Communication Systems

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3 Recommended Reading

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- 2. A.B. Carlson, P. Crilly, and P.B. Crilly. *Communication Systems*. McGraw-Hill Education, 2009. ISBN: 9780073380407
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- 4. S. Haykin and M. Moher. An Introduction to Analog and Digital Communications, 2nd Edition. Wiley, 2006. ISBN: 9781118313107
- 5. John G. Proakis. Digital Communications. McGraw-Hill, 1995
- 6. Edward A Lee and David G Messerschmitt. *Digital communication*. Springer Science & Business Media, 2012

Part I

Basic Definitions and Theorems

1 Types of Communication

Definition 1 (Digital communication). Communication is said to be digital communication if the source can send only one of the predefined messages. Usually, the predefined messages are binary, i.e. 0 or 1.

Definition 2 (Analogue communication). Communication is said to be analogue communication if the source can send one of infinite number of messages.

2 Periodicity and Finite Energy

Definition 3 (Finite energy signal). A signal x(t) is said to have finite energy if

$$\int_{-\infty}^{\infty} \left| x(t) \right|^2 \mathrm{d}t < \infty$$

Definition 4 (Periodic signal). A signal x(t) is said to be T_0 -periodic if for all t, $x(t+T_0)=x(t)$

3 Fourier Series Representation

Theorem 1 (Fourier series representation). A T_0 -periodic signal x(t) can be expressed as a Fourier series

$$x(t) = \sum_{k=-\infty}^{\infty} a_k e^{jk\omega_0 t}$$

where

$$\omega_0 = \frac{2\pi}{T_0}$$

and

$$a_k = \frac{1}{T_0} \int_{T_0} x(t) e^{-jk\omega_0 t} dt$$

4 Fourier Transform

Theorem 2 (Time and frequency domain expressions). A finite energy signal x(t) can be expressed in frequency domain such that

$$X(\omega) = \mathcal{F} \left\{ x(t) \right\}$$

$$= \int_{-\infty}^{\infty} x(t)e^{j\omega t} dt$$

$$x(t) = \mathcal{F}^{-1} \left\{ X(\omega) \right\}$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} X(\omega)e^{j\omega t} d\omega$$

Theorem 3 (Linearity of Fourier transform). The Fourier transform is linear, i.e.

$$y(t) = a_1 x_1(t) + a_2 x_2(t)$$

if and only if

$$Y(\omega) = a_1 X_1(\omega) + a_2 X_2(\omega)$$

Theorem 4 (Time shift). A time delay corresponds to multiplication by a tone in frequency domain, i.e.

$$y(t) = x(t - \tau)$$

if and only if

$$Y(\omega) = e^{-j\omega\tau}X(\omega)$$

Theorem 5 (Frequency shift). A shift in frequency corresponds to a tone in time domain, i.e.

$$y(t) = e^{j\omega_0 t} x(t)$$

if and only if

$$Y(\omega) = X(\omega - \omega_0)$$

Theorem 6 (Time reversal). A reversal in time corresponds to a reversal in frequency, i.e.

$$y(t) = x(-t)$$

if and only if

$$Y(\omega) = X(-\omega)$$

Theorem 7 (Time conjugation). A conjugation in time corresponds to a conjugation and a reversal in frequency, i.e.

$$y(t) = x^*(t)$$

if and only if

$$Y(\omega) = X^*(-\omega)$$

Theorem 8 (Time conjugation and reversal). A conjugation and a reversal in time corresponds to a conjugation in frequency, i.e.

$$y(t) = x^*(-t)$$

if and only if

$$Y(\omega) = X^*(\omega)$$

Theorem 9 (Convolution in time). A convolution in time corresponds to multiplication in frequency, i.e.

$$y(t) = h(t) * x(t)$$
$$= \int_{-\infty}^{\infty} h(\tau)x(t-\tau) d\tau$$

if and only if

$$Y(\omega) = H(\omega)X(\omega)$$

Theorem 10 (Multiplication in time). A multiplication in time corresponds to convolution in frequency, i.e.

$$y(t) = c(t)x(t)$$

if and only if

$$Y(\omega) = \frac{1}{2\pi} C(\omega) X(\omega)$$
$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} C(\sigma) X(\omega - \sigma) d\sigma$$

Definition 5 (Dirac delta function). The Dirac delta function is defined to be $\delta(t)$ such that for a < b,

$$\int_{a}^{b} \delta(t) dt = \begin{cases} 1 & ; & a < 0 < b \\ 0 & ; & \text{otherwise} \end{cases}$$

Hence, the value of the function for non-zero values of t may or may not be zero, but the integral of the function over any interval which excludes zero is 1. Hence, for all non-zero values of t, the function may have rapid oscillations.

For example, the delta function expressed as a limiting case of a Gaussian is zero at all non-zero point and infinite at zero, while the delta function expressed as a limiting case of a sinc function has rapid oscillations at non-zero points.

Theorem 11 (Dirac delta in time). A Dirac delta in time corresponds to a constant 1 in frequency, i.e.

$$x(t) = \delta(t)$$

if and only if

$$X(\omega) = 1$$

Definition 6 (Rectangular pulse function).

$$rect(t) = \begin{cases} 1 & ; & |t| \le \frac{1}{2} \\ 0 & ; & |t| > \frac{1}{2} \end{cases}$$

Definition 7 (Triangular pulse function).

$$tri(t) = \begin{cases} 1 - |t| & ; & |t| \le 1 \\ 0 & ; & |t| > 1 \end{cases}$$

Definition 8 (Sinc function).

$$\operatorname{sinc}(t) = \begin{cases} 1 & ; \quad t = 0\\ \frac{\sin(t)}{t} & ; \quad t \neq 0 \end{cases}$$

Theorem 12 (Dirac delta in frequency). A Dirac in frequency corresponds to a constant 1 in time, i.e.

$$x(t) = 1$$

if and only if

$$X(\omega) = 2\pi\delta(\omega)$$

Proof. Let

$$y(t) = \operatorname{rect}\left(\frac{t}{T_0}\right)$$

Hence,

$$Y(\omega) = \frac{2}{\omega} \sin\left(\omega \frac{T_0}{2}\right)$$
$$= T_0 \operatorname{sinc}\left(\omega \frac{T_0}{2}\right)$$

Therefore,

$$x(t) = \lim_{T_0 \to \infty} y(t)$$

Hence,

$$X(\omega) = \lim_{T_0 \to \infty} Y(\omega)$$
$$= c\delta(\omega)$$

where c is a constant. Also,

$$x(0) = \frac{1}{2\pi} \int_{-\infty}^{\infty} X(\omega) d\omega$$

Therefore,

$$1 = x(0)$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} c\delta(\omega) d\omega$$

$$= \frac{c}{2\pi}$$

Therefore,

$$c=2\pi$$

Hence,

$$X(\omega) = 2\pi\delta(\omega)$$

Theorem 13 (Fourier transform in terms of temporal frequency).

$$\widetilde{X}(f) = X(\omega)\Big|_{\omega=2\pi f}$$

Hence,

$$\widetilde{X}(f) = \int_{-\infty}^{\infty} x(t)e^{-j2\pi ft} dt$$

$$x(t) = \int_{-\infty}^{\infty} \widetilde{X}(f)e^{j2\pi ft} df$$

Theorem 14 (Impulse train in time). An impulse train in time corresponds to an impulse train in frequency, i.e.

$$x(t) = \sum_{n=-\infty}^{\infty} \delta(t - nT_0)$$

if and only if

$$X(\omega) = \frac{2\pi}{T_0} \sum_{k=-\infty}^{\infty} \delta\left(\omega - \frac{2\pi}{T_0}k\right)$$

Proof.

$$x(t) = \sum_{k=-\infty}^{\infty} a_k e^{j\omega_0 kt}$$

where

$$a_k = \frac{1}{T_0} \int_{-\frac{T_0}{2}}^{\frac{T_0}{2}} x(t)e^{-j\omega_0 kt} dt$$
$$= \frac{1}{T_0} \int_{-\frac{T_0}{2}}^{\frac{T_0}{2}} \delta(t)e^{-j\omega_0 kt} dt$$
$$= \frac{1}{T_0}$$

Therefore,

$$x(t) = \frac{1}{T_0} \sum_{k=-\infty}^{\infty} e^{j\omega_0 kt}$$

Hence,

$$X(\omega) = \frac{1}{T_0} \sum_{k=-\infty}^{\infty} 2\pi \delta(\omega - k\omega_0)$$
$$= \frac{2\pi}{T_0} \sum_{k=-\infty}^{\infty} \delta\left(\omega - \frac{2\pi}{T_0}k\right)$$

Theorem 15 (Sampling in time). A sampling in time corresponds to replication in frequency, i.e.

$$y(t) = x(t) \sum_{n = -\infty}^{\infty} \delta(t - nT_0)$$
$$= \sum_{n = -\infty}^{\infty} x(nT_0)\delta(t - nT_0)$$

if and only if

$$Y(\omega) = X(\omega) * \sum_{k=-\infty}^{\infty} \frac{2\pi}{T_0} \delta\left(\omega - \frac{2\pi}{T_0}k\right)$$
$$= \frac{1}{T_0} \sum_{k=-\infty}^{\infty} X\left(\omega - \frac{2\pi}{T_0}k\right)$$

5 Stochastic Signals

Definition 9 (Mean of stochastic signal). Let x(t) be a sample function of a random process. The mean of x(t) is defined to be

$$\widetilde{\eta}_X(t) = \mathrm{E}\left[x(t)\right]$$

Definition 10 (Autocorrelation function of stochastic signal). Let x(t) be a sample function of a random process. The autocorrelation function of x(t) is defined to be

$$\widetilde{R}_{XX}(t_1, t_2) = \mathbb{E}\left[x(t_1)x^*(t_2)\right]$$

Theorem 16. For a real stochastic signal x(t),

$$\widetilde{R}_{XX}(t_1, t_2) = \widetilde{R}_{XX}(t_2, t_1)$$

Definition 11 (Wide sense stationary random process). A random process X is said to be wide sense stationary if

$$\widetilde{\eta}_X(t) = \eta_X$$

$$\widetilde{R}_{XX}(t_1, t_2) = R_{XX}(t_1 - t_2)$$

that is, the mean is independent of time and the autocorrelation function is dependent on the time difference only and is independent of absolute time.

Theorem 17. For a WSS random process X,

$$R_{XX}(\tau) = R_{XX}^*(-\tau)$$

Proof.

$$R_{XX}(-\tau) = E \left[x(t-\tau)x^*(t) \right]$$
$$= E \left[x^*(t)x(t-\tau) \right]$$
$$= E \left[x(t)x(t-\tau) \right]^*$$
$$= R_{XX}^*(\tau)$$

Definition 12 (Spectrum of WSS random process).

$$S_{XX}(\omega) = \int_{-\infty}^{\infty} R_{XX}(\tau) e^{-j\omega\tau} d\tau$$

Theorem 18. The spectrum of a random process is the mean of the squared absolute value of the Fourier transform of a long enough segment of a sample function of the process, normalized by the length of the segment, i.e.

$$S_{XX}(\omega) = \lim_{T \to \infty} \frac{1}{T} \operatorname{E} \left[\left| \int_{0}^{T} x(t)e^{-j\omega t} dt \right| \right]$$

Proof. Let x(t) be a sample function of a WSS random process. As $R_{XX}(0) = \mathbb{E}\left[\left|x(t)\right|^2\right]$ is constant irrespective of the absolute time, the signal x(t) never converges. Therefore, it is not a finite energy signal and hence does not have a Fourier transform.

Hence, let

$$X_T(\omega) = \int_0^T x(t)e^{-j\omega t} dt$$

Therefore,

$$\frac{1}{T} \operatorname{E} \left[\left| X_{T}(\omega) \right|^{2} \right] = \frac{1}{T} \operatorname{E} \left[\int_{0}^{T} x(t_{1}) e^{-j\omega t_{1}} dt_{1} \int_{0}^{T} x^{*}(t_{2}) e^{j\omega t_{2}} dt_{2} \right]
= \frac{1}{T} \int_{0}^{T} \int_{0}^{T} \operatorname{E} \left[x(t_{1}) x^{*}(t_{2}) \right] e^{-j\omega t_{1}} e^{j\omega t_{2}} dt_{1} dt_{2}
= \frac{1}{T} \int_{0}^{T} \int_{0}^{T} \widetilde{R}_{XX}(t_{1}, t_{2}) e^{-j\omega t_{1}} e^{j\omega t_{2}} dt_{1} dt_{2}
= \frac{1}{T} \int_{0}^{T} \int_{0}^{T} R_{XX}(t_{1} - t_{2}) e^{-j\omega (t_{1} - t_{2})} dt_{1} dt_{2}$$

Let

$$\tau = t_1 - t_2$$
$$\sigma = t_1 + t_2$$

Therefore,

$$\begin{pmatrix} \tau \\ \sigma \end{pmatrix} = \begin{pmatrix} 1 & -1 \\ 1 & 1 \end{pmatrix} \begin{pmatrix} t_1 \\ t_2 \end{pmatrix}$$

Therefore,

$$\left| \frac{\partial(\tau, \sigma)}{\partial(t_1, t_2)} \right| = 2$$

Therefore,

$$\frac{1}{T} \operatorname{E} \left[\left| X_{T}(\omega) \right|^{2} \right] = \frac{1}{T} \int_{-T}^{T} \int_{|\tau|}^{2T - |\tau|} R_{XX}(\tau) e^{-j\omega\tau} \frac{1}{2} \, d\sigma \, d\tau$$

$$= \int_{-T}^{T} R_{XX}(\tau) e^{-j\omega\tau} \frac{1}{T} \int_{|\tau|}^{2T - |\tau|} d\sigma \, d\tau \frac{1}{2}$$

$$= \frac{-T}{T} R_{XX}(\tau) e^{-j\omega\tau} \frac{1}{2} \left(\frac{2T - 2|\tau|}{2} \right) d\tau$$

$$= \int_{-T}^{T} R_{XX}(\tau) e^{-j\omega\tau} \left(1 - \frac{|\tau|}{T} \right) d\tau$$

$$= \int_{-T}^{\tau} R_{XX}(\tau) e^{-j\omega\tau} d\tau - \frac{1}{T} \int_{-T}^{\tau} |\tau| R_{XX}(\tau) e^{-j\omega\tau} d\tau$$

Therefore, assuming the Ergodicity condition $\int_{-\infty}^{\infty} |\tau R_{XX}(\tau)| d\tau < M < \infty,$

$$\lim_{T \to \infty} \frac{1}{T} \operatorname{E} \left[\left| X_T(\omega) \right|^2 \right] = \lim_{T \to \infty} \int_{-\tau}^{\tau} R_{XX}(\tau) e^{-j\omega\tau} \, d\tau - \frac{1}{T} \int_{-\tau}^{\tau} \left| \tau \right| R_{XX}(\tau) e^{-j\omega\tau} \, d\tau$$
$$= \int_{-\infty}^{\infty} R_{XX}(\tau) e^{-j\omega\tau} \, d\tau$$
$$= S_{XX}(\omega)$$

Theorem 19.

$$S_{XX}(\omega) \ge 0$$

for all ω .

Proof.

$$S_{XX}(\omega) = \lim_{T \to \infty} \frac{1}{T} \operatorname{E} \left[\left| X_T(\omega) \right|^2 \right]$$

$$\geq 0$$

Theorem 20 (Time shift for stochastic signal). Let x(t) be a WSS random process with spectrum $S_{XX}(\omega)$. Then,

$$y(t) = x(t - t_0)$$

if and only if

$$S_{YY}(\omega) = S_{XX}(\omega)$$

Proof.

$$R_{YY}(\tau) = E \left[y(t+\tau)y^*(t) \right]$$
$$= E \left[x(t-t_0+\tau)x^*(t-t_0) \right]$$
$$= R_{XX}(\tau)$$

Hence,

$$S_{YY}(\omega) = S_{XX}(\omega)$$

Theorem 21 (Frequency shift for stochastic signal). Let x(t) be a WSS random process with spectrum $S_{XX}(\omega)$.
Then

$$y(t) = x(t)e^{j\omega_0 t}$$

if and only if

$$S_{YY}(\omega) = S_{XX}(\omega - \omega_0)$$

Proof.

$$R_{YY}(\tau) = E \left[y(t+\tau)y^*(t) \right]$$

$$= E \left[x(t+\tau)e^{j\omega_0(t+\tau)}x^*(t)e^{-j\omega_0t} \right]$$

$$= e^{j\omega_0\tau} E \left[x(t+\tau)x^*(t) \right]$$

$$= e^{j\omega_0\tau} R_{XX}(\tau)$$

Therefore,

$$S_{YY}(\omega) = S_{XX}(\omega - \omega_0)$$

Theorem 22 (Time reversal for stochastic signal). Let x(t) be a WSS random process with spectrum $S_{XX}(\omega)$.

