

APPLIED MECHANICS DEPARTMENT
AML835: MECHANICS OF COMPOSITE MATERIALS

SEMESTER – II, 2007-2008

MAJOR

TIME: 2 hrs

MAX. MARKS: 100

Note: Answer all questions.

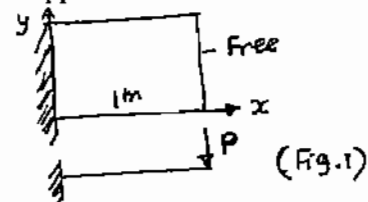
1. a) Name two types of laminates, with a specific example in each case, for which $B_{ij}=0$, $A_{16}=A_{26}=D_{16}=D_{26}=0$.
 b) Show that for cross-ply anti-symmetric laminate, $B_{22}=-B_{11}$ and other elements in B_{ij} matrix are zero.
 c) Using the stress-strain relation of a lamina and definition of stress resultants N and M , obtain the plate constitutive relations relating N , M with strain terms $\epsilon^0, \bar{\chi}$ according to classical laminate theory, in presence thermal loading. (3, 5, 5)

2. A two-layer cross-ply $[0/90]$ laminate is cooled down during curing from a temperature of T_2 to T_1 .
 a) Show that for the given laminate $A_{11}=A_{22}$ and $D_{11}=D_{22}$.
 b) Show that for this case, thermal stress resultants $N_{xT} = N_{yT}$ and $M_{xT} = -M_{yT}$.
 c) Show that if no external mechanical load is applied during the curing process, the curvatures

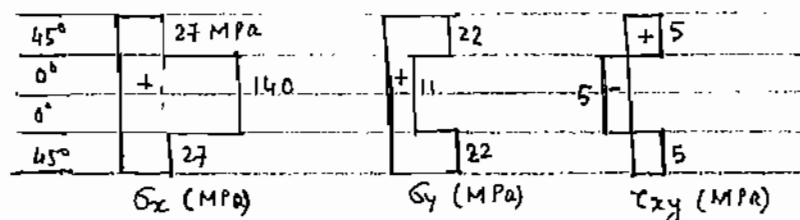
$$\chi_1, \chi_2 \text{ of the plate after cooling are given by } \chi_1 = -\chi_2 = \frac{(A_{11} + A_{12})M_{xT} - B_{11}N_{xT}}{(A_{11} + A_{12})(D_{11} - D_{12}) - B_{11}^2}. \quad (3, 3, 6)$$

3. A rectangular four-ply cross-ply $[0/90]_s$ composite plate with each ply of 1 mm thickness is clamped at one edge at $x=0$ and free at other three edges. It is subjected to a line load at the edge at $x=1$ m (Fig. 1) such that a bending moment of $M_x = 20$ kN-mm/mm is induced at the support end.

For the laminae, $Q = \begin{bmatrix} 140 & 3 & 0 \\ 3 & 10 & 0 \\ 0 & 0 & 5 \end{bmatrix}$ GPa.



- a) Find the inplane strains and curvature of the plate at $x=0$.
 b) Show the distribution of σ_x across the thickness of the laminate with all key values.
 c) Obtain the transverse shear stress τ_{xz} at $x=0$ at the mid-surface using the post-processing approach based on three-dimensional stress equilibrium equations. (8, 5, 5)
4. A four-ply laminate $[45/0]_s$ with each ply of 3 mm thickness is subjected to inplane loads $N_x = 1000$ N and $N_y/N_x = 0.2$ which induce the following stresses in the layers.



- a) Find the layer stresses in the principal material directions.
 b) Compute the axial load N_x (with $N_y = 0.2 N_x$) corresponding to the first-ply failure (FPF). Use Tsai-Hill criteria for failure with the following strengths: $F_{1t}=500$ MPa, $F_{1c}=350$ MPa, $F_{2t}=75$ MPa, $F_{2c}=35$ MPa. (5, 5)

5. The governing equation of motion in z direction for a rectangular composite plate is given by

$$M_{x,xx} + 2M_{xy,xy} + M_{y,yy} + p = I_0 \ddot{w}_0 + I_1 (\ddot{u}_{0,x} + \ddot{v}_{0,y}) - I_2 (\ddot{w}_{0,xx} + \ddot{w}_{0,yy})$$

- a) Obtain the differential equation for deflection w_0 for the case of symmetric cross-ply laminate.
 b) Solve the above equation for static deflection of a simply-supported rectangular plate under a sinusoidal pressure load $p = p_0 \sin(\pi x/a) \sin(\pi y/b)$.
 c) Also obtain the expression for undamped bending natural frequencies of the plate. (6, 3, 4)

6. A rectangular four-ply laminated plate $[0/90]_s$ with each ply of 1mm thickness is subjected to a temperature rise of 100°C and 50°C at top and bottom surfaces, respectively. The plate is supported on all sides such that all displacements and rotations are restrained.

