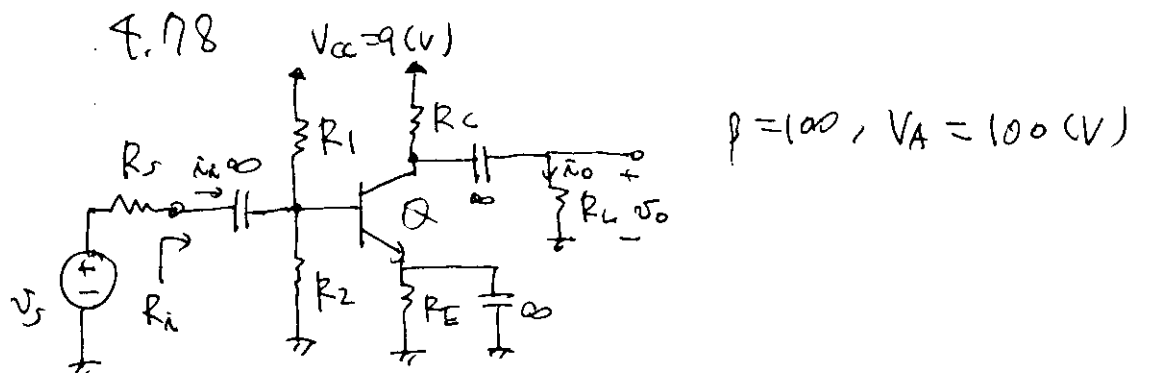
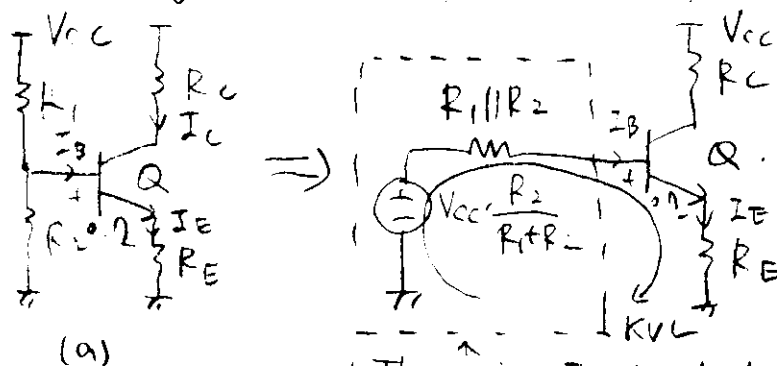


## HW #6 Solution



$$R_1 = 20k, R_2 = 15k, R_E = 1.2k, R_C = 2.2k, R_S = 10k, R_L = 2k$$

① D.C. Analysis (capacitor = open circuit)



By assuming Q is in active region,

$$\text{KVL: } V_{CC} \cdot \frac{R_2}{R_1 + R_2} = (R_1 \parallel R_2) \cdot I_B + 0.7 + I_E \cdot R_E, \quad I_B = \frac{I_C}{\beta}, \quad I_E = \frac{I_C}{\alpha}$$

$$= \left[ (R_1 \parallel R_2) \cdot \frac{1}{\beta} + \frac{R_E}{\alpha} \right] \cdot I_C + 0.7$$

$$\Rightarrow I_C = \frac{V_{CC} \cdot \frac{R_2}{R_1 + R_2} - 0.7}{(R_1 \parallel R_2) \cdot \frac{1}{\beta} + \frac{R_E}{\alpha}} = 1.92 \text{ mA}$$

$$I_E = \frac{I_C}{\alpha} = 1.94 \text{ mA}$$

Hence,

$$g_m = \frac{I_C}{V_T} = 0.0769 \text{ (A/V)}$$

$$r_{\pi} = \frac{\beta}{g_m} = 1.3 \text{ k}\Omega$$

$$r_o = \frac{V_A}{I_C} = 52 \text{ k}\Omega$$

check!

