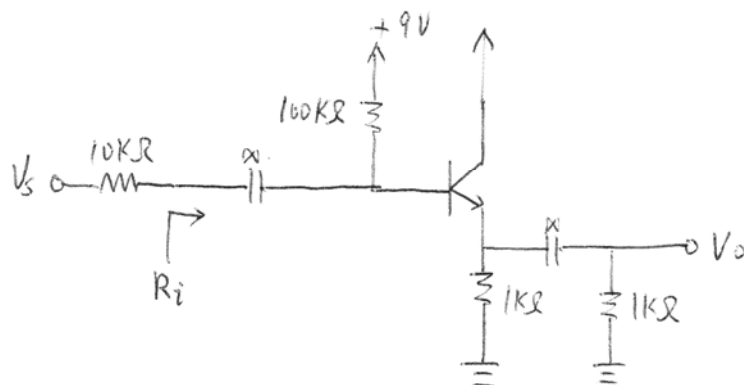


4.91

①



(a)

$$\text{For } \beta = 20 \quad I_E = \frac{(9 - 0.7)V}{\frac{100k\Omega}{\beta + 1} + 1k\Omega} = 1.44 \text{ mA}$$

$$V_E = I_E \cdot 1k\Omega = 1.44 \text{ V}$$

$$V_B = V_E + 0.7 = 2.14 \text{ V}$$

$$\text{For } \beta = 200 \quad I_E = 5.54 \text{ mA}$$

$$V_E = 5.54 \text{ V}$$

$$V_B = 6.24 \text{ V}$$

$$(b) \quad R_i = 100k\Omega \parallel [r_{\pi} + (\beta + 1)(1k\Omega \parallel 1k\Omega)] = 100k\Omega \parallel (\beta + 1)[r_e + 0.5k\Omega]$$

$$\text{For } \beta = 20, \quad I_E = 1.44 \text{ mA}, \quad r_e = \frac{V_T}{I_E} = 17.4\Omega, \quad r_{\pi} = \frac{V_T}{I_B} = (\beta + 1)r_e = 365.4\Omega$$

$$R_i = 100k\Omega \parallel 21 \cdot [0.0174k\Omega + 0.5k\Omega] \\ = 9.8k\Omega$$

$$\text{For } \beta = 200, \quad I_E = 5.54 \text{ mA}, \quad r_e = 4.51\Omega, \quad r_{\pi} = (\beta + 1)r_e = 906.51\Omega$$

$$R_i = 100 \parallel 201 (0.0045 + 0.5) k\Omega \\ = 50.3k\Omega$$

②

$$(c) \frac{V_o}{V_s} = \frac{R_i}{R_i + R_s} \cdot \frac{1k\Omega // 1k\Omega}{1k\Omega // 1k\Omega + r_{\pi}/\beta + 1}$$

For $\beta = 20$

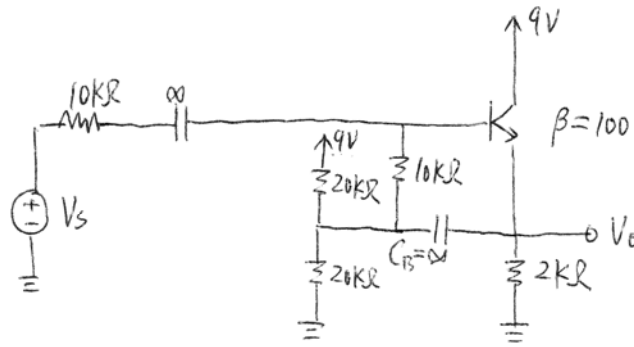
$$\frac{V_o}{V_s} = \frac{9.8}{9.8 + 10} \cdot \frac{0.5k\Omega}{0.5k\Omega + 0.0174k\Omega} = 0.478$$

For $\beta = 200$

$$\frac{V_o}{V_s} = \frac{50.3k\Omega}{50.3k\Omega + 10k\Omega} \cdot \frac{0.5k\Omega}{0.5k\Omega + 0.00451k\Omega} = 0.827$$

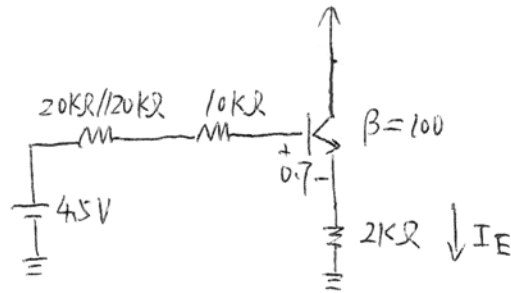
4.95

(3)

boot-strapped
Follower

(a) DC Analysis

Original circuit can be simplified as:



