

**MAJOR EXAM**  
**APPLIED PLASTICITY**  
**(AML833)**

**Date: 03/05/2009**  
**Time: 10:30-12:30am**

**Max Marks: 100**  
**Max Time: 02Hrs**

Q.1 (a) Derive Henky's and Geiringer's compatibility equations, and write the main differences between the two. (10)

(b) Using slip lines, determine the stress and velocity distribution in a semi infinite body indented by a frictionless flat rigid punch. Write assumptions made. (10)

Q.2 (a) State and prove upper bound theorem and derive its simple formula in plane strain. (10)

(b) Determine the upper bound to the extrusion force in symmetrical wedge- shaped die. (10)

Q.3. (a) Explain the sand heap analogy. Determine the torque required to make a rectangular shaft of perfectly plastic material fully plastic, using sand heap analogy. (10)

(b) For the case of internal pressure loading in a hollow sphere,

$$P_{crit} = (2/3) ( \beta^3 - 1 ) / \beta^3$$

Determine pressure required to cause plastic zone to reach a radius  $r_c$ . (10)

Q.4. (a) For a beam of rectangular cross-section, derive expressions for moment and shear stress distribution using a nonlinear stress-strain relation :

$$\sigma = E e + F e^n \quad (10)$$

(b) Using the concept of plastic hinges, determine the collapse load for a given portal frame loaded as shown, given the horizontal beam takes a moment 1.5 times the moment taken by vertical beams.  $Q=2P$  and  $b/a = 3$  (10)

Q.5. (a) Derive expressions for equivalent stress and equivalent strain and using these quantities derive Prandtl-Reuss equations for a perfectly plastic material (10)

(b) Given that  $\sigma_0$  is the yield stress in simple tension. Derive the expression for yield stress in pure shear for Tresca and Von-Mises criteria. Also calculate the radius of yield locus for Von-Mises yield criteria in Haigh-Westergaard stress space. (10)

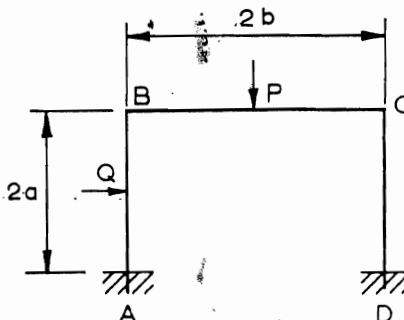


Figure for Question 4 (b)