

# Fully screen-printed bifacial large area 22.6% N-type Si solar cell with lightly doped ion-implanted boron emitter and tunnel oxide passivated rear contact

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## ABSTRACT

We report on the fabrication of fully screen-printed bifacial large area (239 cm<sup>2</sup>) high-efficiency n-type Si solar cells with ion-implanted homogeneous boron emitter on the front side and carrier-selective tunnel oxide passivated contact (TOPCon) on the rear. Our phosphorus-doped poly-Si/SiO<sub>x</sub> passivated contact with SiN<sub>x</sub> capping layer gave excellent surface passivation with a very low recombination current density ( $J_{0, \text{TOPCon}}$ ) of  $\sim 1$  fA/cm<sup>2</sup> after a simulated firing treatment at  $\sim 770$  °C without metallization. After screen-printed and fire-through metallization on n-TOPCon with  $\sim 13\%$  metal coverage, metallized  $J_{0, \text{TOPCon}}$  value increased to only  $\sim 5$  fA/cm<sup>2</sup>. In addition, homogenous boron implanted emitter ( $\sim 180$  Ω/□) passivated with ALD Al<sub>2</sub>O<sub>3</sub> layer capped with PECVD SiN<sub>x</sub>/SiO<sub>x</sub> double-layer antireflection (DLAR) coating gave excellent passivation with emitter recombination current density of  $\sim 12$  fA/cm<sup>2</sup> prior to metallization. The industrial screen-printed, fire-through contacts with floating busbars on this boron emitter gave metallized emitter recombination current density of  $\sim 31$  fA/cm<sup>2</sup>. This resulted in a low-cost industrial screen-printed n-type bifacial Si solar cell with 22.6% efficiency and 702 mV open-circuit voltage ( $V_{oc}$ ).

## 1. Introduction

SiO<sub>x</sub>/poly-Si (polycrystalline silicon) carrier-selective passivating contacts, such as tunnel oxide passivated contact (TOPCon), have become an active research area for next-generation industrial silicon solar cells due to the excellent surface passivation, elimination of diffusion into the bulk, no direct metal contact to absorber material, and ability to withstand high temperature [1–5]. An n-type TOPCon (n-TOPCon) is composed of a very thin tunnel oxide (SiO<sub>x</sub>) capped with phosphorus doped  $n^+$  poly-Si. Several investigators have reported very low recombination current density ( $J_0$ ) ( $< 10$  fA/cm<sup>2</sup>) [6–10] for n-TOPCon structure with  $\leq 1.5$  nm SiO<sub>x</sub> capped with  $n^+$  doped poly-Si. As a result, very high efficiency ( $> 25.7\%$ ) small area R&D cells have been reported but with full area evaporated Ag on n-TOPCon on the rear [11]. However, to adapt TOPCon technology for industrial production of large-area Si solar cells, several challenges need to be overcome, including screen-printing induced shunting and degradation of  $J_0$  of n-TOPCon with thin poly-Si [12], parasitic absorption in the doped

poly-Si [13,14], single-side deposition of poly-Si [15], and throughput [16]. The poly-Si thickness needs to be adequate to prevent the penetration of the fire-through metal paste into the thin oxide and oxide/Si interface. This is essential for achieving the lowest metallized  $J_0$  for the TOPCon layer. Recently few investigators have reported low metallized  $J_0$  for fire through screen-printed contacts to n-TOPCon using thicker poly-Si layers, which resulted in cell efficiencies of 21–23.5% [8,12,17–22]. However, thicker poly-Si increases parasitic absorption which decreases short circuit current [13,14]. Recently, Nandakumar et al. reported on reduced parasitic absorption when thick poly-Si layers are partially oxidized during deposition without hurting passivation and contact properties [23], resulting in a  $\sim 23.05\%$  large area, screen-printed n-TOPCon bifacial cell. In addition, they used a plasma-enhanced chemical vapor deposition (PECVD) tool to grow in-situ tunnel oxide and thick  $n^+$  poly-Si in a single step on one side only with very high deposition rate, which brings the TOPCon technology much closer to mass production. In spite of these encouraging results, there is limited quantitative understanding of  $J_0$  contribution from each