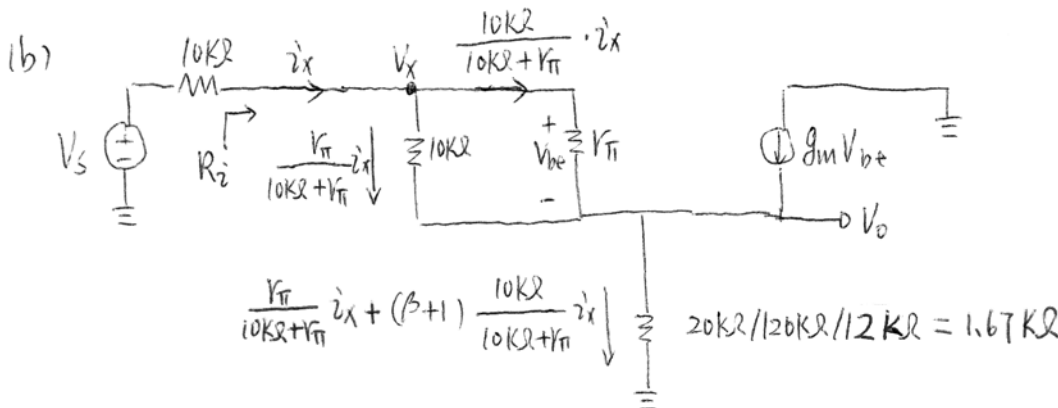
$$I_E = \frac{4.5V - 0.7V}{2k\Omega + \frac{20k\Omega // 20k\Omega + 10k\Omega}{\beta + 1}} = 1.73 \text{ mA}$$

$$I_C = 0.99 I_E = 1.71 \text{ mA}$$

$$g_m = \frac{I_C}{V_T} = 68.5 \text{ mA/V}$$

$$r_e = \frac{V_T}{I_E} = 145\Omega$$

$$r_{\pi} = \frac{\beta}{g_m} = 1.46 \text{ k}\Omega$$



input Resistance :

$$V_X = \frac{10k\Omega}{10k\Omega + r_{\pi}} \cdot i_X \cdot r_{\pi} + \left[(\beta + 1) \frac{10k\Omega}{10k\Omega + r_{\pi}} \cdot i_X + \frac{r_{\pi}}{10k\Omega + r_{\pi}} \cdot i_X \right] \cdot 1.67 \text{ k}\Omega$$

$$R_i = \frac{V_X}{i_X} = \frac{10k\Omega}{10k\Omega + r_{\pi}} \cdot (r_{\pi} + (\beta + 1) \cdot 1.67 \text{ k}\Omega) + \frac{r_{\pi}}{10k\Omega + r_{\pi}} \cdot 1.67 \text{ k}\Omega$$

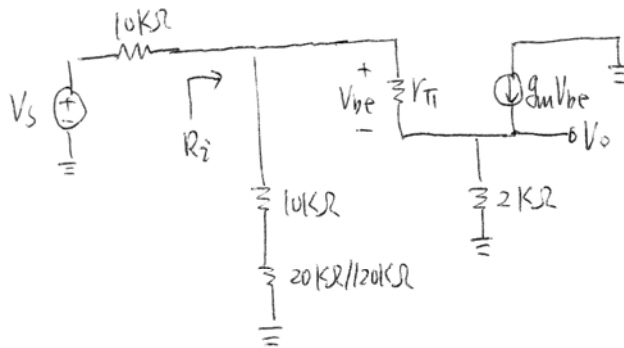
$$= 148.2 \text{ k}\Omega$$

$$\frac{V_o}{V_s} = \frac{V_o}{V_x} \cdot \frac{V_x}{V_s}$$

$$= \frac{R_i}{R_i + 10K\Omega} \cdot \frac{\left[(\beta+1) \frac{10K\Omega}{10K\Omega + r_{\pi}} \cancel{V_x} + \frac{r_{\pi}}{10K\Omega + r_{\pi}} \cancel{V_x} \right] \cdot 1.67K\Omega}{\frac{10K\Omega}{10K\Omega + r_{\pi}} \cancel{V_x} r_{\pi} + (\beta+1) \frac{10K\Omega}{10K\Omega + r_{\pi}} \cancel{V_x} \cdot 1.67K\Omega + \frac{r_{\pi}}{10K\Omega + r_{\pi}} \cancel{V_x} \cdot 1.67K\Omega}$$

$$= 0.93$$

(c) with C_B open-circuit so that boot-strapping is eliminated, we obtain following equivalent model



$$R_i = (10K\Omega + 20K\Omega // 20K\Omega) // (r_{\pi} + (\beta+1)2K\Omega) = 18.21K\Omega$$

