

# **280.371 Process Engineering Operations**

## **Drying Problems Tutorial 2**

### **Example 2**

Lecture 4

### **Example 2: Evaporation from a wet surface (convection and radiation heat transfer)**

A 10cm by 20cm steak is placed under a grilling element to cook. The wet bulb and dry bulb temperatures of the air above the steak are 43°C and 100°C, respectively, and the element temperature is 500°C. The radiation view factor may be taken to be 1 and conduction from under the steak may be ignored. Saturation humidities at 60°C, 70°C, 80°C and 90° are 0.15, 0.28, 0.55 and 1.4 kg/kg, respectively.

- (a) Calculate the initial rate of evaporation from the surface of the steak assuming the surface is wet and the heat transfer coefficient to the steak is 8 W/m<sup>2</sup> K. . What will the surface temperature of the steak be?
- (b) How long will it take to reduce the moisture content of the steak from 2.0 to 1.5, assuming that the steak is 5mm thick with a dry density of 600 kg/m<sup>3</sup> ?

C<sub>p</sub> moist air 1071 J /kg K

$$h_{rad} = F_{12} \cdot 5.67 \times 10^{-8} (T_{rad} + T_S) (T_{rad}^2 + T_S^2) \quad \text{W/m}^2 \text{ K}$$

Temperatures in Kelvins.

## Generic Solution Procedure

- 1 Calculate the mass transfer coefficient from the Lewis analogy
- 2 Assume a surface temperature
- 3 Determine the surface saturation humidity from the psychrometric chart
- 4 Calculate the rate of evaporation using the mass transfer equation
- 5 Calculate the rate of evaporation using the heat transfer equation
- 6 If the rates from steps 4 and 5 are the same, you guessed correctly. Otherwise go back to step 2

# Heat & mass transfer equations

- The rate of mass transfer = drying rate

$$m_v = k'_H A (H_{\text{surface}} - H_{\text{air}})$$

$$R = k'_H (H_{\text{surface}} - H_{\text{air}})$$

- The rate of heat transfer to provide drying rate,  $m_v$

$$\phi = m_v h_{fg}$$

$$R = \frac{\phi}{h_{fg} A}$$

- $h_{fg}$  is the latent heat of evaporation evaluated at the surface temperature
- $\phi = q$   
= rate of heat transfer (W)

$$R = \frac{\text{kg water}}{\text{m}^2 \text{s}}$$

Slide 10 in Course Notes

# Heat & Mass transfer analogy

- The mass transfer coefficient analogy with the heat transfer coefficient is:

$$k_H' \approx \frac{h}{c_{pH}} \text{ Lewis relationship}$$

$$c_{pH} = c_{p,air} + H_{air} c_{p,steam}$$

$c_{p,air}$  – specific heat of dry air at  $\theta_{air}$

$c_{p,steam}$  – specific heat at  $\theta_{WB}$

Slide11 in Course Notes

# Convection & radiation

- *Convection and radiation from above*

$$\phi = h_c A (\theta_{air} - \theta_{surface}) + h_{rad} A (\theta_{radr} - \theta_{surface})$$

Slide 17 in Course Notes

$$h_{rad} = F_{12} \cdot 5.67 \times 10^{-8} (T_{rad}^4 + T_S^4) (T_{rad}^2 + T_S^2) \quad \text{W/m}^2 \text{ K}$$

Temperatures in Kelvins.

$h_{rad}$  “pseudo heat transfer coefficient” for radiation

$F_{12}$  View factor [-] (assume a value of 1)

$5.67 \times 10^{-8} \text{ W m}^{-2} \text{ K}^{-4}$  this is the value of the Stefan-Boltzmann constant,  $\sigma$ .

$T_{rad}$  Temperature of radiating heat source, K.

$T_{surface}$  Temperature of surface, K.

$\theta_{rad}$  Temperature of radiating heat source, °C.

$\theta_{surface}$  Temperature of surface, °C.

Example 2.

①

Air temperature  $100^\circ\text{C}$  (dry bulb); wet bulb temp  $43^\circ\text{C}$ .

Element temperature  $500^\circ\text{C}$ .

Radiation view factor 1 ( $F_{12}$ )

Conduction under steak can be ignored.

Saturation Humidities GIVEN

$60^\circ\text{C}$	$70^\circ\text{C}$	$80^\circ\text{C}$	$90^\circ\text{C}$	$\text{kg/kg}$
0.15	0.28	0.55	1.4	

$h = 8 \text{ W/m}^2\text{K}$  find  $k'_H$  using Lexis relationship

SLIDE 11 \*

$$k'_H = \frac{8}{1071} = 7.47 \times 10^{-3} \text{ kg/m}^2\text{s}$$

- Guess steak surface temperature

$$60^\circ\text{C}$$
  
 $H_s = 0.15$  (given)

- Mass transfer

SLIDE 10 \*

$$h_{air} \text{ from chart} = 0.033 \text{ kg/kg}$$

$$R_c = 7.47 \times 10^{-3} (0.15 - 0.033) = 8.7 \times 10^{-4} \text{ kg/m}^2\text{s}$$

- Heat transfer

$$R_h = \frac{[h(\theta_{air} - \theta_s) + h_{rad}(\theta_{element} - \theta_s)] / h_{fg}}{2358000} \quad \text{SLIDE 17 *} \\ = \frac{8(100 - 60) + 5.67 \times 10^8 (773 + 333)(773^2 + 333^2)(500 - 60)}{2358000}$$

$$= 8.43 \times 10^{-3} \text{ kg/m}^2\text{s} \quad \uparrow h_{fg} \text{ at } 60^\circ\text{C}$$

10 times as much as mass transfer  
eq. predicts.

Iteration step 1

(.0325)

Example 2 cont'd.

(2)

Re do calculation with another surface temp.

## Iteration step 2

Assume  $88^\circ\text{C} = 361\text{ K}$

- Mass transfer

$$R = 7.47 \times 10^{-3} (1.11 - 0.033) = \underline{\underline{8.045 \times 10^{-3} \text{ kg/m}^2\text{s}}}$$

- Heat transfer

$$R = \frac{8(100 - 88) + 5.67 \times 10^{-8} (773 + 361)(773^2 + 361^2)}{2,288,000} \times (500 - 88) \\ = 8.47 \times 10^{-3} \text{ kg/m}^2\text{s}$$

Close to mass transfer answer  
so use this as the answer

(b) Time to reduce moisture

$$t = \frac{s E_s}{R} (x_1 - x_2)$$

$$= \frac{5 \times 10^{-3} \times 600}{8.47 \times 10^{-3}} (2 - 1.5)$$

$$= 177 \text{ s} \quad (\sim 3 \text{ minutes}).$$