Thin-plate regression splines

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Summary. I discuss the production of low rank smoothers for $d \geq 1$ dimensional data, which can be fitted by regression or penalized regression methods. The smoothers are constructed by a simple transformation and truncation of the basis that arises from the solution of the thinplate spline smoothing problem, and are optimal in the sense that the truncation is designed to result in the minimum possible perturbation of the thin-plate spline smoothing problem given the dimension of the basis used to construct the smoother. By making use of Lanczos iteration the basis change and truncation is computationally efficient. The smoothers allow the use of approximate thin-plate spline models with large datasets; avoid the problems associated with "knot placement" that usually complicate modelling with regression splines or penalized regression splines; provide a sensible way of modelling interaction terms in GAMs; provide low rank approximations to generalized smoothing spline models, appropriate for use with large datasets; provide a means for incorporating smooth functions of more than one variable into non-linear models and improve the computational efficiency of penalized likelihood models incorporating thin-plate splines. Given that the approach produces spline like models with a sparse basis, it also provides a natural way of incorporating un-penalized spline like terms in linear and generalized linear models, and these can be treated just like any other model terms from the point of view of model selection, inference and diagnostics.

Keywords: Thin-plate spline; Regression spline; Generalized additive model

1. Introduction

Smoothing splines (Duchon, 1977; Wahba, 1990; Gu, 2002) provide an excellent means for estimation and inference with models like:

$$y_i = f(x_i) + \epsilon_i, \tag{1}$$

$$y_i = f(x_{1i}, x_{2i}) + \epsilon_i \tag{2}$$

or

$$y_i = f_1(x_{1i}) + f_2(x_{2i}, x_{3i}) + f_3(x_{4i}) + \dots + \epsilon_i$$
(3)

where in all cases y is a response variable, the x's are covariates, the f's are smooth functions and the ϵ terms are random variables (independent for different i).

For example, (1) can be estimated by finding the function from an appropriate reproducing kernel Hilbert space which minimises:

$$\|\mathbf{y} - \mathbf{f}\|^2 + \lambda \int [f''(x)]^2 dx \tag{4}$$

Where y is a vector of y_i 's, f the corresponding vector of $f(x_i)$ values and $\|\cdot\|$ the Euclidian norm. λ is a smoothing parameter, which must be chosen appropriately if the right balance is to be struck between minimising model badness of fit as measured by the first term and model wiggliness as measured by the second. The result of this minimisation turns out to be finite dimensional and is a cubic spline, which is a special case of a thin-plate spline. In general these are obtained as

the solution of the generalization of (4) to problems in which f is a function of any finite number, $d \ge 1$, of covariates and the order, m, of differentiation in the wiggliness penalty can be any integer satisfying 2m > d (see section 2). A further straightforward generalization of (4) is the replacement of the least squares term in the objective with a negative log-likelihood based on an exponential family distribution (see e.g. Green and Silverman, 1994; Gu, 2002).

There are two obstacles to the widespread adoption of thin-plate spline smoothers in practical statistical work. The first is computational. To fit a thin-plate spline to n data requires the estimation of n parameters and an additional smoothing parameter. Except in the case d=1 this involves $O(n^3)$ operations, which is frequently prohibitive. Indeed, without the availability of efficient O(n) algorithms for the d=1 case (e.g. Hutchinson and de Hoog, 1995) it is doubtful that cubic smoothing splines would have achieved their current popularity. (Furthermore, although not generally critical, thin-plate spline fitting problems can have condition numbers in excess of 10^9 , which has the potential to cause problems if a thin plate spline is embedded in a non-linear model, for example.) The second obstacle to widespread adoption of these smoothers is the fact that their use requires a change in modelling methodology relative to conventional linear or generalized linear modelling: the flexibility of a fitted model must be selected by adjusting the smoothing parameter, λ , rather than by adding or dropping model terms. This precludes many model building strategies that are ordinarily used for (generalized) linear models.

One approach to the problem of computational cost is to employ regression splines. The basis implied by solving the spline smoothing problem for a small representative dataset is found and this small basis is used to construct a model for the full dataset of interest. The model is typically fitted as a linear or generalized linear model without imposing a wiggliness penalty. The covariate points used to obtain the reduced basis are known as the "knots" of the regression spline. The number of knots controls the flexibility of the model, but unfortunately their location also tends to have a marked effect on the fitted model (see e.g. Hastie and Tibshirani, 1990, section 9.3). In principle, conventional hypothesis testing based model selection can be used to determine the appropriate flexibility for regression spline models, but in practice there are difficulties. If the knots of order k and order k-1 regression spline models for a data set are arranged to ensure best performance of both models, then the two models will not generally be nested. Alternatively, if knots are not moved, but some knots are simply dropped during model selection then nesting is maintained, but very uneven knot spacings can result: this has undesirable approximation theoretic consequences (see e.g. Wahba 1990, p. ix.). Another more subtle problem with the latter strategy is "knot confounding" (Zhou and Shen, 2001). Finally, when d > 1, even deciding where to place knots so that they appear evenly spread through the covariates can become problematic.

Some of the problems with knot placement can be partially alleviated by abandoning pure regression splines in favour of penalized regression splines (e.g. Wahba, 1980; Parker and Rice, 1985), where the required penalty is that associated with the regression spline basis. But in this case model flexibility is again controlled by a smoothing parameter, λ , rather than the basis dimension, so that some conventional (generalized) linear modelling methods are once again inapplicable.

The first aim of this paper is to find optimal approximations to the thin-plate splines which will remove the computational obstacles to their use, while minimising the deterioration in model performance entailed by the approximation (i.e. to find optimal penalized regression splines). The second aim is to remove the knot placement problem from regression spline modelling in a way that will allow model selection by the hypothesis testing methods usually employed in regression modelling. Two immediate results of achieving these aims are to provide a good way of incorporating smooth function terms into non-linear models, and to provide a way of incorporating thin-plate spline like terms into Generalized Additive Models.

2. Low rank thin-plate spline like smooths

This section begins with standard, but essential, background material on thin-plate splines (Duchon, 1977), and then uses these standard results as the starting point for the production of low-rank smoothers with "good" properties. Purely for simplicity of presentation, I will ignore the possibility of tied covariate values for the moment and cover this later on. Consider the problem of estimating the smooth function $f(\mathbf{x})$ where \mathbf{x} is a d-vector, from $n \geq d$ observations (y_i, \mathbf{x}_i) such that:

$$y_i = f(\mathbf{x}_i) + \epsilon_i$$

where ϵ_i is a random error term. Thin-plate splines can be used to estimate f by finding the function g minimising:

$$\|\mathbf{y} - \mathbf{g}\|^2 + \lambda J_{md}(g) \tag{5}$$

where \mathbf{y} is the vector of y_i data, $\mathbf{g} = (g(\mathbf{x}_1), g(\mathbf{x}_2), \dots, g(\mathbf{x}_n))'$, $J_{md}(g)$ is a penalty functional measuring the wiggliness of g and λ controls the tradeoff between data fitting and smoothness of g. The wiggliness penalty is defined as:

$$J_{md} = \int \dots \int_{\Re^d} \sum_{\nu_1 + \dots + \nu_d = m} \frac{m!}{\nu_1! \dots \nu_d!} \left(\frac{\partial^m g}{\partial x_1^{\nu_1} \dots \partial x_d^{\nu_d}} \right)^2 dx_1 \dots dx_d. \tag{6}$$