- b) Find the stress-temperature coefficients β_i of the laminas, which have the following properties:

$$E_1 = 150 \text{ GPa}, E_2 = 10 \text{ GPa}, G_{12} = 6 \text{ GPa}, \nu_{12} = 0.3, \alpha_1 \cong 0, \alpha_2 = 30 \times 10^{-6} / \text{deg C}.$$

- c) Find the axial force N_x and bending moment M_x developed in the laminate due to the temperature rise. Assume a linear variation of temperature across the thickness. (6, 7)

7. a) The transverse tensile strength F_{2t} is less than the strength of the tensile strength σ_{mu} of matrix. True/False. Explain.

- b) Define the coefficients of mutual influence of first and second kind and show that $\frac{\eta_{12,1}}{E_1} = \frac{\eta_{1,12}}{G_{12}}$.

- c) State the numbers of independent elastic constants for (i) anisotropic, (ii) monoclinic and (iii) orthotropic materials. (2.5, 6, 1.5)

8. a) A unidirectional E-glass-epoxy composite with $\nu_f = 0.65$ has the following properties of its constituents: $E_f = 70 \text{ GPa}$, $E_m = 3.5 \text{ GPa}$, $\nu_f = 0.2$, $\nu_m = 0.36$. Find its transverse modulus using (a) strength of materials approach and (b) Tsai-Halpin equation with $\xi = 2$.

- b) For the above mentioned composite, tensile strengths of fibre and matrix are given as 3500 MPa and 105 MPa, respectively. Find the tensile strength F_{1t} of the composite. Assume elastic behavior to failure for both fibre and matrix. (6,5)

Useful Formulae:

$$\begin{aligned} \begin{bmatrix} \sigma_1 \\ \sigma_2 \\ \tau_{12} \end{bmatrix} &= \begin{bmatrix} c^2 & s^2 & 2cs \\ s^2 & c^2 & -2cs \\ -cs & cs & c^2 - s^2 \end{bmatrix} \begin{bmatrix} \sigma_x \\ \sigma_y \\ \tau_{xy} \end{bmatrix}, \quad \frac{M}{M_m} = \frac{1 + \frac{1}{2} h \eta_f}{1 - \frac{1}{2} \eta_f}, \quad \eta = \frac{M_f/M_m - 1}{M_f/M_m + 1}, \quad E_2 = \frac{E_m}{1 - \sqrt{\eta_f} (1 - E_m/E_{2f})} \\ G_{12} &= \frac{G_m}{1 - \sqrt{\eta_f} (1 - \frac{G_m}{G_{12f}})}, \quad G_{23} = \frac{G_m}{1 - \eta_f (1 - \frac{G_m}{G_{23f}})}, \quad \frac{\sigma_1^2}{F_1^2} + \frac{\sigma_2^2}{F_2^2} - \frac{\sigma_1 \sigma_2}{F_1^2} + \frac{\tau_{12}^2}{F_{12}^2} < 1 \\ Q_{11} &= \frac{E_1}{1 - \nu_{12} \nu_{21}}, \quad Q_{12} = \frac{\nu_{12} E_2}{1 - \nu_{12} \nu_{21}}, \quad Q_{22} = \frac{E_2}{1 - \nu_{12} \nu_{21}}, \quad \hat{\beta}_1 = Q_{11} \alpha_1 + Q_{12} \alpha_2 \\ \hat{\beta}_2 &= Q_{12} \alpha_1 + Q_{22} \alpha_2, \quad N_T = \sum_{k=1}^N \int_{-z_k}^{z_k} \beta^{(k)} T(z) dz, \quad M_T = \sum_{k=1}^N \int_{-z_k}^{z_k} \beta^{(k)} z T(z) dz \\ F_{1t} &\cong \eta_f \sigma_{1T}, \quad \text{i) } F_{1c} \cong \eta_f \sigma_{1c} \quad \text{ii) } F_{1c} = 10 F_{12} + 2.5 \sigma_{1T}, \quad \text{iii) } F_{1c} = \frac{G_m}{1 - \eta_f (1 - \frac{G_m}{G_{12}})} \\ F_{2t} &\cong [1 - \{\sqrt{\eta_f} - \eta_f\} \{1 - \frac{E_m}{E_{f2}}\}] \sigma_{1T}, \quad F_{2c} \cong [1 - (\sqrt{\eta_f} - \eta_f) (1 - \frac{E_m}{E_{f2}})] \sigma_{1c} \end{aligned}$$