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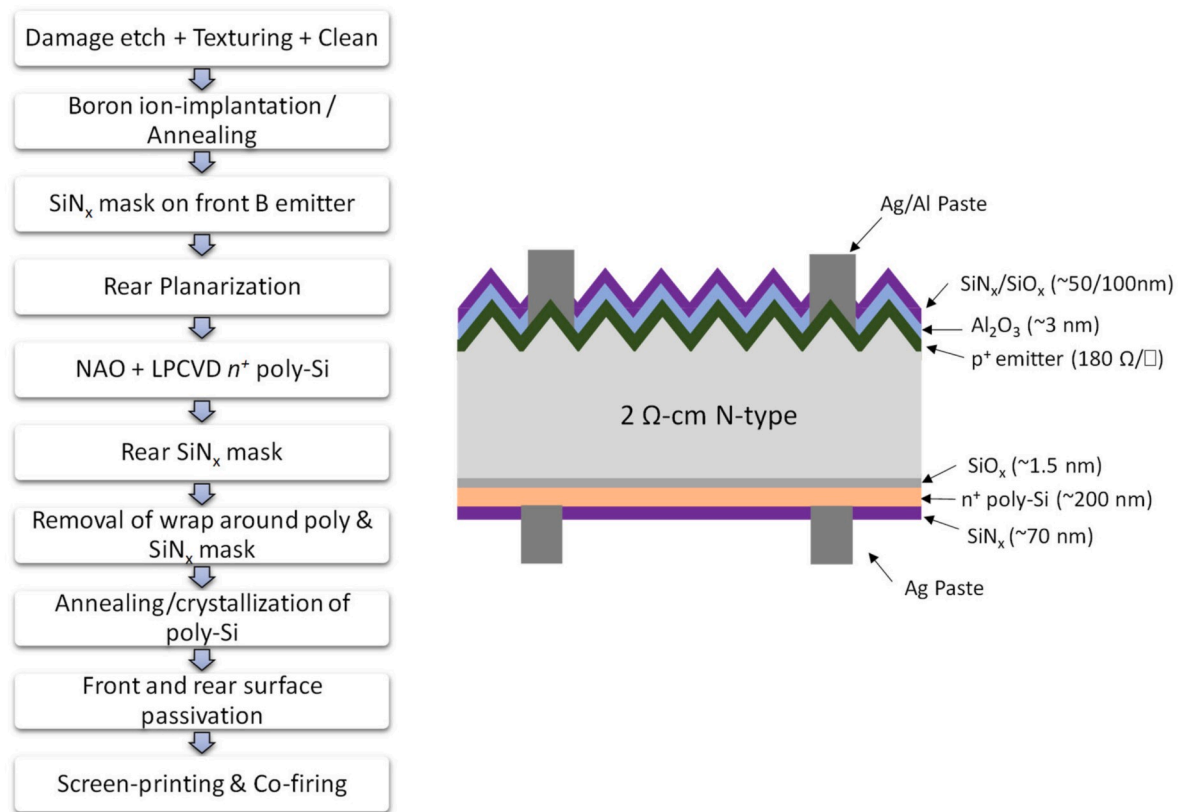


Fig. 1. Process sequence and structure of the screen-printed bifacial n-type Si solar cell with front implanted boron emitter and rear tunnel oxide passivated contact.

layer, bulk lifetime, and contact parameters of fully screen-printed high-efficiency TOPCon cells. This paper reports on the fabrication as well as detailed analysis of such high efficiency commercial size bifacial cells with screen-printed metallization on both sides.

In this paper, industrial size high efficiency fully screen-printed bifacial n-type solar cells were fabricated with ion-implanted homogeneous front boron (B) emitter and rear n-TOPCon. A co-firing process was used to make screen-printed contacts to lightly doped B emitter and n-TOPCon simultaneously. The benefit of floating busbars was also quantitatively examined for the lightly doped implanted homogeneous B emitter by modeling, fabrication, and characterization of cells with five floating as well as fire-through busbars.