Provided that we impose the technical restriction 2m > d, it can be shown that the function minimising (5) has the form:

$$g(\mathbf{x}) = \sum_{i=1}^{n} \delta_i \eta_{md}(\|\mathbf{x} - \mathbf{x}_i\|) + \sum_{j=1}^{M} \alpha_j \phi_j(\mathbf{x})$$
 (7)

where $\pmb{\delta}$ and $\pmb{\alpha}$ are unknown parameter vectors subject to the constraint that $\mathbf{T}'\pmb{\delta} = \mathbf{0}$ and $T_{ij} = \phi_j(\mathbf{x}_i)$. The $M = \begin{pmatrix} m+d-1 \\ d \end{pmatrix}$ functions ϕ_i are linearly independent polynomials spanning the space of polynomials in \Re^d of degree less than m (i.e. the space of polynomials for which J_{md} is zero). Furthermore:

$$\eta_{md}(r) = \begin{cases} \frac{(-1)^{m+1+d/2}}{2^{2m-1}\pi^{d/2}(m-1)!(m-d/2)!} r^{2m-d} \log(r) & d \text{ even} \\ \frac{\Gamma(d/2-m)}{2^{2m}\pi^{d/2}(m-1)!} r^{2m-d} & d \text{ odd.} \end{cases}$$

Now defining matrix ${\bf E}$ by $E_{ij} \equiv \eta_{md}(\|{\bf x}_i - {\bf x}_j\|)$, the spline fitting problem becomes:

minimise
$$\|\mathbf{y} - \mathbf{E}\boldsymbol{\delta} - \mathbf{T}\boldsymbol{\alpha}\|^2 + \lambda \boldsymbol{\delta}' \mathbf{E}\boldsymbol{\delta}$$
 subject to $\mathbf{T}'\boldsymbol{\delta} = \mathbf{0}$ (8)

with respect to δ and α . The function g obtained by solving this system is something of an ideal smoother — it has been constructed by defining exactly what is meant by smoothness, exactly how much weight to give to the conflicting goals of matching the data and making g smooth, and finding the function that best satisfies the resulting smoothing objective. The disadvantage is that the resulting smoother has rather high rank — its computation requires that we estimate as many parameters as there are data: except for the case when d=1 this means that the calculations require $O(n^3)$ operations. See Wahba (1990) or Green and Silverman (1994) for further information about thin-plate splines .

2.1. Constructing an optimal approximating basis

In this section a family of low rank smoothers is constructed by starting from the ideal smoothing problem (8), finding the parameter space basis of a given rank that perturbs this problem as little as possible and solving the resulting low rank problem. The basis of the un-penalized functions is left unchanged — since these are the functions of zero wiggliness according to the measure used, it would make little sense to truncate their basis. I will concentrate instead on the basis for the δ parameter space. The ideal basis would be one that results in minimum change of both the goodness of fit term and the penalty term for any given δ , but of course no single basis can achieve this for all δ , so less ambitious criteria must be adopted.

To motivate the criteria for choosing a truncated basis, consider the rank k matrix Γ_k , the columns of which form a k dimensional orthonormal basis for the δ parameter space, so that $\delta = \Gamma_k \delta_k$ where δ_k is a k vector. Note that k must be greater than M. Within the space spanned by Γ_k problem (8) becomes:

minimise
$$\|\mathbf{y} - \mathbf{E}\Gamma_k \boldsymbol{\delta}_k - \mathbf{T}\boldsymbol{\alpha}\|^2 + \lambda \boldsymbol{\delta}_k' \Gamma_k' \mathbf{E}\Gamma_k \boldsymbol{\delta}_k$$
 subject to $\mathbf{T}'\Gamma_k \boldsymbol{\delta}_k = \mathbf{0}$

Defining the rank k matrices $\tilde{\mathbf{E}}_k = \mathbf{E}\Gamma_k\Gamma_k'$ and $\hat{\mathbf{E}}_k = \Gamma_k\Gamma_k'\mathbf{E}\Gamma_k\Gamma_k'$, (8) can be written as:

minimise
$$\|\mathbf{y} - \tilde{\mathbf{E}}_k \boldsymbol{\delta} - \mathbf{T} \boldsymbol{\alpha}\|^2 + \lambda \boldsymbol{\delta}' \hat{\mathbf{E}}_k \boldsymbol{\delta}$$
 subject to $\mathbf{T}' \boldsymbol{\delta} = \mathbf{0}$ (9)

where $\delta = \Gamma_k \delta_k$. An ideal Γ_k would induce a problem of the form (9) that is as close as possible to the problem (8). To find such a basis requires definition of what constitutes "as close as possible".

Considering the least squares term first, it is clear that the goal of minimising the change in this term for all y, δ (or even for those y, δ consistent with being best fits according to the objective) can not be achieved with a single basis selected independently of the data and parameter values. Instead, for a given δ , I focus on trying to minimise the change in fitted values ($\mathbf{E}\delta + \mathbf{T}\alpha$) caused by the substituting \mathbf{E} with $\tilde{\mathbf{E}}_k$, the rank deficient approximation induced by the change and truncation of basis. The basis change and truncation will cause a change ($\mathbf{E} - \tilde{\mathbf{E}}_k$) δ in the fitted values. It is clearly not possible to find a single basis that will uniformly minimise this quantity for all δ , but a more feasible objective is obtained by weakening requirements further and seeking to minimise the "worst" possible change:

$$\epsilon_k = \max_{oldsymbol{\delta}
eq \mathbf{0}} \frac{\| (\mathbf{E} - \tilde{\mathbf{E}}_k) \boldsymbol{\delta} \|}{\| \boldsymbol{\delta} \|}$$

where $\|\cdot\|$ is the usual Euclidian norm. The scaling by $\|\delta\|$ is necessary to ensure, for example, that the resulting smooths do not have different behaviours when different measurement scales for y_i are used. The intuitive idea is that the basis change and truncation should make minimal change to the model fit, although the measure used for this necessarily weakens the intuitive criterion a little.

Turning to the penalty term, similar reasoning suggests that a suitable measure of the worst possible change introduced by the basis truncation is:

$$e_k = \max_{\boldsymbol{\delta} \neq \mathbf{0}} \frac{\boldsymbol{\delta}'(\mathbf{E} - \hat{\mathbf{E}}_k)\boldsymbol{\delta}}{\|\boldsymbol{\delta}\|^2}$$

and again the aim is to choose the basis minimising this quantity, for a given k. The intuitive idea is that the basis change and truncation should make minimal change to the shape of the smooth function as measured by the penalty functional.

Given the goal of simultaneously minimising e_k and ϵ_k , the appropriate basis to use turns out to be a truncated eigenbasis of **E**. Specifically let $\mathbf{E} = \mathbf{U}\mathbf{D}\mathbf{U}'$ where **D** is a diagonal matrix of

eigenvalues of \mathbf{E} arranged so that $|D_{i,i}| \geq |D_{i+1,i+1}|, i=1,\ldots n-1$, and \mathbf{U} is a matrix whose i^{th} column is the eigenvector corresponding to $D_{i,i}$. The best basis of rank k is given by \mathbf{U}_k (i.e. by setting $\Gamma_k = \mathbf{U}_k$): the first k columns of \mathbf{U} , which implies that $\hat{\mathbf{E}}_k = \tilde{\mathbf{E}}_k = \mathbf{U}_k \mathbf{D}_k \mathbf{U}_k'$ (= \mathbf{E}_k , say).

It is easy to demonstrate that the chosen basis minimises ϵ_k . $\epsilon_k = \|\mathbf{E} - \tilde{\mathbf{E}}_k\|_2$, the spectral norm of $\mathbf{E} - \tilde{\mathbf{E}}_k$ (see e.g. Watkins 1991). But it is well known that of all rank k matrices \mathbf{F}_k , the matrix \mathbf{E}_k based on truncating the eigenvalues of smallest magnitude in the spectral decomposition of \mathbf{E} , minimises $\|\mathbf{E} - \mathbf{F}_k\|_2$ (see, e.g. Watkins 1991, p413).