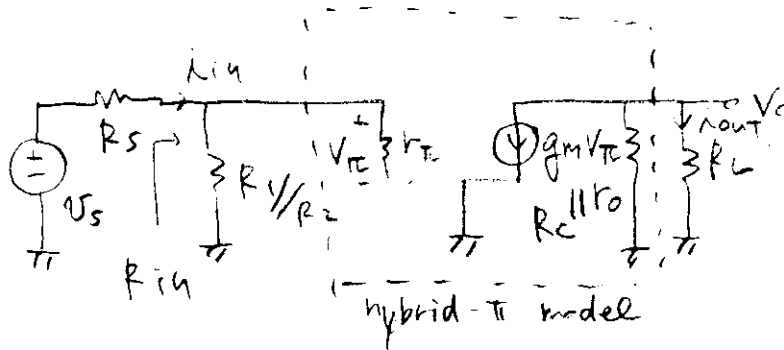
$$V_B = V_{CC} \cdot \frac{R_2}{R_1 + R_2} = 3.21$$

$$V_C = V_{CC} - I_C R_C = 4.77$$

$$V_{BC} = -1.55 \text{ V, so}$$

Q is in active region

② small-signal Analysis ( $\infty$  capacitor = short circuit)  
D.C. sources = zero element



From the law of voltage divider,

$$V_{\pi} = v_s \cdot \frac{R_1 \parallel R_2 \parallel r_{\pi}}{R_1 \parallel R_2 \parallel r_{\pi} + R_s}$$

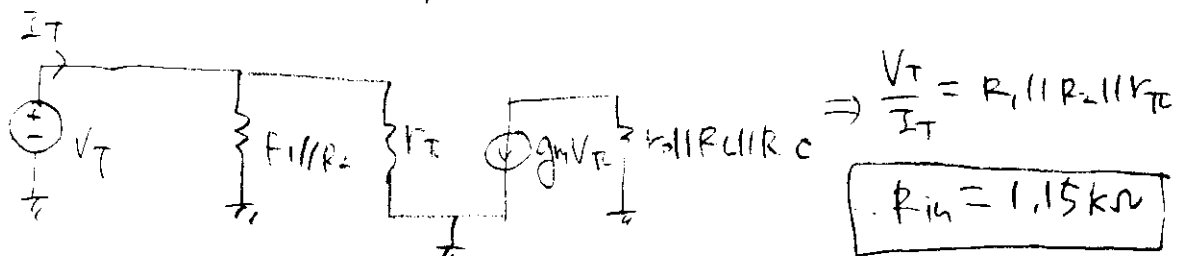
$$V_o = -g_m V_{\pi} (r_o \parallel R_L \parallel R_c)$$

$$= -g_m \cdot \frac{R_1 \parallel R_2 \parallel r_{\pi}}{R_1 \parallel R_2 \parallel r_{\pi} + R_s} \cdot (r_o \parallel R_L \parallel R_c) \cdot v_s$$

$$\Rightarrow \frac{V_o}{v_s} = -8.13$$

To Find  $R_{in}$ , note that  $R_{in}$  is Thevenin Equivalent Resistance at the (specified) input port with output open-circuited

We use test-voltage method to Find  $R_{in}$ . Also,  $R_{in}$  is small-signal quantity, so we use small-signal model