## 2. Experimental

Fig. 1 shows the process flow and structure of the large-area ( $239 \text{ cm}^2$ ) n-type bifacial cells fabricated with an implanted B emitter on front and low pressure chemical vapor deposition (LPCVD) grown n-TOPCon on rear side of  $180 \text{ }\mu\text{m}$  thick  $2 \text{ }\Omega\text{-cm}$  n-type Cz wafers. Since LPCVD grows poly-Si on both sides of the wafer, we implemented a masking

process to etch poly-Si from front side. After standard saw damage etching, texturing and cleaning, the wafers received B ion implantation on the front side with a dose of  $1.2 \times 10^{15} \text{ cm}^{-2}$  at  $10 \text{ KeV}$  ion energy followed by an annealing and oxidation process at high temperature ( $\sim 1050 \text{ }^\circ\text{C}$ ), which resulted in sheet resistance of  $180 \text{ }\Omega/\square$ . After the removal of oxide thermally grown during the implant anneal, a PECVD  $\text{SiN}_x$  was deposited on the front side as a mask to protect the emitter during back planarization and front poly-Si etching. A heated KOH treatment was used to planarize the back. After an acid clean and HF dip, a  $\sim 15 \text{ }\text{\AA}$  tunnel oxide layer was grown by nitric acid oxidation (NAO) at  $100 \text{ }^\circ\text{C}$  for  $\sim 10 \text{ min}$  [24], followed by  $200 \text{ nm}$  LPCVD  $n^+$  poly-Si deposition at  $580 \text{ }^\circ\text{C}$  with in-situ phosphorus doping. Next, a PECVD  $\text{SiN}_x$  masking layer was deposited on the back poly-Si, and then the front poly-Si was removed by wet etching in KOH solution. After that, both front and back  $\text{SiN}_x$  masks were removed by HF treatment. The samples were then annealed at  $855 \text{ }^\circ\text{C}$  for poly-Si crystallization and dopant activation. The B emitter was then passivated by atomic layer deposition (ALD) of  $\text{Al}_2\text{O}_3$  and PECVD  $\text{SiN}_x/\text{SiO}_x$  stack while the back poly-Si was capped with  $\sim 700 \text{ }\text{\AA}$  thick PECVD  $\text{SiN}_x$  layer. For cells with non-floating busbars,  $40 \text{ }\mu\text{m}$  wide 104 grid lines in combination with  $600 \text{ }\mu\text{m}$  wide 5

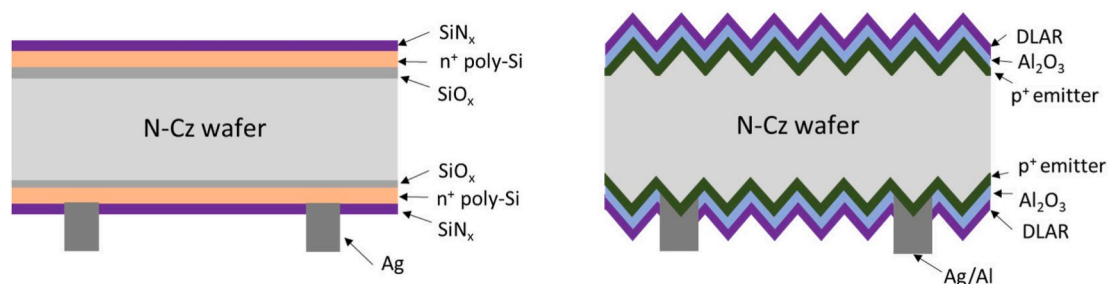


Fig. 2. Schematic of n-TOPCon and implanted boron emitter test structures to investigate the impact of screen-printed metallization on  $J_0$ .

**Table 1**

Light I–V results of best screen-printed, large-area n-TOPCon bifacial cells with non-floating busbars (nFB) and floating busbars (FB).

Busbar	$V_{oc}$ [mV]	$J_{sc}$ [mA/cm <sup>2</sup> ]	FF [%]	$\eta$ [%]	n-factor	$R_s$ [ $\Omega$ -cm <sup>2</sup> ]	$R_{sh}$ [ $\Omega$ -cm <sup>2</sup> ]	pFF[%]
nFB	688	40.1	80.0	22.1	1.17	0.41	5270	82.3
FB	702	40.3	79.7	22.6	1.12	0.59	12800	82.7

busbars were screen-printed on the B emitter using a fire through Ag/Al paste and single print. The screen grid opening was 35  $\mu$ m, resulting in fired grid linewidth of 40  $\mu$ m. Front side metallization with floating busbars (FB) was done using dual-print, where the grid fingers were screen-printed first using the fire-through Ag/Al paste first and then a fritless non-fire-through Ag paste was used to print the busbars. Next, 60  $\mu$ m wide 300 grid lines in combination with 600  $\mu$ m wide 5 busbars were screen-printed on the rear n-TOPCon using fire-through Ag paste and single print. Finally, all samples were co-fired in an industrial-style belt furnace with peak firing temperature of 770 °C. The two SiN<sub>x</sub> masking steps employed in our cell fabrication process can be eliminated by the single side etching tool used in industrial setting.