Demonstrating that the basis also minimises e_k is only slightly more involved. First define the (symmetric) matrix $\Delta_k = \mathbf{E} - \hat{\mathbf{E}}_k$. It is straightforward to produce a square root of Δ_k , $\Delta_k^{1/2}$, by taking square roots of the eigenvalues of Δ_k in its spectral decomposition. This means that:

$$e_k = \max_{\boldsymbol{\delta} \neq \mathbf{0}} \frac{\|\boldsymbol{\Delta}_k^{1/2} \boldsymbol{\delta}\|^2}{\|\boldsymbol{\delta}\|^2}$$

so that $e_k = \|\boldsymbol{\Delta}_k^{1/2}\|_2^2$, the squared spectral norm of $\boldsymbol{\Delta}_k^{1/2}$. Since the spectral norm of a matrix is given by its largest singular value (which here corresponds to the magnitude of its largest (magnitude) eigenvalue), it is clear from the construction of $\boldsymbol{\Delta}_k^{1/2}$ that $\|\boldsymbol{\Delta}_k^{1/2}\|_2^2 = \|\boldsymbol{\Delta}_k\|_2 = \|\mathbf{E} - \hat{\mathbf{E}}_k\|_2$, and hence that e_k is minimised by the same basis that minimizes ϵ_k . (This somewhat remarkable fact is clearly rather special to splines, as is easily verified by considering more general penalized regression problems.)

So, given the choice of basis, $\delta = \mathbf{U}_k \delta_k$ (in which case $\delta_k = \mathbf{U}_k' \delta$) and the approximation to (8) becomes:

minimise
$$\|\mathbf{y} - \mathbf{U}_k \mathbf{D}_k \boldsymbol{\delta}_k - \mathbf{T} \boldsymbol{\alpha}\|^2 + \lambda \boldsymbol{\delta}_k' \mathbf{D}_k \boldsymbol{\delta}_k$$
 subject to $\mathbf{T}' \mathbf{U}_k \boldsymbol{\delta}_k = \mathbf{0}$

Now find any orthogonal column basis \mathbf{Z}_k such that $\mathbf{T}'\mathbf{U}_k\mathbf{Z}_k = \mathbf{0}$ (QR or QT factorization will provide this easily, see e.g. Gill, Murray and Wright, 1981). Restricting $\boldsymbol{\delta}_k$ to this space by writing $\boldsymbol{\delta}_k = \mathbf{Z}_k \tilde{\boldsymbol{\delta}}$ yields the unconstrained problem that must be solved to fit this "best" rank k approximation to the smoothing spline:

$$\text{minimise } \|\mathbf{y} - \mathbf{U}_k \mathbf{D}_k \mathbf{Z}_k \tilde{\boldsymbol{\delta}} - \mathbf{T} \boldsymbol{\alpha}\|^2 + \lambda \tilde{\boldsymbol{\delta}}' \mathbf{Z}_k' \mathbf{D}_k \mathbf{Z}_k \tilde{\boldsymbol{\delta}}$$

with respect to $\tilde{\boldsymbol{\delta}}$ and $\boldsymbol{\alpha}$. Having fitted the model, evaluation of the spline at any point is easy: just evaluate $\boldsymbol{\delta} = \mathbf{U}_k \mathbf{Z}_k \tilde{\boldsymbol{\delta}}$ and use (7). In the rest of this paper I will often refer to the parameter vector and design matrix of a t.p.r.s as $\boldsymbol{\beta}' \equiv [\tilde{\boldsymbol{\delta}}', \boldsymbol{\alpha}']$ and $\mathbf{X} \equiv [\mathbf{U}_k \mathbf{D}_k \mathbf{Z}_k, \mathbf{T}]$ respectively and the wiggliness penalty matrix as \mathbf{S} , which will have $\mathbf{Z}'_k \mathbf{D}_k \mathbf{Z}_k$ in its top left corner and zeroes elsewhere, so that the wiggliness penalty is $\boldsymbol{\beta}' \mathbf{S} \boldsymbol{\beta}$.

These thin-plate regression splines can be treated as pure regression splines by setting λ to zero. In this case model selection becomes a matter of choosing k, which can be performed either by criteria like GCV, AIC etc, or by conventional hypothesis testing based model selection, since the columns of $\mathbf{U}_{k-1}\mathbf{D}_{k-1}\mathbf{Z}_{k-1}$ clearly span a subspace of the space spanned by the columns of $\mathbf{U}_k\mathbf{D}_k\mathbf{Z}_k$ (the subspace of the latter is the intersection of the null space of the constraints and the subspace spanned by $\mathbf{U}_k\mathbf{D}_k$ while the subspace of the former is the intersection of the same null space of the constraints with a subspace of $\mathbf{U}_k\mathbf{D}_k$). Of course the model terms are not orthogonal, but since there is a natural order in which to consider their deletion from the model, this does not matter for practical purposes.

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Alternatively thin-plate regression splines can be treated as penalized regression splines, in which case the value chosen for k will not be critical (see Eilers and Marx, 1996, for illustration of this in the case of "P-splines"), but should be somewhat larger than the degrees of freedom believed to be required for the modelling situation concerned. The actual model degrees of freedom will be controlled by λ , which must be selected by some criterion like GCV, GML, AIC (see e.g. Craven and Wahba,1979; Wahba, 1990; Akaike 1973) or by considering the spline as a random effect. In practice k should probably be increased if the estimated λ is too close to zero: one pragmatic approach would be to increase k if the estimated degrees of freedom (see section 3.1) for a t.p.r.s. exceeds some specified proportion (e.g. 0.8-0.9) of the basis dimension. Note that in the penalized case (6) has not been replaced by an approximate penalty: $\tilde{\delta}' \mathbf{Z}_k' \mathbf{D}_k \mathbf{Z}_k \tilde{\delta}$ is exactly (6) for any function in the truncated space.

Tied covariate values are dealt with by simply reducing the data set to one involving only unique covariate combinations, setting up the thin-plate regression spline for this reduced data set, and then duplicating rows of the resulting $U_kD_kZ_k$ and T matrices as necessary in order to model the full set of data.

This section has presented a way of obtaining approximate thin-plate splines, which are suitable for incorporation into a wide range of model structures. The approximations are "optimal", but in a slightly weak sense: the criteria are not minimized subject to the linear restrictions $\mathbf{T}'\delta=\mathbf{0}$ that are applied for model fitting (it isn't possible to minimize both criteria simultaneously under that restriction). None-the-less, given the good performance of the approximation reported below, it is useful to know the sense in which the approximation is optimal (and in practice it was the search for some sort of optimality that lead to the approach reported here, rather than more obvious approaches).

2.2. Computational issues

Discarding the small magnitude eigenvectors of \mathbf{E} can only improve the numerical conditioning of the thin-plate regression splines relative to full thin-plate splines, but in addition they have two further computational advantages:

- (a) For small datasets they can be implemented very easily using linear algebra routines readily available in standard statistical packages.
- (b) For large datasets it is possible to obtain t.p.r.s. bases very efficiently using Lanczos iteration.

The first point is best appreciated by examining the steps, given in Appendix 1, for implementing thin-plate regression splines using standard software. Such an approach might be appropriate for incorporating smooth functions into a linear, generalized linear or non-linear model of a relatively small set of data.

For larger data sets the potential *computational* benefits of the t.p.r.s. approach relative to full t.p.s. models will only be fully realized if the truncated eigen-decomposition of ${\bf E}$ can be calculated in substantially fewer than the $O(n^3)$ operations required for a full eigen-decomposition. Lanczos iteration (see e.g. Demmel 1997) is a method which obtains the truncated eigen-decomposition in $O(kn^2)$ operations, by iteratively building up a tridiagonal matrix the eigenvalues of which converge (in order of decreasing magnitude) to those required, as iteration proceeds. Appendix 2 gives details of an implementation that is suitable for use with ${\bf E}$. Note, for example, that fitting a t.p.r.s. to 5000 data using k=50, will be of the order of 100 times faster using an $O(kn^2)$ algorithm as opposed to a standard $O(n^3)$ algorithm.

