -\arcsin(u_{as,D}^n), \quad \psi_{nu}^{as} = \arctan_2(u_{as,E}^n, u_{as,N}^n)$$

$$\theta_{nu}^{as} = \begin{bmatrix} 0.567316775 \end{bmatrix} \text{ rad} \quad \begin{bmatrix} 32.5048569 \end{bmatrix} \text{ deg}$$

$$\psi_{nu}^{as} = \begin{bmatrix} -2.89694113 \end{bmatrix} \text{ rad} \quad \begin{bmatrix} -165.9825 \end{bmatrix} \text{ deg}$$

Note: The arguments of the Excel ATAN2 function are the opposite way round