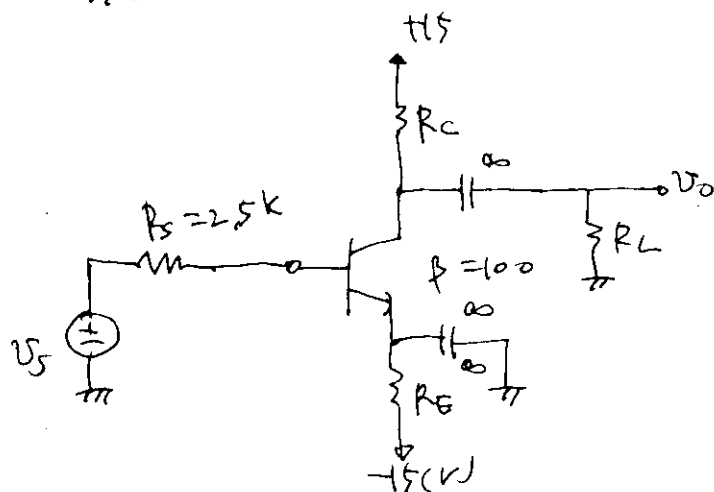
To find current gain ( $A_{i_{arr}}$ ),

$$A_{i_{in}} = \frac{V_{\pi}}{I_1 \parallel R_2 \parallel r_{\pi}}$$

$$A_{out} = -g_m V_{\pi} \cdot \frac{R_c \parallel r_o}{R_c \parallel r_o + R_L}$$

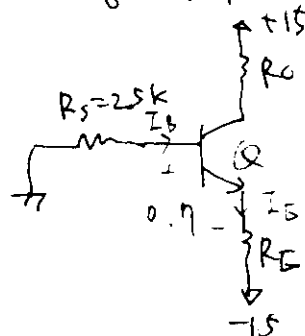
$$\frac{A_{out}}{A_{in}} = - \frac{g_m \cdot R_c \parallel r_o}{R_c \parallel r_o + R_L} \cdot (R_1 \parallel R_2 \parallel r_{\pi}) = \underline{\underline{-45.29}}$$

4.82



(a) D.C. analysis

Since  $v_s$  has zero-average, D.C. value of  $v_s = 0$   
so equivalent ckt for D.C. analysis is as follows



by assuming Q is in active,

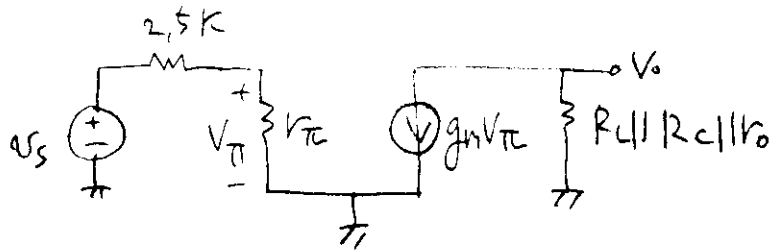
$$\begin{cases} 0 = R_s \cdot I_B + 0.7 + I_E \cdot R_E - 15 \\ I_E = 1 \text{ mA}, I_B = \frac{I_E}{\beta + 1} \end{cases}$$

$$\Rightarrow \boxed{R_E = 14.3 \text{ k}\Omega}$$

$$(b) \begin{cases} V_c = 15 - I_c \cdot R_c = 5 \text{ (V)} \\ I_c = \alpha \cdot I_E = \frac{\beta}{\beta + 1} \cdot I_E \end{cases}$$

$$\Rightarrow R_c = 10 \text{ k}\Omega$$

(c)