In the context of very large data sets, even greater computational efficiency could be achieved by using an approximate eigen-decomposition calculated using the Nyström methods described, for example, in Williams and Seeger (2001) (see also Smola and Schölkopf, 2000, for a related approach — I am grateful to an anonymous referee for pointing this out). However in such cases it is probably more straightforward to subsample the data (e.g. randomly select 1000 data points), produce a t.p.r.s. basis for this subsample and use this basis for the model of the whole data set.

Finally, note two computational tricks for avoiding poor numerical conditioning. Firstly, when m > 2, colinearity in the columns of \mathbf{T} can be avoided by subtracting the mean from each covariate, so that each is centred around zero. Secondly, it is worth linearly transforming the model parameters to ensure that the columns of \mathbf{X} have broadly similar average element sizes, otherwise "poor scaling" of \mathbf{X} can sometimes detract from numerical stability.

3. Practical properties: some simulation results

This section provides some straightforward illustrations of the advantages of the thin-plate regression spline approach, relative to the more obvious "knot placement" approaches and to full spline smoothing.

3.1. Comparison with "knot based" regression splines

The suggested thin-plate regression spline (t.p.r.s.) basis allows model selection using conventional hypothesis testing approaches in a way that is difficult using traditional regression splines. Furthermore, given its theoretical motivation, a t.p.r.s. should be better able to represent most smooth functions than a smoother based on selecting a small set of "knots" with which to construct a basis.

To illustrate the latter point, 100 random x, z points in the unit square were chosen and the test function:

$$f(x,z) = \frac{0.75}{\pi \sigma_x \sigma_z} e^{-(x-0.2)^2/\sigma_x^2 - (z-0.3)^2/\sigma_z^2} + \frac{0.45}{\pi \sigma_x \sigma_z} e^{-(x-0.7)^2/\sigma_x^2 - (z-0.8)^2/\sigma_z^2}$$
(10)

was evaluated at each ($\sigma_x=0.3, \sigma_z=0.4$). The function was then reconstructed by fitting these data using a rank 16 t.p.r.s. and a more traditional rank 16 regression spline. The traditional regression spline was constructed by placing 16 points on a regular lattice across the unit x,z square, and obtaining the basis that would have resulted by fitting a thin-plate spline to response data at these 16 points. This basis was then used to represent the function to be fitted to the 100 data points from the test function. 16 dimensional bases were chosen because this allows a favourable regular lattice to be used for the knot based spline, but is also close to the basis dimension selected by hypothesis testing in the next example in this subsection. The results are shown in figure 1. For this rank of smoother in this example the t.p.r.s. improves considerably on the knot based spline. Such differences become less marked for much higher or lower ranks, but for pure regression spline modelling (as opposed to penalized regression spline modelling), intermediate ranks are of most interest (rank 15 is selected for this test function in the next example). The ability of the t.p.r.s. to represent underlying functions using relatively few parameters should reduce estimator variances relative to approaches requiring more parameters.

The example shown in figure 1 was also repeated with noisy data. 100 parameter sets were generated at each of 7 noise levels. For each replicate, $100 (x_i, z_i)$ points were generated randomly from a uniform distribution on the unit square. (10) was evaluated at each point, and perturbed by additive Gaussian noise with standard deviation σ . The test function was reconstructed by fitting a t.p.r.s. and a knot based spline to each replicate, with the mean square reconstruction error (MSE) calculated for both methods (means taken over the $100 x_i, z_i$ points). The following table summarizes the results in terms of $\Delta_{MSE} = [MSE(\text{knot based}) - MSE(\text{t.p.r.s.})]/MSE(\text{t.p.r.s.})$.

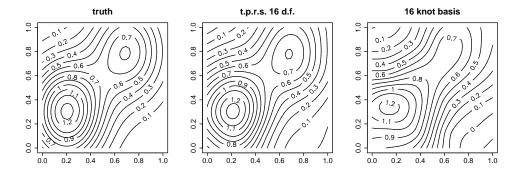


Fig. 1. Comparison of alternative reconstructions of the smooth function shown in the left hand panel, using different low rank spline based approaches. The two right hand panels both show reconstructions from the same set of 100 (noise free) samples from the true function on the left (the sample points were randomly placed over the function domain shown). The middle panel results form using a rank 16 thin-plate regression spline basis of the type proposed in this paper. The right hand panel results from using a rank 16 basis constructed by dividing the domain into 16 equal squares and placing a point at the centre of each. The thin-plate spline basis that would result from fitting a thin-plate spline to data at just these 16 points was then used as the model basis (e.g. Wahba 1980).

σ	mean Δ_{MSE}	min. Δ_{MSE}	max. Δ_{MSE}	$\Delta_{MSE} > 0$
0	4.85	0.31	22.77	100
0.01	4.68	0.40	16.00	100
0.02	3.34	0.44	20.62	100
0.05	1.32	0.01	5.38	100
0.1	0.42	-0.07	1.76	96
0.2	0.12	-0.31	0.83	71
0.5	0.02	-0.49	0.70	52

The final column in the table gives the number of replicates, out of 100, in which the t.p.r.s. had a lower mean square error than the knot based spline. This comparison is of performance in a pure regression context: section 3.2 also reports comparisons of t.p.r.s. and knot based splines in the context of penalized regression modelling.

Turning to model selection: one approach is to start with a basis that is over-parameterized and to truncate it until the truncated model differs significantly from the over-parameterized model according to a conventional hypothesis test. As an example, data were simulated from (10), by randomly choosing $100 \ x_i, z_i$ locations in the unit square, and then forming data:

$$y_i = f(x_i, z_i) + \epsilon_i$$

where the ϵ_i were i.i.d. $N(0,0.1^2)$. Let rss_k denote the residual sum of squares for the rank k t.p.r.s. model of these data. Testing the null hypothesis that the rank k_0 basis describes the model generating the data against the larger alternative that the rank k_1 basis is appropriate uses the standard result that under the null:

$$\frac{(rss_{k_0} - rss_{k_1})/(k_1 - k_0)}{rss_{k_1}/(n - k_1)} \sim F_{k_1 - k_0, n - k_1}$$

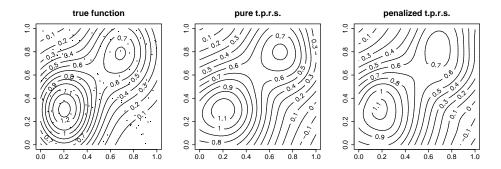


Fig. 2. Comparison of a pure thin-plate regression spline selected by ANOVA and a penalized thin-plate regression spline. The left panel is the true underlying function from which data have been sampled with Gaussian error ($\sigma=0.1$), at the n=100 randomly chosen sample locations shown. The middle panel is a pure regression spline fitted to the data, with the rank (15) of the basis chosen using conventional F-ratio testing. The right panel shows a penalized regression spline fit to the same data, with the smoothing parameter, λ , chosen by GCV (effective degrees of freedom 22).

where n is the number of data. This result depends on the nested nature of the t.p.r.s. bases of different ranks. In practice, starting from a k_1 that is larger than is needed, k_0 is reduced until the above F-ratio is significant at the investigators favourite level. Figure 2 shows the results of applying this approach with a significance level of 5% to select a pure t.p.r.s. model for simulated data and compares this to a penalized t.p.r.s model of the same data where smoothing parameter (λ) selection was by GCV. k_1 was set to 40, as was k for the penalized model. GCV selected 22 effective degrees of freedom for the model (for penalized models effective degrees of freedom are defined as $\operatorname{tr}(\mathbf{X}(\mathbf{X}'\mathbf{X}+\hat{\lambda}\mathbf{S})^{-1}\mathbf{X})$, where $\hat{\lambda}$ is the estimated smoothing parameter, see e.g. Wahba, 1990). Significance testing at the 5% level selected 15 degrees of freedom. This sort of difference is expected, since GCV is a mean square prediction error criterion, while hypothesis testing addresses the question of how simple a model is plausible for a set of data.