Now R_i is much Lower than the value obtained with boot-strapping

$$\frac{V_o}{V_s} = \frac{R_i}{R_i + 10K\Omega} \cdot \frac{(\beta+1)2K\Omega}{r_{\pi} + (\beta+1)2K\Omega} = 0.64$$

Gain is much Lower than the value obtained with boot-strapping
Due to Lower R_i . Boot-strapping raises the component of input Resistance due to the base biasing network

5.6 From Table 5.1 $k_n' = 100 \mu\text{A}/\text{V}^2$ for $t_{ox} = 20 \text{ nm}$

(a) $V_{DS} \leq V_{GS} - V_t \Rightarrow$ triode region

$$\begin{aligned} i_D &= k_n' \frac{W}{L} \left[(V_{GS} - V_t) V_{DS} - \frac{1}{2} V_{DS}^2 \right] \\ &= 100 \times 10^{-6} \times 10 \left[(5 - 0.8) \times 1 - \frac{1}{2} \times 1 \right] \\ &= 5.7 \text{ mA} \end{aligned}$$

(b) $V_{DS} = V_{GS} - V_t \Rightarrow$ saturation

$$\begin{aligned} i_D &= \frac{1}{2} k_n' \frac{W}{L} (V_{GS} - V_t)^2 \\ &= \frac{1}{2} \times 100 \times 10^{-6} \times 10 (5 - 0.8)^2 = 6.72 \text{ mA} \end{aligned}$$

(c) $V_{DS} < V_{GS} - V_t \Rightarrow$ triode

$$\begin{aligned} i_D &= 100 \times 10^{-6} \times 10 \left[(5 - 0.8) \times 0.2 - \frac{1}{2} \times 0.2^2 \right] \\ &= 0.82 \text{ mA} \end{aligned}$$

(d) $V_{DS} > V_{GS} - V_t \Rightarrow$ saturation

$$i_D = \frac{1}{2} \times 100 \times 10^{-6} \times 10 (5 - 0.8)^2 = 8.82 \text{ mA}$$

5.12

V_{GS} constant : $i_D = k_n' \frac{W}{L} \left[(V_{GS} - V_t) V_{DS} - \frac{1}{2} V_{DS}^2 \right]$

At the onset of saturation:

$$I_D = \frac{1}{2} k_n' \frac{W}{L} (V_{GS} - V_t)^2$$

When i_D decreases to $i_D = \alpha I_D$

$$\Rightarrow k_n' \frac{W}{L} \left[(V_{GS} - V_t) V_{DS} - \frac{1}{2} V_{DS}^2 \right] = \frac{\alpha}{2} k_n' \frac{W}{L} (V_{GS} - V_t)^2$$

$$\Rightarrow (V_{GS} - V_t) V_{DS} - \frac{1}{2} V_{DS}^2 = \frac{\alpha}{2} (V_{GS} - V_t)^2$$

$$\Rightarrow V_{DS}^2 - 2(V_{GS} - V_t) V_{DS} + \alpha (V_{GS} - V_t)^2 = 0$$

$$V_{DS} = (V_{GS} - V_t) - \frac{1}{2} \sqrt{4(V_{GS} - V_t)^2 - 4\alpha(V_{GS} - V_t)^2}$$

⑥

$$\Rightarrow V_{DS} = (V_{GS} - V_t) (1 - \sqrt{1 - \alpha})$$

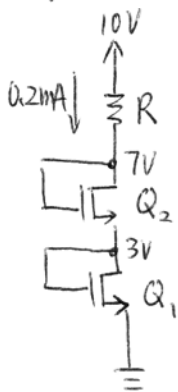
For $V_t = 1V$ and $V_{GS} = 2V$

$$V_{DS} = 1 - \sqrt{1 - \alpha}$$

$$\alpha = 0.5 \Rightarrow V_{DS} = 0.29V$$

$$\alpha = 0.1 \Rightarrow V_{DS} = 0.05V$$

5.37



$$V_t = 2V \quad \mu_n C_{ox} = 20 \mu A/V^2$$

$$\lambda = 0$$

$$L_1 = L_2 = 10 \mu m$$

$$V_{GS1} = 3V$$

$$V_{GS2} = 7V - 3V = 4V$$

Q1 & Q2 both in sat

$$\textcircled{1} I_D = 0.2mA = \frac{1}{2} \mu_n C_{ox} \frac{W_1}{L_1} (V_{GS1} - V_t)^2$$

