

280.371 Process Engineering Operations

Drying Problems Tutorial 2

Example 2

Lecture 4

Example 2: Evaporation from a wet surface (convection and radiation heat transfer)

A 10cm by 20cm steak is placed under a grilling element to cook. The wet bulb and dry bulb temperatures of the air above the steak are 43°C and 100°C, respectively, and the element temperature is 500°C. The radiation view factor may be taken to be 1 and conduction from under the steak may be ignored. Saturation humidities at 60°C, 70°C, 80°C and 90° are 0.15, 0.28, 0.55 and 1.4 kg/kg, respectively.

- (a) Calculate the initial rate of evaporation from the surface of the steak assuming the surface is wet and the heat transfer coefficient to the steak is 8 W/m² K. . What will the surface temperature of the steak be?
- (b) How long will it take to reduce the moisture content of the steak from 2.0 to 1.5, assuming that the steak is 5mm thick with a dry density of 600 kg/m³ ?

C_p moist air 1071 J/kg K

$$h_{\text{rad}} = F_{12} 5.67 \times 10^{-8} (T_{\text{rad}} + T_s)(T_{\text{rad}}^2 + T_s^2) \quad \text{W/m}^2 \text{ K}$$

Temperatures in Kelvins.

Generic Solution Procedure

- 1 Calculate the mass transfer coefficient from the Lewis analogy
- 2 Assume a surface temperature
- 3 Determine the surface saturation humidity from the psychrometric chart
- 4 Calculate the rate of evaporation using the mass transfer equation
- 5 Calculate the rate of evaporation using the heat transfer equation
- 6 If the rates from steps 4 and 5 are the same, you guessed correctly. Otherwise go back to step 2

Heat & mass transfer equations

- The rate of mass transfer = drying rate

$$m_v = k_H' A (H_{\text{surface}} - H_{\text{air}})$$

$$R = k_H' (H_{\text{surface}} - H_{\text{air}})$$

- The rate of heat transfer to provide drying rate, m_v

$$\phi = m_v h_{fg}$$

$$R = \frac{\phi}{h_{fg} A}$$

- h_{fg} is the latent heat of evaporation evaluated at the surface temperature

- $\phi = q$
= rate of heat transfer (W)

$$R = \frac{\text{kg water}}{\text{m}^2 \text{s}}$$

Slide 10 in Course Notes

Heat & Mass transfer analogy

- The mass transfer coefficient analogy with the heat transfer coefficient is:

$$k'_H \approx \frac{h}{c_{pH}} \quad \text{Lewis relationship}$$

$$c_{pH} = c_{p,air} + H_{air} c_{p,steam}$$

$c_{p,air}$ – specific heat of dry air at θ_{air}

$c_{p,steam}$ – specific heat at θ_{WB}

Slide11 in Course Notes

Convection & radiation

- *Convection and radiation from above*

$$\phi = h_c A (\theta_{air} - \theta_{surface}) + h_{rad} A (\theta_{radr} - \theta_{surface})$$

Slide 17 in Course Notes

$$h_{rad} = F_{12} \cdot 5.67 \times 10^{-8} (T_{rad} + T_s)(T_{rad}^2 + T_s^2) \quad \text{W/m}^2 \text{K}$$

Temperatures in Kelvins.

h_{rad} "pseudo heat transfer coefficient" for radiation

F_{12} View factor [-] (assume a value of 1)

$5.67 \times 10^{-8} \text{ W m}^{-2} \text{ K}^{-4}$ this is the value of the Stefan-Boltzmann constant, σ .

T_{rad} Temperature of radiating heat source, K.

$T_{surface}$ Temperature of surface, K.

θ_{rad} Temperature of radiating heat source, °C.

$\theta_{surface}$ Temperature of surface, °C.

$$\theta = 100^\circ\text{C}$$

$$\theta_{wb} = 43^\circ\text{C}$$

$$\Rightarrow H_{air} = 0.0325 \text{ kg/kg}$$

$$\begin{aligned}\Rightarrow c_p &= c_{pair} + H_{air} c_{psteam} \\ &= 1006 + 0.0325 \times 2000 \\ &= 1071\end{aligned}$$

Example 2.

Air temperature 100°C (dry bulb); wet bulb temp 43°C .

Element temperature 500°C .

Radiation view factor 1 (F_{12})

Conduction under steak can be ignored.

Saturation Humidities GIVEN

60°C	70°C	80°C	90°C	
0.15	0.28	0.55	1.4	kg/kg

$h = 8 \text{ W/m}^2\text{K}$ find K'_H using Lewis relationship SLIDE 11 *

$$K'_H = \frac{8}{1071} = 7.47 \times 10^{-3} \text{ kg/m}^2\text{s}$$

• Guess steak surface temperature 60°C
 $H_s = 0.15$ (given)

• Mass transfer SLIDE 10 *

$$H_{air} \text{ from chart} = 0.033 \text{ kg/kg} \quad \leftarrow (.0325)$$

$$R_c = 7.47 \times 10^{-3} (0.15 - 0.033) = 8.7 \times 10^{-4} \text{ kg/m}^2\text{s}$$

• Heat transfer

$$R = [h(\theta_{air} - \theta_s) + h_{rad}(\theta_{element} - \theta_s)] / h_{fg} \quad \text{SLIDE 17} *$$

$$= \frac{8(100 - 60) + 5.67 \times 10^{-8} (773 + 333)(773^2 + 333^2)(500 - 60)}{2358000}$$

$$= 8.43 \times 10^{-3} \text{ kg/m}^2\text{s} \quad \leftarrow h_{fg} \text{ at } 60^\circ\text{C}$$

10 times as much as mass transfer eq. predicts.

Iteration step 1



Iteration step 2

Example 2 contd.

(2)

Re do calculation with another surface temp.

Assume $88^\circ\text{C} = 361\text{ K}$

- Mass transfer

$$R = 7.47 \times 10^{-3} (1.11 - 0.033) = \underline{\underline{8.045 \times 10^{-3} \text{ kg/m}^2\text{s}}}$$

- Heat transfer

$$R = \frac{8(100 - 88) + 5.67 \times 10^{-8} (773 + 361)(773^2 + 361^2)}{2288,000}$$

$$= 8.47 \times 10^{-3} \text{ kg/m}^2\text{s}$$

Close to mass transfer answer
So use this as the answer

(b) Time to reduce moisture

$$t = \frac{S \rho_s (X_1 - X_2)}{R}$$

$$= \frac{5 \times 10^{-3} \times 600 (2 - 1.5)}{8.47 \times 10^{-3}}$$

$$= 177 \text{ s} \quad (\sim 3 \text{ minutes})$$