During the cell fabrication, symmetrical test structures of n-TOPCon and implanted B emitter were prepared to quantify their passivation properties and the impact of screen-printed metallization (Fig. 2). The symmetric  $p^+np^+$  test structures were passivated with thin Al<sub>2</sub>O<sub>3</sub> capped with PECVD SiN<sub>x</sub>/SiO<sub>x</sub> on textured Si wafers to determine the  $J_0$  of the implanted B emitter using the photoconductance decay (PCD) measurement technique proposed by Kane and Swanson [25]. Similarly, symmetric LPCVD grown n-TOPCon structures were prepared on planar Si wafers capped with SiN<sub>x</sub> for the  $J_0$  measurements. In order to quantify the effect of screen-printed fire-through metallization on recombination current density of our implanted B emitter ( $J_{0e}$ ) and rear n-TOPCon ( $J_{0\_TOPCon}$ ), gridlines with different metal coverage were screen-printed only on one side of the symmetric structures. After the simulated contact firing, the excess printed metal was etched away in HCl:H<sub>2</sub>O<sub>2</sub>:H<sub>2</sub>O = 1:1:1 solution, leaving only the embedded metal contact on the surface for the metallized  $J_0$  measurements.

### 3. Results and discussion

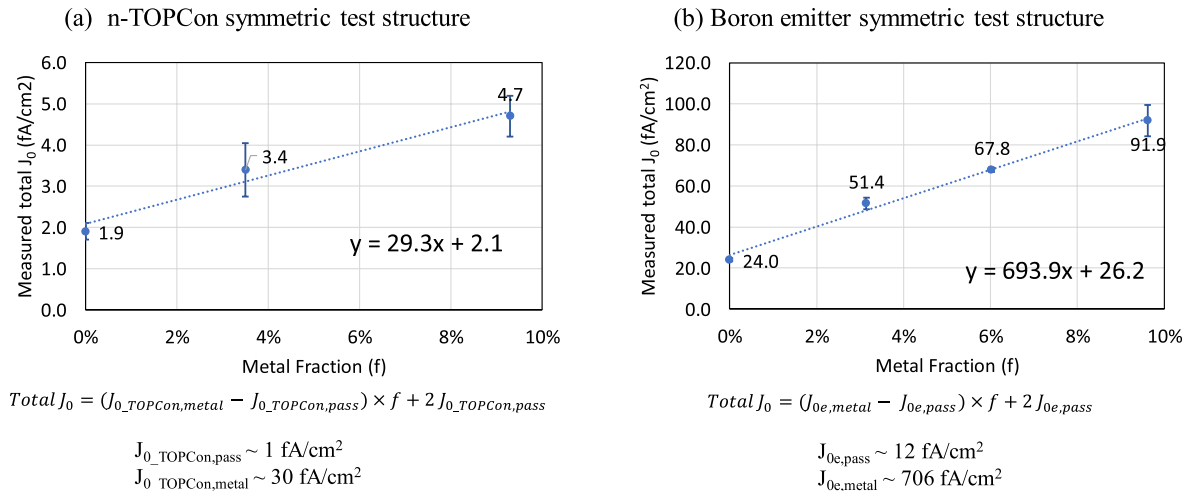
Table 1 shows the cell parameters from light I–V measurements when the cell is illuminated from the front side. Cells were measured in-house using the Fraunhofer ISE certificated reference cell. The fire-through busbar cells showed best cell efficiency of 22.1% with  $V_{oc}$  of 688 mV,  $J_{sc}$  of 40.1 mA/cm<sup>2</sup>, and FF of 80.0%. However, the best cell with floating busbars showed ~14 mV higher  $V_{oc}$ , resulting in a  $V_{oc}$  of 702 mV and efficiency of ~22.6%. The efficiency range was 22.0–22.1% for non-

floating busbar, and 22.4–22.6% for floating busbar cells. Both cells showed high  $J_{sc}$  (>40 mA/cm<sup>2</sup>) due to high EQE, reduced shading from narrow lines, and SiO<sub>2</sub>/SiN<sub>x</sub> two-layer AR coating on front.