3.2. Comparison with "full" spline models

What is gained and what is lost by using thin-plate regression splines rather than full thin-plate splines?

One expected gain is computational speed. To illustrate this some timing experiments were carried out using full generalized smoothing spline models as implemented in R package gss, and using thin-plate regression splines as implemented (by the author) in R package mgcv. The results are for estimating the Generalized Additive Model (see section 4):

$$\log(\mu_i) = f_1(x_i, z_i) + f_2(w_i)$$

where the response variable $y_i \sim \operatorname{Poi}(\mu_i)$, $i=1,\ldots,n$ and the f_1 and f_2 used for simulation were both quadratics. Timings given are CPU seconds (on a PII 400Mhz running Linux). The thin-plate penalized regression spline based model used a total of 50 parameters and all smoothing parameters were estimated by GCV. The results were:

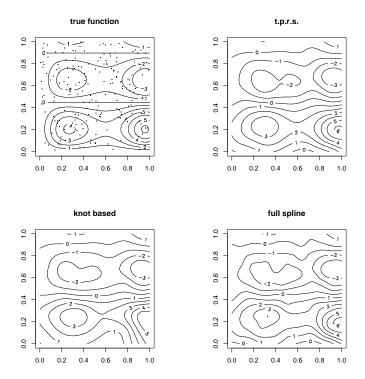


Fig. 3. Example reconstructions of the function in upper left panel, from observations of the function taken at the randomly chosen points plotted on the upper left panel and perturbed with zero mean normal random deviates with standard deviation 0.5. The upper right panel shows a penalized thin-plate regression spline reconstruction using a 49 dimensional basis. The lower left panel shows an equivalent reconstruction using a thin-plate spline with a 49 knot basis, where the knots are on a regular 7×7 grid. The lower right panel shows a full thin-plate spline reconstruction. For all three reconstructions GCV was used to to select the smoothing parameter.

n	gss	t.p.r.s.	
100	2.68	1.75	
200	11.31	2.82	
400	88.07	4.38	
600	316.49	6.46	
1200	2530*	15.65	

The 0.25Gb of memory available on the test computer was insufficient for gss above n=600, so the final gss timing is estimated from the cubic dependence on n. As expected, the thin-plate regression splines produce quite large reductions in the computational effort required. Partly, this is because the t.p.r.s. calculations are at most $O(kn^2)$, rather than the $O(n^3)$ required for GSS models, but the computational saving is actually greater than the simple comparison of leading order terms would suggest, since the computationally costly model selection algorithm is $O(n^3)$ for the GSS case but only $O(nk^2)$ in the t.p.r.s. case.

The obvious expected loss from using thin-plate regression splines would be a degradation of

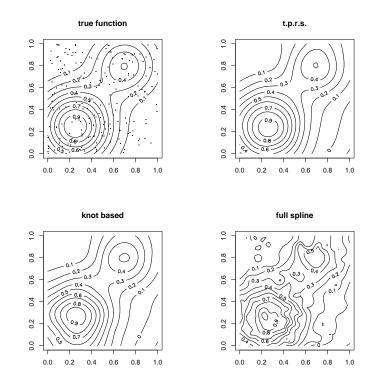


Fig. 4. As figure 3, except that the reconstructions are of the function plotted in the upper left panel and both the knot placement basis and the t.p.r.s. basis were of dimension 36. The noise standard deviation in this case was 0.05. This example shows one of the occasional overfits produced by the full spline model with smoothness selected by GCV.

mean square error performance. To examine this, experiments were performed using two test functions:

$$f_1(x,z) = 1.9[1.45 + e^x \sin(13(x - 0.6)^2)]e^{-z} \sin(7z)$$

and

$$f_2(x,z) = e^{[-(x-0.25)^2 - (z-0.25)^2]/0.1} + 0.5e^{[-(x-0.7)^2 - (z-0.7)^2]/0.07}$$

Each test function was sampled at a set of 200 randomly chosen points in the unit square, and the function values at these points were perturbed with additive independent normal random deviates ($\sigma = 0.5$ for f_1 and $\sigma = 0.05$ for f_2). 100 replicate data sets were generated for each model (design points and error were different for each replicate), and for each replicate the mean square errors (MSE) in reconstructing f_1 and f_2 was assessed for a t.p.r.s., a knot based spline and a full thin-plate spline. For each replicate the MSE was averaged over all design points. The basis dimensions for the knot basis and the t.p.r.s. were both 49 for f_1 and 36 for f_2 : choices made to ensure that the knot basis operated on a favourable square regular grid, while the model estimated degrees of freedom were below 3/4 of the basis dimension. For all models the smoothing parameter, λ , was selected by GCV. The full t.p.s. model was fitted using R package gss, other models were fitted using mgcv. The results are summarized below:

	f_1		f_2	
	full t.p.s.	knot basis	full t.p.s.	knot basis
Outperformed t.p.r.s. /100	5	30	0	9
Best MSE advantage	0.0033	0.0075	_	2.2×10^{-5}
Worst MSE disadvantage	0.18	0.050	2.2×10^{-2}	1.9×10^{-4}
Mean MSE difference	0.0091	0.0084	1.7×10^{-4}	5.5×10^{-5}
Mean MSE	0.059	0.058	5.5×10^{-4}	4.3×10^{-4}

The first row gives the number of times that the MSE of each competing method was lower than the MSE of the t.p.r.s. The t.p.r.s. has superior performance in most cases. The second row shows the largest MSE difference between the t.p.r.s. and a competing method when the t.p.r.s had the larger MSE. The third row shows the largest difference between a competing method and a t.p.r.s. when the t.p.r.s. had the smaller MSE. The fourth row shows the mean difference in MSE between each competing method and the t.p.r.s: note that the t.p.r.s. has the lower mean MSE in all cases. The mean MSE for the t.p.r.s. method was 0.050 for f_1 and 3.8×10^{-4} for f_2 . The table shows that the t.p.r.s. usually has the better MSE performance, and has better MSE performance on average: in the most extreme cases the improvement is of the same order as the t.p.r.s. MSE, while the occasional improvements of the competing methods over the t.p.r.s. are quite modest in size.

Figure 3 shows a randomly chosen example comparison of reconstructions of f_1 using the three alternative methods. Figure 4 shows equivalent example comparative reconstructions for f_2 — for illustrative purposes this shows the worst overfit by the full thin-plate spline model obtained in 3 trial runs

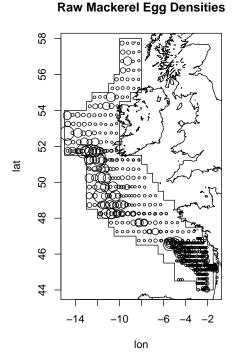
At first sight the improvement of the truncated model relative to the full spline model is counter-intuitive, but it almost certainly reflects the fact that for the full thin plate spline the degree of model complexity is chosen entirely by GCV, while the t.p.r.s. is already restricted to a space of relatively smooth functions: hence the full t.p.s. is free to substantially overfit the data in a way that the t.p.r.s. can not. For these examples, where the underlying truth is smooth and any possible reduction in bias that might be obtainable by using the full t.p.s. is dwarfed by sampling variability, the t.p.r.s. hence has an advantage.