Then

$$y(t) = x(-t)$$

if and only if

$$S_{YY}(\omega) = S_{XX}(-\omega)$$

Proof.

$$R_{YY}(\tau) = \mathbb{E} \left[y(t+\tau)y^*(t) \right]$$
$$= \mathbb{E} \left[x(-t-\tau)x^*(-t) \right]$$
$$= R_{XX}(-\tau)$$

Therefore,

$$S_{YY}(\omega) = S_{XX}(-\omega)$$

Theorem 23 (Time conjugation for stochastic signal). Let x(t) be a WSS random process with spectrum $S_{XX}(\omega)$.

Then

$$y(t) = x^*(t)$$

if and only if

$$S_{YY}(\omega) = S_{XX}(-\omega)$$

Proof.

$$R_{YY}(\tau) = E \left[y(t+\tau)y^*(t) \right]$$
$$= E \left[x^*(t+\tau)x(t) \right]$$
$$= R_{XX}(-\tau)$$

Equivalently,

$$R_{YY}(\tau) = R_{XX}^*(\tau)$$

Therefore,

$$S_{YY}(\omega) = S_{XX}(-\omega)$$

and

$$S_{YY}(\omega) = S_{XX}^*(-\omega)$$

This is consistent with Theorem 19.

Theorem 24 (Time conjugation and reversal for stochastic signal). Let x(t) be a WSS random process with spectrum $S_{XX}(\omega)$. Then

$$y(t) = x^*(-t)$$

if and only if

$$S_{YY}(\omega) = S_{XX}(\omega)$$

Theorem 25 (Convolution in time for stochastic signal). Let x(t) be a WSS random process with spectrum $S_{XX}(\omega)$.

$$y(t) = h(t) * x(t)$$
$$= \int_{-\infty}^{\infty} h(\mu)x(t - \mu) d\mu$$

if and only if

$$S_{YY}(\omega) = |H(\omega)|^2 S_{XX}(\omega)$$

Proof.

$$R_{YY}(\tau) = \mathbb{E}\left[y(t+\tau)y^*(t)\right]$$

$$= \mathbb{E}\left[\int_{-\infty}^{\infty} h(\mu)x(t+\tau-\mu) \,\mathrm{d}\mu \int_{-\infty}^{\infty} h^*(\sigma)x^*(t-\sigma) \,\mathrm{d}\sigma\right]$$

$$= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} h(\mu)h^*(\sigma) \,\mathbb{E}\left[x(t+\tau-\mu)x^*(t-\sigma)\right] \,\mathrm{d}\mu \,\mathrm{d}\sigma$$

$$= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} h(\mu)h^*(\sigma)R_{XX}(t-\mu+\sigma) \,\mathrm{d}\mu \,\mathrm{d}\sigma$$

Let

$$\alpha = \mu - \sigma$$
$$\beta = \mu$$

Therefore,

$$\begin{pmatrix} \alpha \\ \beta \end{pmatrix} = \begin{pmatrix} 1 & -1 \\ 1 & 0 \end{pmatrix} \begin{pmatrix} \mu \\ \sigma \end{pmatrix}$$

Therefore,

$$\left| \frac{\partial(\alpha, \beta)}{\partial(\mu, \sigma)} \right| = 1$$

Therefore,

$$R_{YY}(\tau) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} h(\beta)h^*(\beta - \alpha)R_{XX}(\tau - \alpha) d\alpha d\beta$$

Let

$$g(\alpha) = \int_{-\infty}^{\infty} h(\beta)h^*(\beta - \alpha) d\beta R_{XX}(\tau - \alpha) d\alpha$$

Therefore,

$$S_{YY}(\omega) = G(\omega)S_{XX}(\omega)$$

Additionally, let

$$g(\alpha) = \int_{-\infty}^{\infty} h(\beta) \overline{h}(\alpha - \beta) \, \mathrm{d}\beta$$

Therefore,

$$G(\omega) = H(\omega)\overline{H}(\omega)$$

Hence, by the two definitions of $g(\alpha)$,

$$\overline{h}(\tau) = h^*(-\tau)$$

Therefore,

$$\overline{H}(\omega) = H^*(\omega)$$

Therefore,

$$G(\omega) = H(\omega)H^*(\omega)$$
$$= |H(\omega)|^2$$

Therefore,

$$S_{YY}(\omega) = |H(\omega)|^2 S_{XX}(\omega)$$

Theorem 26 (Multiplication in time for stochastic signal). Let x(t) be a WSS random process with spectrum $S_{XX}(\omega)$.

Let c(t) be a deterministic function.

Let

$$y(t) = c(t)x(t)$$

Then, Y may or may not be a WSS random process. $^{1-2}$

¹This is intuitively correct as, for example, if a WSS random process is multiplied by a finite window, the product is zero outside the window, and hence is not WSS.

²If c(t) is periodic, Y is cyclostationary. See Theorem 27

Proof.

$$R_{YY}(t,\tau) = E \left[y(t+\tau)y^*(t) \right]$$

$$= E \left[c(t+\tau)x(t+\tau)c^*(t)x^*(t) \right]$$

$$= c(t+\tau)c^*(t) E \left[x(t+\tau)x^*(t) \right]$$

$$= c(t+\tau)c^*(t)R_{XX}(\tau)$$

Hence, as the autocorrelation function of Y may be dependent on the absolute time, Y may or may not be WSS.

Definition 13 (Circular random process). A stochastic process is said to be circular or proper if

$$\widetilde{R}_{XX^*}(t_1, t_2) = 0$$

6 Cyclostationary Processes

Definition 14 (Cyclostationary process). A random process is said to be cyclostationary with a cyclic period T_0 if the mean $\tilde{\eta}_X(t)$ and $\tilde{R}_{XX}(t,\tau)$ are T_0 periodic in t, i.e. if for all t and τ ,

$$\widetilde{\eta}_X(t+T_0) = \widetilde{\eta}_X(t)$$

$$\widetilde{R}_{XX}(t+T_0,\tau) = \widetilde{R}_{XX}(t,\tau)$$

Theorem 27 (Multiplication in time for stochastic signal). Let x(t) be a WSS random process with spectrum $S_{XX}(\omega)$. Let c(t) be a T_0 periodic deterministic function. Let

$$y(t) = c(t)x(t)$$

Then, y(t) is cyclostationary with T_0 .

Proof.

$$\widetilde{\eta}_{Y}(t) = \mathbf{E} \left[c(t)x(t) \right]$$

$$= c(t) \mathbf{E} \left[x(t) \right]$$

$$= c(t)\eta_{X}$$

$$= c(t+T_{0})\eta_{X}$$

$$= \widetilde{\eta}_{Y}(t+T_{0})$$

$$R_{YY}(t,\tau) = \mathbf{E} \left[y(t+\tau)y^{*}(t) \right]$$

$$= \mathbf{E} \left[c(t+\tau)x(t+\tau)c^{*}(t)x^{*}(t) \right]$$

$$= c(t+\tau)c^{*}(t) \mathbf{E} \left[x(t+\tau)x^{*}(t) \right]$$

$$= c(t+\tau)c^{*}(t)R_{XX}(\tau)$$

$$= c(t+\tau+T_{0})c^{*}(t+T_{0})R_{XX}(\tau)$$

$$= \widetilde{R}_{YY}(t+T_{0},\tau)$$

Hence, Y is cyclostationary with T_0 .

Theorem 28. Let x(t) be a WSS random process with spectrum $S_{XX}(\omega)$. Let c(t) be a T_0 periodic deterministic function. Let
$$\overline{y}(t) = c(t - \varphi)x(t)$$

where $\varphi \sim U(0, T_0)$ is independent of x(t). Then, $\overline{y}(t)$ is WSS with

$$\eta_{\overline{Y}} = m_c \eta_X$$

$$R_{\overline{YY}}(\tau) = r_c(\tau) R_{XX}(\tau)$$

where

$$m_c = \frac{1}{T_0} \int_0^{T_0} c(t) dt$$
$$r_c(\tau) = \frac{1}{T_0} \int_0^{T_0} c(t+\tau)c^*(t) dt$$

and hence,

$$S_{\overline{YY}}(\omega) = \frac{1}{2\pi} \int_{-\infty}^{\infty} P_c(\sigma) S_{XX}(\omega - \sigma) d\sigma$$

where

$$P_c(\omega) = \mathcal{F}\left\{r_c(\tau)\right\}$$
$$= \int_{-\infty}^{\infty} r_c(\tau)e^{-j\omega\tau} d\tau$$

Proof. Let

$$\overline{y}(t) = c(t - \varphi)x(t)$$

where φ is a random variable independent of x(t). Therefore,

$$\begin{split} \widetilde{\eta}_{\overline{Y}}(t) &= \mathbf{E} \left[c(t-\varphi)x(t) \right] \\ &= \mathbf{E} \left[\mathbf{E} \left[c(t-\varphi)x(t) \middle| \varphi \right] \right] \\ &= \mathbf{E}_{\varphi} \left[c(t-\varphi)\eta_{X} \right] \\ &= \mathbf{E} \left[c(t-\varphi) \right] \eta_{X} \\ \widetilde{R}_{\overline{YY}}(t,\tau) &= \mathbf{E} \left[\overline{y}(t+\tau)\overline{y}^{*}(t) \right] \\ &= \mathbf{E} \left[\mathbf{E} \left[\overline{y}(t+\tau)\overline{y}^{+}(t) \middle| \varphi \right] \right] \\ &= \mathbf{E} \left[\mathbf{E} \left[c(t+\tau-\varphi)x(t+\tau)c^{*}(t-\varphi)x^{*}(t) \middle| \varphi \right] \right] \\ &= \mathbf{E}_{\varphi} \left[c(t+\tau-\varphi)c^{*}(t-\varphi)R_{XX}(\tau) \right] \\ &= \mathbf{E} \left[c(t+\tau-\varphi)c^{*}(t-\varphi) \right] R_{XX}(\tau) \end{split}$$

As c(t) is T_0 periodic and $\varphi \sim U(0, T_0)$,

$$E\left[c(t-\varphi)\right] = \int_{-\infty}^{\infty} f_{\varphi}(\varphi)c(t-\varphi) d\varphi$$
$$= \frac{1}{T_0} \int_{0}^{T_0} c(t-\varphi) d\varphi$$

Let

$$\varphi' = t - \varphi$$
$$\therefore d\varphi' = d\varphi$$

Therefore,

$$E\left[c(t-\varphi)\right] = \frac{1}{T_0} \int_{t-T_0}^t c(\varphi') d\varphi'$$
$$= \frac{1}{T_0} \int_0^{T_0} c(t) dt$$
$$= m_c$$

Similarly,

$$E\left[c(t+\tau-\varphi)c^*(t-\varphi)\right] = \frac{1}{T_0} \int_0^{T_0} c(t+\tau-\varphi)c^*(t-\varphi) d\varphi$$
$$= \frac{1}{T_0} \int_0^{T_0} c(t+\tau)c^*(t) dt$$
$$= r_c(\tau)$$

Exercise 1.

Consider the zero mean WSS process X(t) with autocorrelation function $R_{XX}(\tau)$. Let

$$Y(t) = X(t)c(t - \varphi)$$

where

$$c(t) = \cos(\omega_0 t)$$

$$F_{\varphi}(\phi) = \begin{cases} \frac{\omega_0}{\pi} \left(1 - \frac{\omega_0}{\pi} \phi \right) & ; & |\phi| \le \frac{\pi}{\omega_0} \\ 0 & ; & \text{otherwise} \end{cases}$$

Show that Y(t) is WSS.

Solution 1.

$$\begin{split} \widetilde{\eta}_{Y}(t) &= \mathbf{E}\left[Y(t)\right] \\ &= \mathbf{E}\left[X(t)c(t-\phi)\right] \\ &= \mathbf{E}\left[X(t)\right] \mathbf{E}\left[\cos\left(\omega_{0}(t-\varphi)\right)\right] \\ &= 0 \\ \widetilde{R}_{YY}(t,\tau) &= \mathbf{E}\left[Y(t+\tau)Y(t)\right] \\ &= \mathbf{E}\left[X(t+\tau)\cos\left(\omega_{0}(t+\tau-\varphi)\right)x^{*}(t)\cos\left(\omega_{0}(t-\varphi)\right)\right] \\ &= \mathbf{E}\left[x(t+\tau)x^{*}(t)\right] \mathbf{E}\left[\cos\left(\omega_{0}(t+\tau-\varphi)\right)\cos\left(\omega_{0}(t-\varphi)\right)\right] \\ &= R_{XX}(\tau) \mathbf{E}\left[\cos\left(\omega_{0}(t+\tau-\varphi)\right)\cos\left(\omega_{0}(t-\varphi)\right)\right] \\ &= \frac{R_{XX}(\tau)}{2} \mathbf{E}\left[\cos\left(\omega_{0}(2t-2\varphi+\tau)\right)+\cos(\omega_{0}\tau)\right] \\ &= \frac{R_{XX}(\tau)}{2} \cos(\omega_{0}\tau) + \frac{R_{XX}(\tau)}{2} \mathbf{E}\left[\cos\left(\omega_{0}(2t-2\varphi+\tau)\right)\right] \end{split}$$

Therefore, solving by definition,

$$E\left[\cos\left(\omega_0(2t-2\varphi+\tau)\right)\right]=0$$

Therefore,

$$\widetilde{R}_{YY}(t,\tau) = \frac{R_{XX}(\tau)\cos(\omega_0\tau)}{2}$$

Therefore, as the mean is independent of time and the autocorrelation function is dependent on the time difference only, Y(t) is WSS.

Part II

Pulse Amplitude Modulation

1 Direct Multiplication / Natural Sampling

Definition 15 (Direct Multiplication PAM). Let x(t) be a deterministic signal with Fourier transform $X(\omega)$.

Let c(t) be given by a train of pulses, such that

$$c(t) = \sum_{n = -\infty}^{\infty} p(t - nT_s)$$

where p(t) is a general pulse. ³ Let the modulated signal be

$$y(t) = c(t)x(t)$$

Such a modulation is called direct multiplication pulse amplitude modulation.

Theorem 29. For a signal x(t) modulated with direct multiplication PAM,

$$Y(\omega) = \sum_{k=-\infty}^{\infty} a_k X(\omega - \omega_s k)$$

Therefore, $Y(\omega)$ is made up of replicas of $X(\omega)$ scaled according to a_k with adjacent replicas separated ω_s , and in the time domain, the pulses are distorted and have the shape of the original signal. ⁴ Hence, in order to avoid aliasing,

$$B < \frac{\omega_s}{2}$$

where $X(\omega)$ is zero outside (-B, B).

Proof. Let

$$\omega_s = \frac{2\pi}{T_s}$$

 $^{{}^{3}\}mathrm{rect}\left(\frac{t}{\Delta}\right)$ is a commonly used pulse.

⁴As these replicas differ by a constant factor only, the signal can be recreated using any replica. In order to avoid noise in the reconstruction, the replica used in reconstruction is that for which the noise is the lowest.