For the quantitative study of the effect of screen-printed fire-through metallization on recombination current density of our implanted B emitter and rear n-TOPCon, the above test structures with different metal fraction on one side (Fig. 2) were measured by the PCD tester with the light flashing on the no-metal side to avoid any shading effect. In addition, specific contact resistance was measured using TLM pattern on the same samples, resulting in 2 and 4 m $\Omega$ -cm<sup>2</sup> values for the n-TOPCon and B emitter, respectively, supporting the excellent co-firing process for front and back metallization. Fig. 3(a) shows the measured total  $J_0$  from the n-TOPCon test structures as a function of metal fraction on one side. The total measured  $J_0$  of the test structures with different metal fractions ( $f$ ) on one side can be expressed as

$$\begin{aligned} \text{Total } J_0 &= J_{0\_TOPCon(\text{no metal})} + J_{0\_TOPCon(\text{with metal fraction } f)} \\ &= J_{0\_TOPCon, \text{pass}} + [J_{0\_TOPCon, \text{pass}} \times (1 - f) + J_{0\_TOPCon, \text{metal}} \times f] \\ &= (J_{0\_TOPCon, \text{metal}} - J_{0\_TOPCon, \text{pass}}) \times f + 2 J_{0\_TOPCon, \text{pass}} \end{aligned}$$

where  $J_{0\_TOPCon, \text{pass}}$  and  $J_{0\_TOPCon, \text{metal}}$  are the full area  $J_0$  values for the un-metallized and metallized n-TOPCon. Fig. 3 (a) shows that without any metal, total  $J_0$  ( $= 2 \times J_{0\_TOPCon, \text{pass}}$ ) of ~2 fA/cm<sup>2</sup> was achieved, which corresponds to a  $J_{0\_TOPCon, \text{pass}}$  of ~1 fA/cm<sup>2</sup>, indicating excellent passivation quality of our SiN<sub>x</sub> capped LPCVD grown unmetallized n-TOPCon after simulated contact firing. However, total  $J_{0\_TOPCon}$  did show a slight increase with increased metal fraction (Fig. 3 (a)). From the intercept and slope of the linear fit to the experimental data in Fig. 3 (a) ( $y = 29.3x + 2.1$ ), we obtained a  $J_{0\_TOPCon, \text{metal}}$  ~30 fA/cm<sup>2</sup> and  $J_{0\_TOPCon, \text{pass}}$  ~1.05 fA/cm<sup>2</sup> for the metallized and unmetallized n-TOPCon regions. This corresponds to a metallized  $J_{0\_TOPCon}$  of 5 fA/cm<sup>2</sup> ( $= 30 \times 13.5\% + 1 \times 86.5\%$ ) for 13.5% metal coverage on the back, resulting from 60  $\mu$ m wide 300 grid lines and 600  $\mu$ m wide 5 busbars in this study. Identical study was conducted on B emitter test structures from which full area  $J_{0e, \text{metal}} = \sim 706$  fA/cm<sup>2</sup> and  $J_{0e, \text{pass}} = \sim 12$  fA/cm<sup>2</sup> were obtained for our 180  $\Omega/\square$  implanted B emitter, as shown in Fig. 4 (b). This corresponds to a metallized  $J_{0e}$  of 31 fA/cm<sup>2</sup> ( $= 706 \times 2.7\% + 12 \times 97.3\%$ ) for 2.7% metal/Si contact fraction for floating busbars and



**Fig. 3.** Measured recombination current density ( $J_0$ ) from (a) n-TOPCon and (b) boron implanted emitter as a function of metal fraction on one side.