4. Example: Generalized additive models

One obvious use of thin-plate regression splines is as a way of efficiently incorporating multidimensional smooths into generalized additive models (GAMs), in a manner that allows statistically well founded model selection for such models. GAMs address the problem of modelling response data y_i from an exponential family distribution, in terms of multiple covariates $x_{1i}, x_{2i}, x_{3i}, \ldots$ using a model structure of the form:

$$q(\mu_i) = \alpha_i + f_1(x_{1i}) + f_2(x_{2i}, x_{3i}) + \dots$$
(11)

where $\mu_i \equiv E(y_i)$, g is a monotonic link function, the f's are smooth functions to be estimated and α_i represents any strictly parametric model components (e.g. a simple constant, or perhaps a linear term in another covariate, or whatever). i.e. the key feature of these models is that the mean of the response depends on the covariates through a sum smooth terms, each of which is a function of only one or a few covariates. Side conditions are required to ensure identifiability. To date users of these methods have had a choice between the mathematically elegant but computationally very costly generalized smoothing spline (GSS) approach of Wahba, Gu and co-workers in which the model estimation problem is formulated as a variational problem in an appropriate reproducing kernel Hilbert space (e.g. Wahba, 1990; Gu and Wahba, 1993; Wahba et al. 1995; Gu 2002), or of the



GAM predicted egg density

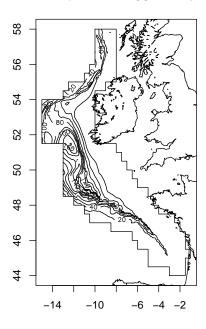


Fig. 5. Raw data and fitted model predictions for the mackerel egg generalised additive modelling example. The left panel shows the raw egg density data: circle area is proportional to density, with the circles being centred on the sample haul locations. The right panel shows the fitted model daily egg production densities.

more ad hoc, but much more efficient methods of Hastie & Tibshirani (1990). The GSS approach has the advantage that it is feasible to select the wiggliness of the components of the GAM using well founded criteria such as GCV, GML or AIC, and that model inference has a solid theoretical underpinning. In order to maintain computational efficiency, Hastie and Tibshirani type GAMs rely on more ad hoc approaches to model selection, and require a slightly less well founded approach to inference. In practice the much greater computational efficiency of Hastie and Tibshirani's approach has meant that it is the more widely used.

The thin-plate regression splines provide a means by which it should be possible to retain many of the advantages of the GSS approach to GAMs in terms of well founded model selection and good practical properties deriving from a firm theoretical basis, while also benefiting from the kind of computational efficiency that characterises Hastie and Tibshirani's approach.

In practice it is straightforward to represent a GAM by producing a thin-plate regression spline basis for each model term. Taking the example of the model (11) and assuming that the parametric term consists only of a constant, then a design matrix \mathbf{X}_i and wiggliness penalty matrix \mathbf{S}_i would be produced for each component smooth function f_i . The design matrix for the whole model is then something like: $\mathbf{X} \equiv [\mathbf{1}, \mathbf{X}_1, \mathbf{X}_2, \ldots]$ (where 1 is a column of 1's). Writing the parameter vector for the i^{th} term as β_i then an appropriate side condition ensuring model identifiability would be

that the sum of f_i evaluated over all observed covariate values should be zero. i.e. $\mathbf{1}'\mathbf{X}_i\boldsymbol{\beta}_i=0$ (where 1 is an appropriate column vector of 1's). Writing $\boldsymbol{\beta}'=[\boldsymbol{\alpha}',\boldsymbol{\beta}_1',\boldsymbol{\beta}_2',\ldots]$ (where $\boldsymbol{\alpha}$ is the vector of parameters of the strictly parametric part of the model α_i), we have that the model would be estimated by maximising the penalized log-likelihood:

$$l(\boldsymbol{\beta}) - \frac{1}{2} \sum_{i} \lambda_{i} \boldsymbol{\beta}_{i}' \mathbf{S}_{i} \boldsymbol{\beta}_{i}. \tag{12}$$

subject to the linear identifiability constraints on β , where l is the log-likelihood of the model, and the penalty terms penalise model components for being wiggly. (12) is solved by penalized iteratively re-weighted least squares (see e.g. Wood, 2000), so that given the k^{th} estimate of the parameter vector, $\beta^{[k]}$, $\beta^{[k+1]}$ is found by solving the weighted penalized least squares problem:

minimise
$$\|\mathbf{W}^{[k]}(\mathbf{z}^{[k]} - \mathbf{X}\boldsymbol{\beta})\|^2 + \sum_i \lambda_i \boldsymbol{\beta}_i' \mathbf{S}_i \boldsymbol{\beta}_i$$

where $\mathbf{z}^{[k]} \equiv \mathbf{X}\boldsymbol{\beta}^{[k]} + \boldsymbol{\Gamma}^{[k]}(\mathbf{y} - \boldsymbol{\mu}^{[k]}), \mathbf{W}^{[k]}$ is a diagonal matrix with $W_{ii}^{[k]} \equiv [g'(\mu_i^{[k]})^2 V_i^{[k]}]^{-1/2},$ $V_i^{[k]}$ is the variance of y_i according to the estimates, $\mu_i^{[k]}$, implied by $\boldsymbol{\beta}^{[k]}$, and $\boldsymbol{\Gamma}^{[k]}$ is a diagonal matrix with $\Gamma_{ii}^{[k]} \equiv g'(\mu_i^{[k]})$. Again, solution is subject to the linear constraints on $\boldsymbol{\beta}$ that ensure identifiability. Estimation of smoothing parameters is performed at each iterate using a generalization (Wood, 2000) of the multiple smoothing parameter GCV method of Gu and Wahba (1991).

As an example of the use of these methods I modelled some fisheries data first analysed using GAMs by Borchers et al. (1997). The response data are densities per m^2 of sea surface of mackerel eggs produced per day at each of 634 survey locations, along with covariates at each station. The response data have been gathered from research vessels by hauling sampling nets vertically through the water column. Some pre-processing was done to convert the raw data to egg densities produced per day. The purpose of the surveys is to estimate total egg production rate, in order to be able to estimate the total mass of parent fish required to produce this rate. An important part of the estimation process is the modelling of the egg distribution. The method is one of the few feasible ways of assessing fish stock size without recourse to commercial fisheries data. The latter tend to suffer from severe biases.

The data to be modelled are shown in the left panel of figure 5. Since the modelling of these data is not the primary purpose of this paper, I will use a relatively unsophisticated error structure, and will not discuss model term selection here, rather I will assume that the important covariates to consider are sea bed depth, distance from the 200m sea bed depth contour, longitude and latitude. Each of the covariates is available for all 634 egg density estimates. In the original GAM analysis of these data, Borchers et al. (1997) modelled egg abundance using a sum of 4 univariate smooths of these 4 covariates, but there are strong arguments for not modelling the dependence on longitude and latitude in this way, instead using a bivariate smooth function of longitude and latitude (given the isotropic nature of thin-plate regression splines there is also an argument for replacing longitude and latitude with co-ordinates on a squarer grid, but to maintain comparability with the Borchers et al. analysis I have not done that here). Consequently, the model structure used was:

$$\sqrt{y_i} = \alpha + f_1(\log_i, \log_i) + f_2(\text{c.dist}_i) + f_3(\text{b.depth}_i) + \epsilon_i$$

where the ϵ_i are i.i.d. normal random variables, y_i is the i^{th} observation of egg density produced per day and lo, la, b.depth and c.dist are longitude, latitude, sea bed depth and distance to the 200m contour respectively. f_2 and f_3 were represented using rank 10 t.p.r.s. bases, while f_1 used a rank 50 t.p.r.s. basis. The square root transform was employed to stabilize variances. Using the mgcv package this model was fitted with the command:

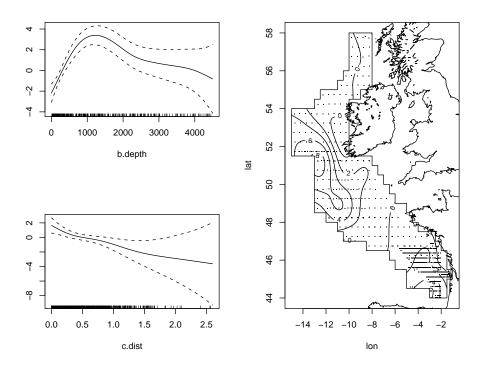


Fig. 6. The estimated model terms for the mackerel egg GAM. The right panel contours the smooth function of longitude and latitude and shows the sample locations. The top left panel shows the smooth function of sea bed depth and 95% confidence limits, while the lower left panel shows the smooth function of distance from 200m contour and its 95% confidence limits.