Therefore,

$$c(t) = \sum_{n=-\infty}^{\infty} p(t - nT_s)$$

Therefore, the Fourier coefficients of c(t) are

$$a_k = \frac{1}{T_s} \int_0^{T_s} c(t)e^{j\omega_s kt} dt$$
$$= \frac{1}{T_s} \int_0^{T_s} \sum_{n=-\infty}^{\infty} p(t - nT_s)e^{j\omega_s kt} dt$$

Let

$$t' = t - nT_s$$

$$\therefore t = t' + nT_s$$

$$\therefore dt = dt'$$

Therefore,

$$a_k = \frac{1}{T_s} \sum_{n=-\infty}^{\infty} \int_{-nT_s}^{-(n-1)T_s} p(t')e^{-j\omega_s k(t'+nT_s)} dt'$$

$$a_k = \frac{1}{T_s} \sum_{n=-\infty}^{\infty} \int_{-nT_s}^{-(n-1)T_s} p(t')e^{-j\omega_s k\left(t'+n\frac{2\pi}{\omega_s}\right)} dt'$$

$$= \frac{1}{T_s} \sum_{n=-\infty}^{\infty} \int_{-nT_s}^{-(n-1)T_s} p(t')e^{-j\omega_s kt'} dt'$$

$$= \frac{1}{T_s} \int_{-\infty}^{\infty} p(t)e^{-j\omega_s kt} dt$$

$$= \frac{1}{T_s} P(\omega_s k)$$

Therefore,

$$X(\omega) = \sum_{k=-\infty}^{\infty} 2\pi a_k \delta(\omega - \omega_s k)$$

Therefore,

$$Y(\omega) = \frac{1}{2\pi}C(\omega) * X(\omega)$$
$$= \sum_{k=-\infty}^{\infty} a_k X(\omega - \omega_s k)$$
$$= \sum_{k=-\infty}^{\infty} \frac{1}{T_s} P(k\omega_s)$$

Therefore, $Y(\omega)$ is made up of replicas of $X(\omega)$ scaled according to a_k with adjacent replicas separated ω_s . Hence, in order to avoid aliasing, $X(\omega)$ must be limited to $\pm \omega_s$, i.e.

$$B < \frac{\omega_s}{2}$$

where $X(\omega)$ is zero outside (-B, B).

Theorem 30. A signal modulated with direct multiplication PAM can be reconstructed as in Figure 1, where the cutoff frequency and the gain of the low pass filter are

$$\omega_c \in [B, \omega_s - B)$$

$$A = \frac{1}{|a_m|}$$

$$= \frac{T_s}{|P(\omega_s m)|}$$

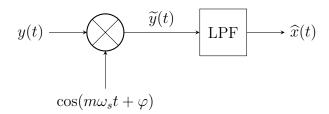


Figure 1: Reconstruction of Signal Modulated with Direct Multiplication PAM

Hence,

$$\widehat{X}(\omega) = \cos(\varphi)X(\omega)$$

Proof.

$$\widetilde{y} = \cos(m\omega_s t + \varphi)y(t)$$

$$= \frac{1}{2} \left(e^{j\varphi} e^{jm\omega_s t} + e^{-j\varphi} e^{-jm\omega_s t} \right) y(t)$$

Therefore,

$$\widetilde{Y}(\omega) = \frac{1}{2} \left(e^{j\varphi} Y(\omega - m\omega_s) + e^{-j\varphi} Y(\omega - m\omega_s) \right)$$

$$= \frac{1}{2} \left(e^{j\varphi} \sum_{k=-\infty}^{\infty} a_k X(\omega - k\omega_s - m\omega_s) + e^{-j\varphi} \sum_{k=-\infty}^{\infty} a_k X(\omega - k\omega_s + m\omega_s) \right)$$

$$= \frac{1}{2} \left(e^{j\varphi} \sum_{k=-\infty}^{\infty} a_k X(\omega - (k+m)\omega_s) + e^{-j\varphi} \sum_{k=-\infty}^{\infty} a_k X(\omega - (k-m)\omega_s) \right)$$

Therefore,

$$\widehat{X}(t) = \frac{1}{2|a_m|} \left(e^{j\varphi} a_{-m} X(\omega) + e^{j\varphi} a_m X(\omega) \right)$$

$$= \frac{1}{2|a_m|} \left(e^{j\varphi} a_m^* + e^{-j\varphi} a_m \right) X(\omega)$$

$$= \frac{1}{|a_m|} \Re \left\{ e^{-j\varphi} a_m \right\} X(\omega)$$

Assuming p(t) is symmetric, a_m is real. Therefore,

$$\widehat{X}(\omega) = \Re \left\{ e^{j\varphi} \right\} X(\omega)$$
$$= \cos(\varphi) X(\omega)$$

2 Flat Sampling

Definition 16 (Flat Sampling PAM). Let x(t) be a deterministic signal with Fourier transform $X(\omega)$.

Let c(t) be given by a train of pulses, such that

$$c(t) = \sum_{n=-\infty}^{\infty} p(t - nT_s)$$

where p(t) is a general pulse. ⁵ Let the modulated signal be

$$y(t) = \sum_{n=-\infty}^{\infty} x(nT_s)p(t - nT_s)$$

that is, the pulses of the modulated signal have the same shape as the original train of pulses. Such a modulation is called flat sampling pulse amplitude modulation.

Theorem 31. For a signal x(t) modulated with flat sampling PAM,

$$Y(\omega) = \frac{1}{T_s} P(\omega) \sum_{k=-\infty}^{\infty} X(\omega - k\omega_s)$$

Therefore, $Y(\omega)$ is made up of replicas of $X(\omega)$ distorted by the Fourier transform of the pulse, with adjacent replicas separated ω_s . Hence, in the time domain, the shape of the pulses is preserved, but the shape of frequency spectrum is distorted, and the distortion of each replica is different. Hence, in order to avoid aliasing,

$$B < \frac{\omega_s}{2}$$

where $X(\omega)$ is zero outside (-B, B).

Proof. Let

$$\widetilde{y}(t) = \sum_{n=-\infty}^{\infty} \delta(t - nT_s)x(t)$$

that is, let $\widetilde{y}(t)$ be the signal sampled at all nT_s . Therefore,

$$\widetilde{y}(t) = \sum_{n=-\infty}^{\infty} x(nT_s)\delta(t - nT_s)$$

Therefore,

$$\widetilde{Y}(\omega) = \frac{1}{2\pi} X(\omega) * G(\omega)$$
$$= \frac{1}{T_s} \sum_{k=-\infty}^{\infty} X(\omega - k\omega_s)$$

 $^{^{5}}$ rect $\left(\frac{t}{\Delta}\right)$ is a commonly used pulse.

Therefore,

$$y(t) = \widetilde{y}(t) * p(t)$$
$$= \sum_{n = -\infty}^{\infty} x(nT_s)p(t - nT_s)$$

Therefore,

$$Y(\omega) = \widetilde{Y}(\omega)P(\omega)$$
$$= \frac{1}{T_s}P(\omega)\sum_{k=-\infty}^{\infty}X(\omega - k\omega_s)$$

Part III

Pulse Position Modulation

Definition 17 (PPM). Let x(t) be a deterministic signal with Fourier transform $X(\omega)$, bounded by x_{\min} and x_{\max} . Let p(t) be a general pulse extending from t=0 to $t=\Delta$.

Let the modulated signal be

$$y(t) = \sum_{n=-\infty}^{\infty} p\left(t - nT_s - \left(\alpha x(nT_s) + \beta\right)\right)$$

where α and β are such that

$$\alpha x_{\min} + \beta = 0$$

$$\alpha x_{\max} + \beta = T_s - \Delta$$

that is, the pulses of the modulated signal have delay corresponding to the amplitude of the original signal at the corresponding multiple of T_s . ⁶ Such a modulation is called pulse position modulation.

⁶The delay of the pulse is measured with respect to the left edge of the pulse.

Part IV

Quantization

Definition 18 (Quantization). Let x(t) be a deterministic signal. Let

$$x[n] = x(nT_s)$$

be the corresponding discrete time signal.

The quantization of the signal is defined to be $x_q[n]$ where x_q can have quantized values only.

The quantization error is defined to be

$$q[n] = x[n] - x_q[n]$$

1 Uniform Quantization

Definition 19 (Dense quantization). If the quantization error q is distributed uniformly in each quantization cell, the quantization is called dense quantization.

Definition 20 (Uniform quantization). If the quantum values are such that each quantization cells have equal width, the quantization is called uniform quantization.

Theorem 32. For uniform and dense quantization,

$$q \sim \mathrm{U}\left(-\frac{\Delta}{2}, \frac{\Delta}{2}\right)$$

Definition 21 (QSNR). The quantization signal to noise ratio is defined to be

$$QSNR = \frac{E\left[x^2\right]}{E\left[q^2\right]}$$

Theorem 33. If x is a uniform random variable quantized by a uniform and dense M level quantizer Q, i.e.

$$x \sim U\left(-\frac{M}{2}\Delta, \frac{M}{2}\Delta\right)$$

$$Q = \begin{cases} x_1 & ; & x \in I_1 \\ & \vdots \\ x_m & ; & x \in I_m \end{cases}$$

then

$$q \sim \mathrm{U}\left(-\frac{\Delta}{2}, \frac{\Delta}{2}\right)$$

Hence,

$$\begin{aligned} \text{QSNR} &= M^2 \\ \text{QSNR}_{\, \text{dB}} &= 20b \log 2 \\ &\approx 6b \end{aligned}$$

where $b = \log_2 M$.

Proof.

$$x \sim U\left(-\frac{M}{2}\Delta, \frac{M}{2}\Delta\right)$$

Therefore,

$$\mathrm{E}\left[x^2\right] = \frac{M^2 \Delta^2}{12}$$

Similarly,

$$q \sim \mathrm{U}\left(-\frac{\Delta}{2}, \frac{\Delta}{2}\right)$$

Therefore,

$$\mathrm{E}\left[q^2\right] = \frac{\Delta^2}{12}$$

Therefore,

$$QSNR = \frac{E[x^2]}{E[q^2]}$$
$$= M^2$$

Therefore,

$$QSNR_{dB} = 10 \log QSNR$$

$$= 10 \log (M^{2})$$

$$= 20 \log M$$

$$= 20 \log (2^{b})$$

$$= 20b \log 2$$

$$\approx 6b$$

Theorem 34. If x is a Gaussian random variable with zero mean and σ_x , quantized by a uniform M level quantizer Q with highest and lowest thresholds $\pm k\sigma_x$,

$$QSNR \approx \frac{k^2}{3M^2} - \frac{2k}{\sqrt{2\pi}} e^{-\frac{1}{2}k^2} + 2Q(k) \left(k^2 + 1\right)$$

$$QSNR_{dB} \approx -10 \log \left(\frac{k^2}{3M^2} - \frac{2k}{\sqrt{2\pi}} e^{-\frac{1}{2}k^2} + 2Q(k) \left(k^2 + 1\right)\right)$$

Proof. Let A be the event that

$$|x| < k\sigma_x$$

Therefore,

$$P(A) = \int_{-k\sigma_x}^{k\sigma_x} \frac{1}{\sqrt{2\pi}\sigma_x} e^{-\frac{1}{2}\frac{x^2}{\sigma_x^2}} dx$$

Let

$$x' = \frac{x}{\sigma_x}$$

Therefore,

$$x = \sigma_x x'$$
$$dx = \sigma_x dx'$$

Therefore,

$$P(A) = \int_{-k}^{k} \frac{1}{\sqrt{2\pi}\sigma_x} e^{-\frac{1}{2}x'} \sigma_x dx'$$
$$= 1 - 2 Q(k)$$

where

$$Q(x) = \int_{k}^{\infty} \frac{1}{\sqrt{2\pi}} e^{-\frac{1}{2}x^2} dx$$

Therefore,

$$E[q^{2}] = P(A) E[q^{2}|A] + (1 - P(A)) E[q^{2}|\overline{A}]$$
$$= (1 - 2Q(k)) E[q^{2}|A] + 2Q(k) E[q^{2}|\overline{A}]$$

If x is in the uniform zone $(-k\sigma_x, k\sigma_x)$, i.e. given A,

$$q \sim \mathrm{U}\left(-\frac{\Delta}{2}, \frac{\Delta}{2}\right)$$

Therefore,

$$E\left[q^2\middle|A\right] = \frac{\Delta^2}{12}$$

$$= \frac{\left(\frac{2k\sigma_x}{M}\right)^2}{12}$$

$$= \frac{k^2\sigma_x^2}{3M^2}$$

If x is outside the uniform zone, i.e. given \overline{A} ,

$$q = \begin{cases} x - k\sigma_x & ; & x > \sigma_x \\ x + k\sigma_x & ; & x < \sigma_x \end{cases}$$

Therefore,

$$\mathrm{E}\left[q^2\Big|\overline{A}\right] = \int_{\overline{A}} q^2 \,\mathrm{f}_{x|\overline{A}} \,\mathrm{d}x$$

Also,

$$\mathbf{f}_{x|\overline{A}} = \begin{cases} \frac{\mathbf{f}_x(x)}{\mathbf{P}(\overline{A})} & ; & |x| > k\sigma_x \\ 0 & ; & |x| > k\sigma_x \end{cases}$$

Therefore,

$$E\left[q^{2}\middle|\overline{A}\right] = \int_{-\infty}^{-k\sigma_{x}} (x+k\sigma_{x})^{2} f_{x|\overline{A}}\left(x\middle|\overline{A}\right) dx + \int_{-k\sigma_{x}}^{\infty} (x-k\sigma_{x})^{2} f_{x|\overline{A}}\left(x\middle|\overline{A}\right) dx$$

$$= 2 \int_{k\sigma_{x}}^{\infty} (x-k\sigma_{x})^{2} \frac{f_{X}(x)}{2 Q(k)} dx$$

$$= \frac{1}{Q(k)} \int_{k\sigma}^{\infty} (x-k\sigma_{x})^{2} \frac{1}{\sqrt{2\pi}\sigma_{x}} e^{-\frac{1}{2}\frac{x^{2}}{\sigma_{x}^{2}}} dx$$

Let

$$x' = \frac{x}{\sigma_x}$$

Therefore,

$$x = x'\sigma_x$$
$$\therefore dx = dx'\sigma_x$$

Therefore,

$$E\left[q^2\middle|\overline{A}\right] = \frac{1}{Q(k)\sqrt{2\pi}} \int_k^\infty (x'\sigma_x - k\sigma_x)^2 \frac{1}{\sigma_x} e^{-\frac{1}{2}x'^2} dx'\sigma_x$$
$$= \frac{\sigma_x^2}{Q(k)\sqrt{2\pi}} \int_k^\infty (x'-k)^2 e^{-\frac{1}{2}x'^2} dx$$

Therefore, integrating by parts,

$$E\left[q^{2}\middle|\overline{A}\right] = \frac{1}{Q(k)\sqrt{2\pi}} \left(ke^{-\frac{1}{2}k^{2}} + Q(k)\sqrt{2\pi} - 2ke^{-\frac{1}{2}k^{2}} + k^{2}Q(k)\sqrt{2\pi}\right)$$
$$= \sigma_{x}^{2} \left(k^{2} + 1 - \frac{k}{Q(k)\sqrt{2\pi}}e^{-\frac{1}{2}k^{2}}\right)$$

Therefore,

$$\begin{split} \mathbf{E}\left[q^{2}\right] &= \left(1 - 2\,\mathbf{Q}(k)\right)\mathbf{E}\left[q^{2}\Big|A\right] + 2\,\mathbf{Q}(k)\,\mathbf{E}\left[q^{2}\Big|\overline{A}\right] \\ &= \left(1 - 2\,\mathbf{Q}(k)\right)\frac{k^{2}\sigma_{x}^{2}}{3M^{2}} + 2\,\mathbf{Q}(k)\sigma_{x}^{2}\left(k^{2} + 1 - \frac{k}{\mathbf{Q}(k)\sqrt{2\pi}}e^{-\frac{1}{2}k^{2}}\right) \\ &= \sigma_{x}^{2}\left(\frac{k^{2}}{3M^{2}} - \frac{2k}{\sqrt{2\pi}}e^{-\frac{1}{2}k^{2}} + 2\,\mathbf{Q}(k)\left(k^{2} + 1 - \frac{k^{2}}{3M^{2}}\right)\right) \end{split}$$

As M >> k, the term $\frac{k^2}{3M^2}$ may be ignored. Also,

$$E\left[x^2\right] = \sigma_x^2$$

Therefore,

QSNR
$$\approx \frac{k^2}{3M^2} - \frac{2k}{\sqrt{2\pi}}e^{-\frac{1}{2}k^2} + 2Q(k)(k^2 + 1)$$

Therefore,

QSNR_{dB}
$$\approx -10 \log \left(\frac{k^2}{3M^2} - \frac{2k}{\sqrt{2\pi}} e^{-\frac{1}{2}k^2} + 2 Q(k) (k^2 + 1) \right)$$

Theorem 35. *If* x > 0,

$$\frac{x}{x^2+1} \frac{1}{\sqrt{2\pi}} e^{-\frac{1}{2}x^2} < Q(x) < \frac{1}{x} \frac{1}{\sqrt{2\pi}} e^{-\frac{1}{2}x^2}$$

Exercise 2.