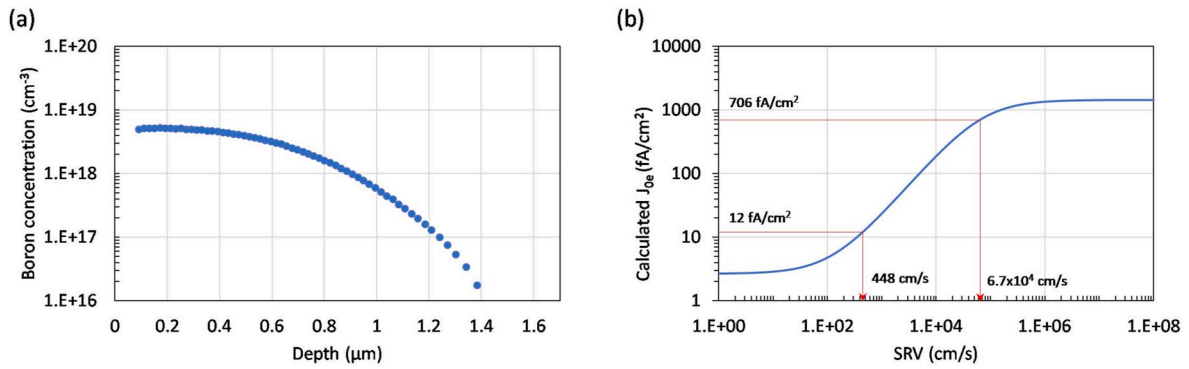


Fig. 4. Measured implanted B profile (a) and calculated  $J_{0e}$  as functions of surface recombination velocity (b).

44 fA/cm<sup>2</sup> ( $= 706 \times 4.6\% + 12 \times 95.4\%$ ) for non-floating busbars (4.6% metal fraction). From the measured cell  $J_{sc}$  and  $V_{oc}$ , a total  $J_0$  of 58 fA/cm<sup>2</sup> was obtained ( $V_{oc} = \frac{kT}{q} \ln \left( \frac{J_{sc}}{J_0} \right)$ ). Finally,  $J_{0,bulk}$  was calculated to be 22 fA/cm<sup>2</sup> by subtracting the metallized  $J_{0e}$  (31 fA/cm<sup>2</sup>) and metallized  $J_{0, TOPCon}$  (5 fA/cm<sup>2</sup>) from the total  $J_0$  (58 fA/cm<sup>2</sup>). This cell analysis reveals that the  $V_{oc}$  of 22.6% cell is limited by the recombination in the bulk and emitter because the metallized  $J_0$  of our TOPCon layer is very small ( $\sim 5$  fA/cm<sup>2</sup>). Table 2 summarizes all the  $J_0$  components in our 22.6% efficient finished cell.

Additional characterization and modeling was performed to improve the fundamental understanding of our 22.6% cell. We used the Sentaurus 2D simulator for modeling which requires surface recombination velocities on the B emitter and n-TOPCon regions rather than  $J_0$  values. Fig. 4 (a) shows the measured profile of our implanted B emitter with  $\sim 5 \times 10^{18}$ /cm<sup>3</sup> surface concentration and junction depth of  $\sim 1.4$  μm. Fig. 4 (b) shows the calculated  $J_{0e}$  as function of surface recombination

velocity for this B emitter profile, obtained from Sentaurus simulation [26,27]. From Fig. 4 (b), a surface recombination velocity value of 448 cm/s was obtained for the unmetallized passivated emitter region, using the measured  $J_{0e} = 12$  fA/cm<sup>2</sup> (Fig. 3(b)). Similarly, SRV of  $\sim 6.7 \times 10^4$  cm/s was extracted (Fig. 4 (b)) for the metallized emitter region from the measured  $J_{0e, metal}$  of 706 fA/cm<sup>2</sup> (Fig. 3(b)). Since the exact tunneling mechanism and tunneling parameters were not fully known for our TOPCon, we measured phosphorus in-diffusion profile in Si bulk by electrochemical capacitance-voltage (ECV) technique and replaced the n-TOPCon region by this profile with an effective surface recombination velocity that produce a  $J_0 = 5$  fA/cm<sup>2</sup>, which is equal to the measured metallized  $J_0$  value of the TOPCon. This profile is formed during the 855 °C n-TOPCon anneal, and has a junction depth of 0.06 μm and a surface concentration of  $4.7 \times 10^{18}$  cm<sup>-3</sup> (Fig. 5 (a)). Sentaurus model was used to generate the  $J_0$  vs S curve for this profile (Fig. 5(b)) from which an effective hole SRV of 328 cm/s was extracted at the tunnel oxide/Si interface using the metallized  $J_{0, TOPCon}$  value of 5 fA/cm<sup>2</sup>. This approach is similar to the one used by Chen et al. [28]. Finally, a complete Sentaurus 2D model was built to match the 22.6% efficient screen-printed TOPCon solar cell using all the measured material and device parameters (contact area, shading area and contact resistance) and the extracted recombination velocities at the passivated and metallized emitter regions and the tunnel oxide/Si interface (Table 4 column 1). The modeled cell parameters matched very well with the measured cell light IV (LIV)