 $mack.mod < -gam(y^0.5 color, la, k=50) + s(c.dist) + s(b.depth), data=mack)$

Figure 6 shows the estimated model terms, while the right panel of figure 5 contours the fitted model egg density daily production estimates (the plots in figure 5 are essentially those produced by using plot.gam from mgcv: plot(mack.mod), although the right hand panel has been modified). The plotted confidence intervals are obtained using the approximation that the parameter estimators are normally distributed about their true values, with a covariance matrix than can be estimated as: $\mathbf{Z}(\mathbf{Z}'\mathbf{X}'\mathbf{W}^2\mathbf{X}\mathbf{Z} + \sum \lambda_i \mathbf{Z}'\mathbf{S}_i \mathbf{Z})^{-1}\mathbf{Z}'\hat{\sigma}^2$, where \mathbf{Z} is a column basis for the null space of the identifiability constraints on the model, $\hat{\sigma}^2 = \|\mathbf{W}(\mathbf{z} - \mathbf{X}\boldsymbol{\beta})\|^2/\mathrm{tr}(\mathbf{I} - \mathbf{A})$ and $\mathbf{A} \equiv \mathbf{X}\mathbf{Z}(\mathbf{Z}'\mathbf{X}'\mathbf{W}^2\mathbf{X}\mathbf{Z} + \sum \lambda_i \mathbf{Z}'\mathbf{S}_i \mathbf{Z})^{-1}\mathbf{Z}'\mathbf{X}'\mathbf{W}^2$, all quantities being estimated at convergence of the iterative fitting procedure. This is based on a Bayesian argument (see Silverman, 1985; Wood, 2000), and the resulting confidence intervals are somewhat similar to those proposed by Wahba (1983).

5. Discussion

The thin-plate regression splines proposed here meet the objectives set out in the introduction. For penalized regression modelling they provide optimal low rank approximations to thin-plate splines that are both computationally efficient and stable. In pure regression contexts they also provide a way of avoiding the problems of knot placement, while allowing model selection to be carried out using methods dependent on model nesting.

This computational efficiency and stability should be beneficial when non-linear models are employed which contain embedded smooth functions (see Wood, 2000, section 5, for example). As demonstrated in section 4, the method provides a computationally efficient way of incorporating multi-dimensional smooth terms into GAMs, in a way that facilitates the well founded approaches to model selection and inference characteristic of the GSS models of Gu, Wahba and co-workers (e.g. Wahba, 1990; Wahba et al. 1995; Gu, 2002), but with the considerable practical advantage of greatly enhanced computational efficiency (see section 3.2). It would also be straightforward to incorporate t.p.r.s. based smooths directly into Hastie and Tibshirani's GAM framework, and by using pure (rather than penalized) thin-plate regression splines GAMs could also be constructed entirely within a GLM framework.

There are a number of interesting open questions relating to thin-plate regression splines. Firstly, the sense in which a t.p.r.s. is optimal is slightly weak: one could argue that the measures of approximation error are formulated in too large a space. It is not clear if it is possible to produce more strongly optimal approximations, although the structure of the problem suggests that it is unlikely that stronger results are possible if any computational advantage over full spline models is to be maintained. In response to this a referee suggested concentrating on only one of ϵ_k or e_k , but working in the space where $T'\delta=0$, which implies setting Γ_k to the first k right singular vectors of $\mathbf{E}\mathbf{Z}_n$ (ordered by decreasing singular values) or to the first k eigenvectors of $\mathbf{Z}'_n\mathbf{E}\mathbf{Z}_n$ (ordered by decreasing eigenvalues), respectively. This has the appeal that the optimality criterion is now in the "correct" space, and in limited numerical simulation for the m=1, d=1 case the results are rather similar to the t.p.r.s. results: the modified e_k basis tends to give slightly more smooth but slightly worse fitting results, while the modified ϵ_k basis gives slightly better fitting but more wiggly estimates. Computational costs are doubled by use of the modified ϵ_k basis (each Lanczos step requiring a vector to be multiplied by $\mathbf{E}\mathbf{Z}_n$ and its transpose), but are almost unchanged by using the modified e_k basis. In a pure regression context both alternative bases are even easier to use than the t.p.r.s. basis since reducing the order of the model function is now a simple matter of dropping design matrix columns. However, minimisation of either ϵ_k or e_k alone is not a satisfactory way of arriving at an optimal basis in general: minimising the change in fitted values without regard to change in function norm has the potential to lead to very wiggly results, while concentrating solely on avoiding big changes in function norm can result in poor fit. This is perhaps most readily appreciated by considering a cubic or thin plate spline parameterized directly in terms of the function values, f, corresponding to the response data y, so that the fitting problem is to minimise: $\|\mathbf{y} - \mathbf{f}\|^2 + \lambda \mathbf{f}' \mathbf{S} \mathbf{f}$, where S is a positive semi-definite matrix — it is clear that an approach based solely on a suitably modified ϵ_k criterion is unlikely to result in a useful truncation here. The likely explanation for the relatively good performance of the bases derived from applying the modified e_k or ϵ_k criteria singly to the t.p.s. in its standard parameterization is that the resulting truncated bases in fact almost minimise the neglected criterion in each case, but it is not obvious how to formalize this statement.

Another open question relates to automatic selection of the basis dimension k in the penalized regression context. If k is not too small then model results should be rather insensitive to its value: practical experience to date suggests that this is so, in which case the pragmatic approach suggested

in section 2.1 is a reasonable one to adopt. Never the less it would be more satisfactory to have some theoretical guidance on this point. A further open issue is the question of when one might want to use a knot based penalized regression spline, rather than the eigen basis proposed here. Purely on computational grounds a knot based scheme should be more efficient because it does not require a truncated eigen-decomposition to be obtained. In principle the computational saving could be "spent" on more knots, in which case the knot based scheme might approach or exceed the eigen based scheme in terms of mean square error performance: however, for models with multiple smoothing parameters or those requiring an iteratively re-weighted least squares method for fitting, I actually found that the eigen- based models tended to converge faster than the knot based models for a given basis dimension. If this is a general phenomenon then it clearly deserves further study. In any case the optimal solution in terms of performance for a given amount of computing effort is probably to select a set of knots intermediate in size between the number of data and the desired number of parameters and to obtain a t.p.r.s. basis from this set of knots.

Finally there is the issue of anisotropy. A t.p.r.s. is an isotropic smoother, which is appropriate for spatial co-ordinates, for example, but may not be as suitable if the arguments of the smooth are covariates measured in different units. One could adopt the approach, taken with many smoothing methods, of rescaling covariates to lie in the unit square, cube or hypercube, but this is essentially arbitrary (when used with all methods, not just splines). In principle the problem could be approached in a non-arbitrary way, by treating the relative scaling of axes as extra smoothing parameters in the problem (see e.g. Wood 2000), and work on the production of a general method for doing this is ongoing.