Let

$$X \sim \text{Exp}(\lambda)$$

Consider a M level dense and uniform quantizer with

$$\Delta = \frac{k\lambda^{-1}}{M}$$

that is, the highest threshold is $k\lambda^{-1}$. Compute the QSNR.

Solution 2.

$$q = x_q - x$$

Therefore,

$$E[q^{2}] = E[q^{2}|x < k\lambda^{-1}] P(x < k\lambda^{-1}) + E[q^{2}|x > k\lambda^{-1}] P(x > k\lambda^{-1})$$
$$= \frac{\Delta^{2}}{12} F_{x}(k\lambda^{-1}) + E[q^{2}|x > k\lambda^{-1}] (1 - F_{x}(k\lambda^{-1}))$$

Also, if $x > k\lambda^{-1}$,

$$q = x_q - x$$
$$= k\lambda^{-1} \left(1 - \frac{1}{2M} \right) - x$$

Let A be the event that $x > k\lambda^{-1}$. Therefore,

$$\begin{split} \mathbf{f}_{q|A}(q|A) &= \mathbf{f}_{x|A}(x_q - q|A) \\ &= \mathbf{f}_{x|A}\left(k\lambda^{-1}\left(1 - \frac{1}{2M}\right) - q\Big|A\right) \\ &= \frac{\mathbf{f}_{x|A}\left(x = k\lambda^{-1}\left(1 - \frac{1}{2M}\right) - q \cap x > k\lambda^{-1}\right)}{\mathbf{P}\left(x > k\lambda^{-1}\right)} \\ &= \begin{cases} e^k \, \mathbf{f}_x\left(k\lambda^{-1}\left(1 - \frac{1}{2M}\right) - q\right) & ; & q < -\frac{k\lambda^{-1}}{2M} \\ 0 & ; & q > -\frac{k\lambda^{-1}}{2M} \end{cases} \\ &= \begin{cases} e^k \lambda e^{-\lambda\left(k\lambda^{-1}\left(1 - \frac{1}{2M}\right) - q\right)} & ; & q < -\frac{k\lambda^{-1}}{2M} \\ 0 & ; & q > -\frac{k\lambda^{-1}}{2M} \end{cases} \\ &= \begin{cases} \lambda e^{\frac{k}{2M}} e^{\lambda q} & ; & q < -\frac{k\lambda^{-1}}{2M} \\ 0 & ; & q > -\frac{k\lambda^{-1}}{2M} \end{cases} \\ &= \begin{cases} \lambda e^{\frac{k}{2M}} e^{\lambda q} & ; & q < -\frac{k\lambda^{-1}}{2M} \\ 0 & ; & q > -\frac{k\lambda^{-1}}{2M} \end{cases} \end{split}$$

Therefore,

$$E\left[q^2\middle|x > k\lambda^{-1}\right] = \int_{-\infty}^{-\frac{k\lambda^{-1}}{2M}} q^2 f_{q|A}(q|A) dq$$
$$= \lambda^{-2} \left(\frac{k^2}{4M^2} + \frac{k}{M} + 2\right)$$

Therefore,

$$E[q^{2}] = \frac{\Delta^{2}}{12} F_{x}(k\lambda^{-1}) + E[q^{2}|x > k\lambda^{-1}] \left(1 - F_{x}(k\lambda^{-1})\right)$$
$$= \frac{\Delta^{2}}{12} F_{x}(k\lambda^{-1}) + \lambda^{-2} \left(\frac{k^{2}}{4M^{2}} + \frac{k}{M} + 2\right) \left(1 - F_{x}(k\lambda^{-1})\right)$$

Similarly,

$$E[q] = E\left[q\middle|x < k\lambda^{-1}\right] P\left(x < k\lambda^{-1}\right) + E\left[q\middle|x > k\lambda^{-1}\right] P\left(x > k\lambda^{-1}\right)$$
$$= -e^{-k}\lambda^{-1}\left(\frac{k}{2M} + 1\right)$$

Therefore,

QSNR =
$$\frac{V(x)}{V(q)}$$

= $\frac{V(x)}{E[x^2] - E[x]^2}$

Also, for reasonable values of k,

$$E\left[q^2\right] >> E[q]^2$$

Therefore,

$$QSNR \approx \frac{-\lambda^{-2}}{E[q^2]}$$

Exercise 3.

Let X be a random variable with PDF $f_X(x)$, such that $\forall |x| > 4$,

$$f_X(x) = 0$$

Consider the quantization

$$Q(x) = \begin{cases} -4 & ; & x < -3 \\ -2 & ; & -3 \le x < -1 \\ 0 & ; & -1 \le x < 1 \\ 2 & ; & 1 \le x < 3 \\ 4 & ; & 3 \le x \end{cases}$$

Find $f_q(q)$, the PDF of the quantization error.

Solution 3.

$$f_q(q) = \sum P(X_q = x_q) f_{q|X_q}(q|x_q)$$

Let D_{x_q} be the domain of q corresponding to x_q . Therefore, the domains corresponding to all possible values of x_q are

x_q	D_{x_q}
-4	[-1, 0]
-2	[-1, 1]
0	[-1, 1]
2	[-1, 1]
4	[0, 1]

Also,
$$\forall q \in D_{x_q}$$
,

$$f_{q,x_q}(q,x_q) = f_X(q-x_q)$$

Therefore,

$$f_{q|x_q}(q|x_q) = \frac{f_{q,x_q}(q, x_q)}{P(X_q = x_q)}$$

$$= \begin{cases} \frac{f_{X(q-x_q)}}{P(X_q = x_q)} & ; & q \in D_{x_q} \\ 0 & ; & q \notin D_{x_q} \end{cases}$$

Therefore,

$$\begin{split} \mathbf{f}_q(q) &= \sum \mathbf{P}(X_q = x_q) \, \mathbf{f}_{q|X_q}(q|x_q) \\ &= \begin{cases} \mathbf{f}_X(-4-q) + \mathbf{f}_X(-2q) + \mathbf{f}_X(-q) + \mathbf{f}_X(2-q) &; \quad q \in [-1,0] \\ \mathbf{f}_X(-2-q) + \mathbf{f}_X(-q) + \mathbf{f}_X(2-q) + \mathbf{f}_X(4-q) &; \quad q \in [0,1] \\ 0 &; \quad \text{otherwise} \end{cases} \end{split}$$

Hence, the quantization error is not uniformly distributed.

Exercise 4.

Let Q be a quantizer with quantization level y, for the cell

$$R_i = [t_{i-1}, t_i]$$

Find the optimal MMSE y_i s.

Solution 4.

The MSE is

$$E[q^{2}] = E[(Q(x) - x)^{2}]$$

$$= E_{R_{i}} \left[E_{X} \left[(Q(x) - x)^{2} \middle| x \in R_{i} \right] \right]$$

$$= \sum_{i=1}^{M} P(x \in R_{i}) E[(Q(x) - x)^{2} \middle| x \in R_{i}]$$

$$= \sum_{i=1}^{M} P(x \in R_{i}) E[(y_{i} - x)^{2} \middle| x \in R_{i}]$$

$$= \sum_{i=1}^{M} P(x \in R_{i}) E[y_{1}^{2} - 2xy_{i} + x^{2} \middle| x \in R_{i}]$$

$$= \sum_{i=1}^{M} P(x \in R_{i}) \left[y_{i}^{2} - 2y_{i} E[x \middle| x \in R_{i}] + E[x^{2} \middle| x \in R_{i}] \right]$$

Therefore, differentiating with respect to y_i , setting to be zero, and solving, the minimal y_i is

$$y_i = \mathbb{E}[x|x \in R_i]$$

2 Companders

Theorem 36. A random variable x can be transformed into a random variable y distributed uniformly between 0 and 1 as

$$y = F_x(x)$$

Proof. Let y = g(x). Therefore, let

$$y_1 = g(x_1)$$
$$y_1 + \Delta y_1 = g(x_1 + \Delta x_1)$$

Therefore,

$$P(x \in (x_1, x_1 + \Delta x)) = f_x(x_1)\Delta x$$
$$= P(y \in (y_1, y_1 + \Delta y))$$
$$= f_y(y_1)\Delta y$$

Therefore,

$$f_x(x) dx = f_y(y) dy$$

$$\therefore f_y(y) = \frac{1}{\left|\frac{dy}{dx}\right|} f_x(x)$$

$$= \frac{1}{\left|g'(x)\right|} f_x(x)$$

In particular, let

$$g(x) = F_x(x)$$

Therefore,

$$g'(x) = f_x(x)$$

Therefore,

$$f_y(y) = 1$$

Hence,

$$y \sim U(0, 1)$$

2.1 μ Law

Definition 22 (μ Law). Let x be a random variable bounded by ± 1 . Let

$$y = g(x)$$

$$= sign(x) \frac{\ln (1 + \mu |x|)}{\ln (1 + \mu)}$$

where $\mu \in (0, 255]$.

Then, y is said to be obtained by transformation of x with the μ law. Hence, the transformation function g(x) is as in Figure 2.

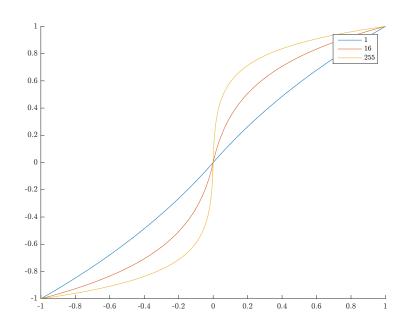


Figure 2: Transformation Function for μ Law

Theorem 37. Let y be a random variable obtained by transformation of x with Definition 22.

Let y be quantized by uniform M level quantizer. Then,

$$E[q^2] = \frac{\ln^2(1+\mu)}{3\mu^2M^2} \left(1 + 2\mu E[|x|] + \mu^2 E[x^2]\right)$$

Proof.

$$\frac{\Delta y}{\Delta x} = g'(x_1)$$

Therefore,

$$\Delta x_m = \frac{\Delta y_m}{g'(x_m)}$$
$$= \frac{\frac{2}{M}}{g'(x_m)}$$

Therefore,

$$E\left[q^{2} \middle| x \in I_{m}\right] = \frac{\Delta x_{m}^{2}}{12}$$
$$= \frac{4}{12M^{2}g'(x_{m})^{2}}$$

Therefore,

$$E[q^{2}] = \sum_{m=1}^{M} E\left[q_{x}^{2} \middle| x \in I_{m}\right] P(I_{m})$$

$$E[q^{2}] = \sum_{m=1}^{M} E\left[q_{x}^{2} \middle| x \in I_{m}\right] f_{x}(x_{m}) \Delta x_{m}$$

$$= \sum_{m=1}^{M} \frac{1}{3M^{2}g'(x_{m})^{2}} f_{x}(x_{m}) \Delta x_{m}$$

Therefore, as $\Delta x_m \to 0$,

$$E[q^{2}] = \int_{-1}^{1} \frac{1}{3M^{2}g'(x)^{2}} f_{x}(x) dx$$
$$= \frac{1}{3M^{2}} E\left[\frac{1}{g'(x)^{2}}\right]$$

Also,

$$g(x) = \begin{cases} \frac{\ln(1+\mu x)}{\ln(1+\mu)} & ; & x > 0\\ -\frac{\ln(1+\mu x)}{\ln(1+\mu)} & ; & x < 0 \end{cases}$$
$$\therefore g'(x) = \begin{cases} \frac{\mu}{\ln(1+\mu)} \frac{1}{1+\mu x} & ; & x > 0\\ \frac{\mu}{\ln(1+\mu)} \frac{1}{1-\mu x} & ; & x < 0 \end{cases}$$

Therefore,

$$E[q^{2}] = \frac{1}{3M^{2}} E\left[\frac{1}{g'(x)^{2}}\right]$$

$$= \frac{1}{3M^{2}} E\left[\left(\frac{\ln(1+\mu)}{\mu} \left(1+\mu|x|\right)^{2}\right)\right]$$

$$= \frac{\ln^{2}(1+\mu)}{3\mu^{2}M^{2}} E\left[\left(1+\mu|x|\right)^{2}\right]$$

$$= \frac{\ln^{2}(1+\mu)}{3\mu^{2}M^{2}} \left(1+2\mu E\left[|x|\right]+\mu^{2} E\left[x^{2}\right]\right)$$

2.2 *A* Law

Definition 23 (A Law). Let x be a random variable bounded by ± 1 . Let

$$y = g(x)$$

$$= \begin{cases} \frac{A|x|}{1 + \log A} \operatorname{sign}(x) & ; & |x| < \frac{1}{A} \\ \frac{1 + \log(A|x|)}{1 + \log A} \operatorname{sign}(x) & ; & |x| > \frac{1}{A} \end{cases}$$

where A > 1.

Then, y is said to be obtained by transformation of x with the A law. Hence, the transformation function g(x) is as in Figure 3.

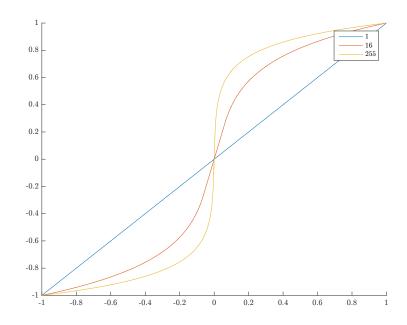


Figure 3: Transformation Function for A Law

3 Max-Lloyd Algorithm

Algorithm 1 Max-Lloyd Algorithm

Require: f(x), the PDF of x, such that f(x) = 0 for $x \notin [\alpha, \beta]$.

Ensure: Dense quantization cells defined by x_i s.

1: Determine arbitrary adjacent quantization cells, with boundaries at b_m , for $0 \le m \le M$, and

$$\alpha = b_0$$
$$\beta = b_M$$

2: For each cell $[b_{m-1}, b_m]$, compute

$$x_m = \operatorname{E}\left[x \middle| x \in [b_{m-1}, b_m]\right]$$

$$= \int_{b_{m-1}}^{b_m} x f(x) dx$$

$$= \int_{b_{m-1}}^{b_m} f(x) dx$$

3: Redetermine all b_m s, such that

$$b_m = \frac{x_m + x_{m+1}}{2}$$

4: Repeat steps 2 and 3 till the x_m s and b_m s converge.

4 Amplitude Shift Keying

Definition 24 (Amplitude shift keying). Let b_n be the *n*th bit of the data to be transmitted ⁷ Consider the information signal

$$s(t) = \sum_{n=-\infty}^{\infty} b_n p(t - nT)$$

⁷This data may be possibly obtained by quantization of an analogue signal.

where p(t) is a pulse chosen according to the requirements. ⁸ Then, the information signal s(t) is said to be obtained by amplitude shift keying or ASK.

Definition 25 (M-ary ASK). Consider the information signal

$$s(t) = \sum_{n=-\infty}^{\infty} c_n p(t - nT)$$

where $0 \le c_n < 2^M$ for each n. Hence, each 'data point' in the information signal is represented by one of 2^M levels. Then, the information signal s(t) is said to be obtained by M-ary ASK.

4.1 Gray Coding

Definition 26 (Gray coding). A coding of 2^M levels ordered in a way that the difference between any two adjacent levels is of exactly one bit is called a Gray coding.