Table 2

Summary of recombination current density for each region of our 22.6% n-TOPCon cell.

Cell regions	Full area (100%) $J_0$ (fA/cm <sup>2</sup> )	Area fraction (%)	Area-weighted $J_0$ (fA/cm <sup>2</sup> )
Passivated boron emitter	12	97.3%	11.7
Metallized boron emitter	706	2.7%	19.1
Bulk	22	100%	21.8
Rear passivated TOPCon	1	86.5%	0.9
Rear metallized TOPCon	30	13.5%	4.0
Full Cell			57.5

Table 3

Comparison of measured and modeled screen-printed TOPCon solar cell parameters.

	$V_{oc}$ (mV)	$J_{sc}$ (mA/cm <sup>2</sup> )	FF (%)	Eff (%)
Experiment	702	40.3	79.7	22.6
Model	701	40.3	79.6	22.5

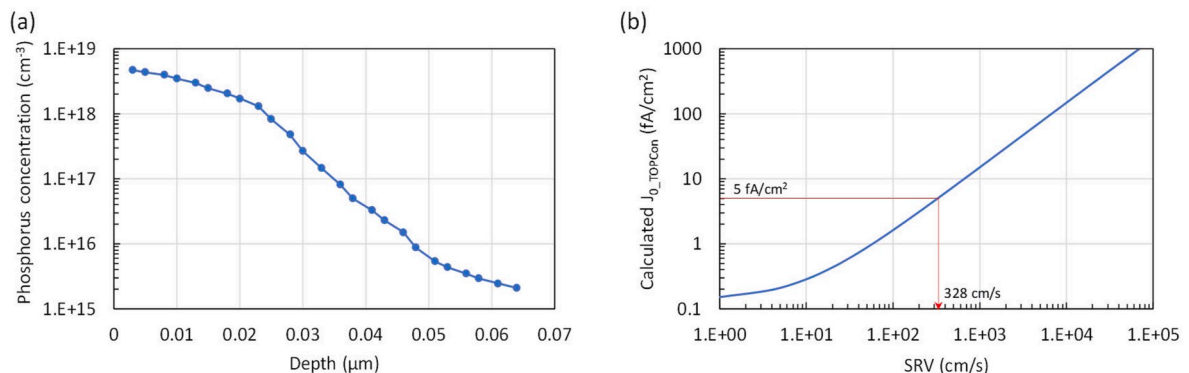


Fig. 5. Measured phosphorus in-diffusion profile in bulk Si (a) and calculated  $J_{0, TOPCon}$  as functions of effective hole surface recombination velocity (b).

**Table 4**

Sentaurus 2D modeling of the 22.6% TOPCon cell and a roadmap to ~ 24% efficiency.