$$\Rightarrow W_1 = 200 \mu m$$

$$\textcircled{2} I_D = 0.2mA = \frac{1}{2} \mu_n C_{ox} \frac{W_2}{L_2} (V_{GS2} - V_t)^2$$

$$\Rightarrow W_2 = 50 \mu m$$

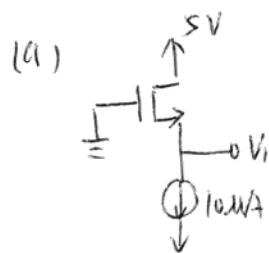
$$R = \frac{(10 - 7)V}{0.2mA} = 15K\Omega$$

5.41

$$V_t = 2V$$

$$K_n' \frac{W}{L} = 0.5 \text{ mA/V}^2$$

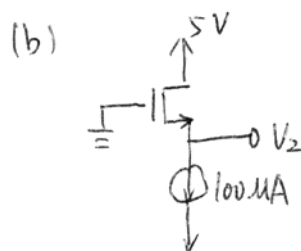
(7)



$$V_b > V_G \Rightarrow \text{saturation}$$

$$10 = \frac{1}{2} 0.5 \times 10^3 (V_{GS} - 2)^2$$

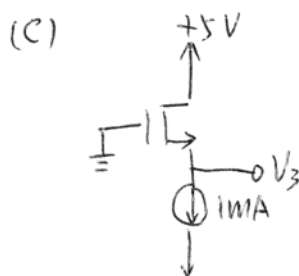
$$V_{GS} = 2.2V \Rightarrow V_1 = -2.2V$$



$$100 = \frac{1}{2} 0.5 \times 10^3 (V_{GS} - 2)^2$$

$$\Rightarrow V_{GS} = 2.63V$$

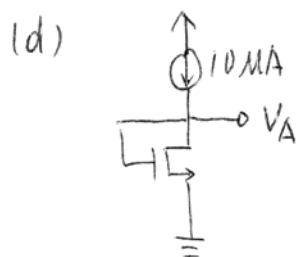
$$\Rightarrow V_2 = -2.63V$$



$$1 = \frac{1}{2} \times 0.5 (V_{GS} - 2)^2$$

$$V_{GS} = 4V$$

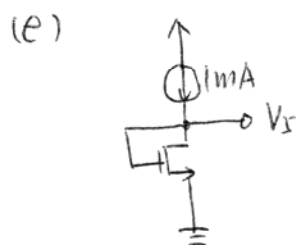
$$V_3 = -4V$$



$$10 = \frac{1}{2} 0.5 \times 10^3 (V_{GS} - 2)^2$$

$$V_{GS} = 2.2V$$

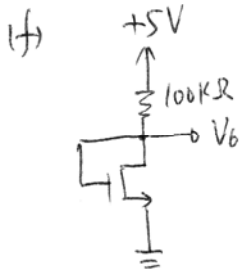
$$V_4 = 2.2V$$



$$1 = \frac{1}{2} \times 0.5 (V_{GS} - 2)^2$$

$$V_{GS} = 4V$$

$$V_5 = 4V$$

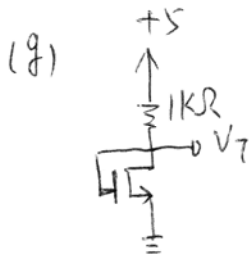


$$\frac{5 - V_6}{100} = \frac{1}{2} \cdot 0.5 (V_6 - 2)^2$$

$$\Rightarrow V_6^2 - 4V_6 + 4 = 0.2 - 0.04V_6$$

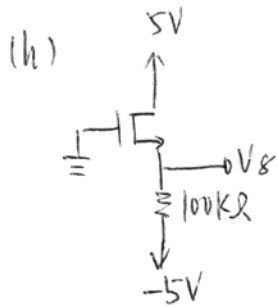
$$V_6 - 3.96V_6 + 3.8 = 0$$

$$\Rightarrow V_6 = 2.33V$$



$$\frac{5 - V_7}{1} = \frac{1}{2} \times 0.5 \times (V_7 - 2)^2$$

$$\Rightarrow V_7 = 4V$$



$$\frac{V_8 + 5}{100} = \frac{1}{2} \cdot 0.5 (-V_8 - 2)^2$$

$$\Rightarrow V_8^2 + 4V_8 + 4 = 0.04V_8 + 0.2$$

$$\Rightarrow V_8^2 + 3.96V_8 + 3.8 = 0$$

$$\Rightarrow V_8 = -2.33V$$