Consider M-ary ASK with consecutive levels defined by standard binary coding e.g. 8 binary levels ordered as (000,001,010,011,100,101,110,111). If a level is misinterpreted by the receiver as one of the adjacent levels, there may be an error of multiple bits. For example, if 011 is misinterpreted as 110, the error is of three bits. Hence, small noise can result in a very large error. This problem can be reduced by using Gray coding, and the error is limited to a single bit.

5 Inter Symbol Interference

Definition 27 (Inter symbol interference). The interference of a pulse corresponding to a 'data point' at one point in time with that corresponding to another is called inter symbol interference or ISI.

Definition 28 (NISI condition). The no-ISI condition is

$$p(t) = 0$$

for all t = nT, except at n = 0, and

$$p(0) = 1$$

⁸For example, if a rectangular pulse is used, a limited number of channels can be used as the rectangular pulse has a large bandwidth. Alternatively, if a sinc is used as a pulse, a higher number of channels can be used as the bandwidth is smaller.

Equivalently, $\forall \omega$,

$$\sum_{k=-\infty}^{\infty} P\left(\omega - \frac{2\pi}{T}k\right) = T$$

Exercise 5.

Consider a signal s_n , represented by four levels, i.e. two bits. The received signal is

$$\widehat{s_n} = \begin{cases} s_n & ; & \text{with probability } 1 - p \\ (s_n + 1) \mod 4 & ; & \text{with probability } p \end{cases}$$

that is, the information is received as sent with probability 1 - p, and is received with error of one level with probability p.

- 1. Find the probability of error if the levels are determined by standard binary coding.
- 2. Find the probability of error if the levels are determined by Gray coding.

Solution 5.

1. Let P_{b_i} be the probability of error in the *i*th bit. Therefore, let $P(b_i|s_j)$ be the probability of error in the *i*th bit, given the value of the *j*th symbol was transmitted. Therefore, the total probability of error in the information is

$$P_b = \frac{1}{k} \sum_{i=0}^{k-1} P_{b_i}$$

$$= \frac{1}{k} \sum_{i=0}^{k-1} \sum_{j=0}^{3} P(b_i | s_j) P(s_j)$$

$$= \frac{1}{k} \sum_{i=0}^{k-1} \left(\frac{1}{4} \sum_{j=0}^{3} P(b_i | s_j) \right)$$

$$= \frac{1}{2} \left(\frac{1}{4} \left((p+p+p+p) + (0+p+0+p) \right) \right)$$

$$= \frac{3p}{4}$$

2. Let P_{b_i} be the probability of error in the *i*th bit. Therefore, let $P(b_i|s_j)$ be the probability of error in the *i*th bit, given the value of the *j*th symbol was

transmitted. Therefore, the total probability of error in the information is

$$P_b = \frac{1}{k} \sum_{i=0}^{k-1} P_{b_i}$$

$$= \frac{1}{k} \sum_{i=0}^{k-1} \sum_{j=0}^{3} P(b_i | s_j) P(s_j)$$

$$= \frac{1}{k} \sum_{i=0}^{k-1} \left(\frac{1}{4} \sum_{j=0}^{3} P(b_i | s_j) \right)$$

$$= \frac{1}{2} \left(\frac{1}{4} \left((p+0+p+0) + (0+p+0+p) \right) \right)$$

$$= \frac{p}{2}$$

Exercise 6.

Consider a information signal $\sum_{n\in\mathbb{Z}} a_n \delta(t-nT)$ where $a_n \in \{-1,1\}$. This signal is passed through a LTI system with transfer function

$$\widetilde{H}(f) = \begin{cases} 1 - T|f| & ; & |f| \le \frac{1}{T} \\ 0 & ; & \text{otherwise} \end{cases}$$

to obtain y(t). y(t) is then sampled at multiples of t_n , and passed through a slicer

$$q(x) = sign(x)$$

to obtain $\widehat{a_n}$.

1. Compute h(t). Prove that $\forall n \neq 0, n \in \mathbb{Z}$,

$$h(nT) = 0$$

- 2. Does the NISI condition hold for $t_n = nT + \frac{T}{4}$?
- 3. For the above sampling times, is it possible that an estimation error of $\widehat{a_n}$ occurs due to ISI?

Solution 6.

1. $\widetilde{H}(f)$ is a triangular function, and hence is a convolution of two rectangular functions with width $\frac{1}{T}$, and height \sqrt{T} . Therefore,

$$h(t) = \mathcal{F}^{-1} \left\{ \widetilde{H}(f) \right\}$$
$$= \left(\frac{1}{\sqrt{T}} \operatorname{sinc} \left(\frac{\pi t}{T} \right) \right)^{2}$$
$$= \frac{1}{T} \operatorname{sinc}^{2} \left(\frac{\pi t}{T} \right)$$

2.

$$h(t)\Big|_{t=t_n} = h\left(nT + \frac{T}{4}\right)$$
$$= \frac{1}{T}\operatorname{sinc}^2\left(\frac{\pi}{T}\left(nT + \frac{T}{4}\right)\right)$$
$$\neq 0$$

3. Without loss of generality, for a_0 , and

$$t_0 = \frac{T}{4}$$

the continuous time signal is

$$y\left(\frac{T}{4}\right) = \sum_{n \in \mathbb{Z}} a_n h\left(t - nT + \frac{T}{4}\right)\Big|_{t = \frac{T}{4}}$$
$$= a_0 h\left(\frac{T}{4}\right) + \sum_{n \in \mathbb{Z} \setminus \{0\}} a_n h\left(t - nT + \frac{T}{4}\right)$$

Hence, in the worst case ⁹, i.e. for $a_0 = 1$ and all other $a_i = -1$ for $i \neq 0$,

$$h\left(t - nT + \frac{T}{4}\right) = \frac{1}{T}\operatorname{sinc}^{2}\left(\frac{\pi}{T}\left(nT + \frac{T}{4}\right)\right)$$

Therefore, an error will occur if and only if

$$y\left(\frac{T}{4}\right) < 0$$

 $^{{}^{9}}$ If y(t) is higher than intended, there would be no error as the signal would be corrected to be 1 due to the slicer. Hence, the worst case is when only a_0 is 1, and all others are -1.

Hence, solving,

$$h\left(nT + \frac{T}{4}\right) > 0$$

Therefore, there be no error due to ISI.

6 The Raised Cosine Family of Pulses

Definition 29 (The raised cosine family of pulses). The set of all p(t), such that

$$P(\omega) = \begin{cases} 1 & ; & |\omega| \le \pi - \Delta \\ g(\omega) & ; & \pi - \Delta < |\omega| < \pi + \Delta \\ 0 & ; & |\omega| \ge \pi + \Delta \end{cases}$$

where

$$g(\omega) = \frac{1}{2} \left(1 - \sin \left(\frac{|\omega| - \pi}{\Delta} \frac{\pi}{2} \right) \right)$$

and

$$\Delta = \rho \pi$$

is called the raised cosine family of pulses. $\rho \in [0,1]$ is called the rolloff factor of the pulse, chosen according to the requirements. Hence, the frequency domain representation of the pulse is as in Figure 4.

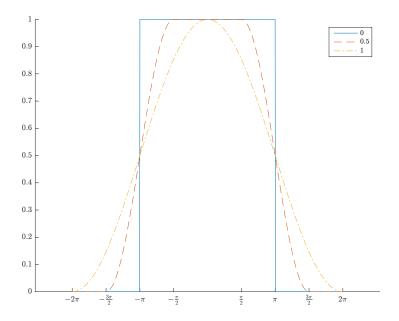


Figure 4: Raised Cosine Pulses in Frequency Domain

Theorem 38. The time domain representation of a raised cosine pulse is

$$p(t) = \operatorname{sinc}\left(\pi \frac{t}{T}\right) \frac{\cos\left(\rho \pi \frac{t}{T}\right)}{1 - \left(\frac{2t\rho}{T}\right)^2}$$

where $\rho \in [0,1]$ is the rolloff factor of the pulse. Hence, the time domain representation of the pulse is as in Figure 5.

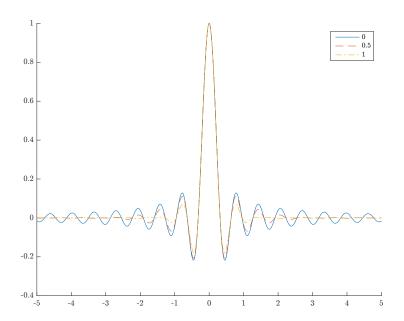


Figure 5: Raised Cosine Pulses in Time Domain

Proof. For simplicity, let T = 1. Let

$$R(\omega) = \operatorname{rect}\left(\frac{w}{2\pi}\right)$$

$$Q(\omega) = \begin{cases} c\cos\left(\frac{\omega}{\Delta}\frac{\pi}{2}\right) & ; & |\omega| < \Delta\\ 0 & ; & \text{otherwise} \end{cases}$$

Therefore,

$$P(\omega) = \frac{1}{2\pi}R(\omega) * Q(\omega)$$

Therefore,

$$\begin{split} r(t) &= \mathrm{sinc}(\pi t) \\ q(t) &= \frac{1}{2\pi} \int\limits_{-\infty}^{\infty} Q(\omega) e^{j\omega t} \, \mathrm{d}\omega \\ &= \frac{1}{2\pi} \int\limits_{-\Delta}^{\Delta} \frac{\pi^2}{2\Delta} \cos\left(\frac{\omega}{\Delta} \frac{\pi}{2}\right) e^{j\omega t} \, \mathrm{d}\omega \\ &= \frac{\pi}{4\Delta} \int\limits_{-\Delta}^{\Delta} \cos\left(\frac{\omega}{\Delta} \frac{\pi}{2}\right) \left(\cos(\omega t) + j \sin(\omega t)\right) \, \mathrm{d}\omega \\ &= \frac{\pi}{4\Delta} \int\limits_{-\Delta}^{\Delta} \cos\left(\frac{\omega}{\Delta} \frac{\pi}{2}\right) \cos(\omega t) \, \mathrm{d}\omega \\ &= \frac{\pi}{4\Delta} \int\limits_{-\Delta}^{\Delta} \frac{1}{2} \left(\cos\left(\omega \left(\frac{\pi}{2\Delta} + t\right)\right) + \cos\left(\omega \left(\frac{\pi}{2\Delta} - t\right)\right)\right) \, \mathrm{d}\omega \\ &= \frac{\pi}{4\Delta} \int\limits_{0}^{\Delta} \left(\cos\left(\omega \left(\frac{\pi}{2\Delta} + t\right)\right) + \cos\left(\omega \left(\frac{\pi}{2\Delta} - t\right)\right)\right) \, \mathrm{d}\omega \\ &= \frac{\pi}{4\Delta} \left(\frac{\sin\left(\omega \left(\frac{\pi}{2\Delta} + t\right)\right)}{\frac{\pi}{2\Delta} + t} + \frac{\sin\left(\omega \left(\frac{\pi}{2\Delta} - t\right)\right)}{\frac{\pi}{2\Delta} - t}\right) \right|_{0}^{\Delta} \\ &= \frac{\pi}{4\Delta} \left(\frac{\sin\left(t\Delta + \frac{\pi}{2}\right)}{\frac{\pi}{2\Delta} + t} + \frac{\sin\left(-t\Delta + \frac{\pi}{2}\right)}{\frac{\pi}{2\Delta} - t}\right) \\ &= \frac{\pi}{4\Delta} \left(\frac{1}{\frac{\pi}{2\Delta} + t} + \frac{1}{\frac{\pi}{2\Delta} - t}\right) \cos(t\Delta) \\ &= \frac{\cos(t\Delta)}{1 - \left(\frac{2t\Delta}{2}\right)^2} \end{split}$$

Therefore,

$$P(\omega) = \frac{1}{2\pi}R(\omega) * Q(\omega)$$

Hence,

$$p(t) = r(t)q(t)$$

$$= \operatorname{sinc}(\pi t) \frac{\cos(t\Delta)}{1 - \left(\frac{2t\Delta}{\pi}\right)^2}$$

Similarly, for a general T,

$$p(t) = \operatorname{sinc}\left(\pi \frac{t}{T}\right) \frac{\cos\left(\rho \pi \frac{t}{T}\right)}{1 - \left(\frac{2t\rho}{T}\right)^2}$$

Exercise 7.

Let

$$p(t) = c(t)r(t)$$

where

$$R(\omega) = \operatorname{rect}\left(\frac{\omega}{2\pi}\right)$$

$$= \begin{cases} 1 & ; & |\omega| \le \pi \\ 0 & ; & \text{otherwise} \end{cases}$$

$$C(\omega) = A \operatorname{tri}\left(\frac{\omega}{\Delta}\right)$$

$$= \begin{cases} A\left(1 - \frac{|\omega|}{\Delta}\right) & ; & |\omega| \le \Delta \\ 0 & ; & \text{otherwise} \end{cases}$$

- 1. Find $P(\omega)$.
- 2. Given

$$\int_{-\infty}^{\infty} c(t) \, \mathrm{d}t = \frac{2\pi}{\Delta}$$

find A.

3. Does the NISI condition hold for the above?

4. Find p(t) for $\Delta \to 0$.

Solution 7.

1.

$$\begin{split} P(\omega) &= \mathcal{F} \left\{ p(t) \right\} \\ &= \mathcal{F} \left\{ c(t)r(t) \right\} \\ &= \frac{1}{2\pi} \, \mathcal{F} \left\{ c(t) \right\} * \, \mathcal{F} \left\{ r(t) \right\} \\ &= \frac{1}{2\pi} C(\omega) * \, R(\omega) \\ &= \frac{1}{2\pi} \int_{-\infty}^{\infty} R(\sigma)C(\omega - \sigma) \, \mathrm{d}\sigma \\ &= \frac{1}{2\pi} \int_{-\infty}^{\infty} R(\sigma)C(\sigma - \omega) \, \mathrm{d}\sigma \\ &= \left\{ \begin{array}{l} 0 & ; \quad \omega < -\pi - \Delta \\ \frac{A\Delta}{4\pi} \left(1 + \frac{\omega + \pi}{\Delta} \right)^2 & ; \quad -\pi - \Delta < \omega \leq -\pi \\ \frac{A\Delta}{4\pi} \left(2 - \left(1 - \frac{\omega + \pi}{\Delta} \right)^2 \right) & ; \quad -\pi < \omega < -\pi + \Delta \\ \frac{A\Delta}{4\pi} \left(2 - \left(1 + \frac{\omega + \pi}{\Delta} \right)^2 \right) & ; \quad \pi - \Delta < \omega < \pi - \Delta \\ \frac{A\Delta}{4\pi} \left(1 - \frac{\omega + \pi}{\Delta} \right)^2 & ; \quad \pi < \Delta < \omega < \pi + \Delta \\ 0 & ; \quad \pi + \Delta < \omega \\ \end{array} \end{split}$$

2.

$$C(\omega) = \int_{-\infty}^{\infty} c(t)e^{-j\omega t} dt$$
$$\therefore C(0) = \int_{-\infty}^{\infty} c(t) dt$$
$$\therefore A = \frac{2\pi}{\Delta}$$

3.

$$p(t) = c(t)r(t)$$
$$= \operatorname{sinc}(\pi t)\operatorname{sinc}^{2}\left(\frac{\Delta t}{2}\right)$$

Therefore, $\forall n \neq 0$,

$$p(nT) = \operatorname{sinc}(n\pi T)\operatorname{sinc}^{2}\left(\frac{n\Delta T}{2}\right)$$
$$= 0$$

4.

$$\lim_{\Delta \to 0} C(\omega) = 2\pi \delta(\omega)$$

Therefore,

$$P(\omega) = \frac{1}{2\pi} R(\omega) * C(\omega)$$
$$= \frac{1}{2\pi} R(\omega) * (2\pi\delta(\omega))$$
$$= R(\omega)$$

This is also obvious as a delta in frequency corresponds to a constant 1 in time. Similarly, as the triangle in frequency converges to a delta, $P(\omega)$ converges a rectangle. Therefore,

$$p(t) = r(t)$$
$$= \operatorname{sinc}(\pi t)$$

Part V

Matched Filters

1 Single Pulse with White Noise

Consider an information signal

$$s(t) = \sum_{n=-\infty}^{\infty} b_n p(t - nT)$$

Let the received signal be

$$x(t) = s(t) + v(t)$$

where v(t) is zero mean Gaussian white noise.