$$g_m = \frac{I_C}{V_T} = 40 \text{ mA/V}$$

$$r_{\pi} = \frac{\beta}{g_m} = 2.5 \text{ k}\Omega$$

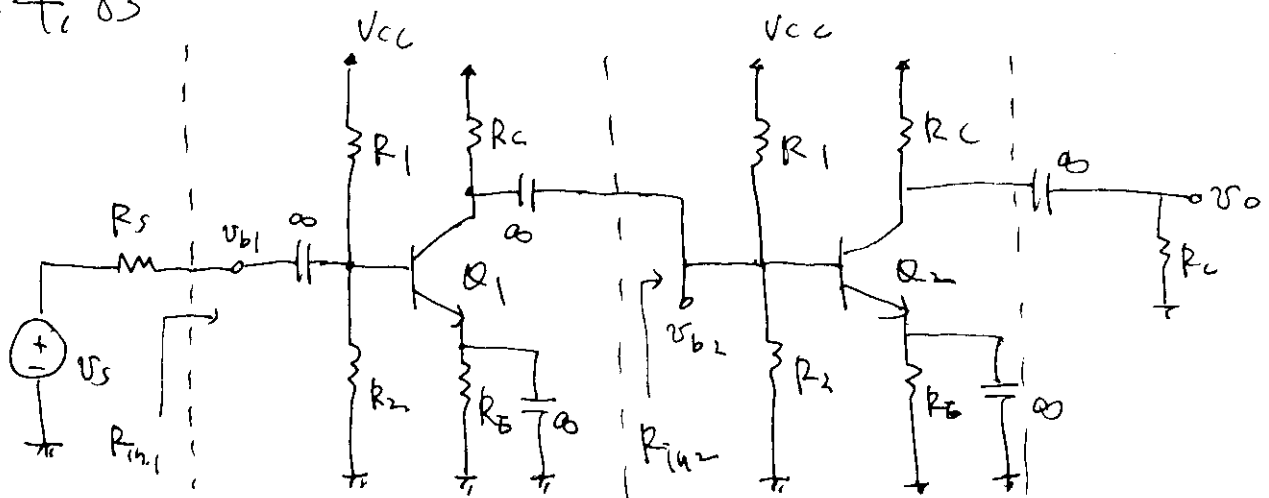
$$V_{\pi} = \frac{r_{\pi}}{r_{\pi} + 2.5 \text{ k}} \cdot v_s$$

$$\Rightarrow v_o = -g_m V_{\pi} (R_L || R_C || r_o)$$

$$= -\frac{r_{\pi}}{r_{\pi} + 2.5 \text{ k}} \cdot g_m \cdot (R_L || R_C || r_o) \cdot v_s$$

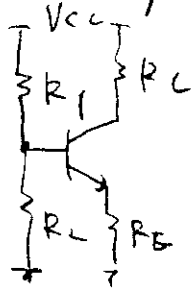
$$\Rightarrow A_v = \frac{v_o}{v_s} = -64.5$$

4.83



$$V_{CC} = 15, R_1 = 100 \text{ k}, R_2 = 40 \text{ k}, R_E = 3.9 \text{ k}, R_C = 6.8 \text{ k}, \beta = 100$$

a) D-C analysis



→ two identical stages for DC analysis  
From P4.13,

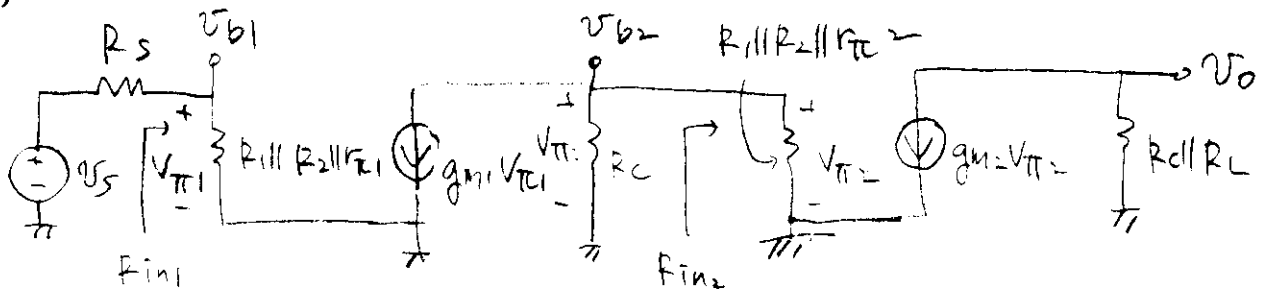
$$I_C = \frac{V_{CC} \cdot \left( \frac{R_2}{R_1 \parallel R_2} \right) - 0.7}{\left( R_1 \parallel R_2 \right) \frac{1}{\beta} + R_E / \alpha} = 0.96 \text{ mA}$$

$$V_C = V_{CC} - R_C \cdot I_C = 8.46 \text{ (V)}$$

$$\boxed{I_C = 0.95 \text{ mA} \text{ for both } Q_1, Q_2}$$

$$\boxed{V_C = 8.46 \text{ (V)}}$$

b)