Thin-plate regression splines are available as part of the author's R package mgcv, available from: www.cran.r-project.org. The package includes full source code in C.

Acknowledgements

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Appendix 1: Implementation using standard software

Here are the steps required to construct a rank k basis for smoothing:

- (a) Form the $n \times n$ matrix **E** and the $n \times M$ matrix **T** defined in section 2.
- (b) Obtain the truncated spectral decomposition $\mathbf{E}_k = \mathbf{U}_k \mathbf{D}_k \mathbf{U}_k'$, by use of any standard eigenroutines to find the full spectral decomposition of \mathbf{E} .
- (c) Using standard routines, form the QR decomposition $\mathbf{QR} = \mathbf{U}_k'\mathbf{T}$ where the last n-M rows of \mathbf{R} are zero and \mathbf{Q} is orthonormal. Then the final n-M columns of \mathbf{Q} give \mathbf{Z}_k , the basis for the null space of the equality constraints. If efficiency matters then \mathbf{Z}_k can be stored as M Householder rotations (see e.g. Watkins 1991).
- (d) Writing the parameter k vector of the t.p.r.s. as $\boldsymbol{\beta} = (\tilde{\boldsymbol{\delta}}', \boldsymbol{\alpha}')'$, then the $n \times k$ design matrix for the t.p.r.s. is $\mathbf{X} = [\mathbf{U}_k \mathbf{D}_k \mathbf{Z}_k, \mathbf{T}]$. Similarly the penalty matrix for using this t.p.r.s. in penalized regression would be:

$$\mathbf{S} = \left[egin{array}{ccc} \mathbf{Z}_k' \mathbf{D}_k \mathbf{Z}_k & \mathbf{0} \ \mathbf{0} & \mathbf{0} \end{array}
ight]$$

where the padding with zero matrices is for notational convenience.

- (e) To fit a pure thin-plate regression spline to response data \mathbf{y} , $\|\mathbf{y} \mathbf{X}\boldsymbol{\beta}\|^2$ is minimized with respect to $\boldsymbol{\beta}$, while the incorporation of the t.p.r.s. into any GLM is simply a matter of incorporating the t.p.r.s. design matrix into the the GLM design matrix.
- (f) To fit a penalized thin-plate regression spline requires minimization of:

$$\|\mathbf{y} - \mathbf{X}\boldsymbol{\beta}\|^2 + \lambda \boldsymbol{\beta}' \mathbf{S}\boldsymbol{\beta}$$

with respect to β , given a value for the smoothing parameter λ .

Evaluation of any bounded linear functional of g is self evidently linear in $(\tilde{\boldsymbol{\delta}}', \boldsymbol{\alpha}')'$, with the coefficients easily obtained given \mathbf{Z}_k , \mathbf{D}_k and \mathbf{U}_k . For example $g(\mathbf{x})$ can be written $g(\mathbf{x}) = \mathbf{a}'\tilde{\boldsymbol{\delta}} + \mathbf{b}'\boldsymbol{\alpha}$ where a_i and b_i are known coefficients, depending only on \mathbf{x} :

$$a_i = \sum_{j=1}^n \eta_{md}(\|\mathbf{x} - \mathbf{x}_j\|)[\mathbf{U}_k \mathbf{Z}_k]_{ji} \quad b_i = \phi_i(\mathbf{x})$$

Appendix 2: Lanczos Iteration

(In this appendix only ${\bf E}$ refers to the same quantity that it refers to in the main body of the paper.) The algorithm is iterative, and at the i^{th} iteration produces an $(i\times i)$ symmetric tri-diagonal matrix (${\bf T}_i$, say), the eigenvalues of which approximate the i largest magnitude eigenvalues of the original matrix: these eigenvalues converge as the iteration proceeds, with those of largest magnitude converging first. The eigenvalues and vectors of ${\bf T}_i$ can be obtained in order i^2 operations (using the usual QR algorithm to find the eigenvalues and then inverse iteration to find the eigenvectors), however the inverse iteration appears to be insufficiently stable in some cases, so it is probably preferable to simply accumulate the eigenvectors as part of the QR algorithm at cost of order i^3 . The eigenvectors of the original matrix are easily obtained from the eigenvectors of ${\bf T}_i$. A complete version of the algorithm, suitable for finding the truncated decomposition of ${\bf E}$ is as follows.

- (a) Let b be an arbitrary non-zero n vector: it may be best to initialize this from a simple random number generator, to reduce the risk of starting out orthogonal to some eigenvector (exact repeatability can be ensured by starting from the same random number generator seed).
- (b) Set $\mathbf{q}_1 \leftarrow \mathbf{b}/\|\mathbf{b}\|$.
- (c) Repeat steps (d) to (l) for $j = 1, 2, \ldots$ until enough eigenvectors have converged.
- (d) Form $\mathbf{z} \leftarrow \mathbf{E}\mathbf{q}_i$.
- (e) Calculate $\alpha_j \leftarrow \mathbf{q}_i' \mathbf{z}$
- (f) Reorthogonalize z to ensure numerical stability, by performing the following step twice:

$$\mathbf{z} \leftarrow \mathbf{z} - \sum_{i=1}^{j-1} (\mathbf{z}'\mathbf{q}_i)\mathbf{q}_i$$

- (g) Set $\beta_j \leftarrow \|\mathbf{z}\|$
- (h) Set $\mathbf{q}_{j+1} \leftarrow \mathbf{z}/\beta_j$
- (i) Let T_j be the $(j \times j)$ tridiagonal matrix with $\alpha_1, \dots \alpha_j$ on the leading diagonal, and $\beta_1, \dots \beta_{j-1}$ on the leading sub- and super- diagonals.
- (j) If iteration has proceeded far enough to make it worthwhile, find the eigen-decomposition (spectral decomposition) $\mathbf{T}_j = \mathbf{V} \mathbf{\Lambda} \mathbf{V}'$, where columns of \mathbf{V} are eigenvectors of \mathbf{T}_j and $\mathbf{\Lambda}$ is diagonal with eigenvalues on leading diagonal.

- (k) Compute "error bounds" for each $\Lambda_{i,i}$: $|\beta_i V_{i,j}|$.
- (l) Use the error bounds to test for convergence of the k largest magnitude eigenvalues. Terminate the loop if all are converged.
- (m) The i^{th} eigenvalue of \mathbf{E} is $\Lambda_{i,i}$. The i^{th} eigenvector of \mathbf{E} is $\mathbf{Q}\mathbf{v}_i$, where \mathbf{Q} is the matrix whose columns are the \mathbf{q}_j (for all j calculated) and \mathbf{v}_i is the i^{th} column of \mathbf{V} (again calculated at the final iteration). Hence \mathbf{D}_k and \mathbf{U}_k can easily be formed.

The given algorithm is stabilized by orthogonalization against all previous vectors \mathbf{q}_j : several selective orthogonalization schemes have been proposed to reduce the computational burden of this step, but I experienced convergence problems when trying to use these schemes with \mathbf{E} , especially in the one dimensional case (d=1): in any case the computational cost of the method is dominated by the $O(n^2)$ step: $\mathbf{z} \leftarrow \mathbf{E}\mathbf{q}_j$, so the efficiency benefits of using a selective method are unlikely to be very great, in the current case (if \mathbf{E} were sparse then selective methods would offer a benefit).

Finally note that **E** need never be formed and stored as a whole: it is only necessary that its product with a vector can be formed. It is this feature that suggests that thin-plate regression splines could be used on very large data sets without causing storage problems. For a fuller treatment of the Lanczos method see Demmel (1997), from which the algorithm given here has been modified.

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