For simplicity, let n = 1. Therefore,

$$x(t) = b_0 p(t) + v(t)$$

Hence, based on x(t), the receiver must decide if b_0 is 0 or 1. Consider the hypotheses

$$H_0:b_0=0$$

$$H_1: b_0 = 1$$

Equivalently,

$$H_0: x(t) = v(t)$$

$$H_1: x(t) = p(t) + v(t)$$

As v(t) is zero mean Gaussian white noise,

$$E[v(t)] = 0$$

$$E[v(t+\tau)v(t)] = \frac{N_0}{2}\delta(t)$$

$$S_{vv}(\omega) = \frac{N_0}{2}$$

Therefore, let y(t) be the signal obtained by passing x(t) through a LTI system with $h(\tau)$, and let z be a sample of this y(t) taken at t_0 . Let the critical value be λ , such that H_0 is accepted if and only

$$z < \lambda$$

and H_1 is accepted if and only if

$$z > \lambda$$

Hence, the filter is as in

$$x(t), p(t), v(t) \longrightarrow \widetilde{h}(\tau) = \widetilde{p}^* \left(\widetilde{t_0} - \tau\right) \longrightarrow \mathcal{Y} \longrightarrow y(t_0) \geq \lambda$$

Figure 6: Matched Filter for a Single Pulse with White Noise

Under either of the hypotheses, the variance of y(t) is

$$\sigma^2 = \frac{N_0}{2} \int_{-\infty}^{\infty} |h(\tau)|^2 dt$$

Under H_0 , the expectation of y(t) is

$$E[y(t)] = 0$$

Under H_1 , the expectation of y(t) is

$$\mu = \mathbf{E} [y(t)]$$
$$= \int_{-\infty}^{\infty} h(\tau) p(t_0 0 \tau) d\tau$$

Hence, under H_0 ,

$$z = \mathcal{N}\left(0, \sigma^2\right)$$

and under H_1 ,

$$z = N(\mu, \sigma^2)$$

Hence, the critical value should be

$$\lambda = \frac{\mu}{2}$$

Therefore, the probability of a type 1 error 10 is

$$P\left(z > \lambda \middle| H_0\right) = \int_{\lambda}^{\infty} \frac{1}{\sqrt{2\pi}\sigma} e^{-\frac{1}{2}\frac{z^2}{\sigma^2}} dz$$
$$= Q\left(\frac{\lambda}{\sigma}\right)$$
$$= Q\left(\frac{\mu}{2\sigma}\right)$$

Hence, in order to minimize the probability of a type 1 error, $\frac{|\mu|^2}{\sigma^2}$ should be maximized. Hence, by the Cauchy-Schwartz inequality for integrals over complex valued functions ¹¹,

$$\left| \int_{-\infty}^{\infty} h(\tau) p(t_0 - \tau) d\tau \right|^2 \leq \int_{-\infty}^{\infty} |h(\tau)|^2 dt \int_{-\infty}^{\infty} |p^*(t_0 - \tau)|^2 d\tau$$

Hence, for the equality to be satisfied, i.e. for minimal error, the LTI system must be chosen such that

$$h(\tau) = p^*(t_0 - \tau)$$

Furthermore, t_0 must be chosen such $h(\tau)$ is causal. Let t_f be the time at which the pulse p(t) ends. Hence, for $h(\tau)$ to be causal,

$$t_0 > t_f$$

Hence, the optimal filter, matched to the pulse, is given by

$$h_{\text{optimal}}(\tau) = p^*(t_f - \tau)$$

 $H_{\text{optimal}}(\omega) = e^{-j\omega \tilde{t_0}} \widetilde{P}^*(\omega)$

¹⁰False positive

$$\left| \int_{a}^{b} w_{1}(t)w_{2}^{*}(t) dt \right|^{2} \leq \int_{a}^{b} \left| w_{1}(t) \right|^{2} dt \int_{a}^{b} \left| w_{2}(t) \right|^{2} dt$$

and the equality holds if and only if $\exists \rho, \theta$, such that $w_2 = \rho e^{j\theta} w_1$.

2 Single Pulse with Coloured Noise

Theorem 39 (Paley-Wiener Theorem). If $S_{vv}(\omega)$ is positive and bounded for all ω , then there exists a stable and causal system $G(\omega)$ with a stable and causal inverse, such that

$$S_{vv}(\omega) = G(\omega)G^*(\omega)$$
$$= |G(\omega)|^2$$

A matched filter for a single pulse, affected by coloured noise, can be implemented using a matched filter for white noise, as in Figure 7.

$$x(t), p(t), v(t) \xrightarrow{\frac{1}{G(\omega)}} \underset{\text{whitening filter}}{\underbrace{\frac{\widetilde{x}(t)}{\widetilde{p}(t)}}} \underbrace{\widetilde{x}(t)}_{\widetilde{p}(t)} \underbrace{\widetilde{p}(t)}_{\widetilde{v}(t)} \underbrace{\widetilde{h}(\tau) = \widetilde{p}^*\left(\widetilde{t_0} - \tau\right)}_{\widetilde{w}(t)} \xrightarrow{\widetilde{t_0}} \underbrace{\widetilde{t_0}}_{\widetilde{v}(t)} \geqslant \widetilde{\lambda}$$

Figure 7: Matched Filter for Coloured Noise Implemented Using a Matched Filter for White Noise

3 Multiple Pluses with White Noise

Theorem 40. For a information signal

$$s(t) = \sum_{n=-\infty}^{\infty} b_n p(t - nT)$$

$$\overline{H}(\omega) = H_T(\omega)H_R(\omega)$$

$$= P(\omega)e^{-j\omega t_0}p^*(\omega)$$

$$= e^{-j\omega t_0} |P(\omega)|^2$$

Hence, let

$$R(\omega) = |P(\omega)|^2$$

Therefore,

$$\overline{s}(t) = \sum_{n = -\infty}^{\infty} b_n r(t - nT)$$

Hence, in order to have no ISI, $|P(\omega)|^2$ must satisfy the NISI condition. Hence, a raised cosine signals cannot be used, and root raised cosine pulses must be used.

4 Single Pulse with Non-binary Levels

Let H_i where $0 \le i \le m-1$ be the hypotheses

$$b_i = l_i$$

Therefore,

$$E\left[y(t_0)\middle|H_m\right] = \int_{-\infty}^{\infty} h(\tau)l_m p(t_0 - \tau) d\tau$$
$$= l_m \int_{-\infty}^{\infty} h(\tau)p(t_0 - \tau) d\tau$$

Let

$$\mu = \int_{-\infty}^{\infty} h(\tau) p(t_0 - \tau) \, d\tau$$

Therefore,

$$\mathbb{E}\left[y(t_0)\Big|H_m\right] = l_m\mu$$

Similarly,

$$V\left(y(t_0)\middle|H_m\right) = \sigma^2$$

$$= \frac{N_0}{2} \int_0^\infty |h(\tau)|^2 d\tau$$

Therefore, as for the case with binary levels, in order to minimize the probability of a type 1 error, $\frac{|\mu|^2}{\sigma^2}$ should should be maximized. Hence, the matched filter is the same as for the case with binary levels, with the comparison with the threshold λ replaced by approximation to the nearest $l_i\mu$.

5 Quadrature Phase Shift Keying

Consider a complex modulated signal

$$s_{\rm RF}(t) = s(t)\cos(\omega_c t)$$
$$= \Re\left\{s(t)e^{j\omega_c t}\right\}$$

where s(t) is the information signal, and ω_c is the carrier frequency. Hence, assuming zero noise, the received signal is

$$x_{RF}(t) = s_{RF}(t)$$

$$= \Re \left\{ s(t)e^{j\omega_c t} \right\}$$

$$= \frac{1}{2}s(t)e^{j\omega_c t} + \frac{1}{2}s^*(t)e^{-j\omega_c t}$$

Let

$$\widetilde{y}(t) = 2e^{-j\omega_c t} x_{RF}(t)$$
$$= s(t) + s(t)e^{-2j\omega_c t}$$

Hence, s(t) can be reconstructed from y(t) by applying a LPF with cutoff frequency less than $2\omega_c$.

This complex multiplication of x(t) with $2e^{-j\omega_c t}$ can be implemented by splitting $2e^{-j\omega_c t}$ as

$$2e^{-j\omega_c t} = 2\cos(\omega_c t) - j\left(2\sin(\omega_c t)\right)$$

and then multiplying x(t) separately by the two terms, and treating the first product as the real part, and the second as the imaginary part. Hence, s(t) can be reconstructed as in Figure 8.

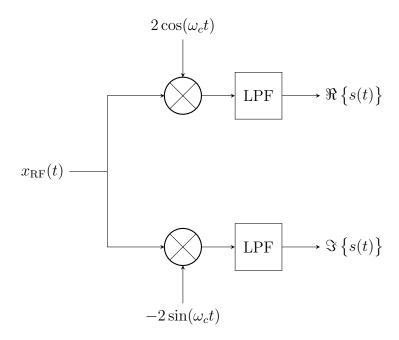


Figure 8: Reconstruction of Complex Valued Signal Implemented by Separately Treating Real and Imaginary Parts

Hence, as it is possible to use a complex valued information signal, the coding levels can occupy complex values, i.e. for example, the levels 0 to 3 can be represented by $\pm\sqrt{0.5}\pm\sqrt{0.5}$. Hence, the levels are more loosely packed in QPSK, in comparison with ASK, as in Figure 9.

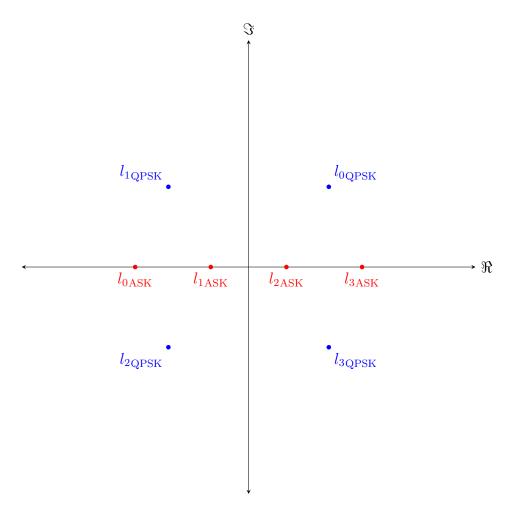
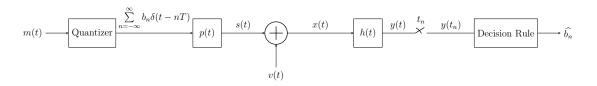


Figure 9: Comparison of QPSK and ASK Levels

Although QPSK is more immune to noise than ASK, it is sensitive to the phase shift of the transmitter. That is, if the transmitter works with $e^{j(\omega_c t + \varphi)}$ instead of $e^{j\omega_c t}$, the reconstructed signal will be shifted by φ with respect to the original signal.

This can be resolved by using a predetermined training sequence, known to both the transmitter and the receiver, to synchronize the phase shift.

Exercise 8.



Consider a communication scheme as shown, where

- m(t) is uniformly distributed between -1 and 1
- The quantizer is a four level MMSE quantizer with Gray coding
- v(t) is white Gaussian noise with zero mean and variance $\frac{N_0}{2}$

•

$$T = \frac{3}{2}$$

•

$$p(t) = u(t) - u(t-2)$$

1. Find

$$P(\omega) = \mathcal{F}\left\{p(t)\right\}$$

- 2. Find h(t) such that the error probability is minimal.
- 3. Given

$$m(0) = 0.11$$

 $m(T) = 0.53$
 $m(2T) = -0.41$
 $m(3T) = -0.9$
 $\widetilde{v}(t_0 + T) = 0.4$

find the estimated symbol at the receiver for m(T).

Solution 8.

1.

$$p(t) = \operatorname{rect}\left(\frac{t-1}{2}\right)$$

Therefore,

$$P(\omega) = \mathcal{F}\left\{ \operatorname{rect}\left(\frac{t-1}{2}\right) \right\}$$
$$= e^{-j\omega} \mathcal{F}\left\{ \operatorname{rect}\left(\frac{t}{2}\right) \right\}$$
$$= 2e^{-j\omega} \operatorname{sinc}(\omega)$$

2.

$$H(\omega) = e^{-jt_0\omega} P^*(\omega)$$

$$= e^{-2j\omega} 2e^{-j\omega} \operatorname{sinc}(\omega)$$

$$= 2e^{-j\omega} \operatorname{sinc}(\omega)$$

$$= P(\omega)$$

3. Let the quantization values be between 0 and 1. Therefore,

$$l_0 = 0$$

$$l_1 = \frac{1}{3}$$

$$l_2 = \frac{2}{3}$$

$$l_3 = 1$$

Therefore, according to the given values of m(nT),

$$b_0 = \frac{2}{3}$$

$$b_1 = 1$$

$$b_2 = \frac{1}{3}$$

$$b_3 = 0$$

As m(T) is obtained from

$$y(t_0 + T) = \widetilde{s}(t_0 + T) + \widetilde{v}(t_0 + T)$$

$$= \sum_{n = -\infty}^{\infty} b_n \widetilde{h}(t - nT) \Big|_{t_0 - nT} + 0.4$$

$$= \left(\frac{1}{2}b_0 + 2b_1 + \frac{1}{2}b_2\right) + 0.4$$

$$= \frac{1}{3} + 2 + \frac{1}{6} + 0.4$$

$$= 2.9$$

Therefore,

$$\widetilde{l}_{1} = \underset{l_{n} \in \left\{0, \frac{1}{3}, \frac{2}{3}, 1\right\}}{\operatorname{argmin}} \left| \mu l_{n} - \widetilde{y}(t_{0} + T) \right|$$

$$\widetilde{l}_{1} = \underset{l_{n} \in \left\{0, \frac{1}{3}, \frac{2}{3}, 1\right\}}{\operatorname{argmin}} \left| 2l_{n} - 2.9 \right|$$

$$= l_{3}$$

$$= 1$$

Therefore,

$$\tilde{s_1} = 0.75$$

6 Delta Pulse Code Modulation

Definition 30 (Delta PCM). A modulation in which the difference between the current data and the previous data is transmitted, rather than transmitting the data itself, is called delta pulse code modulation.

A naïve implementation of delta PCM is as in Figure 10 and Figure 11. However, in such an implementation, the transmitter predictor and the receiver predictor operated based on u_{n-1} and $\widetilde{u_{n-1}}$ respectively, their outputs may differ. As there is no way to fix the discrepancy between these errors, this error between the prediction errors accumulates.

This can be corrected by implementing the transmitter as in Figure 12. In such an implementation, the discrepancy can be fixed by anticipating the error between errors, and using the same inputs for the transmitter predictor as the receiver predictor.

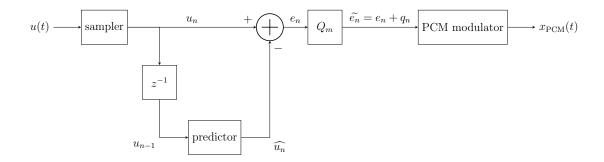


Figure 10: Conceptual Implementation of PCM Transmitter

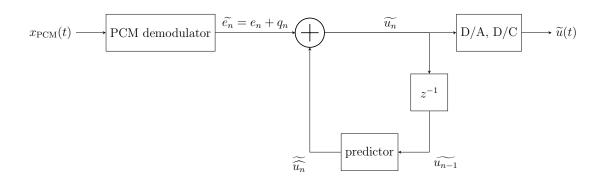


Figure 11: Implementation of PCM Receiver

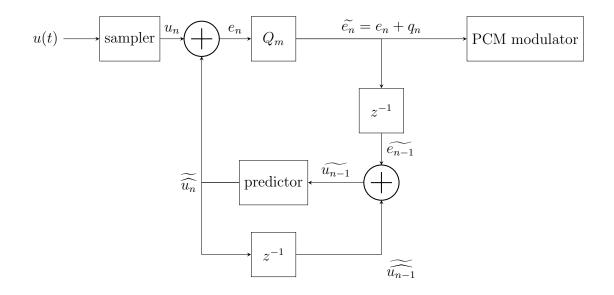


Figure 12: Practical Implementation of PCM Transmitter

7 Delta Modulation

Definition 31 (Delta modulation). A modulation scheme in which the sign of the difference between the data at a particular time and that of the previous time is transmitted is called delta modulation. Hence, a value of $+\Delta$ is transmitted if the data point is higher than the previous data point, and a value of $-\Delta$ is transmitted if it is lower.