$$c) R_{in1} = R_1 \parallel R_2 \parallel r_{\pi 1}$$

$$\boxed{= 2.4 \text{ k}}$$

$$\frac{v_{b1}}{v_S} = \frac{R_1 \parallel R_2 \parallel r_{\pi 1}}{R_S + R_1 \parallel R_2 \parallel r_{\pi 1}} = 0.3247$$

$$d) R_{in2} = R_1 \parallel R_2 \parallel r_{\pi 2} = \boxed{2.4 \text{ k}}$$

$$v_{b2} = -g_{m1} v_{\pi 1} (R_C \parallel R_{in2}), v_{\pi 1} = v_{b1}$$

$$\Rightarrow \frac{v_{b2}}{v_{b1}} = -g_{m1} \cdot (R_C \parallel R_{in2}) = \boxed{-68.3}$$

e)  $R_L = 2k$ ,

$$v_o = -g_{m2} \cdot v_{\pi 2} \cdot R_C \parallel R_L, v_{\pi 2} = v_{b2}$$

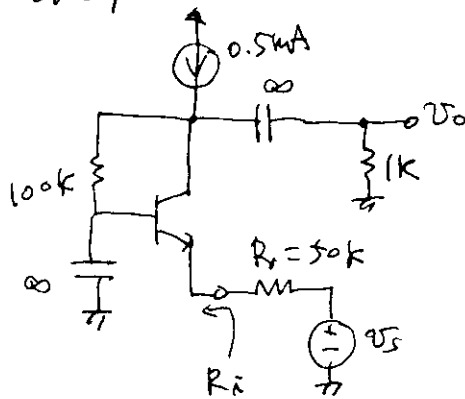
$$\Rightarrow \frac{v_o}{v_{b2}} = -g_{m2} R_C \parallel R_L = \boxed{-59.45}$$

f)  $\frac{v_o}{v_s} = \frac{v_{b1}}{v_s} \cdot \frac{v_{b2}}{v_{b1}} \cdot \frac{v_o}{v_{b2}}$

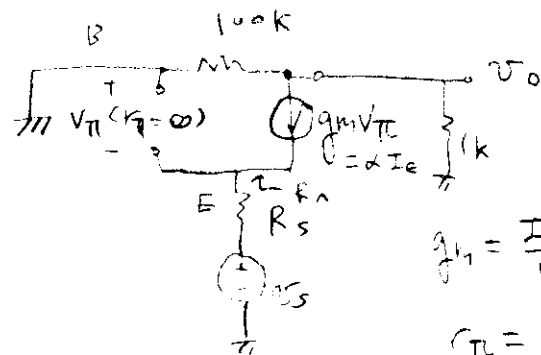
$$= 0.3277 \times (-68.3) \times (-59.45)$$

$$= \boxed{1319}$$

4.89

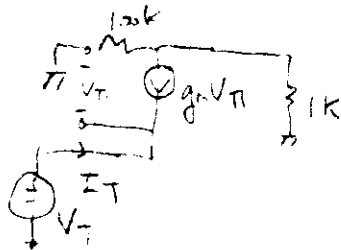


assume  $\beta \rightarrow \infty$  &  $\alpha \rightarrow 1$   
Then, small-signal model is,



$$g_m = \frac{I_C}{V_T} = \frac{I_E}{V_T} \quad (\because \alpha = 1)$$

$$r_{\pi} = \beta / g_m = \infty$$

i)  $R_i$ 

Since  $v_{\pi} = -v_T$ ,

$$I_T = g_m v_T$$

$$\Rightarrow R_{in} = \frac{v_T}{I_T} = \frac{1}{g_m} = \boxed{50}$$

ii)  $v_o/v_s$ 

$$v_o = -g_m v_{\pi} \cdot (1k \parallel 100k)$$

$$v_{\pi} = -\frac{R_{in}}{R_{in} + R_s} \cdot v_s$$

$$\Rightarrow \frac{v_o}{v_s} = +g_m (1k \parallel 100k) \left( \frac{R_n}{R_s + R_n} \right)$$

$$= \boxed{9.9}$$