Parameters	22.6% floating busbar TOPCon cell	30 $\Omega/\square$ selective emitter	3 ms bulk lifetime	Multiwire contact
Voc [mV]	701	704	709	710
Jsc [ $\text{mA}/\text{cm}^2$ ]	40.3	40.3	40.3	40.7
FF [%]	79.6	80.1	81.8	82.8
Efficiency [%]	22.5	22.7	23.4	23.9
Front finger width $W_f$ ( $\mu\text{m}$ )	40	40	40	40
Front shading coverage	4.59%	4.59%	4.59%	3.56%
Busbar number/width ( $\mu\text{m}$ )	5/600	5/600	5/600	14/100
Wafer thickness ( $\mu\text{m}$ )	180	180	180	180
Field emitter profile	Measured	Measured	Measured	Measured
Field emitter sheet resistance ( $\Omega/\square$ )	~180	~180	~180	~180
Front contact resistance ( $\text{m}\Omega\text{-cm}^2$ )	4	1	1	1
Selective emitter profile	N/A	Measured	Measured	Measured
Selective emitter sheet resistance ( $\Omega/\square$ )	N/A	~30	~30	~30
Selective emitter surface concentration ( $\text{cm}^{-3}$ )	N/A	$\sim 3 \times 10^{19}$	$\sim 3 \times 10^{19}$	$\sim 3 \times 10^{19}$
Selective emitter junction depth ( $\mu\text{m}$ )	N/A	1.9	1.9	1.9
Selective emitter junction width ( $\mu\text{m}$ )	N/A	100	100	100
Substrate resistivity ( $\Omega\text{-cm}$ )	2	2	2	2
Substrate doping ( $\text{cm}^{-3}$ )	$2.38 \times 10^{15}$	$2.38 \times 10^{15}$	$2.38 \times 10^{15}$	$2.38 \times 10^{15}$
Front passivated FSRV ( $\text{cm/s}$ )	448	448	448	448
Wing FSRV ( $\text{cm/s}$ )	N/A	721	721	721
Front contact FSRV ( $\text{cm/s}$ )	$6.7 \times 10^4$	$10^7$	$10^7$	$10^7$
Lifetime (ms)	1	1	3	3
Back contact resistance ( $\text{m}\Omega\text{-cm}^2$ )	2	2	2	2
Back contact hole SRV at n + Si/ tunnel oxide interface ( $\text{cm/s}$ )	328	328	328	328

data, as shown in Table 3. In order to establish directions for further efficiency improvement, we extended the 2D Sentaurus modeling. Table 4 shows that a combination of selective emitter (30/180  $\Omega/\square$ ), increased bulk lifetime from 1 to 3 ms, and 100  $\mu\text{m}$  wide 14 floating busbars for multiwire application can raise the cell efficiency to ~ 24%.

#### 4. Conclusions

A fully screen-printed large area ~22.6% efficient bifacial n-type Si solar cell was fabricated with implanted lightly doped homogeneous B emitter (180  $\Omega/\square$ ) on the front and n-TOPCon on the back of a 2  $\Omega\text{-cm}$  n-type Cz Si.  $\text{SiN}_x$  capped LPCVD grown 200 nm  $n^+$  poly-Si on ~15  $\text{\AA}$  tunnel oxide produced unmetallized  $J_0$  value of ~1  $\text{fA}/\text{cm}^2$  and metallized  $J_0$  of ~5  $\text{fA}/\text{cm}^2$  with 13.5% metal coverage. Floating busbars on the front emitter gave ~14 mV increase in  $V_{OC}$  with ~0.5% efficiency enhancement due to reduced front metal/Si contact area on the lightly

doped B emitter. Detailed analysis was performed to determine the  $J_0$  component and interface recombination velocity of each region. Results indicated that the metallized  $J_0$  of the lightly doped B emitter ( $J_{0e} = \sim 31 \text{ fA}/\text{cm}^2$ ) and ~1 ms bulk lifetime wafer ( $J_{0\text{bulk}} = 22 \text{ fA}/\text{cm}^2$ ) limited the voltage to 702 mV and cell efficiency to 22.6%. Model calculations also showed that a combination of B selective emitter, improved bulk lifetime and multiwire contacts on the front can raise the cell efficiency to ~24%.

#### Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

#### CRediT authorship contribution statement

**Ying-Yuan Huang:** Conceptualization, Methodology, Validation, Formal analysis, Investigation, Data curation, Writing - review & editing, Visualization. **Young-Woo Ok:** Investigation, Writing - review & editing, Visualization, Supervision. **Keeya Madani:** Investigation, Formal analysis. **Wookjin Choi:** Investigation, Formal analysis. **Ajay D. Upadhyaya:** Investigation, Formal analysis. **Vijaykumar D. Upadhyaya:** Investigation. **Ajeet Rohatgi:** Project administration, Funding acquisition, Supervision.

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#### Appendix A. Supplementary data

Supplementary data to this article can be found online at <https://doi.org/10.1016/j.solmat.2020.110585>.

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