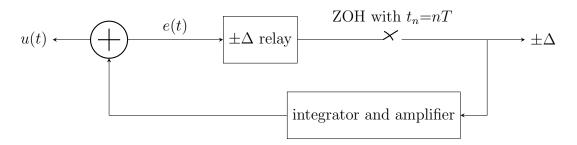


Figure 13: Delta Modulation Transmitter

As the transmitted values are $\pm \Delta$, the reconstructed signal changes by a large amount even if the real signal changes by a very small amount. This results in large oscillations in the reconstruction when the input is relatively constant. This phenomenon is called granular noise.

Also, if the real signal increases very rapidly, hence the reconstructed signal cannot keep up with the rate of increase, and results in a slower response. This phenomenon is called slope overload noise.

8 Complex Envelope Representation of Band Pass Signals

Definition 32 (Band pass signal). A signal whose spectrum is around some high frequency ω_c , such that the bandwidth B of the signal is much smaller than ω_c , is called a band pass signal.

Definition 33. A complex function

$$g(t) = x(t) + jx(t)$$

is said to be the complex envelope of a band pass signal v(t), if

$$v(t) = \Re \left\{ g(t)e^{j\omega_c t} \right\}$$
$$= \frac{1}{2}g(t)e^{j\omega_c t} + \frac{1}{2}g^*(t)e^{-j\omega_c t}$$

Hence,

$$x(t) = \Re \left\{ g(t) \right\}$$

is called the in-phase component of v(t), and

$$y(t) = \Im \left\{ g(t) \right\}$$

is called the quadrature component of v(t).

Theorem 41. A band pass signal v(t) can be represented as

$$v(t) = R(t)\cos(\omega_c t + \varphi(t))$$

where

$$R(t) = \sqrt{x^2(t) + y^2(t)}$$

$$\varphi(t) = \operatorname{atan2}(y(t), x(t))$$

Theorem 42. For a bandpass signal v(t) with complex envelope g(t),

$$V(\omega) = \frac{1}{2}G(\omega - \omega_c) + \frac{1}{2}G^* \left(-(\omega + \omega_c) \right)$$
$$\widetilde{R}_{vv}(t_1, t_2) = \frac{1}{2}\Re \left\{ \widetilde{R}_{gg}(t_1, t_2)e^{j\omega_c(t_1 - t_2)} + \widetilde{R}_{gg^*}(t_1, t_2)e^{j\omega_c(t_1 + t_2)} \right\}$$

and if g(t) is WSS and circular¹²,

$$R_{vv}(\tau) = \frac{1}{4} \left(R_{gg}(\tau) e^{j\omega_c \tau} + R_{gg^*}(\tau) e^{-j\omega_c \tau} \right)$$

and hence

$$S_{vv}(\omega) = \frac{1}{4} \left(S_{gg}(\omega - \omega_c) + S_{gg}^* \left(-(\omega + \omega_c) \right) \right)$$
$$S_{vv}(\omega) = \frac{1}{4} \left(S_{gg}(\omega - \omega_c) + S_{gg} \left(-(\omega + \omega_c) \right) \right)$$

Theorem 43. Let v(t) be a band pass signal with complex envelope g(t). If v(t) and g(t) are deterministic,

$$E_v = \frac{1}{2}E_g$$

where E_v and E_g are the energies of v(t) and g(t), respectively. If v(t) and g(t) are stochastic,

$$P_v = \frac{1}{2}P_g$$

where P_v and P_g are the powers of v(t) and g(t), respectively.

 $^{^{12}}$ See Definition 13.

Proof. If v(t) and g(t) are deterministic, the energy of v(t) is

$$E_{v} = \int_{-\infty}^{\infty} v^{2}(t) dt$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} |V(\omega)|^{2} d\omega$$

$$= \int_{-\infty}^{\infty} |\widetilde{V}(f)| df$$

$$= 2 \int_{-\infty}^{\infty} |\frac{1}{2}\widetilde{G}(f)|^{2} df$$

$$= \frac{1}{2} \int_{-\infty}^{\infty} |\widetilde{G}(f)|^{2} df$$

$$= \frac{E_{g}}{2}$$

If v(t) and g(t) are stochastic, the power of v(t) is

$$P_{v} = \operatorname{E}\left[v^{2}(t)\right]$$

$$= R_{vv}(0)$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{vv}(\omega) d\omega$$

$$= \int_{-\infty}^{\infty} \widetilde{S}_{vv}(f) df$$

$$= 2 \int_{-\infty}^{\infty} \frac{1}{4} \widetilde{S}_{gg}(f) df$$

$$= \frac{1}{2} \int_{-\infty}^{\infty} \widetilde{S}_{gg}(f) df$$

$$= \frac{1}{2} P_{g}$$

Exercise 9.

Consider a band pass signal

$$v(t) = A\sin(\omega_0 t)\cos(\omega_c t + m(t))$$

where

$$m(t) = 10\pi t$$

- 1. Find the complex envelope g(t) of v(t).
- 2. Find the in-phase and quadrature components x(t) and y(t) of v(t).
- 3. Find $G(\omega)$ and $V(\omega)$.

Solution 9.

1.

$$v(t) = \Re \left\{ A \sin(\omega_0 t) e^{j(\omega_c t + m(t))} \right\}$$
$$= \Re \left\{ \left(A \sin(\omega_0 t) e^{jm(t)} \right) e^{j\omega_c t} \right\}$$

Hence,

$$g(t) = A \sin(\omega_0 t) e^{jm(t)}$$
$$= A \sin(\omega_0 t) e^{j10\pi t}$$

2.

$$x(t) = \Re \left\{ g(t) \right\}$$

$$= \Re \left\{ \sin(\omega_0 t) e^{j10\pi t} \right\}$$

$$= A \sin(\omega_0 t) \cos(10\pi t)$$

$$y(t) = \Im \left\{ g(t) \right\}$$

$$= \Im \left\{ \sin(\omega_0 t) e^{j10\pi t} \right\}$$

$$= A \sin(\omega_0 t) \sin(10\pi t)$$

3.

$$G(\omega) = \mathcal{F} \left\{ g(t) \right\}$$

$$= \mathcal{F} \left\{ A \sin(\omega_0 t) e^{j10\pi t} \right\}$$

$$= A \mathcal{F} \left\{ \sin(\omega_0 t) e^{j10\pi t} \right\}$$

$$= A \mathcal{F} \left\{ \sin(\omega_0 t) \right\} \Big|_{\omega = 10\pi}$$

$$= \frac{A\pi}{j} \left(\delta(\omega - 10\pi - \omega_0) - \delta(\omega - 10\pi + \omega_0) \right)$$

$$= jA\omega \left(\delta(\omega - 10\pi + \omega_0) - \delta(\omega - 10\pi - \omega_0) \right)$$

Similarly,

$$V(\omega) = \mathcal{F}\left\{v(t)\right\}$$

$$= \frac{1}{2}\left(G(\omega - \omega_c) + G^*(-\omega - \omega_c)\right)$$

$$= \frac{jA\pi}{2}\left(\delta(\omega - \omega_c - 10\pi + \omega_0) - \delta(\omega - \omega_c - 10\pi - \omega_0) + \delta(-\omega - \omega_c - 10\pi - \omega_0) - \delta(-\omega - \omega_c - 10\pi + \omega_0)\right)$$

$$= \frac{jA\pi}{2}\left(\delta(\omega - (10\pi - \omega_0 + \omega_c)) - \delta(\omega - (10\pi + \omega_0 + \omega_c)) - \delta(\omega - (-10\pi + \omega_0 - \omega_c))\right)$$

$$-\delta(\omega - (-10\pi + \omega_0 - \omega_c)) + \delta(\omega - (-10\pi - \omega_0 - \omega_c))\right)$$

Exercise 10.

Let g(t) be complex random process with mean $\widetilde{\eta}_g(t)$, ACF $\widetilde{R}_{gg}(t_1, t_2)$, and pseudo ACF $\widetilde{R}_{gg^*}(t_1, t_2)$.

- 1. Compute $\widetilde{\eta}_v(t)$ and $\widetilde{R}_{vv^*}(t_1,t_2)$
- 2. Given

$$\widetilde{R}_{gg}(t) = 0$$

$$\widetilde{R}_{gg}(t_1, t_2) = \widetilde{R}_{gg}(t_1 - t_2)$$

is v(t) WSS?

Solution 10.

1.

$$\widetilde{\eta}_{v}(t) = \mathbf{E} \left[v(t) \right]$$

$$= \mathbf{E} \left[\Re \left\{ g(t)e^{j\omega_{c}t} \right\} \right]$$

$$= \mathbf{E} \left[\frac{1}{2}g(t)e^{j\omega_{c}t} + \frac{1}{2}g^{*}(t)e^{-j\omega_{c}t} \right]$$

$$= \frac{1}{2}\widetilde{\eta}_{g}(t)e^{j\omega_{c}t} + \frac{1}{2}\widetilde{\eta}_{g}^{*}(t)e^{-j\omega_{c}t}$$

$$= \Re \left\{ \widetilde{\eta}_{g}(t)e^{j\omega_{c}t} \right\}$$

Similarly,

$$\widetilde{R}_{vv^*}(t_1, t_2) = \mathbf{E} \left[\left(\frac{1}{2} g(t_1) e^{j\omega_c t_1} + \frac{1}{2} g^*(t_1) e^{-j\omega_c t_1} \right) \right]$$

$$\left(\frac{1}{2} g^*(t_2) e^{-j\omega_c t_2} + \frac{1}{2} g(t_2) e^{-j\omega_c t_2} \right)$$

$$= \frac{1}{2} \Re \left\{ \widetilde{R}_{gg}(t_1, t_2) e^{j\omega_c (t_1 + t_2)} + \widetilde{R}_{gg^*}(t_1, t_2) e^{j\omega_c (t_1 + t_2)} \right\}$$

2.

$$\begin{split} \widetilde{\eta}_v(t) &= \Re\left\{\widetilde{\eta}_g(t)e^{j\omega_c t}\right\} \\ &= 0 \\ &= \eta_v \\ \widetilde{R}_{vv}(t_1, t_2) &= \frac{1}{2}\Re\left\{\widetilde{R}_{gg}(t_1 - t_2)e^{j\omega_c(t_1 - t_2)} + \widetilde{R}_{gg^*}(t_1, t_2)e^{j\omega_c(t_1 + t_2)}\right\} \end{split}$$

Hence, as the ACF is dependent on $t_1 + t_2$, v(t) is not WSS

Part VI

Noise

1 Thermal Noise

Theorem 44. Thermal noise can be modelled as white Gaussian noise n(t) with spectral level $\frac{N_0}{2}$, i.e.

$$N(\omega) = \frac{N_0}{2}$$

where

$$N_0 = KT$$

where K is the Boltzmann constant, and T is the absolute temperature. Hence, at $290\,\mathrm{K}$.

$$N_0 = 4 \times 10^{-21} \frac{\text{W}}{\text{Hz}}$$
$$= 4 \times 10^{-18} \frac{\text{mW}}{\text{Hz}}$$
$$= 4 \times 10^{-12} \frac{\text{mW}}{\text{MHz}}$$
$$= -114 \frac{\text{dBm}}{\text{MHz}}$$

Hence, the power corresponding to thermal noise is

$$P_{noise} = N_0 B$$

Equivalently, the power is the sum of N_0 and the bandwidth, both expressed in decibels.

Exercise 11.

What is the power corresponding to a noise with bandwidth 2 MHz at 290 K?

Solution 11.

$$P = N_0 B$$
$$= -114 + 3$$
$$= -111 \, dBm$$

Exercise 12.

Given a white Gaussian thermal noise at 290 K going through a BPF with a unilateral width of

$$B = 4 \, \mathrm{MHz}$$

what is the power of the output noise?

Solution 12.

$$P_{\text{out}} = N_0 B$$

$$= \left(4 \times 10^{-12} \frac{\text{mW}}{\text{MHz}}\right) (4 \text{ MHz})$$

$$= 1.6 \times 10^{-11} \text{ mW}$$

Equivalently,

$$(P_{\text{out}})_{\text{dB}} = N_0 B$$

= $(N_0)_{\text{dB}} + B_{\text{dB}}$
= $-114 \frac{\text{dBm}}{\text{MHz}} + 6 \text{dB MHz}$
= -108dBm

2 Component Noise Model

Definition 34 (Signal to noise ratio). The signal to noise ratio is defined to be the ratio of the powers of the signal and the noise, i.e.

$$SNR = \frac{S}{N}$$

where S and N are the powers of the signal and the noise, respectively.

Definition 35 (Noise figure). A component's noise figure is defined to be the SNR degradation inflicted by the component, i.e.

$$F = \frac{\frac{S_{\text{in}}}{N_{\text{in}}}}{\frac{S_{\text{out}}}{N_{\text{out}}}}$$

where the Ss and Ns are the powers of the corresponding signals and noises.

Theorem 45. A typical RF component can be modelled as in Figure 14.

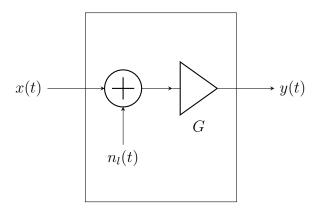


Figure 14: Model of RF component for Noise Calculations

Hence,

$$F = 1 + \frac{N_l}{N_{in}}$$
$$= 1 + \frac{T_l}{T_{in}}$$

where T_l is the equivalent temperature of the internal noise, i.e. the temperature at which the thermal noise is equal to the internal noise for the component, and T_{in} is the equivalent temperature of the input noise.

Proof.

$$S_{\text{out}} = GS_{\text{in}}$$

$$N_{\text{out}} = G(N_{\text{in}} + N_l)$$

Therefore,

$$F = \frac{\frac{S_{\text{in}}}{N_{\text{in}}}}{\frac{S_{\text{out}}}{N_{\text{out}}}}$$

$$= \frac{N_{\text{in}} + N_{l}}{N_{\text{in}}}$$

$$= 1 + \frac{N_{l}}{N_{\text{in}}}$$

$$= 1 + \frac{T_{l}}{T_{\text{in}}}$$

Therefore, let T_l be the equivalent temperature of the internal noise, i.e. the temperature at which the thermal noise is equal to the internal noise for the component. Similarly, let $T_{\rm in}$ be the equivalent temperature of the input noise. \Box

Definition 36.

$$F_0 = 1 + \frac{T_l}{T_0}$$

where

$$T_0 = 290 \,\mathrm{K}$$

Theorem 46. For passive components, i.e. with G < 1, T_l is usually assumed to be T_0 , and hence,

$$S_{out} = \frac{1}{A}$$
$$N_{out} = N_{in}$$

where A is the attenuation.

Theorem 47 (Frii's Formula). For a chain of components with parameters G_i , N_i , F_i , the equivalent parameters are

$$\overline{G} = \prod_{i=1}^{L} G_i$$

$$\overline{F} = \sum_{i=1}^{L} \frac{1}{\prod_{j=1}^{i-1} G_j} (F_i - 1)$$

3 Narrowband Noise

Theorem 48. Let n(t) be a narrowband noise obtained by passing a white Gaussian noise through band pass filter with unilateral width B. Hence, let

$$v_c(t) = n(t) \left(2\cos(\omega_0 t + \theta) \right)$$
$$v_s(t) = n(t) \left(2\sin(\omega_0 t + \theta) \right)$$

Hence, let x(t) and y(t) be the signals obtained by filtering $v_c(t)$ and $v_s(t)$, respectively, by low pass filters of widths $\frac{B}{2}$.

Then, $v_c(t)$ and $v_s(t)$ are Gaussian but not WSS, and x(t) and y(t) are Gaussian and WSS. Also, if

$$S_{nn} = P(\omega - \omega_0) + \overline{P}(\omega - \omega_0)$$

where

$$\overline{P}(\omega) = P(-\omega)$$

then

$$S_{xx} = P(\omega) + \overline{P}(\omega)$$

$$S_{yy} = P(\omega) + \overline{P}(\omega)$$

$$S_{xy} = j\left(\overline{P}(\omega) - P(\omega)\right)$$

Also,

$$E[x^{2}(t)] = E[y^{2}(t)]$$

$$= E[n^{2}(t)]$$

$$= N_{0} \int_{-\infty}^{\infty} P(\omega) d\omega$$

Part VII

Analogue Modulation Schemes

1 Double Side Band Modulation

Definition 37 (DSB modulation). A modulation scheme in which the information signal m(t) is multiplied by $A\cos(\omega_0 t + \varphi)$ where ω_0 is the carrier frequency, in order to obtain the modulated signal, is called double side band or DSB modulation. Hence,

$$v(t) = Am(t)\cos(\omega_0 t + \varphi)$$

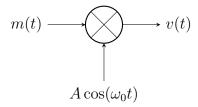


Figure 15: DSB Transmitter

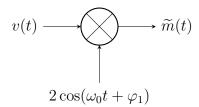


Figure 16: DSB Receiver

Theorem 49. Let m(t) be modulated with DSB modulation, such that

$$v(t) = Am(t)\cos(\omega_0 t + \varphi)$$

Then, if m(t) is deterministic,

$$V(\omega) = \frac{A}{2} \left(e^{j\varphi} M(\omega - \omega_0) + e^{-j\varphi} M(\omega + \omega_0) \right)$$

and if m(t) is stochastic, and φ uniformly distributed between 0 and 2π , and independent of m(t), then

$$R_{vv}(\tau) = \frac{A^2}{2} R_{mm}(\tau) \cos(\omega_0 \tau)$$
$$S_{vv}(\omega) = \frac{A^2}{4} \left(S_{mm}(\omega - \omega_0) + S_{mm}(\omega + \omega_0) \right)$$

Proof.

$$v(t) = Am(t)\frac{1}{2} \left(e^{j(\omega_0 t + \varphi)} + e^{-j(\omega_0 t + \varphi)} \right)$$
$$= \frac{A}{2} \left(e^{j\varphi} m(t) e^{j\omega_0 t} + e^{-j\varphi} m(t) e^{-j\omega_0 t} \right)$$

Hence, if m(t) is considered to be deterministic, with Fourier transform $M(\omega)$, and assuming φ to be deterministic,

$$V(\omega) = \frac{A}{2} \left(e^{j\varphi} M(\omega - \omega_0) + e^{-j\varphi} M(\omega + \omega_0) \right)$$

Similarly, if m(t) is considered to be a WSS process, with spectrum $S_{mm}(\omega)$ and ACF $R_{mm}(\tau)$, and assuming φ to be deterministic,

$$R_{vv}(t,\tau) = E\left[v(t+\tau)v(t)\right]$$

$$= A^{2} E\left[m(t+\tau)\cos\left(\omega_{0}(t+\tau)+\varphi\right)\right)m(t)\cos(\omega_{0}t+\varphi)$$

$$= A^{2}R_{mm}(\tau)\cos\left(\omega_{0}t+\omega_{0}\tau+\varphi\right)\cos(\omega_{0}t+\varphi)$$

$$= \frac{A^{2}}{2}R_{mm}(\tau)\left(\cos(2\omega_{0}t+\omega_{0}\tau+2\varphi)+\cos(\omega_{0}\tau)\right)$$

Hence, v(t) is cyclostationary with period $\frac{\pi}{\omega_0}$. If φ is assumed to be uniformly distributed between 0 and 2π and independent of m(t), the ACF of v(t) given φ is equal to the ACF of v(t) for a deterministic φ . Hence,

$$R_{vv}(t,\tau|\varphi) = \frac{A^2}{2} R_{mm}(\tau) \left(\cos(2\omega_0 t + \omega_0 \tau + 2\varphi) + \cos(\omega_0 \tau) \right)$$

Therefore,

$$R_{vv}(t,\tau) = \mathbb{E}\left[R_{vv}(t,\tau|\varphi)\right]$$

$$= \int_{-\infty}^{\infty} R_{vv}(t,\tau|\varphi) \,\mathrm{d}\varphi$$

$$= \frac{1}{\pi} \int_{0}^{\pi} R_{vv}(t,\tau|\varphi) \,\mathrm{d}\varphi$$

$$= \frac{1}{\pi} \int_{0}^{\pi} \frac{A^{2}}{2} R_{mm}(\tau) \left(\cos\left(2\omega_{0}t + \omega_{0}\tau + 2\varphi\right) + \cos(\omega_{0}\tau)\right) \,\mathrm{d}\varphi$$

$$= \frac{A^{2}}{2} R_{mm}(\tau) \cos(\omega_{0}\tau)$$

Hence,

$$S_{vv}(\omega) = \mathcal{F}\left\{R_{vv}(\tau)\right\}$$

$$= \mathcal{F}\left\{\frac{A^2}{2}R_{mm}(\tau)\frac{1}{2}\left(e^{j\omega_0\tau} + e^{-j\omega_0\tau}\right)\right\}$$

$$= \frac{A^2}{4}\left(S_{mm}(\omega - \omega_0) + S_{mm}(\omega + \omega_0)\right)$$

 $u(t) = v(t)2\cos(\omega_0 t + \varphi_1)$ $= Am(t)2\cos(\omega_0 t + \varphi)\cos(\omega_0 t + \varphi_1)$ $= Am(t)\left(\cos(2\omega_0 t + \varphi + \varphi_1) + \cos(\varphi_1 - \varphi)\right)$ $= Am(t)\cos(2\omega_0 t + \varphi + \varphi_1) + Am(t)\cos(\varphi_1 - \varphi)$

Hence, after passing u(t) through the LPF,

$$\widetilde{m}(t) = Am(t)\cos(\varphi_1 - \varphi)$$

Hence, the receiver reconstructs the signal with an error of $\cos(\varphi_1 - \varphi)$. This issue can be solved by sending the carrier frequency along with the modulated signal, as in amplitude modulation.

2 Amplitude Modulation

Definition 38 (Amplitude modulation). A modulation scheme in which the information signal m(t) is modulated such that

$$v(t) = A(1 + m(t))\cos(\omega_0 t + \varphi)$$

is called amplitude modulation.

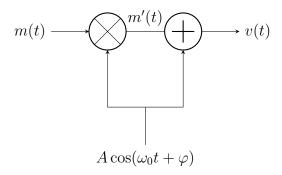


Figure 17: AM Transmitter

Let

$$m'(t) = 1 + m(t)$$

If m(t) is deterministic,

$$\mathcal{F}\left\{1+m(t)\right\}=2\pi\delta(\omega)+M(\omega)$$

Therefore,

$$V(\omega) = \frac{A}{2} \left(2\pi \varphi(\omega - \omega_0) + M(\omega - \omega_0) + 2\pi \varphi(\omega + \omega_0) + M(\omega + \omega_0) \right)$$

If m(t) is stochastic,

$$R_{m'm'}(\tau) = E\left[\left(1 + m(t + \tau)\right)\left(1 + m(t)\right)\right]$$
$$= 1 + 2\eta_m + R_{mm}(\tau)$$

Usually,

$$\eta_m = \mathbf{E} \left[m(t) \right] \\
= 0$$

Therefore,

$$R_{m'm'}(\tau) = 1 + R_{mm}(\tau)$$

Hence.

$$S_{m'm'}(\omega) = 2\pi\delta(\omega) + S_{mm}(\omega)$$

Therefore, assuming φ to be uniformly distributed between 0 and 2π ,

$$S_{vv}(\omega) = \frac{A^2}{4} \left(2\pi \delta(\omega - \omega_0) + S_{mm}(\omega - \omega_0) + 2\pi \delta(\omega + \omega_0) + S_{mm}(\omega + \omega_0) \right)$$

In amplitude modulation, the carrier wave is enveloped by $\pm Am'(t)$, i.e. by $\pm A(1+m(t))$. Hence, let the modulation indices be defined as in Definition 39.

Definition 39 (Modulation indices for amplitude modulation).

$$\mu_{+} = \max_{t} m(t)$$

$$\mu_{-} = -\min_{t} m(t)$$

$$\mu = \frac{1}{2} (\mu_{+} + \mu_{-})$$

$$= \frac{1}{2} \left(\max_{t} m(t) - \min_{t} m(t) \right)$$

Hence,

$$\mu_{+} = \frac{\max_{t} v(t) - A}{A}$$

$$\mu_{-} = \frac{A - \min_{t} v(t)}{A}$$

Hence, the signal can be reconstructed using a envelope detector as in Figure 18.

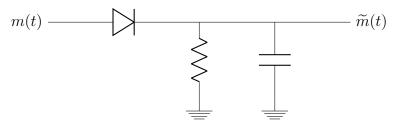


Figure 18: Envelope Detector

Definition 40 (Efficiency index). The efficiency index of AM with respect to DSB is defined to be

$$\eta = \frac{\mathrm{E}\left[v_{\mathrm{DSB}}^{2}(t)\right]}{\mathrm{E}\left[v_{\mathrm{AM}}^{2}(t)\right]}$$

3 Single Side Band Modulation

$$M_L(\omega) = \begin{cases} M(\omega) & ; & \omega \le 0 \\ 0 & ; & \omega > 0 \end{cases}$$

$$M_U(\omega) = \begin{cases} 0 & ; & \omega \le 0 \\ M(\omega) & ; & \omega > 0 \end{cases}$$

Hence,

$$M(\omega) = M_L(\omega) + M_U(\omega)$$

Let $v_{\text{USB}}(t)$ and $v_{\text{LSB}}(t)$ be signals such that

$$V_{\text{USB}}(\omega) = A \left(M_U(\omega - \omega_0) + M_L(\omega + \omega_0) \right)$$

$$V_{\text{LSB}}(\omega) = A \left(M_L(\omega - \omega_0) + M_U(\omega + \omega_0) \right)$$

Also, let $\widehat{M}(\omega)$ be the Hilbert transform of $M(\omega)$, i.e.

$$\widehat{M}(\omega) = -j \operatorname{sign} M(\omega)$$
$$= jM_L(\omega) - jM_U(\omega)$$

Therefore,

$$M_U(\omega) = \frac{1}{2} \left(M(\omega) + j \widehat{M}(\omega) \right)$$
$$M_L(\omega) = \frac{1}{2} \left(M(\omega) - j \widehat{M}(\omega) \right)$$

Therefore,

$$V_{\text{USB}}(\omega) = A \left(M_U(\omega - \omega_0) + M_L(\omega + \omega_0) \right)$$

= $\frac{1}{2} \left(M(\omega - \omega_0) + M(\omega + \omega_0) \right) + \frac{-1}{2j} \left(\widehat{M}(\omega - \omega_0) - \widehat{M}(\omega + \omega_0) \right)$

Therefore,

$$v_{\text{USB}}(t) = A \left(m(t) \cos(\omega_0 t) - \widehat{m}(t) \sin(\omega_0 t) \right)$$

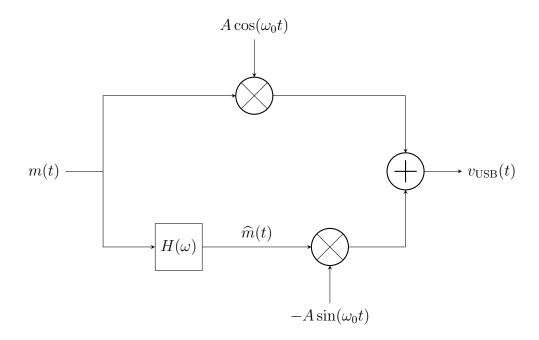


Figure 19: Implementation of USB Transmitter with Hilbert Transformer

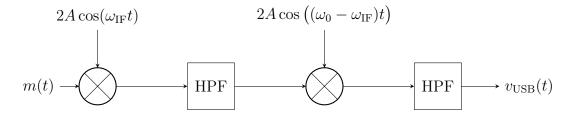


Figure 20: Implementation of USB Transmitter with Frequency Domain Slicing

$$\begin{split} \widetilde{M}(\omega) &= A \left(\cos(\varphi) M(\omega) + \sin(\varphi) \widehat{M}(\omega) \right) \\ &= A \left(\cos(\varphi) + \sin(\varphi) \left(-j \operatorname{sign}(\omega) \right) \right) M(\omega) \\ &= \begin{cases} A M(\omega) e^{j\varphi} & ; & \omega \leq 0 \\ A M(\omega) e^{-j\varphi} & ; & \omega > 0 \end{cases} \end{split}$$

Part VIII

Phase Modulations

Definition 41 (Phase modulation). Modulation schemes in which the phase of the carrier wave is modulated according to the data signal are called phase modulations. Hence, the modulated signal is

$$v(t) = R(t)\cos(\omega_0 t + \theta(t))$$

1 Phase Modulation

Definition 42 (Phase modulation). A phase modulation scheme in which the phase is modulated according to the data signal, i.e.

$$\theta(t) = D_P m(t)$$

is called phase modulation. Hence,

$$v(t) = A\cos\left(\omega_0 t + D_P m(t)\right)$$

where D_p is a constant.

2 Frequency Modulation

Definition 43 (Instantaneous frequency). Let

$$\psi(t) = \omega_0 t + \theta(t)$$

Hence, the instantaneous frequency is defined to be

$$f_i = \frac{1}{2\pi} \frac{\mathrm{d}\psi(t)}{\mathrm{d}t}$$

Definition 44 (Frequency modulation). A phase modulation scheme in which the phase is modulated according to the data signal, i.e.

$$\theta(t) = D_{\omega} \int_{-\infty}^{t} m(\tau) \, d\tau$$

is called frequency modulation. Hence,

$$\psi(t) = \omega_0 t + \theta(t)$$

$$= \omega_0 t + D_\omega \int_{-\infty}^t m(\tau) d\tau$$

$$= 2\pi f_0 t + D_\omega \int_{-\infty}^t m(\tau) d\tau$$

Hence, the instantaneous frequency is

$$f_i(t) = \frac{1}{2\pi} \left(2\pi f_0 + D_\omega m(t) \right)$$
$$= f_0(t) + \frac{D_\omega}{2\pi} m(t)$$

Theorem 50. The maximum frequency deviation for a FM signal is

$$\Delta f = \frac{D_{\omega}}{2\pi} \max_{t} \left| m(t) \right|$$

Definition 45. For a data signal with frequency f_m ,

$$\beta = \frac{\Delta f}{f_m}$$

2.1 Narrow Band FM Generation

$$v(t) = \Re\left\{g(t)e^{j\omega_0 t}\right\}$$

where

$$g(t) = Ae^{j\theta(t)}$$

Let

$$|\theta(t)| << 1$$

Therefore,

$$g(t) = A \left(1 + j\theta(t) \right)$$

Therefore,

$$v(t) = \Re \left\{ g(t)e^{j\omega_0 t} \right\}$$

$$= \Re \left\{ A \left(1 + j\theta(t) \right) \left(\cos(\omega_0 t) + j\sin(\omega_0 t) \right) \right\}$$

$$= A \left(\cos(\omega_0 t) - \theta(t)\sin(\omega_0 t) \right)$$

Hence, a narrow band FM signal can be generated as in Figure 21.

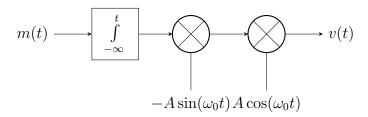


Figure 21: Narrow Band FM Transmitter

Similarly, a receiver can be designed as in Figure 22.

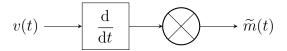


Figure 22: Narrow Band FM Receiver

2.2 Non Narrow Band FM Generation



Figure 23: Non Narrow Band FM Transmitter